

LINEAR INTEGRATED CIRCUITS

2nd EDITION

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INTRODUCTION

This databook contains data sheets on the SGS-ATES range of linear integrated circuits for professional, industrial and consumer applications.

Selection guides are provided in the following pages to facilitate rapid identification of the most suitable device for the intended use.

The information on each product has been specially presented in order that the performance of the product can be readily evaluated within any required equipment design.

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APPLICATION GUIDE: CONSUMER CIRCUITS

TV

FUNCTION		DEVICE
Complete sound channel		TDA1190 TDA1190Z TDA 2190 TDA3190
Deflection	Horizontal	TDA1180F TDA1180P
	Vertical	TDA1170 TDA1170S TDA1270 TDA1470
Video IF system		TDA440S TDA4420
Chroma	Oscillator	TDA2140
	Lumin. & Chromin.	TDA2151
	Demodulator	TDA2161
TV signal identification		TDA4431 TDA4433
Varicap supply		TAA550A TAA550B TAA550C

Preamplifiers

FUNCTION	DEVICE
General purpose	TBA231A
Tape	TDA1054M TDA2054M TDA3410
Hi-Fi	TDA2310

Tape Recorders

FUNCTION	DEVICE
DC Motor Regulators	TCA900 TCA910 TDA1151
Multifunction	TDA7270S TDA7770

Audio Power Amplifiers

APPLICATION	DEVICE
Car radio	TBA810P TBA810S TBA810CB TDA2002 TDA2003 TDA2004 TDA2005
Portable radio	TAA611A TAA611B TAA611C TBA820 TBA820M TCA830S TDA1905
TV receiver	TBA800 TCA940N TDA1905 TDA1908 TDA2006 TDA2008
Hi-Fi and Hi-Fi TV	TDA1910 TDA2010 TDA2020 TDA2030
Driver	TDA2020D

Radio

FUNCTION	DEVICE
IF/FM radio system	TCA3089 TCA3189 TDA1200
AM/FM radio	TDA1220A

Transistor Array

FUNCTION	DEVICE
NPN array	LS159 TBA331 TDA3310

APPLICATION GUIDE: PROFESSIONAL CIRCUITS

Operational Amplifiers

FUNCTION	DEVICE
General purpose	LS107 LS207 LS307 LS141 LS141A LS141C LS148 LS148A LS148C LS709 LS709A LS709C
High performance	LS101 LS201 LS301
Programmable	LS776 LS776C
Dual-high performance	LS204 LS204A LS204C
Quad-high performance	LS404 LS404C

Telecommunication Circuits

FUNCTION	DEVICE
Balanced modulator	LS025
Channel amplifier	LS045
Compressor	LS150
Speech circuit and multifrequency interface	LS285/A LS342
Op-amps for active filter	LS204 LS404

Positive Voltage Regulators

FUNCTION	DEVICE
Standard fixed	L129 L130 L131 L2000 series L7800 series L78S00 series TBA435 TBA625A TBA625B TBA625C
Fixed (with integrated rectifying bridge)	L194-5 L194-12 L194-15
Adjustable	L123 L146 L200
Automotive	L2600 series

Industrial Circuits

FUNCTION	DEVICE
Power operational amplifier	L165
DC motor positioning system	L290 L291 L292
Motor driver	L293
Darlington array	L201/2/3/4 L601/2/3/4 L702
Current booster	L149 TDA1410A TDA1420A TDA1420L
Triac/SCR control	L120A L121A

AUDIO POWER AMPLIFIERS

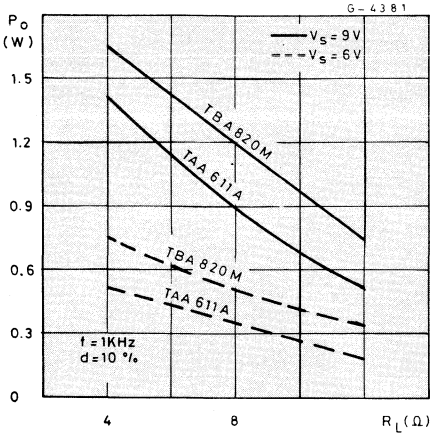
Selection table (test conditions; $d = 10\%$, $f = 1 \text{ kHz}$)

Supply (V)	Device	Output Power (W)			
		$R_L = 2 \Omega$	$R_L = 4 \Omega$	$R_L = 8 \Omega$	$R_L = \dots$
4	TBA820M		0.35		
6	TAA611A TBA810S TBA820M		0.5 1 0.75	0.35 0.45	
9	TAA611A TAA611B TBA810P TBA820 TBA820M TCA830S TDA1905	3.4	1.8 1.8 2.5 1.6 1.6 2 2.5	1.15 1.15 1.2 1.2 1.25 1.3	
12	TAA611B TAA611C TBA820 TCA830S		3 3.4	2.1 2.1 2 2.3	
14.4	TBA810CB TBA810P TDA1905 TDA1908 TDA2002 TDA2003 TDA2004 TDA2005	7 7 8 10 10 10	6 6 5.4 5.8 5.2 6 6.5 6.5/20 (°)	3 3	12 11 $R_L = 1.6 \Omega$ 11
18	TBA800 TCA940N TDA1905 TDA1908		9 9	4.5 5 5.5 5	
20	TDA2008		12	8	
24	TBA800 TDA1905 TDA1908 TDA1910*		10	7	5 5.3 $R_L = 16 \Omega$ 5
28	TDA2006 TDA2010* TDA2030*		14 10 14	9 8 9	
36	TDA2020*		18	15	
40	TDA2020D •		40		

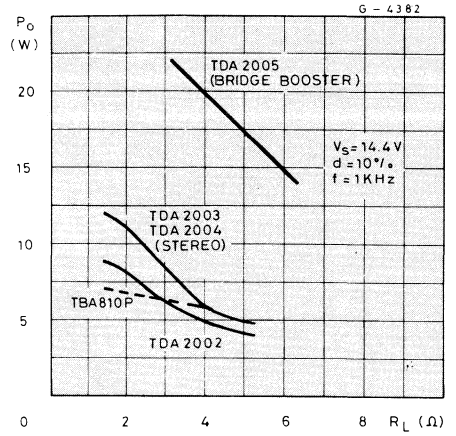
* Hi-Fi ($d = 0.5\%$) • Driver (°) Bridge.

AUDIO POWER AMPLIFIERS

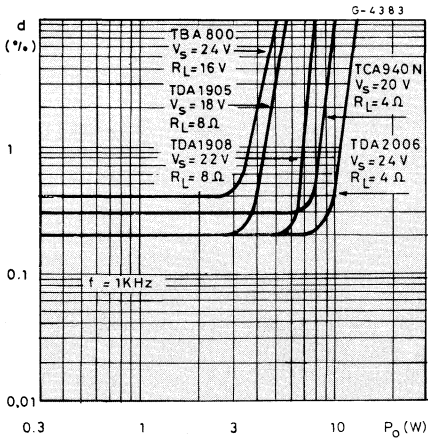
Portable radio



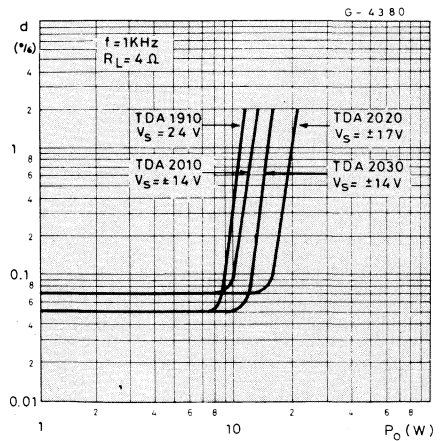
Car radio



TV receiver



Hi-Fi power








VOLTAGE REGULATORS

I_o max (A)	Device	Regulated output voltage (V)										Package		
		5	7.5	8.5	9	10	12	15	18	24	36			
2	L200CH/CV	2.9											36	Pentawatt [®] TO-3(4-lead)
	L200CT/T	2.9											36	
	L2000CT/T	•	•		•	•	•	•	•	•	•	•		
	L2000CV	•	•		•	•	•	•	•	•	•	•		
	L78S00CT/T	•	•		•	•	•	•	•	•	•	•		
	L78S00CV	•	•		•	•	•	•	•	•	•	•		
1.5	L7800CT/T	•	•		•	•	•	•	•	•	•		TO-3 Versawatt	
	L7800CV	•	•		•	•	•	•	•	•	•			
0.6	L129	•											TO-126 Versawatt TO-3	
		•												
		•												
0.5	L130						•						TO-126 Versawatt TO-3 Pentawatt [®] Pentawatt [®] Pentawatt [®] Versawatt	
	L194/5*	•					•							
	L194/12*						•							
	L194/15*							•						
	L2600	•		•		•			•					
0.45	L131								•				TO-126 Versawatt TO-3	
									•					
										•				
0.15	L123CB	2											14-lead copper TO-100 14-lead copper TO-100 TO-39 TO-39 TO-39 TO-39	
	L123CT/T	2												
	L146CB	2												
	L146CT/T	2												
	TBA435				•									
	TBA625A	•												
	TBA625B							•						
	TBA625C								•					

* With integrated rectifying bridge.

OPERATIONAL AMPLIFIERS

Device	Temperature Range (°C)	Frequency compensat.	CMRR (dB)	Input Bias Curr. (nA)	Slew Rate (V/μs)	Max supply Voltage (V)	Package
LS101T	-55 to 125		90	120	10	± 22	
LS101AT	-55 to 125		96	30	10	± 22	
LS107T	-55 to 125	●	96	30	0.7	± 22	
LS141T	-55 to 125	●	90	80	0.5	± 22	
LS141AT	-55 to 125	●	95	30	0.7	± 22	
LS141CT	0 to 70	●	90	80	0.5	± 18	
LS148T	-55 to 125		90	80	5.5	± 22	
LS148AT	-55 to 125		95	20	5.5	± 22	
LS148CT	0 to 70		90	80	5.5	± 22	
LS201T	0 to 70		90	250	10	± 22	
LS201AT	-25 to 85		96	30	10	± 22	
LS207T	-25 to 85	●	96	30	0.7	± 22	
LS301AT	0 to 70		90	70	10	± 18	
LS307T	0 to 70	●	90	70	0.5	± 18	
LS709T	-55 to 125		90	200	0.25	± 18	
LS709AT	-55 to 125		110	100	0.25	± 18	
LS709CT	0 to 70		90	300	0.25	± 18	
LS776T	-55 to 125	●	90	15	0.35	± 18	
LS776CT	0 to 70	●	90	15	0.8	± 18	
LS204T*	-25 to 85	●	100	50	1.5	± 18	
LS204AT*	-55 to 125	●	100	50	1.5	± 18	
LS204CT*	0 to 70	●	95	80	1	± 18	
LS141CB	0 to 70	●	90	80	0.5	± 18	
LS148CB	0 to 70		90	80	5.5	± 22	
LS201B	0 to 70		90	250	10	± 22	
LS301AB	0 to 70		90	70	10	± 18	
LS307B	0 to 70	●	90	70	0.5	± 18	
LS776CB	0 to 70	●	90	15	0.8	± 18	
LS204CB*	0 to 70	●	95	80	1	± 18	
LS141CM	0 to 70	●	90	80	0.5	± 18	
LS148CM	0 to 70		90	80	5.5	± 22	
LS201M	0 to 70		90	250	10	± 22	
LS301AM	0 to 70		90	70	10	± 18	
LS307M	0 to 70	●	90	70	0.5	± 18	
LS776CM	0 to 70	●	90	15	0.8	± 18	
LS204M*	-25 to 85	●	100	50	1.5	± 18	
LS204CM*	0 to 70	●	95	80	1	± 18	
LS404M**	-25 to 85	●	94	50	1	± 18	
LS404CM**	0 to 70	●	90	100	1	± 18	
LS709CB	0 to 70		90	300	0.25	± 18	
LS404C**	0 to 70	●	90	100	1	± 18	

* Dual

** Quad

SEMICONDUCTOR USERS RELIABILITY EVALUATION

SGS-ATES **Sure II** Programme aims to inform customers of basic production operations and internal quality and reliability assurance procedures, paying particular attention to the tests and guarantees on the finished product.

This programme covers the set of 100% operations, controls and testing operations undergone by devices produced to standard specification, i.e. without any special customer requirements.

Sure II Programme contains the following sections:

GENERAL INFORMATION

Typical block diagram of production process steps

Screening options which the customer can request by referring directly to this programme are also indicated.

QUALITY LEVELS GUARANTEED BY GROUP A TESTS

These are the parameters checked on every delivery during final acceptance. The Group A tests tables show the guaranteed quality levels for standard material (level C) and for purchased materials with the programme's two optional screening levels (levels A and B).

GROUP B AND C TESTS

These reliability tests are performed to maintain the processes under control, to collect data useful in calculating the failure rates of our products and, when requested, to supply summarized reliability information to the customer.

Group B tests are normally carried out every 1 to 3 months and group C tests every 6 to 12 months. Precise test frequencies are established within the above limits by the Quality and Reliability Assurance Manager of the various plants; the product is delivered and guaranteed according to results obtained in these tests and in the failure analyses, which are regularly performed on any rejected devices. Unlike the Group A tests, these tests are not effected on individual delivery lots, but on production lots, selected according to the criterion of structural similarity.

To complement Sure II Programme, SGS-ATES performs realtime reliability tests on certain products. These tests are normally effected under accelerated conditions and greatly reduced duration in order to provide frequent and rapid feedback to Production.

However, due to their highly technical character, the description of these tests is outwith the scope of the Sure II Programme.

GENERAL INFORMATION

This information is valid for all products ordered from SGS-ATES as standard, i.e. in accordance with Sure II Programme, or which are ordered in full accordance with one of the two Sure Programme options.

Marking

Each device will be marked in a contrasting ink with the following standard information (if sufficient space is available):

- 1 - SGS-ATES logo
- 2 - Device type as shown in the detail specification
- 3 - Manufacturing plant number
- 4 - Lot code (Production lot)

GENERAL INFORMATION (continued)

Packing

Devices will be packed in the vendor's standard package, unless otherwise specified on the purchase order.

The following information will be marked on the std. package:

- 1 - SGS-ATES logo
- 2 - Device type as shown on the detail specification
- 3 - Quantity in the package
- 4 - SGS-ATES order confirmation

Certification

Certificate of conformance will be enclosed with the devices for level A only, unless otherwise agreed.

Reference specification

- a) Basic Sampling Procedures and tables for inspection by attributes:
MIL-STD-105D-IEC 410.
- b) The Sure II Programme has been prepared considering the following specs.:
IEC 68-1, IEC 68-2, MIL-STD-883A, MIL-STD-750B, MIL-STD-202E, CECC 50.000, CECC 90.000, MIL-STD-19510E, MIL-STD-38510C.
It should be noted that conformance with these specs. should be assumed only where specifically stated in this programme.

Essential terms and definitions

For the purpose of interpretation of this general specification the following terms and definition apply:

Detail specification

A specification which covers a particular component or range of components, and which describes that component including rated and/or limiting values and characteristics. The detail specification will also give the inspection requirements or appropriate reference to this general specification.

Inspection lot

A quantity of structurally similar components presented together for inspection, from which a sample is to be drawn and inspected to determine conformance with the acceptance criteria of the specification.

Delivery lot

A quantity of components delivered to an order at one time. One delivery lot may consist of one or more inspection lots or parts thereof.

Structurally similar devices

Structurally similar devices are those devices produced concurrently through final seal by the same fabrication techniques, using the same type of machines and apparatus and having the same basic design rules and the same packaging.

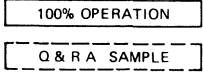
Details of structural similarity for various components will be defined, when required, by the SGS-ATES Quality Assurance Mgr(s).

Certificate of Conformance

A document issued with a delivery lot stating that the components have been taken from one or more inspection lots accepted under the requirements of the particular specification.

TYPICAL BLOCK DIAGRAM OF PRODUCTION PROCESS STEPS

KEY



NOTES

- ※ NOT FOR TO-3
- ACCORDING TO OUR INTERNAL SPECS FOR PLASTIC DEVICES
- CIRCULAR METAL CAN ONLY
- NOT FOR PLASTIC DEVICES

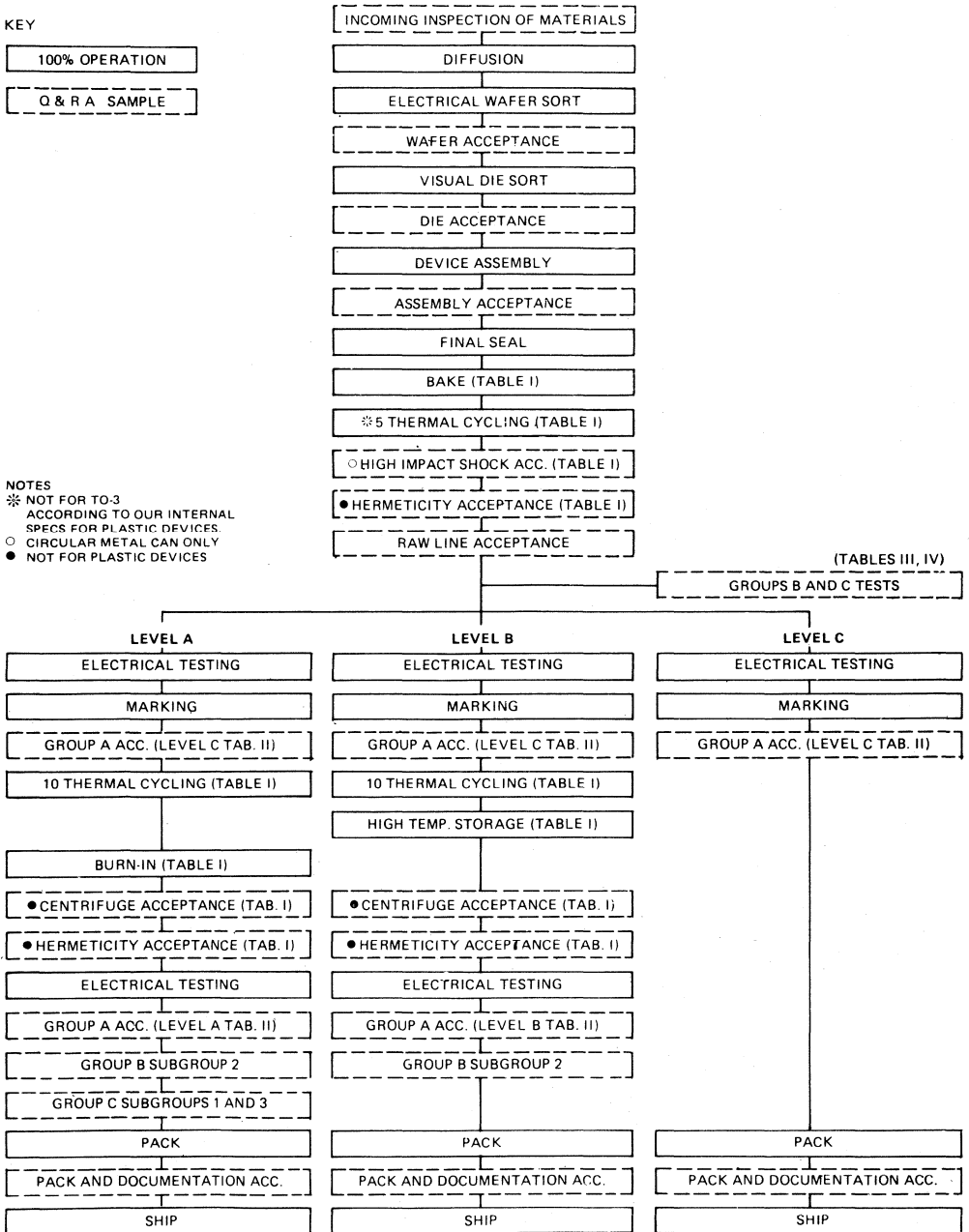


TABLE I
Conditions for tests shown in block diagram of production process (excepting Group A, B and C)

Tests	Description
Thermal Cycling	$T_{amb} = -65^{\circ}\text{C}$ to $+150^{\circ}\text{C}$ 30 minutes at extreme temperatures, 5 minutes max transfer time.
Centrifuge	20 000 G, 1 minute, Y1 axis only
High Impact Shock	20 000 G, $t = 0.25 \mu\text{s}$ minimum, Y1 axis only.
High temperature Storage (Optional)	100 h at: $T_{amb} = +150^{\circ}\text{C}$
Bake	16 h at $+180^{\circ}\text{C}$ for plastic devices. According to our internal specs. for other devices.
Burn-in (optional)	168 h according to spec. device type.
Hermeticity	- Fine leak: helium leak detector after pressurization in He for 1 h at 5 atm. The limits vary from device to device and can be provided on request. - Gross leak: bubble test in mineral oil at $T_{amb} = +125^{\circ}\text{C}$ after pressurization for 1 h in He at 5 atm.
Other acceptance shown in the block diagram of the production process (excepting group A, B C tests).	Performed according to SGS-ATES internal specs.

TABLE II - Group "A" acceptance (Reference MIL-STD-105D, IEC 410)

Sub-group	Parameters	AQL CUMUL.			Inspection Level
		A (Opt.)	B (Opt.)	C (Std.)	
A1	Visual and mechanical inspection Major Minor	0.65 1.5	0.65 1.5	0.65 1.5	I
A2	Inoper. failure (electr. and mechanical) at $+25^{\circ}\text{C}$	0.15	0.15	0.25	II
A3	DC parameters and selected AC parameters* at $+25^{\circ}\text{C}$	0.4	0.65	1	II
A4	AC parameters at $+25^{\circ}\text{C}$	1	1.5	2.5	S4

NOTES:

- 1) Electrical parameters are indicated on data sheets.
- 2) Major defects (significant mechanical defects, but not functional defects). e.c. open packages, deformed leads.
- 3) Minor defects. e.g. marking difficult to read, cosmetic defects, package dimensions.
- 4) Inoperative mechanical defects (critical defects). e.g. pin indication, marking or splitting wrong, broken lead or short circuits between leads.

* Selected AC parameters: are fundamental parameters which guarantee the function.

Sample size code letters (group A tests)

Lot or batch size			Special inspection levels				General inspection levels		
			S-1	S-2	S-3	S-4	I	II	III
2	to	8	A	A	A	A	A	A	B
9	to	15	A	A	A	A	A	B	C
16	to	25	A	A	B	B	B	C	D
26	to	50	A	B	B	C	C	D	E
51	to	90	B	B	C	C	C	E	F
91	to	150	B	B	C	D	D	F	G
151	to	280	B	C	D	E	E	G	H
281	to	500	B	C	D	E	F	H	J
501	to	1200	C	C	E	F	G	J	K
1201	to	3200	C	D	E	G	H	K	L
3201	to	10000	C	D	F	G	J	L	M
10001	to	35000	C	D	F	H	K	M	N
35001	to	150000	D	E	G	J	L	N	P
150001	to	500000	D	E	G	J	M	P	Q
500001	and over		D	E	H	K	N	Q	R

Single sampling plans for normal inspection (group A tests)

Sample size code letter	Sample size	Acceptable Quality Levels (normal inspection)																											
		0.010	0.015	0.025	0.040	0.065	0.10	0.15	0.25	0.40	0.65	1.0	1.5	2.5	4.0	6.5	10	15	25	40	65	100	150	250	400	650	1000		
		Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	Ac Rc	
A	2	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓		
B	3	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓		
C	5	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓		
D	8	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓		
E	13	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓		
F	20	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓		
G	32	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓		
H	50	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓		
J	80	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓		
K	125	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓		
L	200	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓		
M	315	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓		
N	500	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓		
P	800	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓		
Q	1250	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓		
R	2000	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓		

Double and multiple sampling plan inspection may be used.

↓ = Use first sampling plan below arrow. If sample size equals, or exceeds, lot or batch size, do 100 percent inspection.

↑ = Use first sampling plan above arrow.

Ac = Acceptance number.

Rc = Rejection number.

TABLE III – Group "B" Tests

Tests	Test conditions	LTPD	Max. acc. n°
Subgroup 1 PHYSICAL DIMENSIONS MARKING PERMANENCY	Major dimensions according to data sheet. 5 minutes immersion in trichloroethylene at T _{amb} . Rub marking with a soft brush 10 times. Marking shall appear legible.	20	4
Subgroup 2 SOLDERABILITY	5 s (min.) in rosin-based flux 2 ± 0.5 s in Sn (60) Pb (40) at +230°C ± 5°C. Depth of immersion 0.8 to 2.3 mm from case or half the length of the leads. Under 10X magnification leads shall be covered with a smooth and bright solder coating with no more than traces (approx. 5%) of scattered imperfections such as pin-holes or un-wetted or de-wetted areas. These imperfections shall not be concentrated in one area.	15	3
Subgroup 3 THERMAL SHOCK THERMAL CYCLING HERMETICITY (Not for plastic devices) MOISTURE RESISTANCE	15 shocks -0°C to +100°C liquid-to-liquid 5 minutes at extreme temperatures 5 s max transfer time. 10 cycles: T _{amb} = -65°C to +150°C 30 minutes at extreme temperatures 5 minutes max transfer time. <i>Fine leak</i> – Helium leak detector after pressurization in He at 5 atm. for 1 h. 5 × 10 ⁻⁸ cc/s for I.C.V. * ≤ 0.1 cc 5 × 10 ⁻⁷ cc/s for I.C.V. * between 0.1 cc and 10 cc. * (I.C.V. = Internal Cavity Volume) <i>Gross leak</i> – Bubble test in mineral oil at T = +125°C after pressurization for 1 h in He at 5 atm. 10 cycles of 24 h T _{amb} = 25°C to 65°C; RH 80% to 98% 5 cycles to -10°C for 3 h.	15	3
Subgroup 4 OPERATING AND/OR INTERMITTENT LIFE TEST	According to device type spec. 5000 cycles min. for intermittent life test t = 340h min for operating life test.	10	2
Subgroup 5 LEAD FATIGUE*	Two leads for each device. <i>Dual-in-line pack</i> : 3 arcs; leads shall be bent inward for 15° permanent angle and shall be returned to their original position. <i>Wire leads</i> : 3 arcs, 90° ± 5° with a force of .229 ± 0.014 Kg. <i>Failure</i> : any broken leads.	20	4
Subgroup 6 PRESSURE POT	+121°C, 2 atm. from 48 to 96 h according to package type. Plastic devices only.	15	3

* Not applicable for TO-3.

TABLE IV — Group "C" tests

Tests	Test conditions	LTPD	Max. acc. n°
Subgroup 1 DESIGN AND TEMPERATURE ELECTRICAL CHARACTERISTICS	This subgroup comprises those parameters complementary to group A parameters. As alternative to LTPD sampling plan, X-R charts may be used to keep the process under control.	30	4
Subgroup 2 MECHANICAL SHOCK VARIABLE FREQUENCY VIBRATION CONSTANT ACCELERATION	Not for Plastic devices. 1500 G - 0.5 ms - 5 blows in each of the 6 orientations. Non operating. 20 G; 3 orientations; f = 40 to 2000 cps. Four 4-minute cycles, 48 minutes total. Non operating. 20 000 G - 1 minute - (3 orientations).	15	3
Subgroup 3 OPERATING LIFE TEST ELECTRICAL MEASUREMENTS	t = 1000 h. According to spec. device type. Key parameters at 0, 340, 670 and 1000 h.	10	2
Subgroup 4 HIGH TEMPERATURE STORAGE LIFE TEST ELECTRICAL MEASUREMENTS	1000 h at T _{amb} = +150°C Key parameters at 0, 340, 670 and 1000 h.	15	3
Subgroup 5 SALT ATMOSPHERE	10 to 50 g. of NaCl per square metre per day for 24 h at T _{amb} = +35°C. Post test inspection: check for destructive corrosion.	20	4
Subgroup 6 HUMIDITY TEST ELECTRICAL MEASUREMENTS	Plastic devices only. 85°C/85% RH with bias, t = 1000 h. Key parameters at 0, 340, 670 and 1000 h.	15	3
Subgroup 7 INTERMITTENCY TEST	Electrical continuity measured between 25°C and 100°C or according to spec. device type. Plastic devices only.	1.5	1
Subgroup 8 SOLDERABILITY TEST WITH PRECONDITIONING	Preconditioning at +155°C for 16 h. After a period between 1 and 2 h, the device shall be subjected to solderability test (Group B - Subgroup 2).	15	3
Subgroup 9 SOLDERING HEAT	No flux; +260 ± 5°C for 10 ⁺² ₋₀ s.	15	3

PROGRAMMES OTHER THAN THE SURE II

In addition to the treatment of the standard product described in this Sure II Programme, other test programmes can be agreed upon with the customer, in which case prices generally differ from those for the standard product.

Following are the main programmes existing outwith the limits of the Sure II Programme.

Guaranteed Reliability products (G-Rel.)

In this case, the customer requests that for every delivery lot, certain reliability tests are performed with established acceptance levels and in certain cases also with certification from the Q. & R. Manager of the relative factory.

Products with Source Inspection by a recognized external authority.

Several SGS-ATES factories are qualified under the CECC System (European Q.A. system). The customer can request products inspected by the national supervision service, these products are then delivered with certification from the Q.A. Manager of the relative factory. It should be noted that these national inspectorates are mutually recognized by the member countries of the CECC.

High Reliability products (Hi-Rel)

These products, required for the most sophisticated, generally low-volume applications (e.g. aerospace), are assembled on a special line; this is the Hi-Rel line which employs a sophisticated set of screenings and reliability tests in order to reach, demonstrate and certify the highest reliability levels possible today.

DATA-SHEETS

LINEAR INTEGRATED CIRCUIT

TRIAC/SCR PHASE CONTROL

The L 120A is a monolithic integrated circuit in 16-lead dual in-line plastic package. It incorporates the following functions:

- AC supply 50/60 Hz
- Zero-voltage and zero-current detector
- Ramp generator
- Inhibition of casual firing pulses
- Stabilization of the internal positive DC supply
- High gain operational amplifier
- Output short-circuit protection

The L 120A is intended for use as a phase controller in industrial and consumer applications.

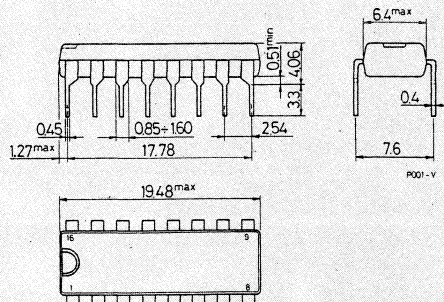
ABSOLUTE MAXIMUM RATINGS

I_g	AC peak supply current	60	mA
I_{14}	Max input current (pin 14)	20	mA
I_{D1}, I_{D2}	Input diodes peak current	1	A
V_{8-12}	Positive clamp voltage	15	V
V_{10-12}	Negative clamp voltage	15	V
V_{1-2}	Differential input voltage	± 7	V
V_{3-5}	Differential input voltage	± 8	V
P_{tot}	Total power dissipation at $T_{amb} = 85^\circ\text{C}$	800	mW
T_{stg}	Storage temperature	-55 to 150	$^\circ\text{C}$
T_{op}	Operating junction temperature	-25 to 150	$^\circ\text{C}$

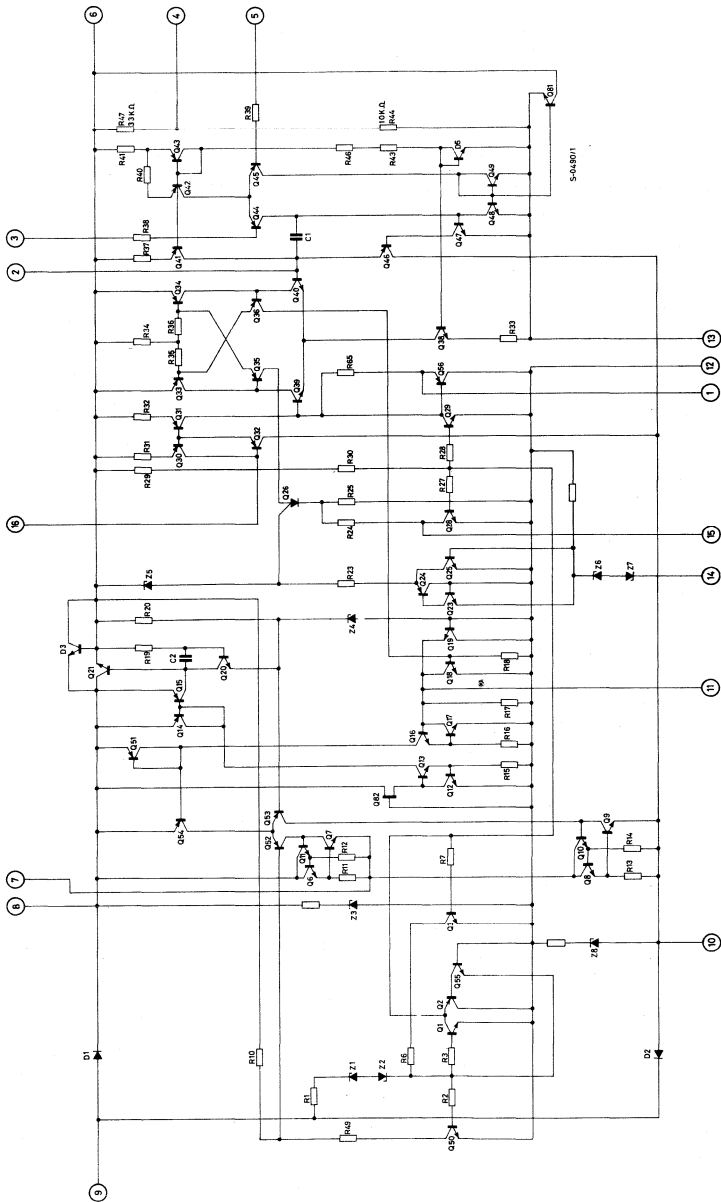
ORDERING NUMBER: L 120AB

MECHANICAL DATA

Dimensions in mm

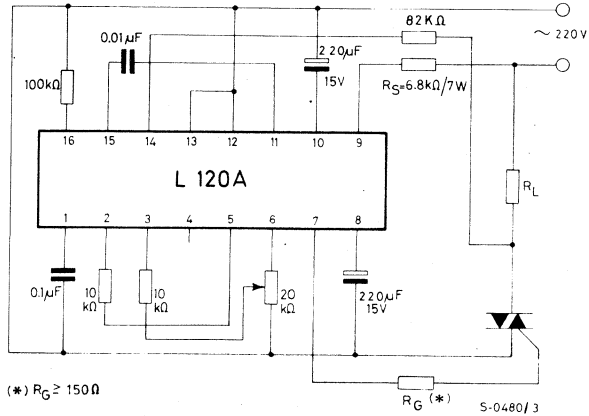


SCHEMATIC DIAGRAM



L 120A

TEST CIRCUIT



THERMAL DATA

$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	80	°C/W
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ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^\circ\text{C}$, refer to the test circuit unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_{8-12}	Positive clamp voltage	10	11.5	13	V
V_{10-12}	Negative clamp voltage	10	11.5	13	V
V_{8-12}	External DC supply voltage	10.5			V
V_{10-12}	External DC supply voltage	-10.5			V
V_{9-12}	Sync input threshold		± 12.5		V
V_{14-12}	Zero current threshold	± 8.8	± 10	± 11.2	V

ELECTRICAL CHARACTERISTICS (continued)

Parameter		Test conditions	Min.	Typ.	Max.	Unit
V ₁₀₋₁₄ V ₈₋₁₄	Zero current threshold		1.2			V
I ₁₄	Operative input current to avoid inhibition (pin 14)		0.4			mA
V ₁₋₁₂	Ramp discharge level				1.1	V
V ₁₋₁₂	Maximum ramp level		7.2			V
V ₁₋₂	Comparat. differential trigger level			70	100	mV
G _v	Amplifier voltage gain (open loop)	V ₂ (peak to peak) = 6V	60	70		dB
V ₂₋₁₃	Max output voltage		7			V
V ₂₋₁₃	Min output voltage				0.9	V
V ₃₋₁₃ , V ₅₋₁₃	Input offset voltage	R ₃₋₁₃ = R ₅₋₁₃ = 50Ω		3	6	mV
I _b	Input bias current (pin 3, 5)			0.1	1	μA
V ₃₋₅	Differential input voltage				± 7	V
V ₃₋₁₃ , V ₅₋₁₃	Input voltage range		0.5		7.5	V
CMR	Common mode rejection	R ₃₋₁₃ = R ₅₋₁₃ ≤ 1kΩ		60		dB
V ₆₋₁₃	Regulator output voltage		8.3		9.5	V
I ₆	Max regulator output current		3			mA
$\frac{\Delta V_6}{V_6}$	Load regulation	I ₆ = 0 to 3 mA		0.5	2	%
$\frac{\Delta V_6}{\Delta V_8}$	Line regulation	V ₈ = 12 to 14V I ₆ = 0		46		dB
SVR	Supply voltage rejection	V ₈ = 12V f _{ripple} = 50 Hz V _{ripple} (peak to peak) = 4V		46		dB
V ₄	Reference voltage	I ₄ = 10 μA		1.5		V
V ₇₋₁₂	Firing pulse amplitude	R ₇₋₁₂ = 1 kΩ	positive	4.5	5.5	V
			negative	8	9.5	V
I ₇	Maximum output current	R ₇₋₁₂ = 10Ω	80			mA
t _{pw}	Output pulse width	R ₇₋₁₂ = 50Ω		200		μs
t _r	Output pulse rise time			200		ns

L 120A

Fig. 1 - Peak supply current vs. dropping resistor R_S

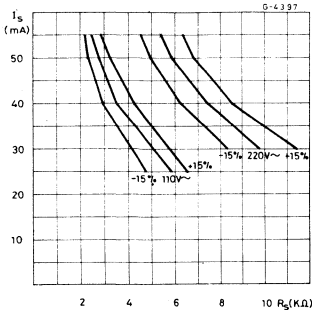


Fig. 2 - Maximum allowable average supply current vs. ambient temperature

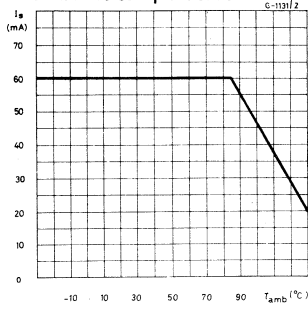


Fig. 3 - Gate pulse amplitude vs. gate resistance

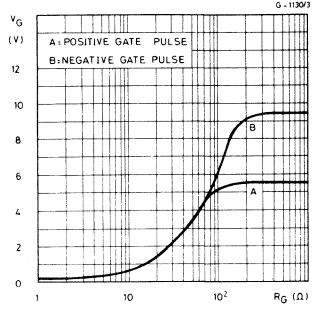


Fig. 4 - Gate current variation vs. ambient temperature

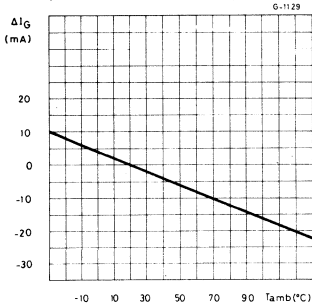
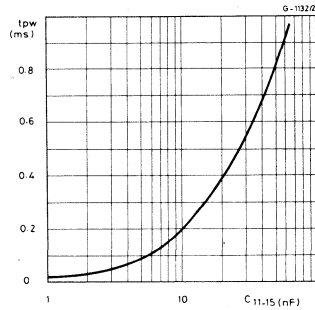
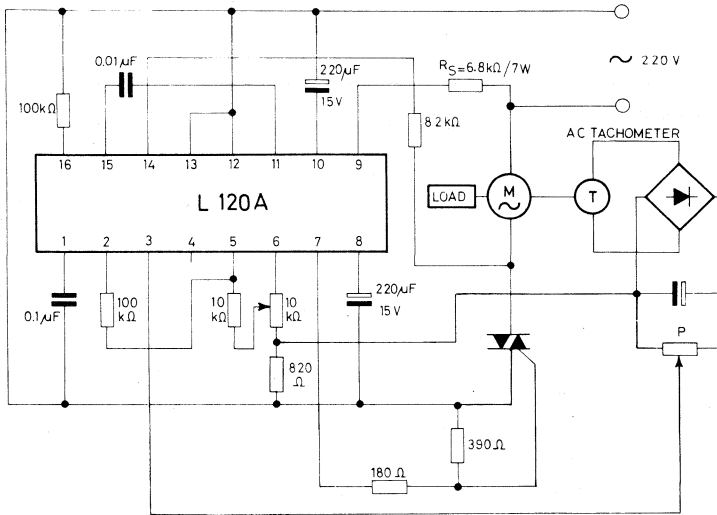


Fig. 5 - Gate pulse width vs. C_{11-15}



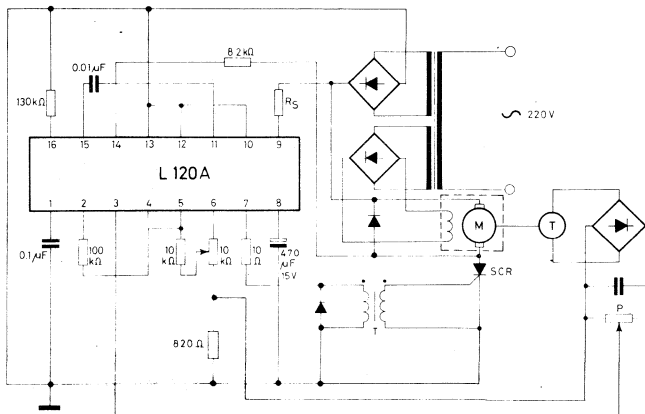
APPLICATION INFORMATION

Fig. 6 - Application circuit for AC motor speed regulators



5-453/4

Fig. 7 - Application circuit for DC motor speed regulators



5-0456/4

LINEAR INTEGRATED CIRCUIT

TRIAC/SCR BURST CONTROL

The L 121A is a monolithic integrated circuit in 16-lead dual in-line plastic package. It incorporates the following functions:

- AC supply 50/60 Hz
- Zero-voltage detector
- Ramp generator
- Inhibition of casual firing pulses
- Stabilization of the internal positive DC supply
- High gain operational amplifier
- Output short-circuit protection

The L 121A is intended for use as a burst controller in industrial and consumer applications.

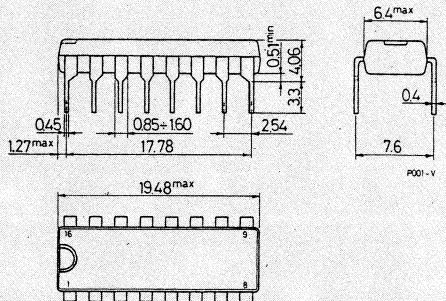
ABSOLUTE MAXIMUM RATINGS

I_g	AC Peak supply current	60	mA
I_{D1}, I_{D2}	Input diodes peak current	1	A
V_{14}	Maximum voltage (pin 14)	20	V
V_{8-12}	Positive clamp voltage	15	V
V_{10-12}	Negative clamp voltage	15	V
V_{1-2}	Differential input voltage	± 7	V
V_{3-5}	Differential input voltage	± 8	V
P_{tot}	Total power dissipation at $T_{amb} = 85^\circ\text{C}$	800	mW
T_{stg}	Storage temperature	-55 to 150	$^\circ\text{C}$
T_{op}	Operating junction temperature	-25 to 150	$^\circ\text{C}$

ORDERING NUMBER: L 121AB

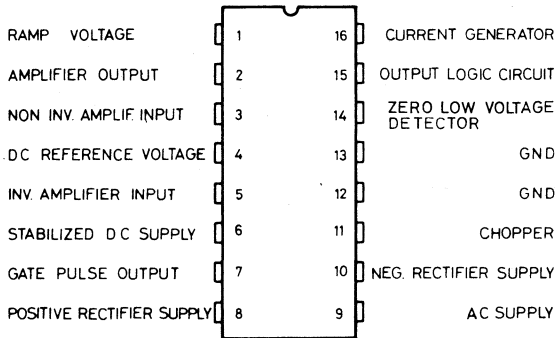
MECHANICAL DATA

Dimensions in mm



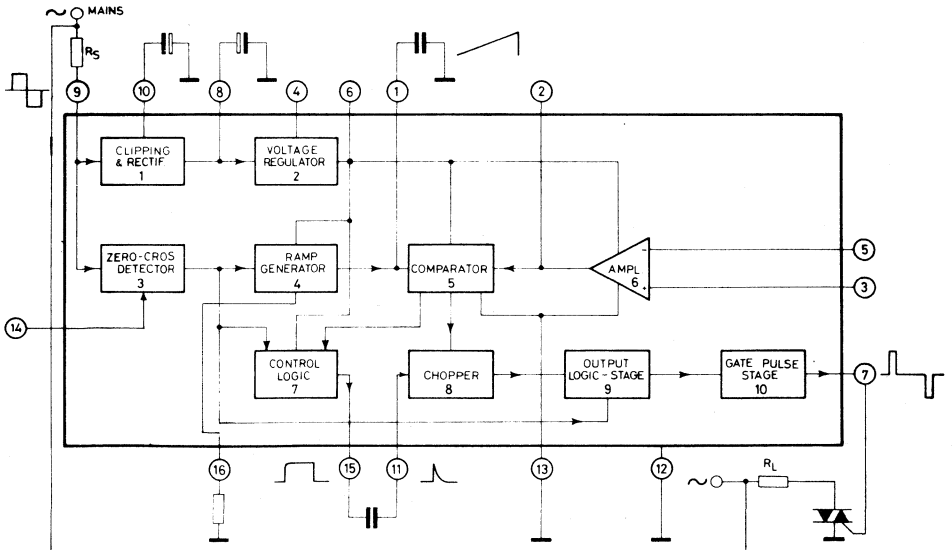
L 121A

CONNECTION DIAGRAM (top view)



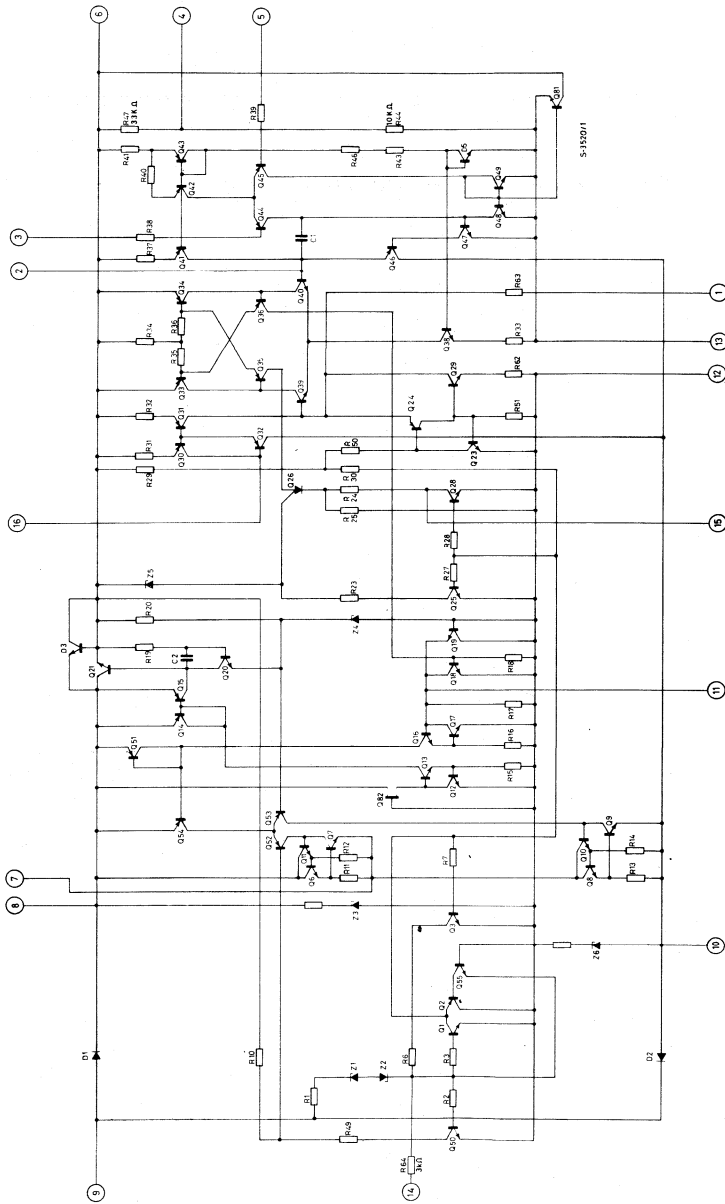
S-3517/1

BLOCK DIAGRAM



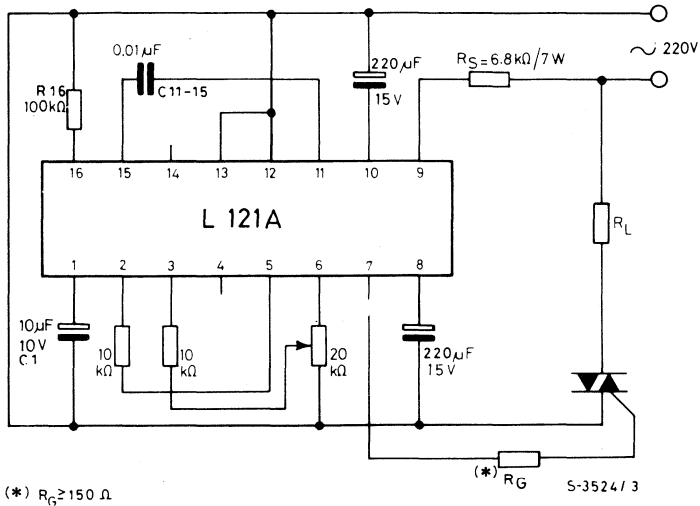
S-3518

SCHEMATIC DIAGRAM



L 121A

TEST CIRCUIT



THERMAL DATA

$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	80	$^{\circ}C/W$
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ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^{\circ}C$, refer to the test circuit unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_{8-12}	Positive clamp voltage	10	11.5	13	V
V_{10-12}	Negative clamp voltage	10	11.5	13	V
V_{8-12}	External DC supply voltage	10.5			V
V_{10-12}	External DC supply voltage	-10.5			V
V_{9-12}	Sync input threshold		± 12.5		V

ELECTRICAL CHARACTERISTICS (continued)

Parameter		Test conditions	Min.	Typ.	Max.	Unit
V ₁₄₋₁₂	Minimum input voltage	(pin 9 open)	±2.5			V
V ₁₋₁₂	Ramp discharge level				1.2	V
V ₁₋₁₂	Maximum ramp level		5.2			V
V ₁₋₂	Comparator differential trigger level			70	100	mV
G _v	Amplifier voltage gain (open loop)	V ₂ (peak to peak) = 6V	60	70		dB
V ₂₋₁₃	Max output voltage		7			V
V ₂₋₁₃	Min output voltage				0.9	V
V ₃₋₁₃ , V ₅₋₁₃	Input offset voltage	R ₃₋₁₃ = R ₅₋₁₃ = 50Ω		3	6	mV
I _b	Input bias current			0.1	1	μA
V ₃₋₅	Differential input voltage				± 7	V
V ₃₋₁₃ , V ₅₋₁₃	Input voltage range		0.5		7.5	V
CMR	Common mode rejection	R ₃₋₁₃ = R ₅₋₁₃ ≤ 1kΩ		60		dB
V ₆₋₁₃	Regulator output voltage		8.3		9.5	V
I ₆	Max regulator output current		3			mA
$\frac{\Delta V_6}{V_6}$	Load regulation	I ₆ = 0 to 3 mA		0.5	2	%
$\frac{\Delta V_6}{\Delta V_8}$	Line regulation	V ₈ = 12 to 14V I ₆ = 0		46		dB
SVR	Supply voltage rejection	V ₈ = 12V f _{ripple} = 50 Hz V _{ripple} (peak to peak) = 4V		46		dB
V ₄	Reference voltage	I ₄ = 10μA		1.5		V
V ₇₋₁₂	Firing pulse amplitude	R ₇₋₁₂ = 1 kΩ	positive	4.5	5.5	V
			negative	8	9.5	V
I ₇	Maximum output current	R ₇₋₁₂ = 10Ω	80			mA
t _{pw}	Output pulse width	R ₇₋₁₂ = 50Ω		200		μs
t _r	Output pulse rise time			200		ns

L 121A

Fig. 1 - Peak supply current vs. dropping resistor R_S

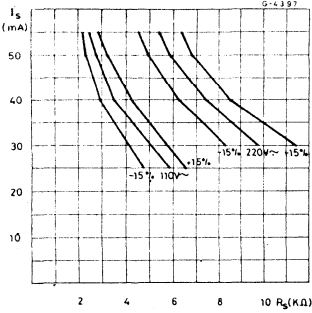


Fig. 2 - Maximum allowable average supply current vs. ambient temperature

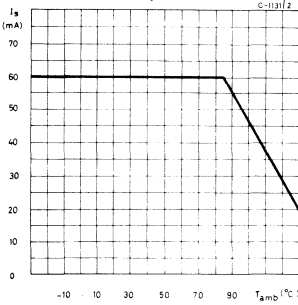


Fig. 3 - Gate pulse amplitude vs. gate resistance

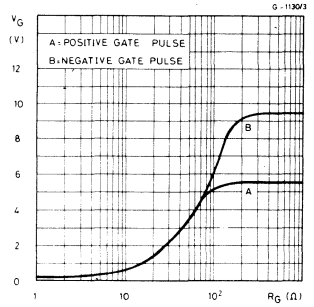


Fig. 4 - Gate current variation vs. ambient temperature

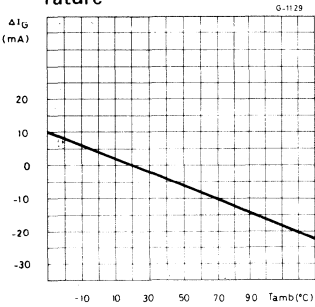


Fig. 5 - Gate pulse width vs. C_{11-15}

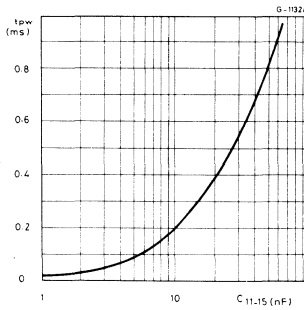
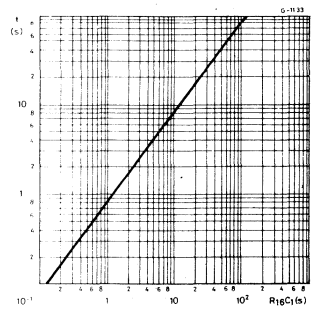


Fig. 6 - Ramp width vs. external time constant $R_{16} \cdot C_1$



APPLICATION INFORMATION

Fig. 7 - Application circuit for temperature control (proportional type)

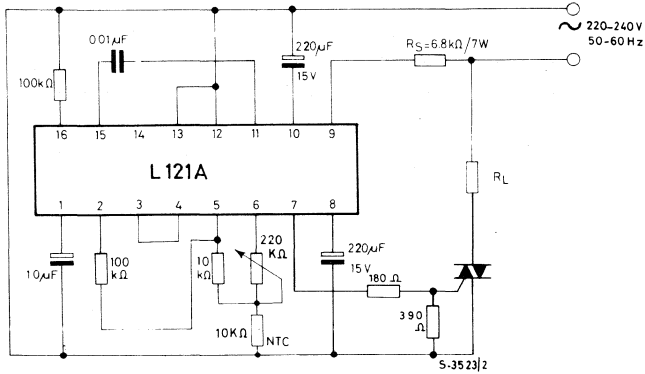
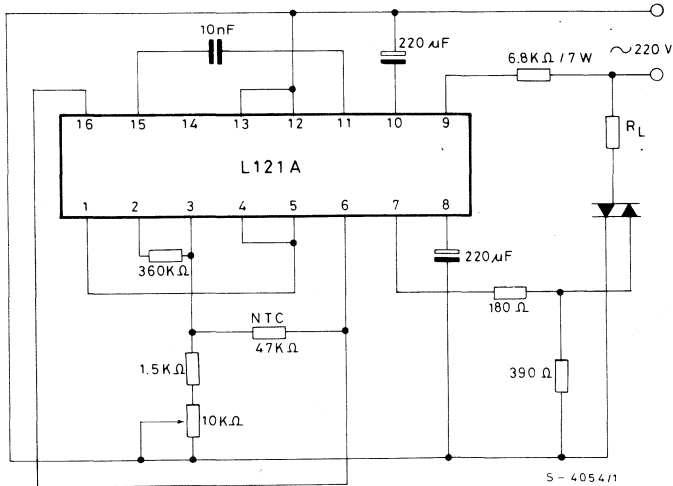


Fig. 8 - Application circuit for temperature control (ON-OFF type)



L 121A

Fig. 9 – Application circuit for **low AC supply voltage** (by using pin 14)

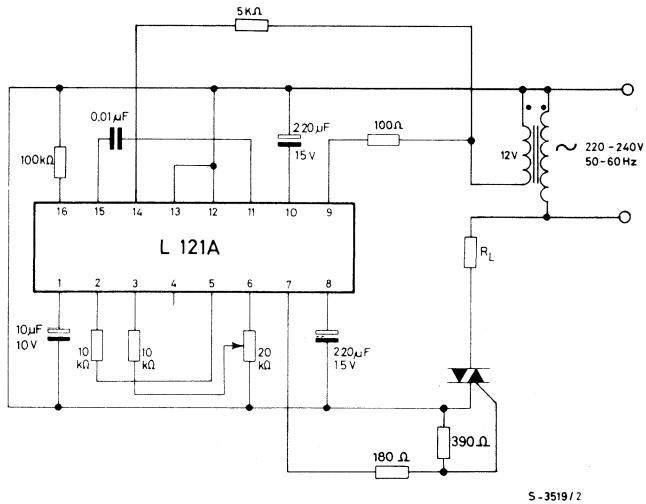


Fig. 10 – ON-OFF control circuit diagram with single pulses for Triac firing

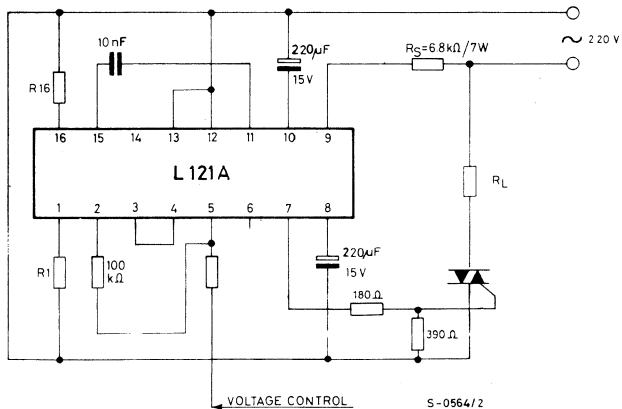


Fig. 11 - ON-OFF control circuit with series of pulses for Triac firing

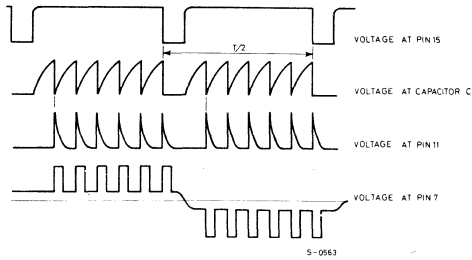
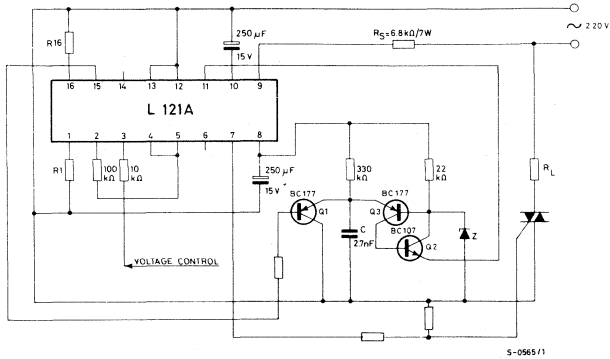
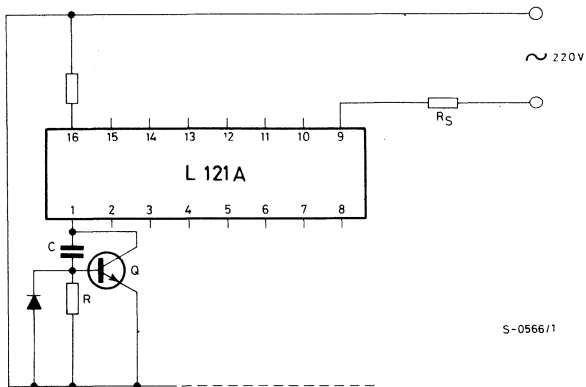
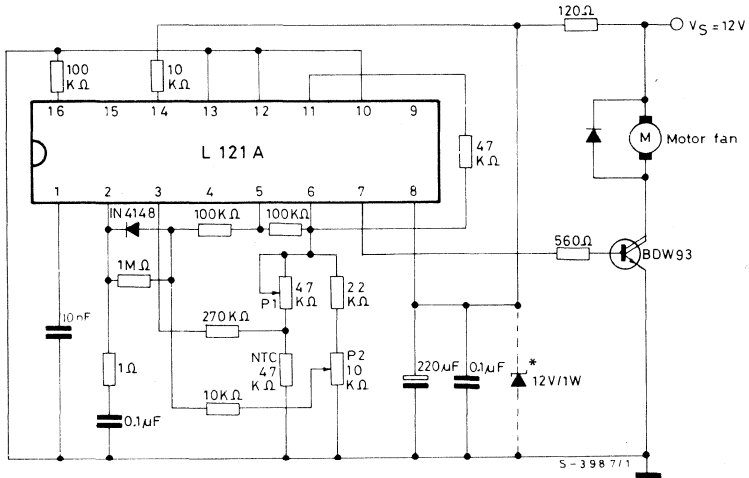


Fig. 12 - Integrator for high time constants



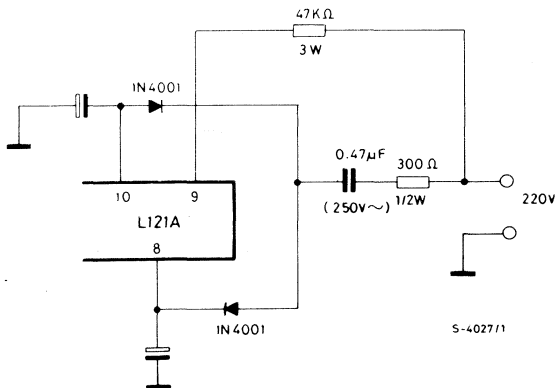
L 121A

Fig. 13 – Climate control for cars.



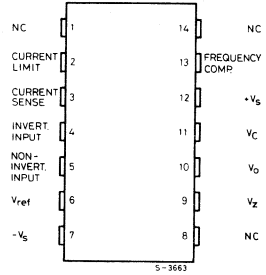
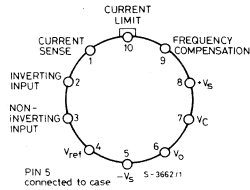
* Protection against overvoltages.
 P₁ : system hysteresis setting
 P₂ : temperature setting

Fig. 14 – Alternative system for L121A power supply (reduction of power dissipation).



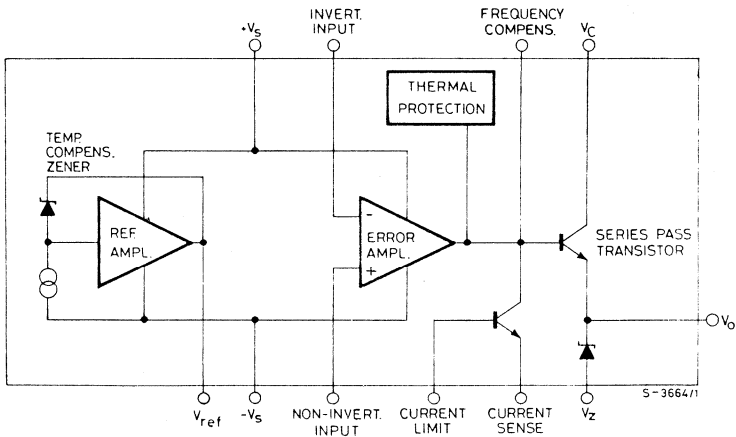
L 123

CONNECTION DIAGRAM AND ORDERING NUMBERS (top views)



Type	TO-100	Plastic DIP
L123	L123T	—
L123C	L123CT	L123CB

BLOCK DIAGRAM

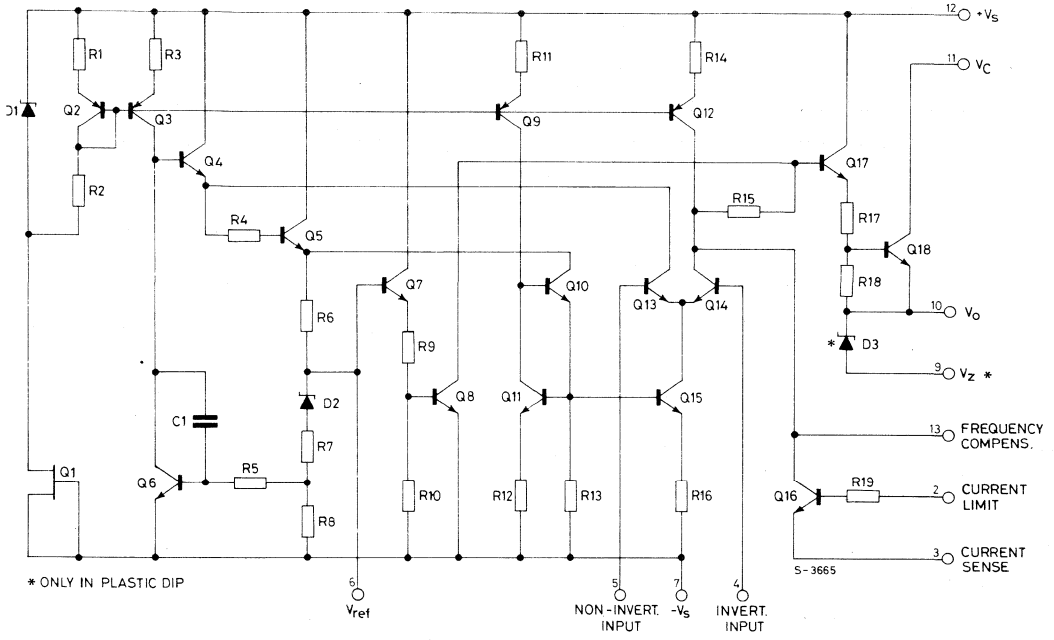


THERMAL DATA

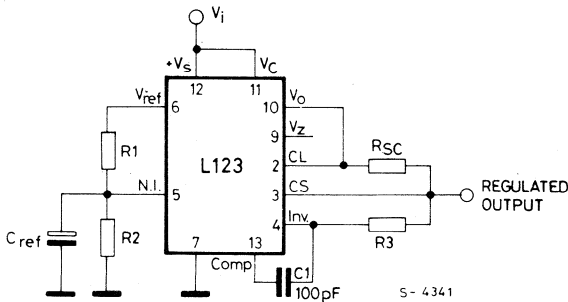
	TO-100	Plastic DIP
$R_{th\ j-amb}$ Thermal resistance junction-ambient	max	max
	155 °C/W	80 °C/W

L 123

SCHEMATIC DIAGRAM (Pin numbers relative to the plastic package)



TEST CIRCUIT (Pin configuration relative to the Plastic package)



$V_i = 12V$
 $V_o = 5V$
 $I_o = 1mA$
 $R_1 // R_2 \leq 10 K\Omega$

L123

ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $T_{amb} = 25^{\circ}\text{C}$ unless otherwise specified)

Parameter	Test conditions	L123C			L123			Unit
		Min.	Typ.	Max.	Min.	Typ.	Max.	
$\frac{\Delta V_o}{\Delta V_i}$	Line regulation $V_i = 12$ to 15V $V_i = 12$ to 40V $V_i = 12$ to 15V ; $T_{min} \leq T_{amb} \leq T_{max}$		0.01	0.1		0.01	0.1	%
			0.1	0.5		0.02	0.2	%
				0.3			0.3	%
$\frac{\Delta V_o}{V_o}$	Load regulation $I_o = 1$ to 50mA $T_{min} \leq T_{amb} \leq T_{max}$ $I_o = 1$ to 10mA		0.03	0.2		0.03	0.15	%
				0.6			0.6	%
V_{ref}	Reference voltage $I_{ref} = 160\ \mu\text{A}$	6.8	7.15	7.5	6.95	7.15	7.35	V
SVR	Ripple rejection $f \approx 100\text{Hz}$ to 10KHz $C_{ref} = 0$ $C_{ref} = 5\ \mu\text{F}$		74 86			74 86		dB dB
$\frac{\Delta V_o}{\Delta T}$	Output voltage drift			150			150	$\frac{\text{ppm}}{^{\circ}\text{C}}$
I_{sc}	Short circuit current limiting $R_{sc} = 10\ \Omega$ $V_o = 0$		65			65		mA
V_i	Input voltage range	9.5		40	9.5		40	V
V_o	Output voltage range	2		37	2		37	V
$V_i - V_o$		3		38	3		38	V
I_d	Quiescent drain current $I_o = 0$ $V_i = 30\text{V}$		2.3	4		2.3	5	mA
	Long term stability		0.1			0.1		$\frac{\%}{1000\text{hrs}}$
e_N	Output noise voltage $\text{BW} = 100\text{Hz}$ to 10KHz $C_{ref} = 0$ $C_{ref} = 5\ \mu\text{F}$		20 2.5			20 2.5		μV μV
V_z	Output zener voltage (for plastic package only) $I_z = 1\text{mA}$	6.9		7.7				V

Note: $T_{min} = 0^{\circ}\text{C}$ (L123C); -25°C (L123).
 $T_{max} = 70^{\circ}\text{C}$ (L123C); 150°C (L123).

Fig. 1 - Maximum output current vs. voltage drop

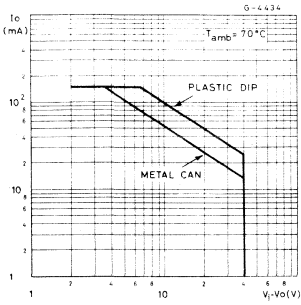


Fig. 2 - Current limiting characteristics

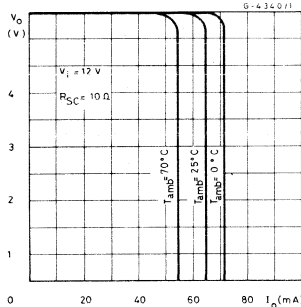


Fig. 3 - Current limiting characteristics vs. junction temperature

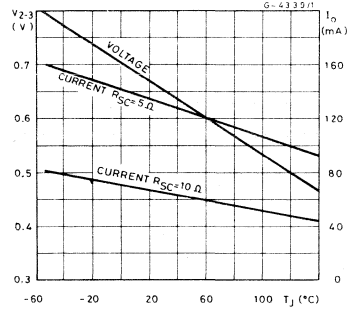


Fig. 4 - Load regulation characteristics without current limiting

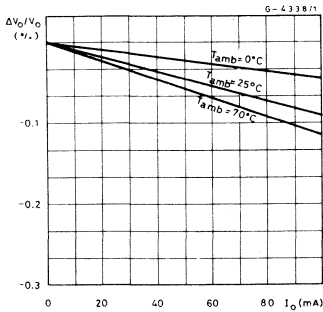


Fig. 5 - Load regulation characteristics with current limiting

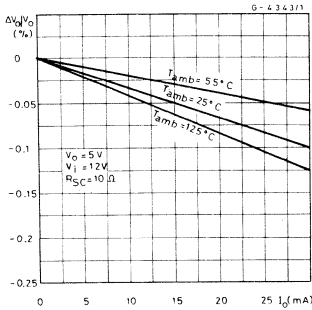


Fig. 6 - Load regulation characteristics with current limiting

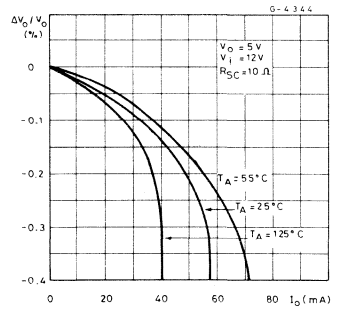


Fig. 7 - Line regulation vs. voltage drop

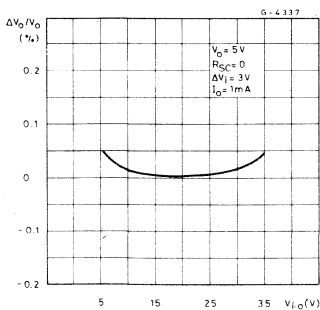


Fig. 8 - Load regulation vs. voltage drop

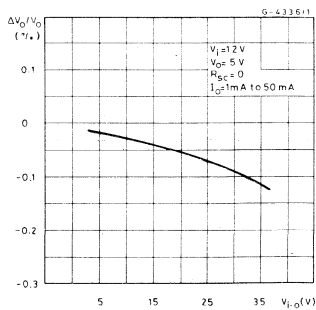


Fig. 9 - Quiescent drain current vs. input voltage

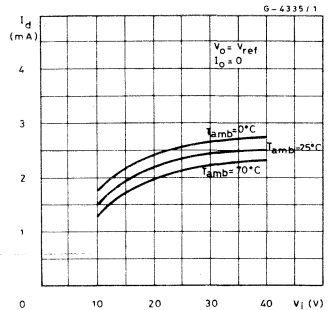


Fig. 10 - Line transient response

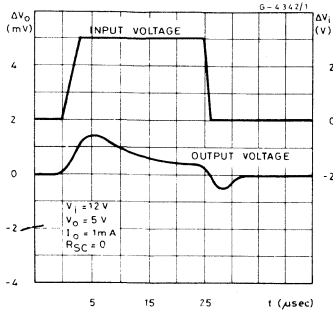


Fig. 11 - Load transient response

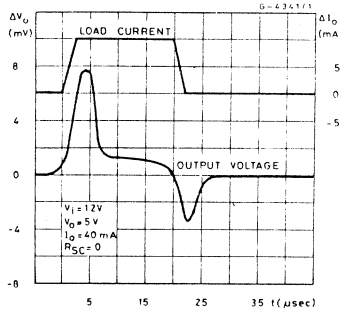


Fig. 12 - Output impedance vs. frequency

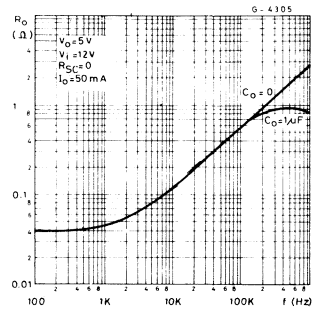


Table I - Resistor values (K Ω) for standard output voltages

Output Voltage	Applicable Figures	Fixed Output $\pm 5\%$		Output Adjustable $\pm 10\%$ ($^{\circ}$)			Output Voltage	Applicable Figures	Fixed Output $\pm 5\%$		Output Adjustable $\pm 10\%$ ($^{\circ}$)		
		R ₁	R ₂	R ₁	P ₁	R ₂			R ₁	R ₂	R ₁	P ₁	R ₂
+ 3	13, 16, 17 18, 21, 23	4.12	3.01	1.8	0.5	1.2	+100	19	3.57	102	2.2	10	91
+ 5	13, 16, 17 18, 21, 23	2.15	4.99	0.75	0.5	2.2	+250	19	3.57	255	2.2	10	240
+ 6	13, 16, 17 18, 21, 23	1.15	6.04	0.5	0.5	2.7	- 6($^{\circ\circ}$)	15	3.57	2.43	1.2	0.5	0.75
+ 9	14, 16, 17 18, 21, 23	1.87	7.15	0.75	1	2.7	- 9	15	3.48	5.36	1.2	0.5	2
+12	14, 16, 17 18, 21, 23	4.87	7.15	2	1	3	- 12	15	3.57	8.45	1.2	0.5	3.3
+15	14, 16, 17 18, 21, 23	7.87	7.15	3.3	1	3	- 15	15	3.65	11.5	-1.2	0.5	4.3
+28	14, 16, 17 18, 21, 23	21	7.15	5.6	1	2	- 28	15	3.57	24.3	1.2	0.5	10
+45	19	3.57	48.7	2.2	10	39	- 45	20	3.57	41.2	2.2	10	33
+75	19	3.57	78.7	2.2	10	68	-100	20	3.57	97.6	2.2	10	91
							-250	20	3.57	249	2.2	10	240

Note: ($^{\circ}$) Replace R₁/R₂ divider with the circuit of fig. 24.
 ($^{\circ\circ}$) V⁺ must be connected to a +3V or greater supply.

Table II - Formulae for intermediate output voltages

Outputs from +2 to +7 volts Fig. 13, 17, 18, 21, 23, 16 $V_O = [V_{ref} \times \frac{R_2}{R_1 + R_2}]$	Outputs from +4 to +250 volts Fig. 19 $V_O = [\frac{V_{ref}}{2} \times \frac{R_2 - R_1}{R_1}]; R_3 = R_4$	Current Limiting $I_{LIMIT} = \frac{V_{SENSE}}{R_{SC}}$
Outputs from +7 to +37 volts Fig. 14, 16, 17, 18, 21, 23 $V_O = [V_{ref} \times \frac{R_1 + R_2}{R_2}]$	Output from -6 to -250 volts Fig. 15, 20 $V_O = [\frac{V_{ref}}{2} \times \frac{R_1 + R_2}{R_1}]; R_3 = R_4$	Foldback Current Limiting $I_{KNEE} = [\frac{V_O}{R_{SC}} \frac{R_3}{R_4} + \frac{V_{SENSE}}{R_{SC}} \frac{(R_3 + R_4)}{R_4}]$ $I_{SHORT\ CKT} = [\frac{V_{SENSE}}{R_{SC}} \times \frac{R_3 + R_4}{R_4}]$

APPLICATION INFORMATION (Pin numbers relative to the plastic package)

Fig. 13 – Basic low voltage regulator ($V_o = 2$ to 7V)

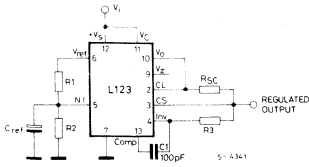
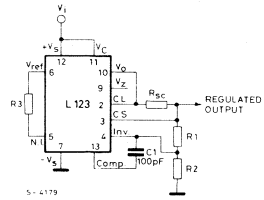


Fig. 14 – Basic high voltage regulator ($V_o = 7$ to 37V)



NOTE: $R_3 = \frac{R_1 \cdot R_2}{R_1 + R_2}$ for minimum temperature drift.

R_3 may be eliminated for minimum component count.

NOTE: $\frac{R_1 \cdot R_2}{R_1 + R_2}$ for minimum temperature drift.

R_3 may be eliminated for minimum component count.

Typical performance

Regulated Output Voltage 5V
 Line Regulation ($\Delta V_i = 3V$) 0.5 mV
 Load Regulation ($\Delta I_o = 50$ mA) 1.5 mV

Typical performance

Regulated Output Voltage 15V
 Line Regulation ($\Delta V_i = 3V$) 1.5 mV
 Load Regulation ($\Delta I_o = 50$ mA) 4.5 mV

Fig. 15 – Negative voltage regulator

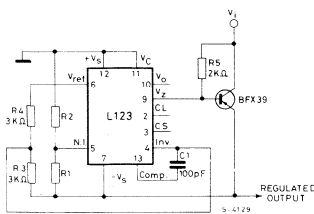
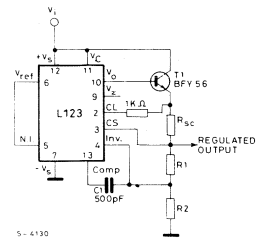


Fig. 16 – Positive voltage regulator (External NPN Pass Transistor)



Typical performance

Regulated Output Voltage -15V
 Line Regulation ($\Delta V_i = 3V$) 1 mV
 Load Regulation ($\Delta I_o = 100$ mA) 2 mV

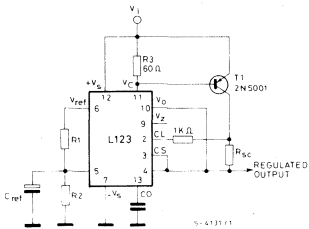
Typical performance

Regulated Output Voltage +15V
 Line Regulation ($\Delta V_i = 3V$) 1.5 mV
 Load Regulation ($\Delta I_o = 1A$) 15 mV

L123

APPLICATION INFORMATION (continued)

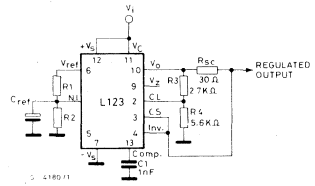
Fig. 17 - Positive voltage regulator (External PNP Pass Transistor)



Typical performance

Regulated Output Voltage +5V
 Line Regulation ($\Delta V_i = 3V$) 0.5 mV
 Load Regulation ($\Delta I_O = 1A$) 5 mV

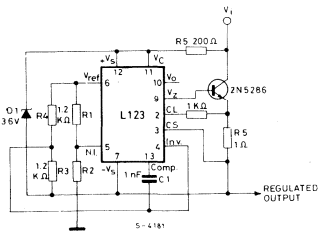
Fig. 18 - Foldback current limiting



Typical performance

Regulated Output Voltage +5V
 Line Regulation ($\Delta V_i = 3V$) 0.5 mV
 Load Regulation ($\Delta I_O = 10 mA$) 1 mV
 Current Limit Knee 20 mA

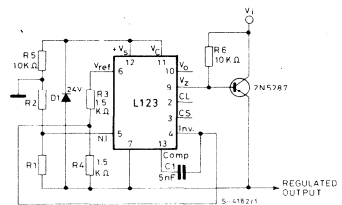
Fig. 19 - Positive floating regulator



Typical performance

Regulated Output Voltage +100V
 Line Regulation ($\Delta V_i = 20V$) 15 mV
 Load Regulation ($\Delta I_O = 50 mA$) 20 mV

Fig. 20 - Negative floating regulator



Typical performance

Regulated Output Voltage -100V
 Line Regulation ($\Delta V_i = 20V$) 30 mV
 Load Regulation ($\Delta I_O = 100 mA$) 20 mV

L 129
L 130
L 131

LINEAR INTEGRATED CIRCUITS

3-TERMINAL POSITIVE VOLTAGE REGULATORS

- OUTPUT VOLTAGES OF 5, 12, 15V
- OUTPUT CURRENT 600 mA, 500 mA, 450 mA
- SHORT CIRCUIT PROTECTION
- OUTPUT TRANSISTOR SOA PROTECTION
- EXCELLENT TRANSIENT RESPONSE

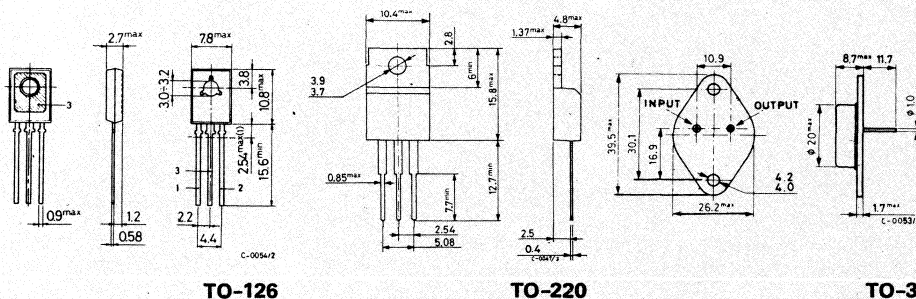
The L129, L130, L131 three-terminal positive voltage regulators are available in SOT-32, TO-220 and TO-3 packages with 3 fixed output voltages, making them useful in a wide range of applications. These regulators can provide local on-card regulation eliminating the distribution problems associated with single point regulation. Each type employs internal overload protection and short circuit protection. Although designed primarily as fixed voltage regulators, these devices can be used with external components to obtain adjustable output voltages and currents.

ABSOLUTE MAXIMUM RATINGS

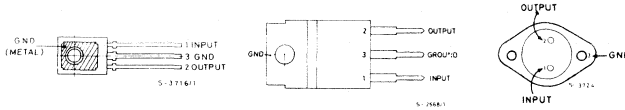
V_i	DC input voltage	L 129	20	V
		L 130, L 131	27	V
P_{tot}	Power dissipation at $T_{amb} = 25^\circ\text{C}$ (SOT-32)		1.25	W
	at $T_{case} = 25^\circ\text{C}$ (SOT-32)		14	W
T_{stg}	Storage temperature		-55 to 150	$^\circ\text{C}$
T_{op}	Operating junction temperature		-20 to 150	$^\circ\text{C}$

MECHANICAL DATA

Dimensions in mm

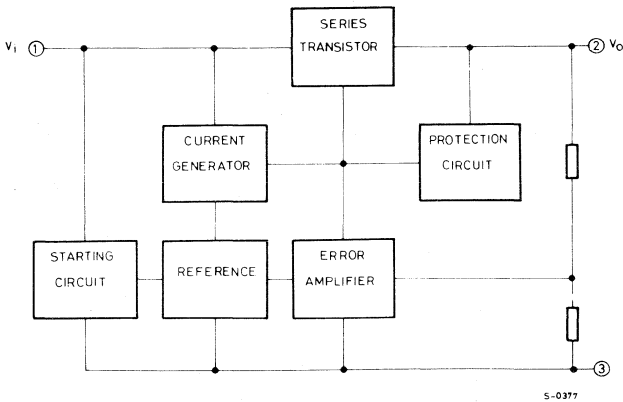


CONNECTION DIAGRAMS AND ORDERING NUMBERS



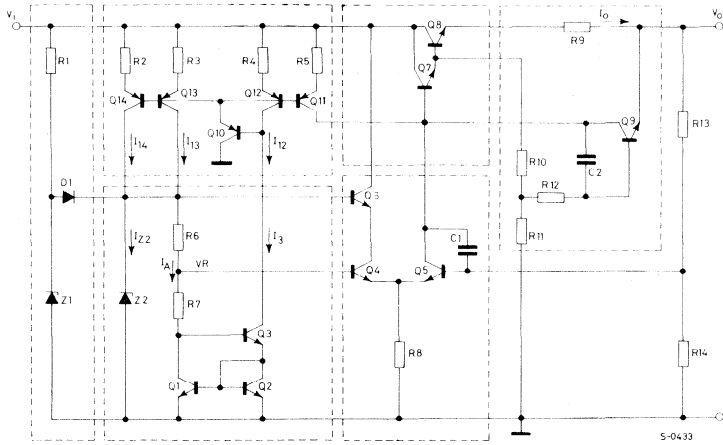
Type	SOT-32	TO-220	TO-3	Output Voltage
L129	L129	L129V	L005 T1	5V
L130	L130	L130V	L036 T1	12V
L131	L131	L131V	L037 T1	15V

BLOCK DIAGRAM



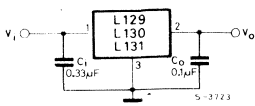
L 129 L 130 L 131

SCHEMATIC DIAGRAM

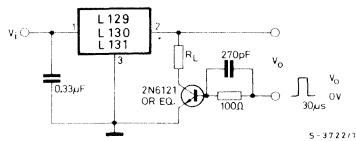


TEST CIRCUITS

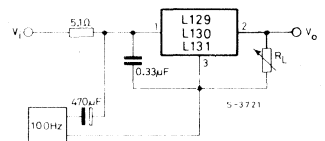
DC Parameter



Load regulation



Ripple rejection



THERMAL DATA

			SOT-32	TO-220	TO-3
$R_{th\ j-case}$	Thermal resistance junction-case	max	9 °C/W	3 °C/W	4 °C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	100 °C/W	50 °C/W	35 °C/W

ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^{\circ}C$, $I_o = 10\ mA$, $C_L = 10\ \mu F$ unless otherwise specified)

Parameter			Test conditions	Min.	Typ.	Max.	Unit
V_o	Output voltage	L129 L130 L131	$V_i = 7.5\ to\ 20V$ $V_i = 14.5\ to\ 27V$ $V_i = 17.5\ to\ 27V$	4.75 11.4 14.25	5 12 15	5.25 12.6 15.75	V
ΔV_o	Load regulation		$I_o = 10\ to\ 600\ mA$		0.3	1	%
I_o	Regulated output current	L129 L130 L131	$\frac{\Delta V_o}{V_o} \leq 1\%$	600 500 450	850 720 600		mA
$I_o\ MAX$	Maximum output current	L129 L130 L131	$T_{case} = 25^{\circ}C$ $T_{case} = 85^{\circ}C$ $T_{case} = 25^{\circ}C$ $T_{case} = 85^{\circ}C$ $T_{case} = 25^{\circ}C$ $T_{case} = 85^{\circ}C$		0.93 1 0.75 0.8 0.68 0.8	1.2 1 0.9	A A A
I_{sc}	Output short-circuit current	L129 L130 L131			200 100 85	250 200 160	mA
I_d	Quiescent drain current				9		mA
ΔV_o	Line regulation	L129 L130 L131	$V_i = 7.5\ to\ 12V$ $V_i = 14.5\ to\ 21V$ $V_i = 17.5\ to\ 24V$		5 6 6	23 33 33	mV
$\frac{\Delta V_o}{\Delta T_{amb}}$	Temperature coefficient	L129 L130 L131	$T_{amb} = -20\ to\ 85^{\circ}C$		0.5 1.2 1.5		mV/°C
e_N	Output noise voltage	L129 L130 L131	$C_L = 20\ \mu F$ $B = 10\ Hz\ to\ 100\ kHz$		70 150 180		μV
R_o	Output resistance	L129 L130 L131	$I_o = 600\ mA$ $I_o = 500\ mA$ $I_o = 450\ mA$		15 20 60		m Ω
SVR	Supply voltage rejection	L129 L130 L131	$\Delta V_i = 4V_{pp}$ $f = 100\ Hz$	46 46 46	60 60 56		dB

L129 L130 L131

Fig. 1 - Output voltage vs. output current (L129)

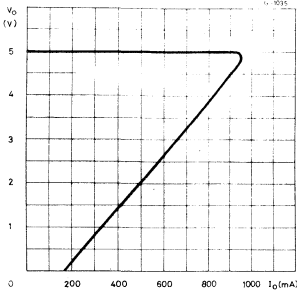


Fig. 2 - Output voltage vs. output current (L130)

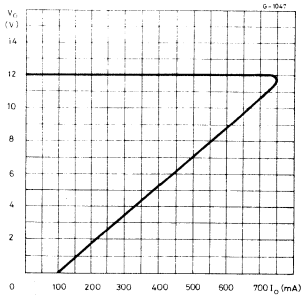


Fig. 3 - Output voltage vs. output current (L131)

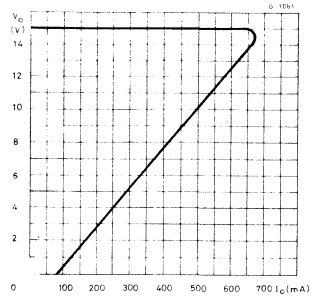


Fig. 4 - Power rating chart (for SOT-32)

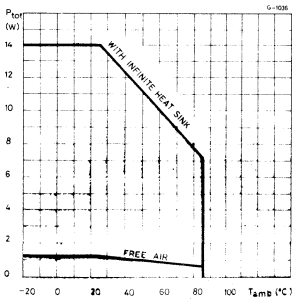


Fig. 5 - Regulated output current vs. junction temperature

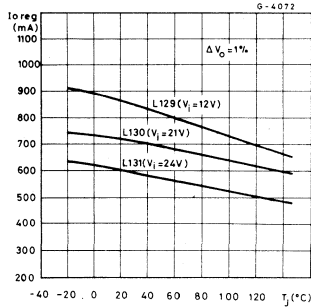


Fig. 6 - Maximum output current vs. junction temperature

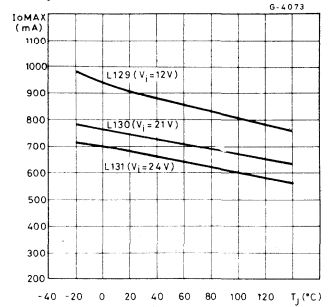


Fig. 7 - Dropout voltage vs. junction temperature (L129)

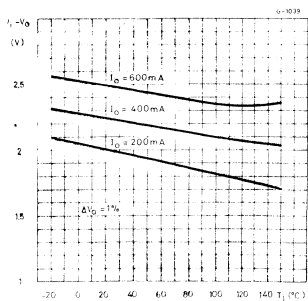


Fig. 8 - Dropout voltage vs. junction temperature (L130)

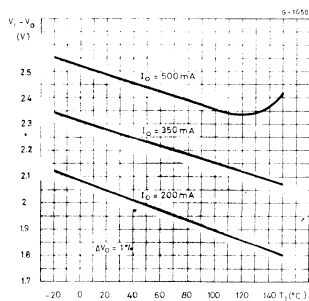


Fig. 9 - Dropout voltage vs. junction temperature (L131)

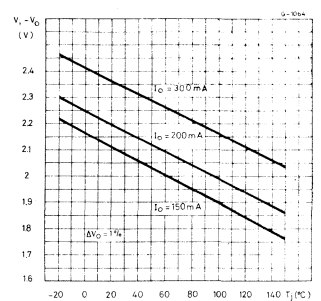


Fig. 10 - Short-circuit current vs. input voltage (L129)

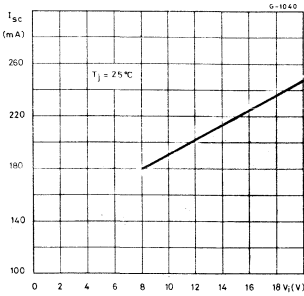


Fig. 11 - Short-circuit current vs. input voltage (L130)

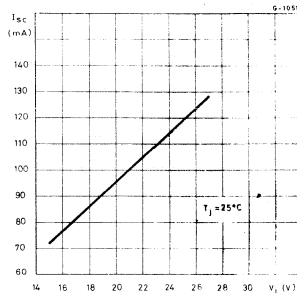


Fig. 12 - Short-circuit current vs. input voltage (L131)

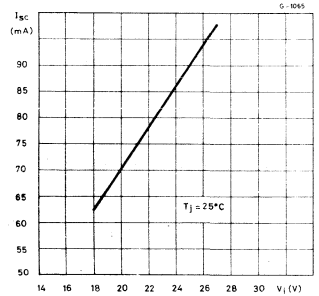


Fig. 13 - Short-circuit vs. junction temperature (L129)

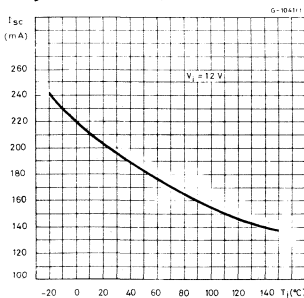


Fig. 14 - Short-circuit vs. junction temperature (L130)

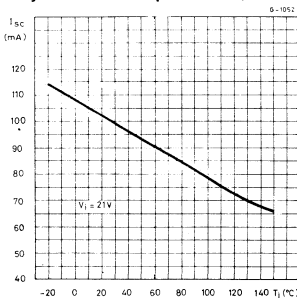


Fig. 15 - Short-circuit vs. junction temperature (L131)

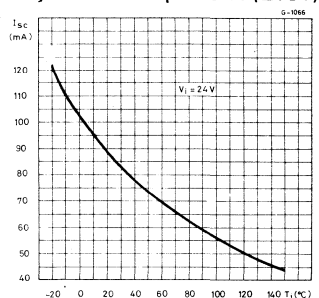


Fig. 16 - Quiescent drain current vs. junction temperature (L129)

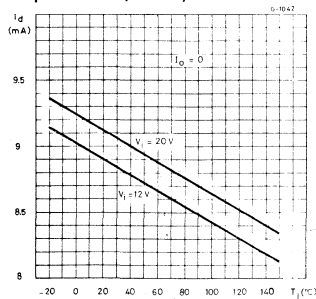


Fig. 17 - Quiescent drain current vs. junction temperature (L130)

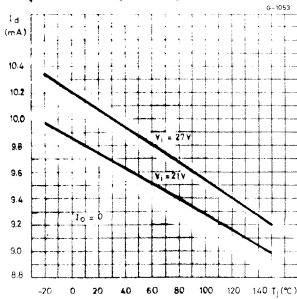
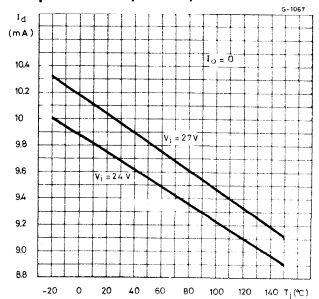


Fig. 18 - Quiescent drain current vs. junction temperature (L131)



L129 L130 L131

Fig. 19 - Quiescent drain current variation vs. junction temperature (L129)

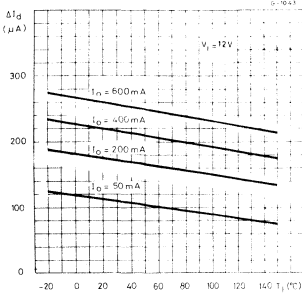


Fig. 20 - Quiescent drain current variation vs. junction temperature (L130)

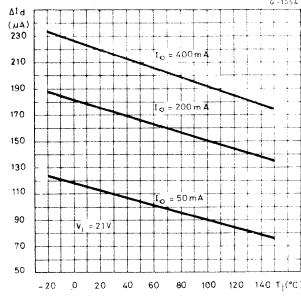


Fig. 21 - Quiescent drain current variation vs. junction temperature (L131)

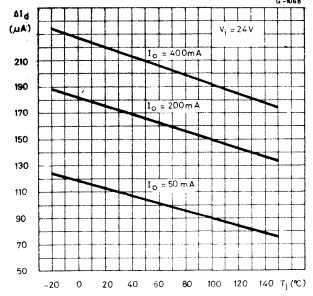


Fig. 22 - Supply voltage rejection vs. frequency

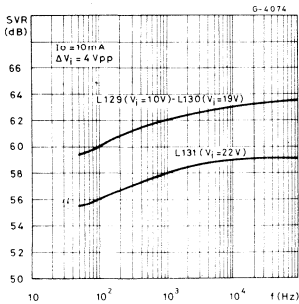


Fig. 23 - Supply voltage rejection vs. regulated output current

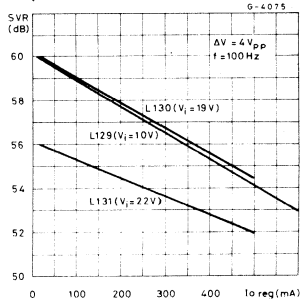


Fig. 24 - Output resistance vs. frequency

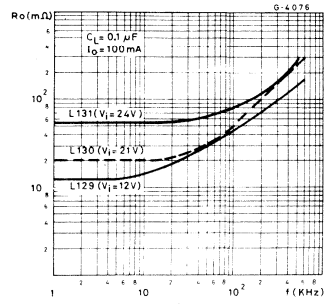
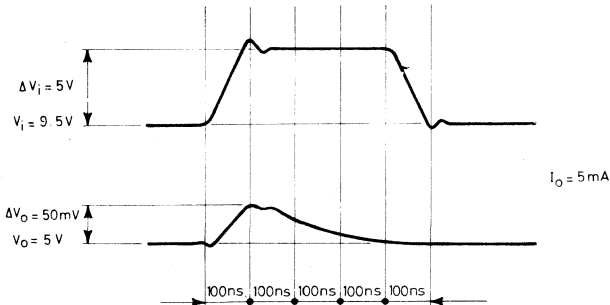
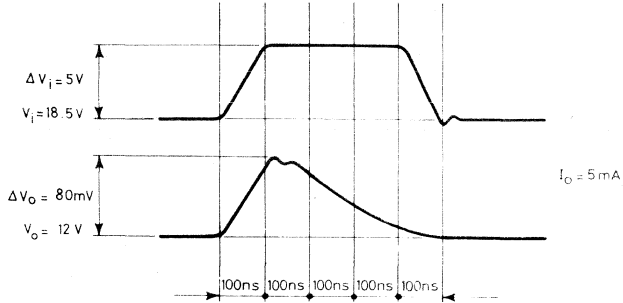


Fig. 25 - Line transient response (L129)



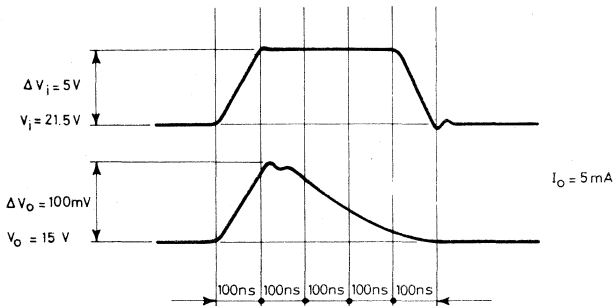
S-0437

Fig. 26 - Line transient response (L130)



S-0445

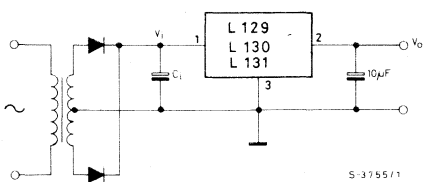
Fig. 27 - Line transient response (L131)



S-0412

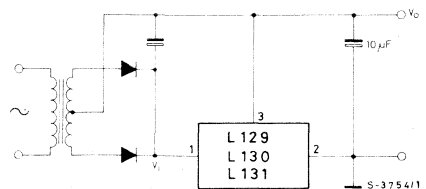
APPLICATION INFORMATION

Fig. 28 - Positive regulator



S-3755/1

Fig. 29 - Negative regulator

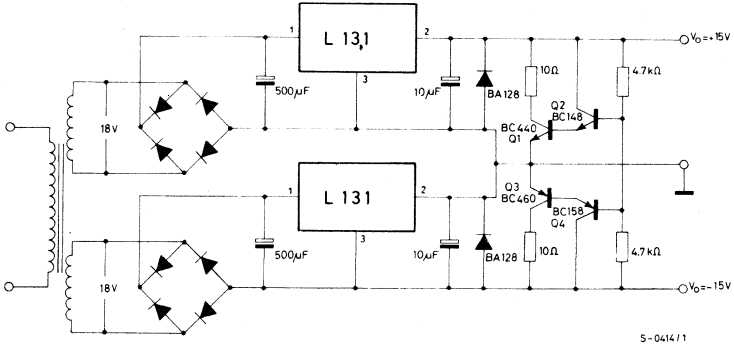


S-3754/1

L 129 L 130 L 131

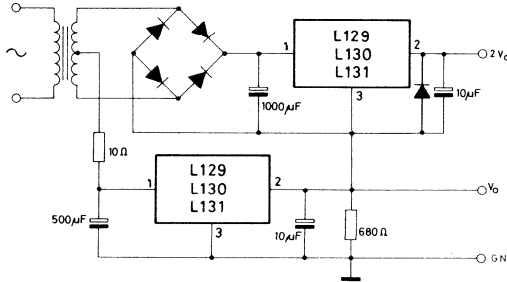
APPLICATION INFORMATION (continued)

Fig. 30 - Symmetrical ± 15V voltage regulator circuit



5-0414 / 1

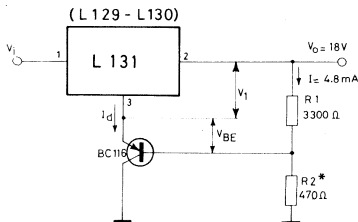
Fig. 31 - Series regulators circuit connection



5-0415 / 2

Fig. 32 - Low consumption circuit to increase output voltage

$$V_o = V_1 \left(1 + \frac{R_2}{R_1} \right) + V_{BE} \left(1 + \frac{R_2}{R_1} \right) + \frac{I_d}{h_{FEQ1}} \cdot R_2$$



$$\begin{aligned} I_d &= 10 \text{ mA} \\ V_i &= 25 \text{ V} \\ \frac{\delta I_d}{\delta T_{amb}} &= -7 \mu\text{A}/^\circ\text{C typ.} \\ \frac{\delta I_d}{\delta V_i} &= 30 \mu\text{A/V typ.} \\ \frac{\delta V_{BE}}{\delta T_{amb}} &= -2 \text{ mV}/^\circ\text{C} \end{aligned}$$

* Fixed or adjustable

5-0416 / 2

LINEAR INTEGRATED CIRCUIT

HIGH PRECISION HIGH VOLTAGE REGULATOR

- INPUT VOLTAGE UP TO 80V
- OUTPUT VOLTAGE ADJUSTABLE FROM 2 TO 77V
- POSITIVE OR NEGATIVE SUPPLY OPERATION
- SERIES, SHUNT, SWITCHING OR FLOATING OPERATION
- OUTPUT CURRENT UP TO 150 mA WITHOUT EXTERNAL PASS TRANSISTOR
- ADJUSTABLE CURRENT LIMITING
- THERMAL PROTECTION

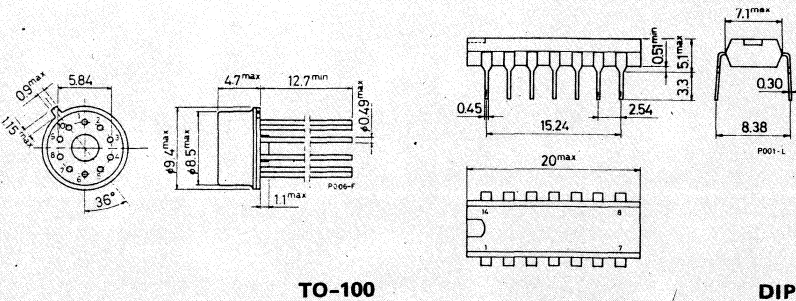
The L146 is a monolithic integrated programmable voltage regulator in 14 lead dual in-line plastic package and 10 lead Metal Can (TO-100 type). It is made with high voltage technology and provides internal current limiting and thermal shut down protection; when current exceeds 150 mA an external NPN or PNP pass element may be used. Provisions are made for adjustable current limiting and remote shut down. The L146 is intended to widen the application range of L123 up to 80V.

ABSOLUTE MAXIMUM RATINGS

V_i	Input voltage	80	V
$V_i - V_o$	Voltage drop	78	V
I_o	Output current	150	mA
I_{ref}	Current from V_{ref}	8	mA
P_d	Power dissipation (at $T_{amb} = 70^\circ\text{C}$) Plastic DIP TO-100	1 520	W mW
T_{op}	Operating junction temperature L146 L146C	-25 to +85 0 to +70	$^\circ\text{C}$ $^\circ\text{C}$
T_{stg}	Storage temperature	-65 to +150	$^\circ\text{C}$

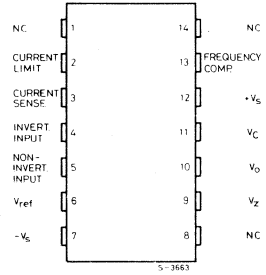
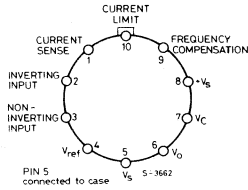
MECHANICAL DATA

Dimensions in mm



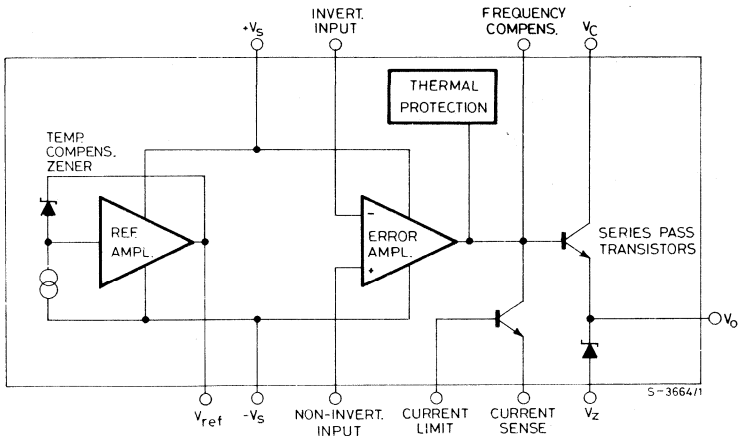
L 146

CONNECTION DIAGRAMS (top view)



Type	TO-100	Plastic DIP
L 146	L146 T	
L 146 C	L146 CT	L146 CB

BLOCK DIAGRAM

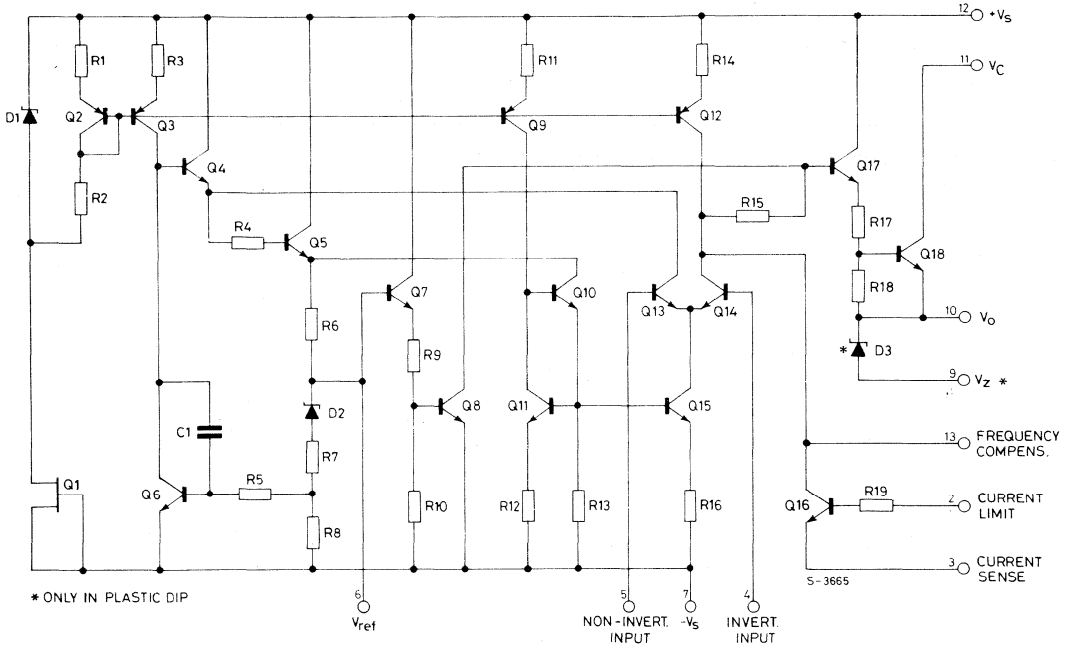


THERMAL DATA

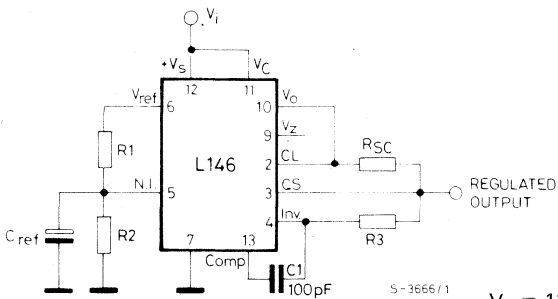
	TO-100	Plastic DIP
$R_{th\ j-amb}$ Thermal resistance junction-ambient	max 155°C/W	80°C/W

L146

SCHEMATIC DIAGRAM (pin number relative to the plastic package)



TEST CIRCUIT



$$V_i = 12V$$

$$V_o = 5V \quad I_o = 1mA$$

$$R_1 // R_2 \leq 10 K\Omega$$

L146

ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $T_{amb} = 25^{\circ}\text{C}$ unless otherwise specified)

Parameter	Test conditions	L146 C			L146			Unit
		Min.	Typ.	Max.	Min.	Typ.	Max.	
$\frac{\Delta V_o}{\Delta V_i}$ Line regulation	$V_i = 12$ to 15V $V_i = 12$ to 40V $V_i = 40$ to 80V		0.05 0.1 0.1	0.15 0.5 0.5		0.05 0.1 0.1	0.15 0.2 0.2	%
$\frac{\Delta V_o}{V_o}$ Load regulation	$V_i = 12\text{V}$ $V_o = 5\text{V}$ $I_o = 1$ to 50 mA		0.03	0.2		0.03	0.15	%
	$V_i = 40\text{V}$ $V_o = 37\text{V}$ $I_o = 1$ to 10 mA		0.1	0.5		0.1	0.3	%
	$V_i = 80\text{V}$ $V_o = 77\text{V}$ $I_o = 1$ to 10 mA		0.12	0.8		0.12	0.5	%
V_{ref} Reference voltage	$I_{ref} = 160$ μA	7.75	8.15	8.55	7.9	8.15	8.4	V
ΔV_{ref}	$I_{ref} = 160$ μA to 5 mA		4	14		4	14	mV
SVR Ripple rejection	$f = 100$ Hz to 10 KHz $C_{ref} = 0$ $C_{ref} = 5$ μF		60 88			60 88		dB
$\frac{\Delta V_o}{\Delta T}$ Output voltage drift				150			150	$\frac{\text{ppm}}{^{\circ}\text{C}}$
I_{sc} Short circuit current limiting	$R_{sc} = 10\Omega$ $V_o = 0$	50	60	70	50	60	70	mA
V_i Input voltage range		10		80	10		80	V
V_o Output voltage range		2		77	2		77	V
$V_i - V_o$ Voltage drop		3		78	3		78	V
I_d Quiescent drain current	$I_o = 0$ (including $I_{ref} = 160$ μA) $V_o = 5\text{V}$ $V_i = 12\text{V}$ $V_i = 40\text{V}$ $V_i = 80\text{V}$		4 5.6 6	5.5 7 7.5		4 5.6 6	5.5 7 7.5	mA
ΔI_d Quiescent drain current change	$I_o = 1$ mA $V_o = 5\text{V}$	$V_i = 12$ to 40V		2.2			1.6	mA
		$V_i = 12$ to 80V		2.6			2	mA
Long term stability			0.1			0.1		$\frac{\%}{1000 \text{ hrs}}$
e_N Output noise voltage	BW = 100 Hz to 10 KHz $C_{ref} = 0$ $C_{ref} = 5$ μF		300 30			300 30		μV
V_z Output zener voltage (for plastic package only)	$I_z = 1$ mA	6.9		7.7				V

Fig. 1 - Maximum output current vs. voltage drop

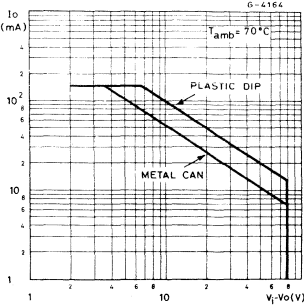


Fig. 2 - Load regulation vs. output current (with current limiting)

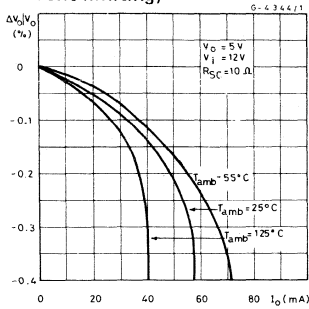


Fig. 3 - Load regulation vs. output current (with current limiting)

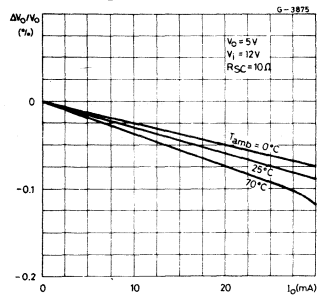


Fig. 4 - Load regulation vs. output current (without current limiting)

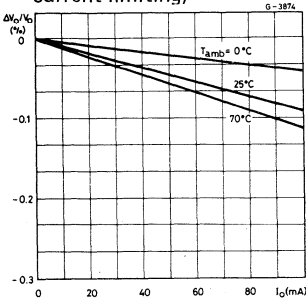


Fig. 5 - Current limiting characteristics

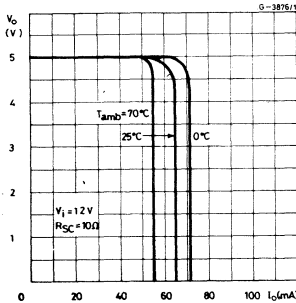


Fig. 6 - Current limiting characteristics vs. junction temperature

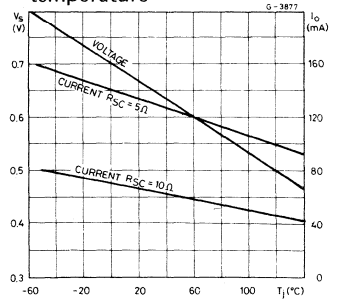


Fig. 7 - Line transient response

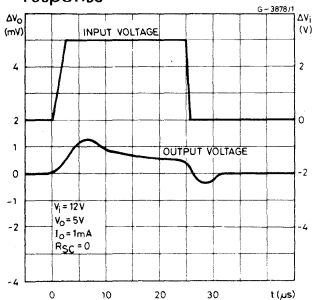


Fig. 8 - Load transient response

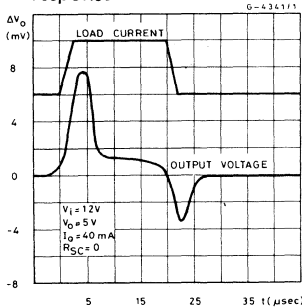
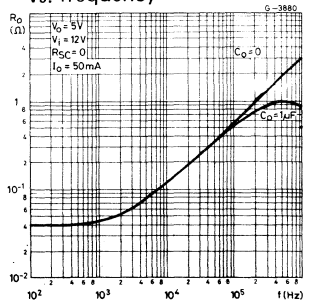


Fig. 9 - Output impedance vs. frequency



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Table I -- Resistor values (K Ω) for standard output voltage

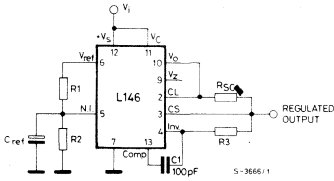
Positive output voltage	Applicable figures	Fixed output $\pm 5\%$		Negative output voltage	Applicable figures	Fixed output $\pm 5\%$	
		R ₁	R ₂			R ₁	R ₂
+6	10, 13, 14 18, 20	2.4	6.8	-9	12	2.2	2.7
+12	11, 13, 14, 15, 18, 20	3.2	6.8	-12		1.5	3
+30		15	5.6	-30		4.7	30
+50		24	47	-50		2.7	30
+70	16	30	39	-100	17	2	47
+100		2.7	68	-250		2	120
+250		4.7	120				

Table II -- Formulae for intermediate output voltages

Outputs from +2 to +7 volts Fig. 10, 13, 14, 15, 18, 20 $V_{OUT} = \left[V_{REF} \times \frac{R_2}{R_1 + R_2} \right]$	Outputs from +4 to +250 volts Fig. 16 $V_{OUT} = \left[\frac{V_{REF}}{2} \times \frac{R_2 - R_1}{R_1} \right]; R_3 = R_4$	Current Limiting $I_{LIMIT} = \frac{V_{SENSE}}{R_{sc}}$
Outputs from +7 to +77 volts Fig. 11, 13, 14, 15, 18, 20 $V_{OUT} = \left[V_{REF} \times \frac{R_1 + R_2}{R_2} \right]$	Output from -6 to -250 volts Fig. 12, 17 $V_{OUT} = \left[\frac{V_{REF}}{2} \times \frac{R_1 + R_2}{R_1} \right]; R_3 = R_4$	Foldback Current Limiting $I_{KNEE} = \left[\frac{V_{OUT}}{R_{sc}} \frac{R_3}{R_4} + \frac{V_{SENSE}}{R_{sc}} \frac{(R_3 + R_4)}{R_4} \right]$ $I_{SHORT\ CKT} = \left[\frac{V_{SENSE}}{R_{sc}} \times \frac{R_3 + R_4}{R_4} \right]$

APPLICATION CIRCUITS (continued)

Fig. 10 - Basic low voltage regulator
($V_{OUT} = 2$ to $7V$)



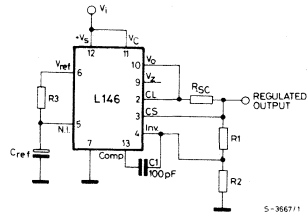
NOTE: $R3 = \frac{R1 \cdot R2}{R1 + R2}$ for minimum temperature drift.

R3 may be eliminated for minimum component count.

Typical performance

Regulated Output Voltage $5V$
Line Regulation ($\Delta V_i = 3V$) 0.5 mV
Load Regulation ($\Delta I_o = 50$ mA) 1.5 mV

Fig. 11 - Basic high voltage regulator
($V_{OUT} = 7$ to $77V$)



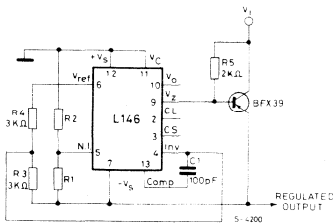
NOTE: $R3 = \frac{R1 \cdot R2}{R1 + R2}$ for minimum temperature drift.

R3 may be eliminated for minimum component count.

Typical performance

Regulated Output Voltage $15V$
Line Regulation ($\Delta V_i = 3V$) 1.5 mV
Load Regulation ($\Delta I_o = 50$ mA) 4.5 mV

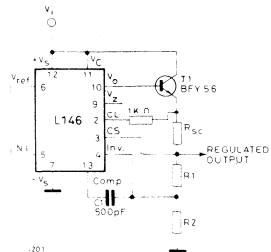
Fig. 12 - Negative voltage regulator



Typical performance

Regulated Output Voltage $+15V$
Line Regulation ($\Delta V_i = 3V$) 1.5 mV
Load Regulation ($\Delta I_o = 1$ A) 15 mV

Fig. 13 - Positive voltage regulator (External NPN Pass Transistor)



Typical performance

Regulated Output Voltage $15V$
Line Regulation ($\Delta V_i = 3V$) 1 mV
Load Regulation ($\Delta I_o = 100$ mA) 2 mV

L 146

APPLICATION CIRCUITS (continued)

Fig. 14 - Positive voltage regulator (External PNP Pass Transistor)

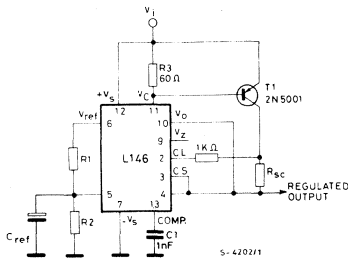
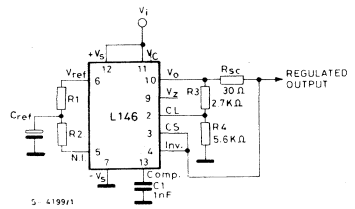


Fig. 15 - Foldback current limiting



Typical performance

Regulated Output Voltage +5V
 Line Regulation ($\Delta V_i = 3V$) 0.5 mV
 Load Regulation ($\Delta I_o = 1A$) 5 mV

Typical performance

Regulated Output Voltage +5V
 Line Regulation ($\Delta V_i = 3V$) 0.5 mV
 Load Regulation ($\Delta I_o = 10 mA$) 1 mV
 Current Limit Knee 20 mA

Fig. 16 - Positive floating regulator

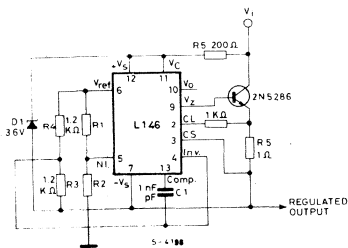
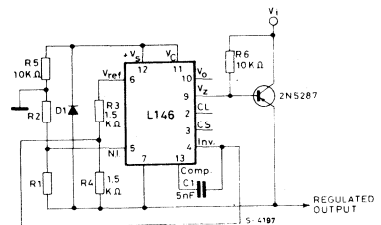


Fig. 17 - Negative floating regulator



Typical performance

Regulated Output Voltage +100V
 Line Regulation ($\Delta V_i = 20V$) 15 mV
 Load Regulation ($\Delta I_o = 50 mA$) 20 mV

Typical performance

Regulated Output Voltage -100V
 Line Regulation ($\Delta V_i = 20V$) 30 mV
 Load Regulation ($\Delta I_o = 100 mA$) 20 mV

APPLICATION CIRCUITS (continued)

Fig. 18 - Positive switching regulator

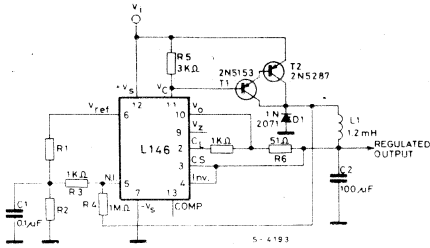
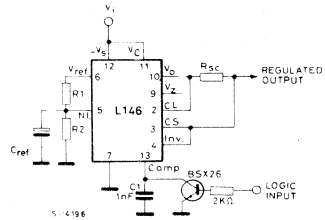


Fig. 19 - Remote shutdown regulator with current limiting



Typical performance

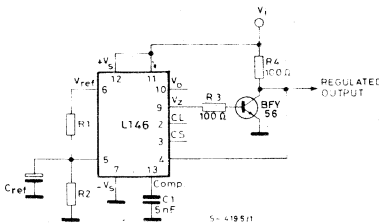
Regulated Output Voltage +5V
 Line Regulation ($\Delta V_i = 30V$) 10 mV
 Load Regulation ($\Delta I_o = 2A$) 80 mA

Typical performance

Regulated Output Voltage5V
 Line Regulation ($\Delta V_i = 3V$) 0.5V
 Load Regulation ($\Delta I_o = 50 mA$) 1.5 mV

NOTE: Current limit transistor may be used for shutdown if current limiting is not required.

Fig. 20 - Shunt regulator



Typical performance

Regulated Output Voltage +5V
 Line Regulation ($\Delta V_i = 10V$) 2 mV
 Load Regulation ($\Delta I_o = 100 mA$) 5mV

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APPLICATION CIRCUITS (continued)

Fig. 21 - 50V voltage regulator with foldback characteristic

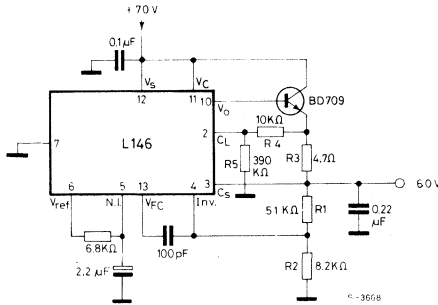
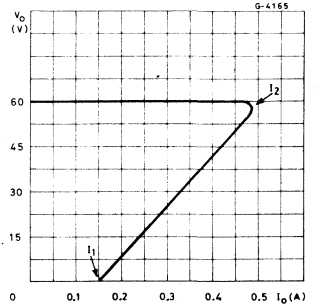
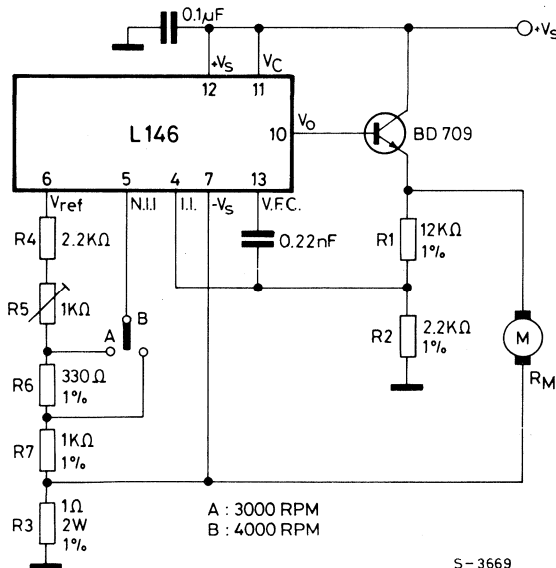


Fig. 22



$$I_2 = \frac{V_o \frac{R_4}{R_5} + V_{2-3}}{R_{SC}} ; \quad I_1 = \frac{V_{2-3}}{R_{SC}} \left(1 + \frac{R_4}{R_5}\right); \quad V_{2-3} \cong 0.7V$$

Fig. 23 - Motor speed control

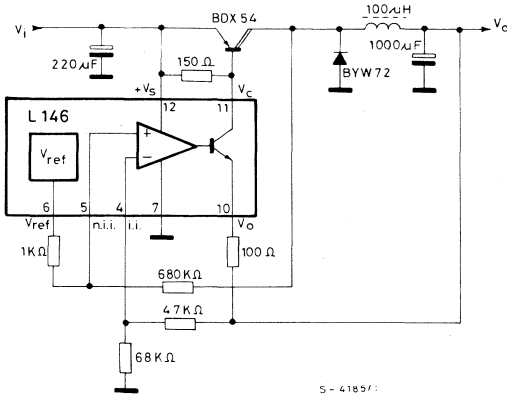


APPLICATION CIRCUITS (continued)

Fig. 24 - Step-down switching regulator for 12V car radio

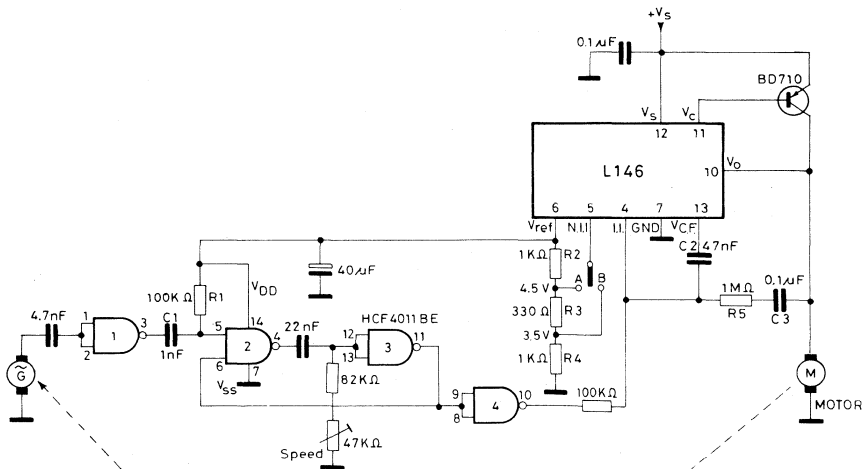
Performance:

Output voltage	13.5V
Max output current	3A
Input voltage range	20 to 30V
Line regulation	50 dB ($I_O = 2A$) $\Delta V_i = 10V$
Load regulation	0.1% ($\Delta I_O = 3A$)
Ripple	100 mVpp
Efficiency	75% ($I_O = 3A$)
Switching frequency	25 KHz



S-4185/F

Fig. 25 - 30W motor speed regulator with tacho adjustment and speed change-over switch



S-4186/1

MONOLITHIC HIGH GAIN POWER OUTPUT STAGE

The L149 is a general purpose power booster in Pentawatt[®] package consisting of a quasi-complementary darlington's output stage with the associated biasing system and inhibit facility.

The circuit features are:

- High output current (4A peak)
- High current gain (10 000 typ.)
- Operation up to $\pm 20V$
- Thermal protection
- Short circuit protection
- Operation within SOA
- High slew-rate

The device is particularly suited for use with an operational amplifier inside a closed loop configuration to increase output current ($P_o = 20W$, $d = 0.5\%$, $R_L = 4\Omega$, $V_s = \pm 16V$).

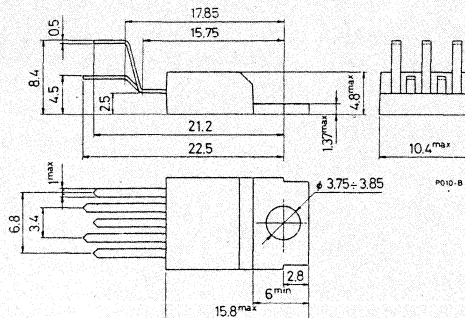
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	± 20	V
V_i	Input voltage	V_s	
I_o	DC output current	3	A
I_o	Peak output current (internally limited)	4	A
V_{INH}	Input inhibit voltage	$-V_s + 5$	V
		$-V_s - 1.5$	V
P_{tot}	Power dissipation at $T_{case} = 70^\circ C$	26	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ C$

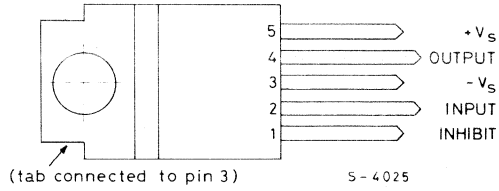
ORDERING NUMBER: L149V

MECHANICAL DATA

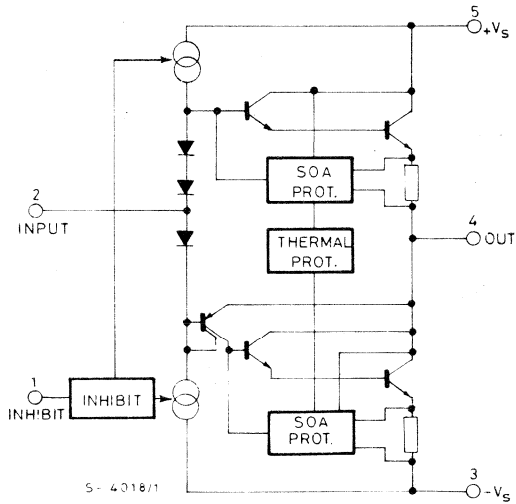
Dimensions in mm



CONNECTION DIAGRAM (top view)



SCHEMATIC DIAGRAM



L 149

THERMAL DATA

$R_{th\ j-case}$	Thermal resistance junction-case	max	3	$^{\circ}C/W$
------------------	----------------------------------	-----	---	---------------

ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^{\circ}C$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s	Supply voltage			± 20	V
I_d	Quiescent drain current	$V_s = \pm 16V$	30		mA
I_{in}	Input current	$V_s = \pm 16V$ $V_i = 0V$	200	400	μA
h_{FE}	DC current gain	$V_s = \pm 16V$ $I_o = 3A$	6000	10000	—
G_v	Voltage gain	$V_s = \pm 16V$ $I_o = 1.5A$	1		—
V_{CEsat}	Saturation voltage (for each transistor)	$I_o = 3A$		3.5	V
V_{os}	Input offset voltage	$V_s = \pm 16V$		0.3	V
V_{INH}	Inhibit input voltage (pins 1-3)	ON condition		± 0.3	V
		OFF condition	± 1.2		
R_{INH}	Inhibit input resistance	$f = 1\text{ KHz}$	2.0		K Ω
SR	Slew rate		30		V/ μs
B	Power bandwidth	$V_s = \pm 18V$, $d = 1\%$, $R_L = 8\Omega$	200		KHz

TEST CIRCUIT

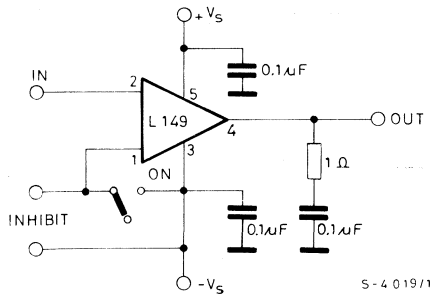


Fig. 1 - Maximum saturation voltage vs. output current

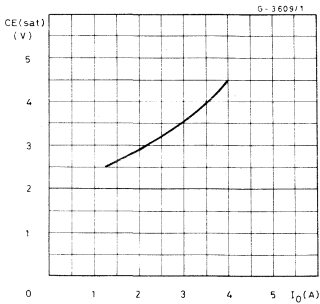


Fig. 2 - Current limiting characteristics

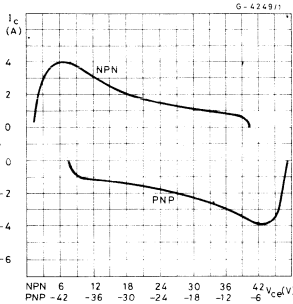
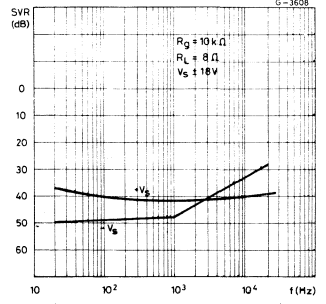


Fig. 3 - Supply voltage rejection vs. frequency



APPLICATION INFORMATION

Fig. 4 - High power amplifier with single power supply ($G_v = 30$ dB)

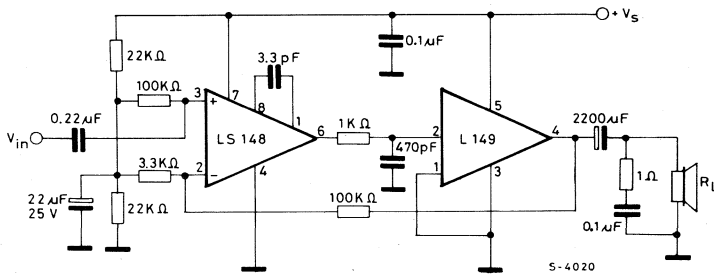


Fig. 5 - Distortion vs. output power ($f = 1$ KHz)

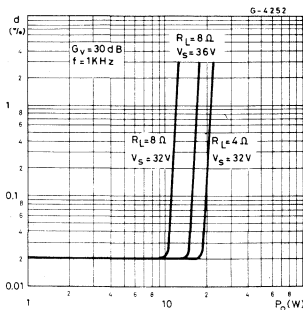


Fig. 6 - Distortion vs. output power ($f = 10$ KHz)

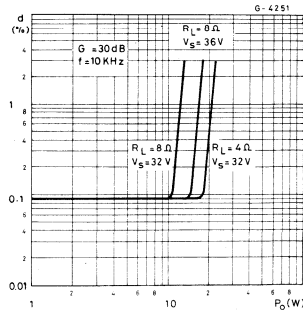
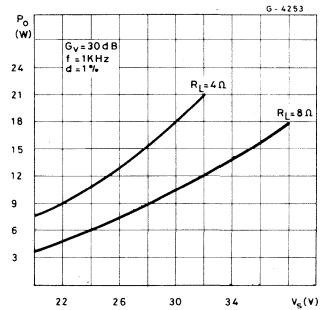


Fig. 7 - Output power vs. supply voltage



APPLICATION INFORMATION (continued)

Fig. 8 - High power amplifier with split power supply ($G_v = 30$ dB)

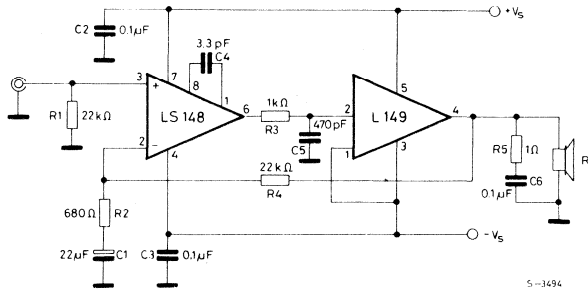


Fig. 9 - Bidirectional speed control of DC motor

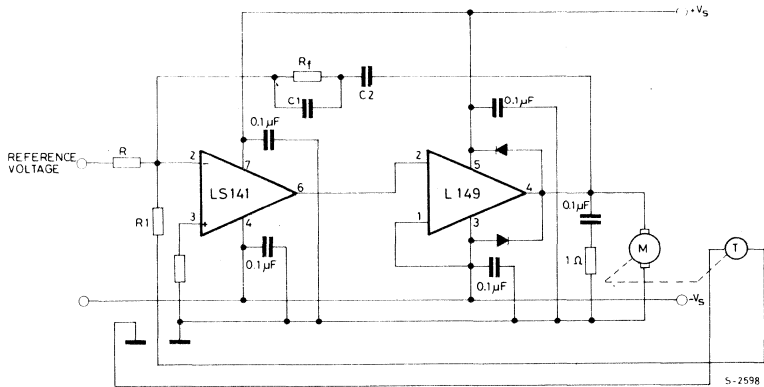
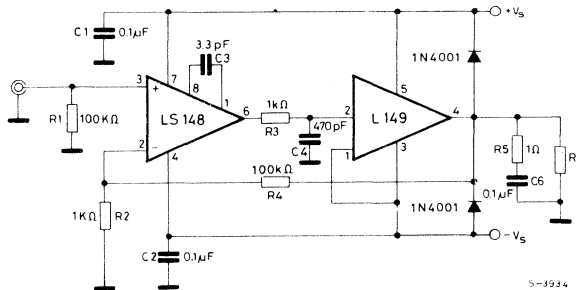


Fig. 10 - High slew-rate power operational amplifier



APPLICATION INFORMATION (continued)

Fig. 11 - 720W Switched Mode Power Supply using the L149 as driver stage for the power transistors

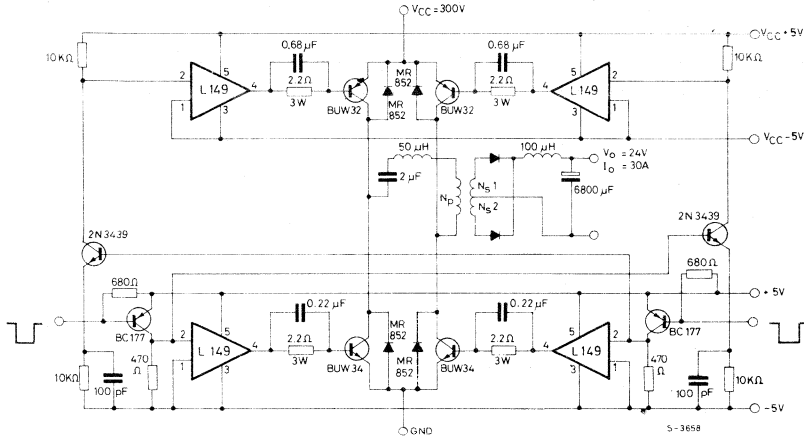
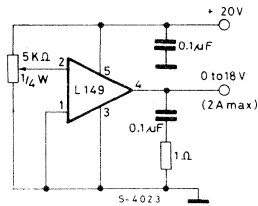


Fig. 12 - Electronic potentiometer (short-circuit protected)



L 165

LINEAR INTEGRATED CIRCUIT

PRELIMINARY DATA

3A POWER OPERATIONAL AMPLIFIER

The L165 is a monolithic integrated circuit in Pentawatt[®] package, intended for use as power operational amplifier in a wide range of applications, including servo amplifiers and power supplies. The high gain and high output power capability provide superior performance wherever an operational amplifier/power booster combination is required,

- Output current up to 3A.
- Large common-mode and differential mode ranges.
- SOA protection.
- Thermal protection.

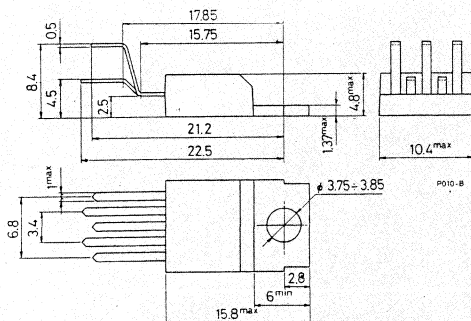
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	± 18	V
V_i	Input voltage	V_s	
V_i	Differential input voltage	± 15	V
I_o	Peak output current (internally limited)	3.5	A
P_{tot}	Power dissipation at $T_{case} = 90^\circ\text{C}$	20	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBER: L165V

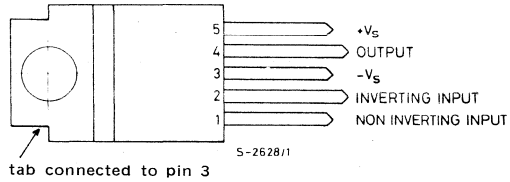
MECHANICAL DATA

Dimensions in mm

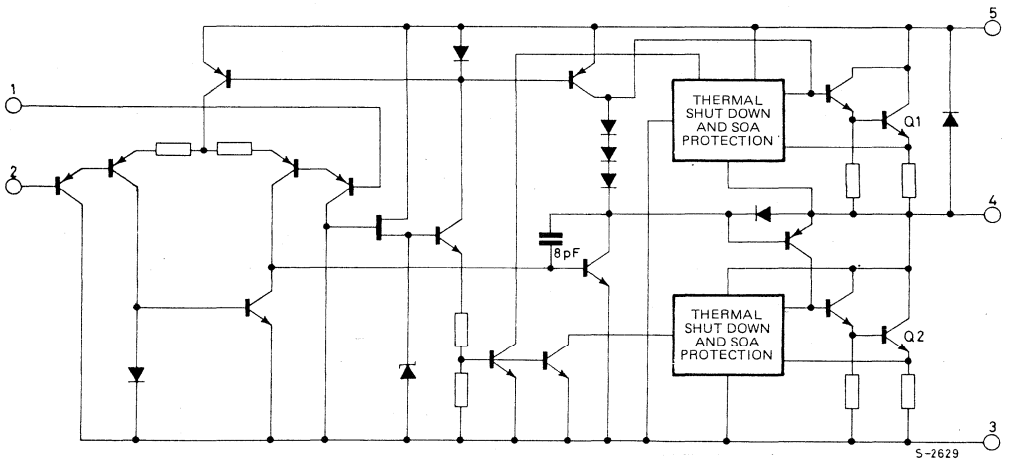


L 165

CONNECTION DIAGRAM (top view)



SCHEMATIC DIAGRAM



THERMAL DATA

$R_{th\ j-case}$ Thermal resistance junction-case

max 3 °C/W

L 165

ELECTRICAL CHARACTERISTICS ($V_s = \pm 15V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter		Test conditions		Min.	Typ.	Max.	Unit
V_s	Supply voltage			± 6		± 18	V
I_d	Quiescent drain current	$V_s = \pm 18V$			40	60	mA
I_b	Input bias current				0.2	1	μA
V_{os}	Input offset voltage				± 2	± 10	mV
I_{os}	Input offset current				± 20	± 200	nA
SR	Slew-Rate	$G_v = 10$			8		V/ μs
		$G_v = 1^{(*)}$			6		
V_o	Output voltage swing	$f = 1 \text{ kHz}$	$I_p = 0.3A$ $I_p = 3A$		27 24		V_{pp}
		$f = 10 \text{ kHz}$	$I_p = 0.3A$ $I_p = 3A$		27 23		V_{pp}
R_i	Input resistance (pin 1)	$f = 1 \text{ KHz}$		100	500		K Ω
G_v	Voltage gain (open loop)				80		dB
e_N	Input noise voltage	$B = 10 \text{ to } 10\,000 \text{ Hz}$			2		μV
i_N	Input noise current				100		pA
CMR	Common mode rejection	$R_g \leq 10 \text{ K}\Omega$ $G_v = 30 \text{ dB}$			70		dB
SVR	Supply voltage rejection	$R_g = 22 \text{ k}\Omega$ $V_{ripple} = 0.5 V_{rms}$ $f_{ripple} = 100 \text{ Hz}$	$G_v = 10$		60		dB
			$G_v = 100$		40		dB
η	Efficiency	$f = 1 \text{ kHz}$ $R_L = 4\Omega$	$I_p = 1.6A$; $P_o = 5W$		70		%
			$I_p = 3A$; $P_o = 18W$		60		%
T_{sd}	Thermal shut-down case temperature	$P_{tot} = 12W$			110		$^\circ C$
		$P_{tot} = 6W$			130		

(*) Circuit of fig. 8.

Fig. 1 - Open loop frequency response

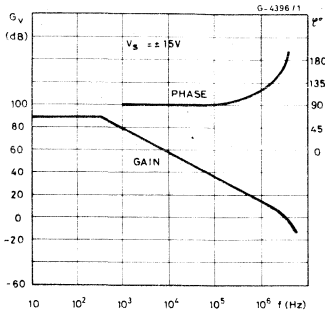


Fig. 2 - Closed-loop frequency response (circuit of fig. 8)

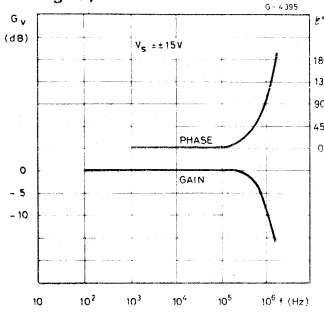


Fig. 3 - Large signal frequency response

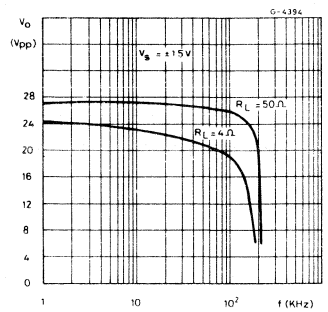


Fig. 4 - Maximum output current vs. voltage [V_{CE}] across each output transistor

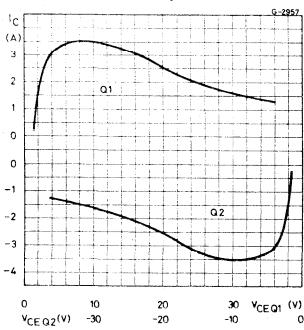


Fig. 5 - Safe operating area and collector characteristics of the protected power transistor

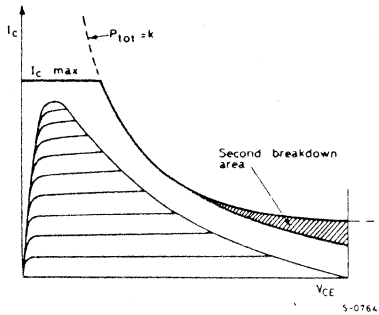


Fig. 6 - Maximum allowable power dissipation vs. ambient temperature

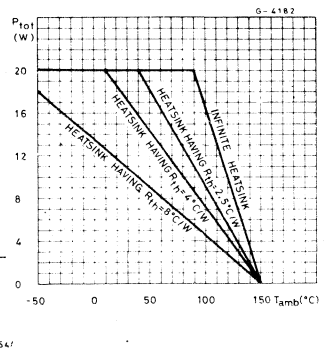


Fig. 7 - Application circuit ($G_V > 10$)

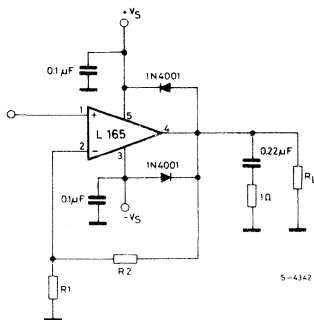
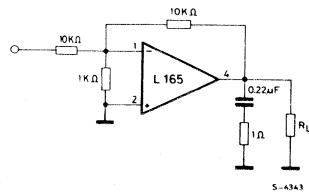
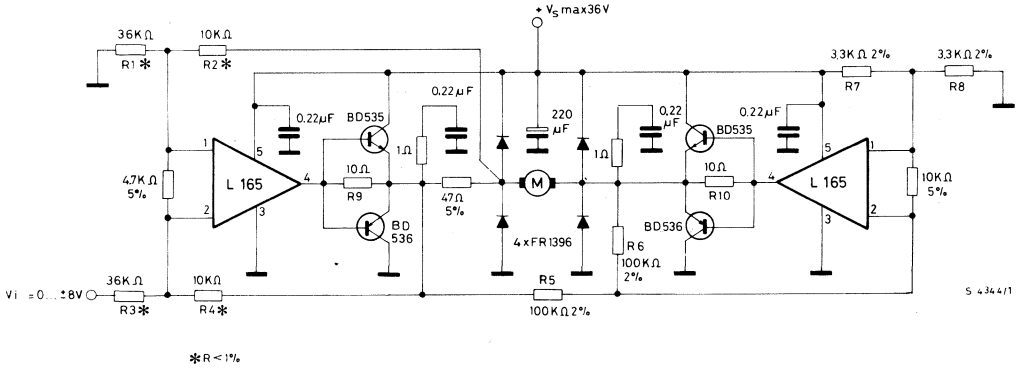


Fig. 8 - Unity gain configuration



L 165

Fig. 9 - Motor speed control circuit with external power transistors ($I_{motor} > 3.5A$)



Note: The input voltage level is compatible with L291 (5-BIT D/A converter)

Fig. 10 - High current tracking regulator

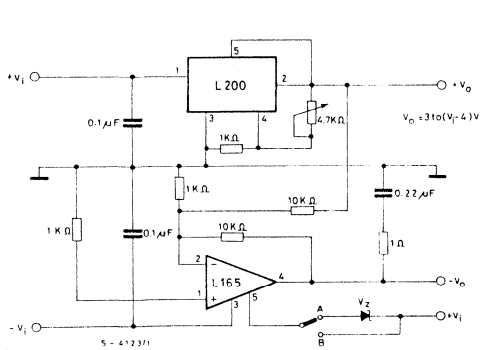
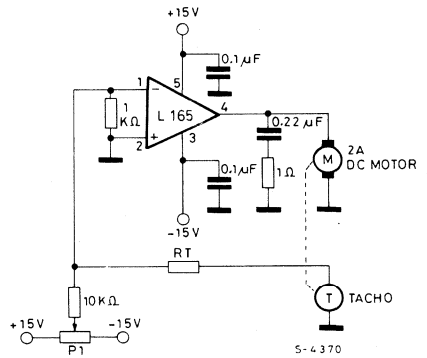


Fig. 11 - Bidirectional speed control of DC motor



A: for $\pm 18 \leq V_i \leq \pm 32$

Note - V_z must be chosen in order to verify
 $2 V_i - V_z \leq 36V$

B: for $V_i \leq \pm 18V$

LINEAR INTEGRATED CIRCUITS

PRELIMINARY DATA

POSITIVE VOLTAGE REGULATORS WITH RECTIFYING BRIDGE

- OUTPUT VOLTAGE: 5V, 12V AND 15V
- OUTPUT CURRENT UP TO 500 mA
- SHORT CIRCUIT PROTECTION
- THERMAL OVERLOAD PROTECTION
- OVERVOLTAGE PROTECTION (60V - 10 ms)

The L194-5, L194-12 and L194-15 are fixed voltage regulators assembled in Pentawatt[®] package. They incorporate a rectifying diode bridge with 7A surge current capability.

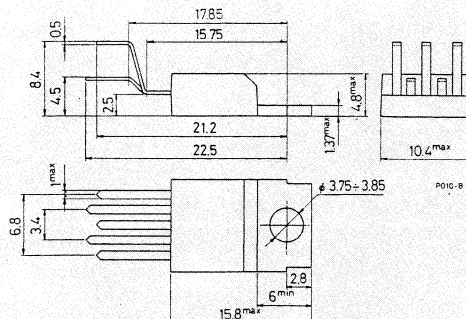
ABSOLUTE MAXIMUM RATINGS

V_i	Peak input voltage (10ms)	60	V
V_i	DC input voltage (at pin 2)	40	V
V_i	AC input voltage (rms)	28	V
V_R	Peak reverse voltage across each diode	80	V
I_D	Input diode repetitive current	2	A
I_{DS}	Input diode surge current (10 ms)	7	A
I_o	Output current	Internally limited	
P_{tot}	Power dissipation	Internally limited	
T_{stg}	Storage temperature	-65 to +150	°C
T_j	Operating junction temperature	-25 to +150	°C

ORDERING NUMBERS: L194-5V ($V_o = 5V$)
 L194-12V ($V_o = 12V$)
 L194-15V ($V_o = 15V$)

MECHANICAL DATA

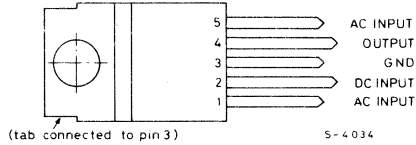
Dimensions in mm



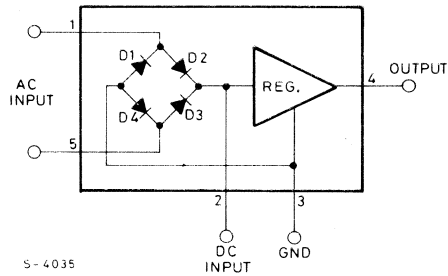
L 194 Series

CONNECTION DIAGRAM

(top view)



BLOCK DIAGRAM



THERMAL DATA

$R_{th\ j-case}$	Thermal resistance junction-case	max	4	$^{\circ}C/W$
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	50	$^{\circ}C/W$

ELECTRICAL CHARACTERISTICS ($T_j = 25^{\circ}C$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
I_d Quiescent drain current	$I_o = 0$ V_i (pin 2) = 28V		5	14	mA
V_o Output voltage	$I_o = 100\text{ mA}$ $V_i = 15\text{V}$ (L194-5) $V_i = 22\text{V}$ (L194-12) $V_i = 25\text{V}$ (L194-15)	4.75 11.4 14.25	5 12 15	5.25 12.6 15.75	V
ΔV_o Line Regulation	$I_o = 100\text{ mA}$ $V_i = 8\text{ to }18\text{V}$ (L194-5) $V_i = 15\text{ to }25\text{V}$ (L194-12) $V_i = 18\text{ to }28\text{V}$ (L194-15)		5 10 15		mV

L194 Series

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
$\frac{\Delta V_o}{V_o}$ Load Regulation	$I_o = 10$ to 250 mA $V_i = 15$ V (L194-5) $V_i = 22$ V (L194-12) $V_i = 25$ V (L194-15)		1 1 1		%
V_{i-o} Dropout voltage (pin 2-4)	$I_o = 300$ mA		2	3	V
$\frac{\Delta V_o}{\Delta T}$ Output voltage drift	$I_o = 100$ mA $V_i = 15$ V (L194-5) $V_i = 22$ V (L194-12) $V_i = 25$ V (L194-15)		0.3 0.6 0.8		mV/°C
I_o Output current	$\frac{\Delta V_o}{V_o} \leq 1\%$ L194-5/12 L194-15 (*)	500 300			mA
I_{sc} Short-circuit current	$V_i = 15$ V (L194-5) $V_i = 22$ V (L194-12) $V_i = 25$ V (L194-15)		700 500 400		mA
I_p Peak output current		0.7		1.4	A
SVR Supply voltage Rejection	$f = 100$ Hz $I_o = 200$ mA $\Delta V_i = 10$ V		46 40		dB
R_o Output Resistance	$f = 1$ kHz $I_o = 100$ mA		80		m Ω
V_d Diode Forward Voltage	$I_f = 1$ A $I_f = 5$ A		1.6 4.5		V

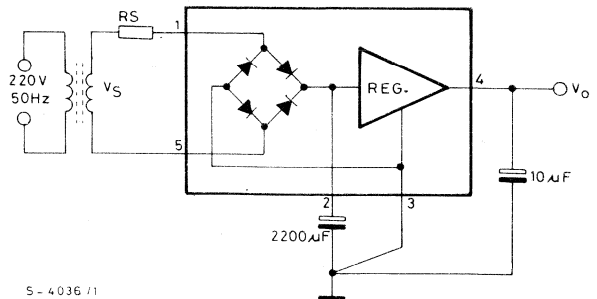
(*) See diagram of fig. 1.

APPLICATION CIRCUIT

In the design of power supplies using the L194, it must be always verified that:

$$I_{\text{peak}} = \frac{\sqrt{2} V_s}{R_s} < 7A$$

where R_s is the sum of the transformer resistance, the equivalent diode resistance and external resistors.



S - 4036 / 1

L 194 Series

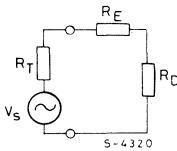
APPLICATION INFORMATION

The Absolute Maximum Ratings guarantee a max of 40V at pin 2 with max peak current of 7A in the rectifying diodes.

To avoid to damage the device, a suitable transformer secondary must be used so that even when there are network variations the limits set are always respected during operation.

For example, with a nominal voltage of 24 V_{rms} the maximum variations due to the transformer tolerance are $\pm 20\%$.

In order to limit (to the maximum value allowed) the current peak, which occurs in diodes during switch-on, an external resistance R_E , in series with the secondary of the transformer, must be introduced. Supposing that the capacitor of the filter is discharged at switch-on, the following equivalent circuit can be drawn:



V_S = Secondary voltage.

R_T = Secondary resistances of transformer.

R_D = Resistance produced by the diode pair involved in conduction.

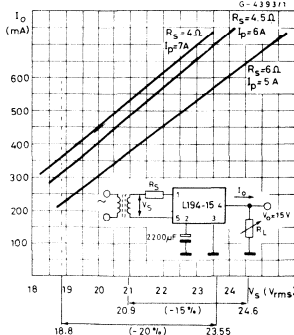
If values R_T and R_D are known R_E is calculated in such a way that the peak current at switch-on does not exceed 7A.

$$R_E \geq \frac{V_{S \text{ peak}} - 7 (R_T + R_D)}{7}$$

For the 5V, with the nominal voltage of the 10VA transformer at 12V and with a total voltage variation of $\pm 15\%$, the transformer secondary is connected directly to pins 1 and 5.

For correct use of the device at 15V the graph in fig. 1 gives the max output current.

Fig. 1 - Guaranteed output current vs. secondary voltage



Note:

$V_S \text{ nom} = 24.6 V_{rms}$ for 220V $\pm 15\%$.

$V_S \text{ nom} = 23.55 V_{rms}$ for 220V $\pm 20\%$.

L200

LINEAR INTEGRATED CIRCUIT

ADJUSTABLE VOLTAGE AND CURRENT REGULATOR

- ADJUSTABLE OUTPUT CURRENT UP TO 2A (GUARANTEED UP TO $T_j = 150^\circ\text{C}$)
- ADJUSTABLE OUTPUT VOLTAGE DOWN TO 2.85V
- INPUT OVERVOLTAGE PROTECTION (UP TO 60V, 10 ms)
- SHORT CIRCUIT PROTECTION
- OUTPUT TRANSISTOR S.O.A. PROTECTION
- THERMAL OVERLOAD PROTECTION
- LOW BIAS CURRENT ON REGULATION PIN
- LOW STANDBY CURRENT DRAIN

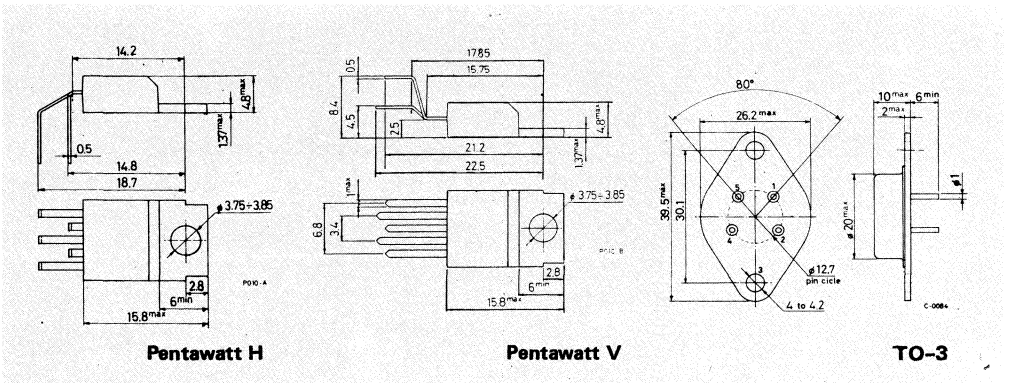
The L200 is a monolithic integrated circuit for voltage and current programmable regulation. It is available in Pentawatt[®] package or 4-lead TO-3 metal case. Current limiting, power limiting, thermal shutdown and input overvoltage protection (up to 60V) make the L200 virtually blowout proof. The L200 can be used to replace fixed voltage regulators when high output voltage precision is required and eliminates the need to stock a range of fixed voltage regulators.

ABSOLUTE MAXIMUM RATINGS

V_i	DC input voltage	40	V
$V_{i\text{ peak}}$	Peak input voltage (10 ms)	60	V
ΔV_{i-o}	Dropout voltage	32	V
I_o	Output current	internally limited	
P_{tot}	Power dissipation	internally limited	
T_{stg}	Storage temperature	-55 to 150	$^\circ\text{C}$
T_{op}	Operating junction temperature for L200C for L200	-25 to 150 -55 to 150	$^\circ\text{C}$ $^\circ\text{C}$

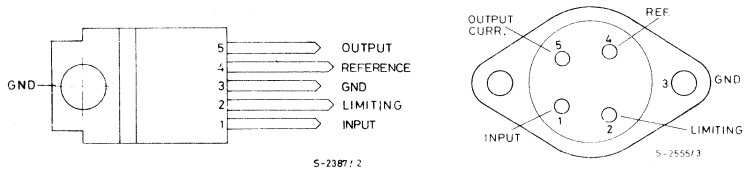
MECHANICAL DATA

Dimensions in mm



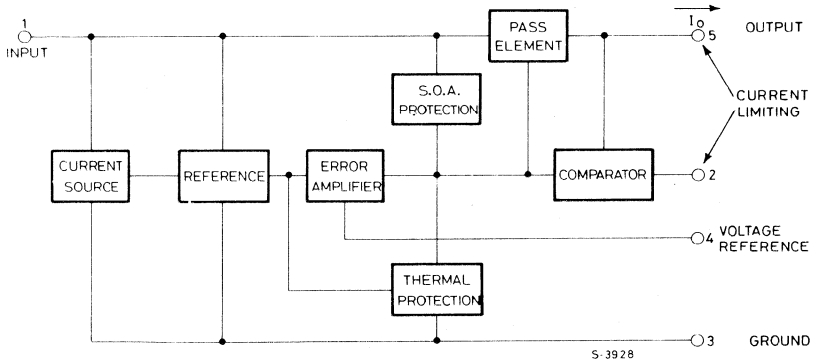
L 200

CONNECTION DIAGRAMS AND ORDERING NUMBERS (top views)

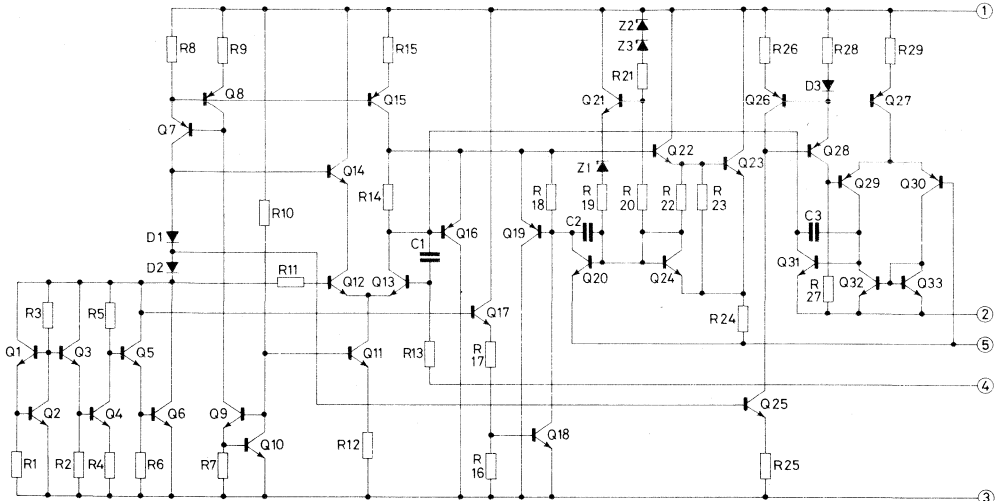


Type	Pentawatt [®]	TO-3
L 200		L 200 T
L 200 C	L 200 CH L 200 CV	L 200 CT

BLOCK DIAGRAM



SCHEMATIC DIAGRAM



5-2385

THERMAL DATA

			TO-3	Pentawatt®
$R_{th\ j-case}$	Thermal resistance junction-case	max	4 °C/W	3 °C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	35 °C/W	50 °C/W

ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^{\circ}C$, unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
-----------	-----------------	------	------	------	------

VOLTAGE REGULATION LOOP

I_d	Quiescent drain current (pin 3)	$V_i = 20V$		4.2	9.2	mA
e_N	Output noise voltage	$V_o = V_{ref}$ $B = 1\text{ MHz}$	$I_o = 10\text{ mA}$	80		μV
V_o	Output voltage range		$I_o = 10\text{ mA}$	2.85	36	V
$\frac{\Delta V_o}{V_o}$	Voltage load regulation (note 1)	$\Delta I_o = 2A$ $\Delta I_o = 1.5A$		0.15 0.1	1 0.5	% %
$\frac{\Delta V_i}{\Delta V_o}$	Line regulation	$V_o = 5V$ $V_i = 8\text{ to }18V$	$I_o = 500\text{ mA}$	54	70	dB
SVR	Supply voltage rejection	$V_o = 5V$ $\Delta V_i = 10\text{ V}_{pp}$ $f = 100\text{ Hz}$ (note 2)	$I_o = 500\text{ mA}$	60	70	dB

L 200

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
ΔV_{i-o}	Droupout voltage between pins 1 and 5 $I_o = 1.5A$ $\Delta V_o \leq 2\%$		2	2.5	V
V_{ref}	Reference voltage (pin 4) $V_i = 20V$ $I_o = 10 \text{ mA}$	2.65	2.77	2.85	V
ΔV_{ref}	Average temperature coefficient of reference voltage $V_i = 20V$ $I_o = 10 \text{ mA}$ for $T_j = -25$ to 125°C for $T_j = 125$ to 150°C		-0.25 -1.5		mV/ $^\circ\text{C}$ mV/ $^\circ\text{C}$
I_4	Bias current at pin 4		3	10	μA
$\frac{\Delta I_4}{\Delta T \cdot I_4}$	Average temperature coefficient (pin 4)		-0.5		%/ $^\circ\text{C}$
Z_o	Output impedance $V_i = 10V$ $V_o = V_{ref}$ $I_o = 0.5A$ $f = 100 \text{ Hz}$		1.5		m Ω

CURRENT REGULATION LOOP

V_{sc}	Current limit sense voltage between pins 5 and 2 $V_i = 10V$ $V_o = V_{ref}$	0.39	0.45	0.51	V
$\frac{\Delta V_{sc}}{\Delta T \cdot V_{sc}}$	Average temperature coefficient of V_{sc}		0.03		%/ $^\circ\text{C}$
$\frac{\Delta I_o}{I_o}$	Current load regulation $V_i = 10V$ $\Delta V_o = 3V$ $I_o = 0.5A$ $I_o = 1A$ $I_o = 1.5A$		1.4 1 0.9		% % %
I_{sc}	Peak short circuit current $V_i - V_o = 14V$ (pins 2 and 5 short circuited)			3.6	A

Note 1): A load step of 2A can be applied provided that input-output differential voltage is lower than 20V (see fig. 1).

Note 2): The same performance can be maintained at higher output levels if a bypassing capacitor is provided between pins 2 and 4.

Fig. 1 - Typical safe operating area protection

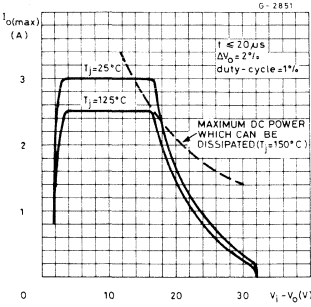


Fig. 2 - Quiescent current vs. supply voltage

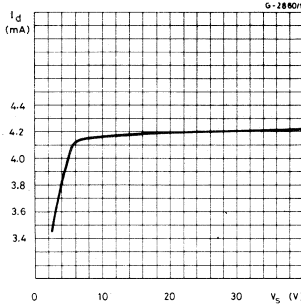


Fig. 3 - Quiescent current vs. junction temperature

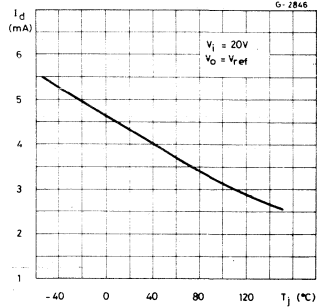


Fig. 4 - Quiescent current vs. output current

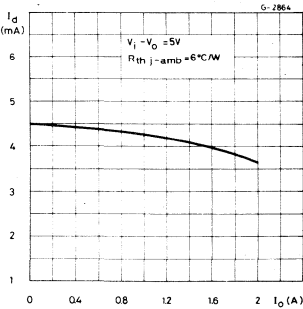


Fig. 5 - Output noise voltage vs. output voltage

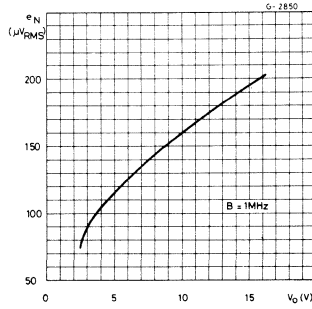


Fig. 6 - Output noise voltage vs. frequency

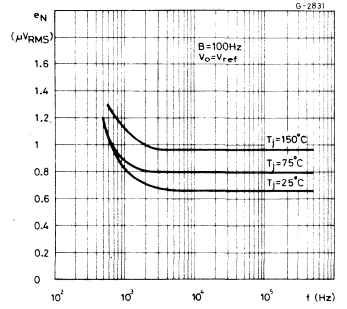


Fig. 7 - Reference voltage vs. junction temperature

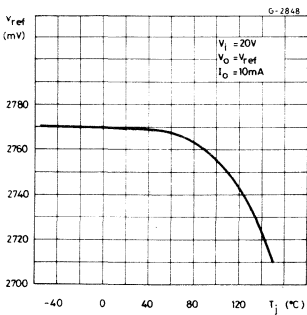


Fig. 8 - Voltage load regulation vs. junction temperature

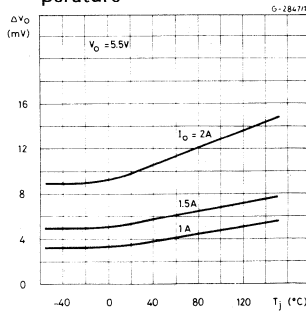
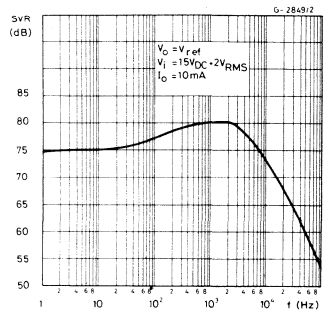


Fig. 9 - Supply voltage rejection vs. frequency



L 200

Fig. 10 - Dropout voltage vs. junction temperature

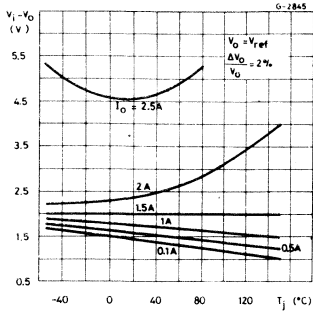


Fig. 11 - Output impedance vs. frequency

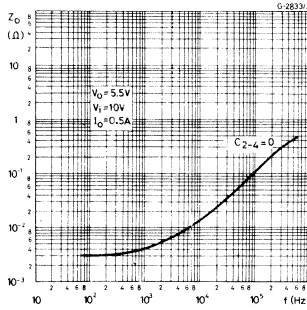


Fig. 12 - Output impedance vs. output current

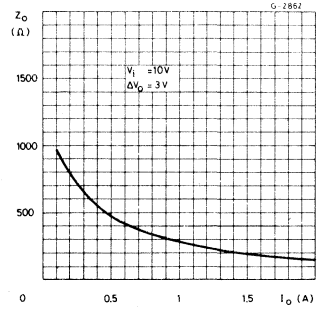


Fig. 13 - Voltage transient response

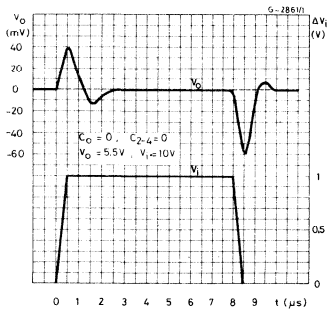


Fig. 14 - Load transient response

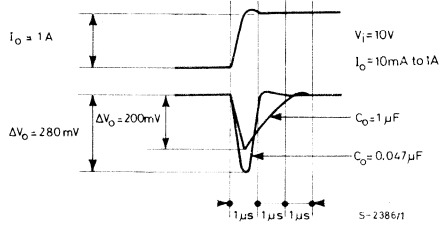


Fig. 15 - Load transient response

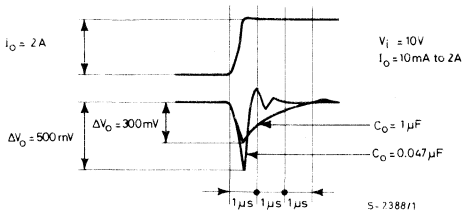
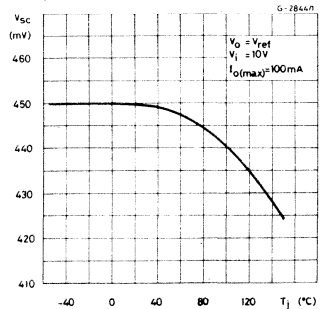


Fig. 16 - Current limit sense voltage vs. junction temperature



APPLICATION CIRCUITS

Fig. 17 - Programmable current regulator

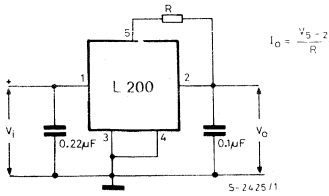


Fig. 18 - Programmable voltage regulator

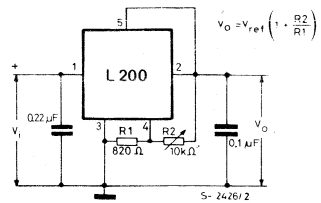


Fig. 19 - Programmable voltage regulator with current limiting

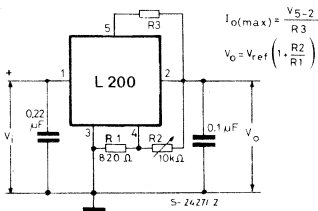


Fig. 20 - Switching regulator

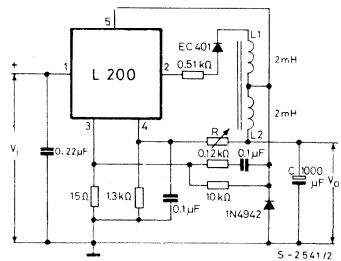


Fig. 21 - High current voltage regulator with short circuit protection

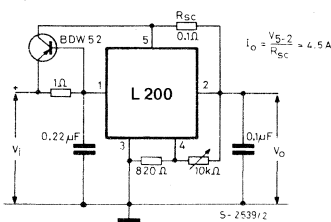
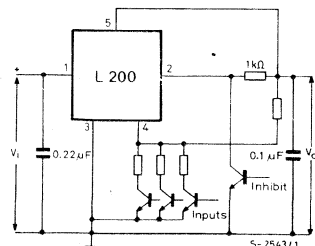


Fig. 22 - Digitally selected regulator with inhibit



L 200

APPLICATION CIRCUITS (continued)

Fig. 23 - Positive and negative regulator

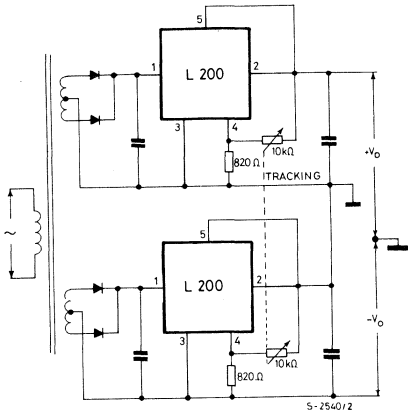
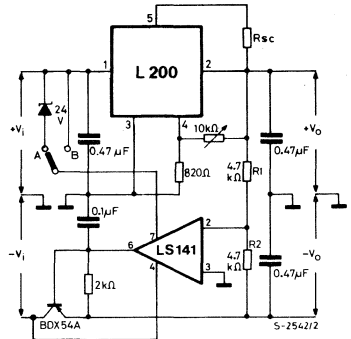


Fig. 24 - Tracking voltage regulator



A : $V_i(\max) \leq \pm 34V$; $3 < V_O < 30$.
 B : $V_i(\max) \leq \pm 22V$; $3 < V_O < 18$.

Fig. 25 - High current regulator with NPN pass transistor

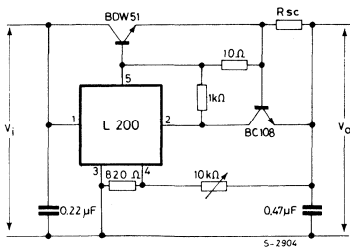
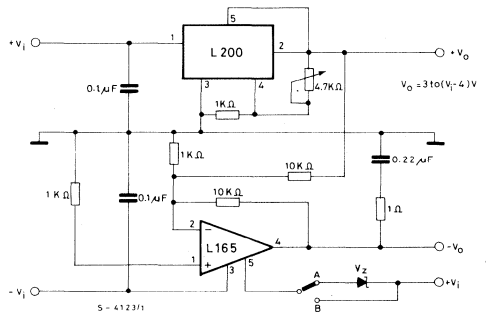


Fig. 26 - High current tracking regulator



A : for $\pm 18 \leq V_i \leq \pm 32$

Note - V_Z must be chosen in order to verify
 $2V_i - V_Z \leq 36V$

B : for $V_i \leq \pm 18V$

APPLICATION CIRCUITS (continued)

Fig. 27 - High input and output voltage

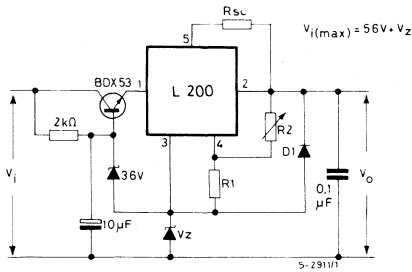
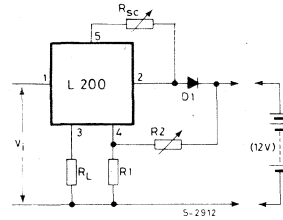


Fig. 28 - Constant current battery charger



The resistors R_1 and R_2 determine the final charging voltage and R_{sc} the initial charging current. D_1 prevents discharge of the battery through the regulator.

The resistor R_L limits the reverse currents through the regulator (which should be 100 mA max) when the battery is accidentally reverse connected. If R_L is in series with a bulb of 12V/50 mA rating this will indicate incorrect connection.

Fig. 29 - 30W Motor speed control

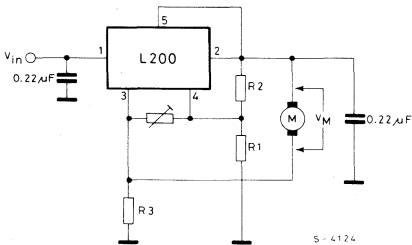


Fig. 30 - Low turn on

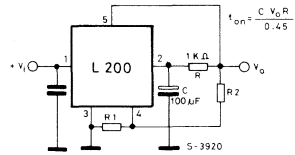
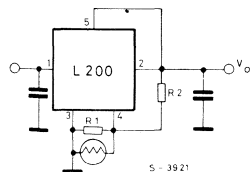


Fig. 31 - Light controller



$$R_3 = \frac{R_1}{R_2} \cdot R_M$$

$$V_M = V_{ref} \cdot \left(1 + \frac{R_2}{R_1}\right)$$

LINEAR INTEGRATED CIRCUITS

L 201 L 202 L 203 L 204

HIGH-VOLTAGE, HIGH-CURRENT DARLINGTON TRANSISTOR ARRAYS

These high-voltage, high-current Darlington transistor arrays comprise seven silicon NPN Darlington pairs on a common monolithic substrate. All units feature open collector outputs and integral suppression diodes for inductive loads. Peak currents of 600 mA can be withstood, making them ideal for driving tungsten filament lamps.

The L 201 is a general-purpose array which may be used with DTL, TTL, PMOS, CMOS, etc. It is pinned with inputs opposite outputs to facilitate circuit board layout and is priced to compete directly with discrete transistor alternatives.

The L 202 was specifically designed for use with 14 to 25V PMOS devices.

Each input has a Zener diode and resistor in series in order to limit the input current to a safe value.

The L203 has a series base resistor to each Darlington pair allowing operation directly with TTL or CMOS operating at a supply voltage of 5V.

The L204 has a series base resistor to each Darlington pair, allowing operation directly with PMOS or CMOS utilizing supply voltage of 6 to 15V.

In all cases, the individual Darlington pair collector current rating is 500 mA. However, outputs may be paralleled for higher load current capability. The devices are supplied in a 16-lead dual in-line plastic package with copper frame.

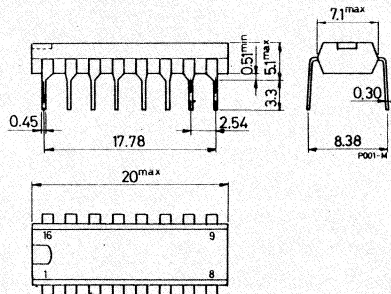
ABSOLUTE MAXIMUM RATINGS

V_i	Input voltage (for L 202, L 203 and L 204)	30	V
V_o	Output voltage (collector-emitter)	50	V
$V_{CEO(sus)}$	Collector-emitter sustaining voltage	36	V
I_C	Collector current	500	mA
I_B	Base current (for L 201 only)	25	mA
P_{tot}	Total power dissipation at $T_{amb} = 25^\circ\text{C}$	1.8	W
T_{op}	Operating junction temperature	-25 to 150	$^\circ\text{C}$
T_{stg}	Storage temperature	-55 to 150	$^\circ\text{C}$

ORDERING NUMBERS: L201B, L203B
L202B, L204B

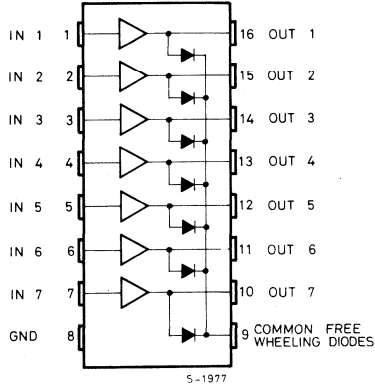
MECHANICAL DATA

Dimensions in mm



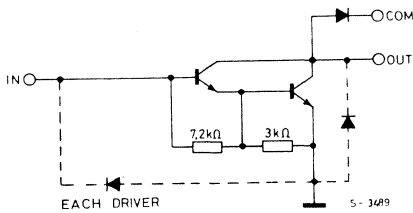
L 201 L 202 L 203 L 204

CONNECTION DIAGRAM (top view)

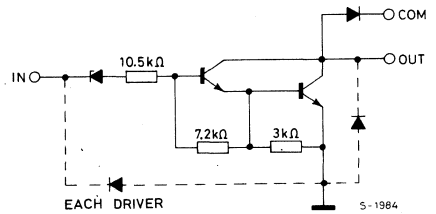


SCHEMATIC DIAGRAM

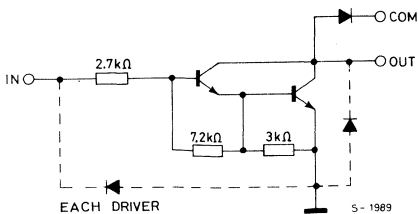
For L 201



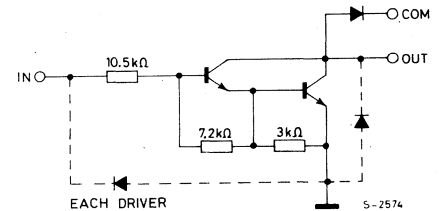
For L 202



For L 203



For L 204



Thermal Data

$R_{th\ j-amb}$ Thermal resistance junction-ambient	max. 70 °C/W
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Electrical Characteristics ($T_{amb} = 25^{\circ}C$, unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig. No.
I_{CEX} Collector cutoff current	for L 201 $V_{CE} = 50V$		0.2	3	μA	1
	for L 202 $V_{CE} = 50V \quad V_i = 7V$		0.2	3	μA	2
	for L 203, L 204 $V_{CE} = 50V \quad I_i = 0$		0.2	3	μA	1
$V_{CE(sat)}$ Collector-emitter saturation voltage	$I_C = 350\ mA \quad I_B = 500\ \mu A$		1.25	1.6	V	3
	$I_C = 200\ mA \quad I_B = 350\ \mu A$		1	1.3	V	
	$I_C = 100\ mA \quad I_B = 250\ \mu A$		0.85	1.1	V	
I_i Input current	for L 202 $V_i = 17V$		0.75	1.3	mA	5
	for L 203 $V_i = 3.85V$		0.9	1.35	mA	
	for L 204 $V_i = 5V$		0.35	0.5	mA	
	$V_i = 12V$		1.1	1.45	mA	
$I_{C(off)}$	$V_{CE} = 50V \quad I_i = 25\ \mu A$			25.	μA	4
V_i Input voltage	for L 202 $I_C = 300\ mA \quad V_{CE} = 2V$		10.5	13	V	7
	for L 203 $I_C = 300\ mA \quad V_{CE} = 2V$		1.8	3	V	
	$I_C = 250\ mA \quad V_{CE} = 2V$		1.7	2.4	V	
	for L 204 $V_{CE} = 2V \quad I_C = 200\ mA$		4.5	6	V	
	$V_{CE} = 2V \quad I_C = 350\ mA$		5	8	V	
h_{FE} DC current gain (for L 201 only)	$I_C = 350\ mA \quad V_{CE} = 2V$	1000	3000		—	3
I_R Parallel diode reverse current	$V_R = 50V$		0.5	50	μA	6
V_F Parallel diode forward voltage	$I_F = 350\ mA$		1.4	2	V	8
t_{PLH} Turn-on delay time	0.5 V_i to 0.5 V_o			5	μs	—
t_{PHL} Turn-off delay time	0.5 V_i to 0.5 V_o			5	μs	—

L 201 L 202 L 203 L 204

TEST CIRCUITS

Fig. 1 - For L 201, L 203
and L 204

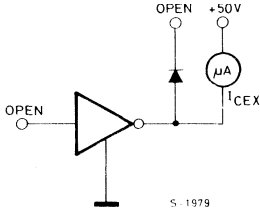


Fig. 2 - For L 202

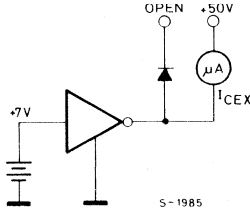


Fig. 3 - For L 201, L 202,
L 203 and L 204

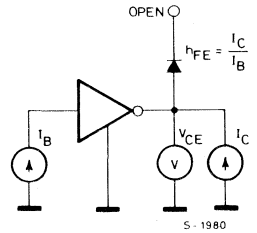


Fig. 4 - For L 201, L 202,
L 203 and L 204

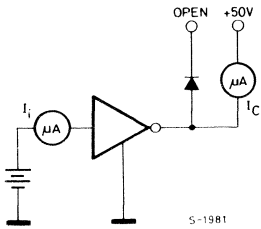


Fig. 5 - For L 202, L 203,
and L 204

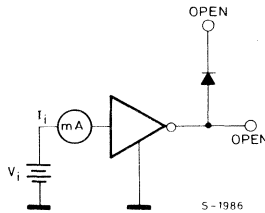


Fig. 6 - For L 201, L 202,
L 203 and L 204

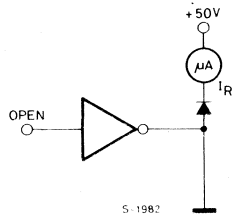


Fig. 7 - For L 202, L 203,
and L 204

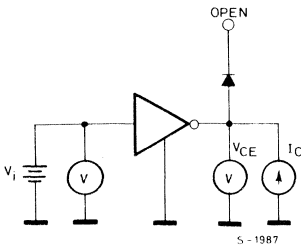
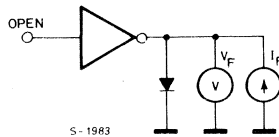
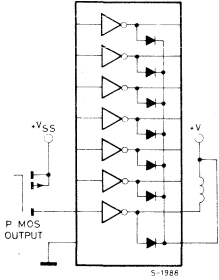


Fig. 8 - For L 201, L 202,
L 203 and L 204

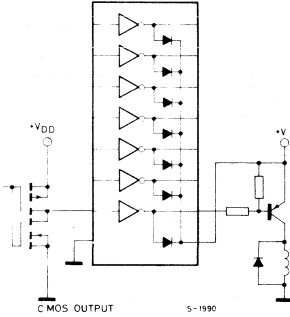


APPLICATION CIRCUITS

PMOS to load
(L 202 and L 204)



Buffer for high current load
(L 203 and L 204)



TTL to load (L 203)

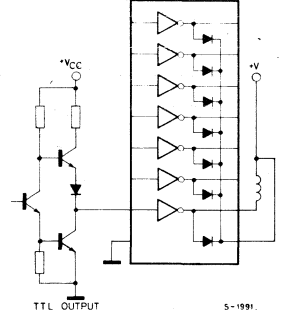


Fig. 9 - DC current gain vs. collector current (for L 201)

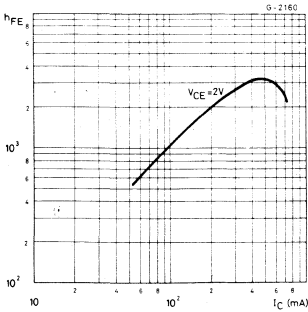


Fig. 10 - Collector current vs. collector emitter saturation voltage

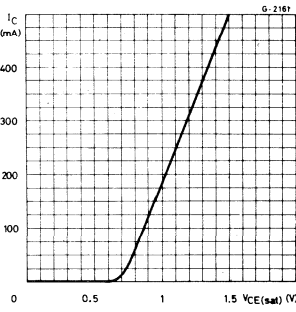


Fig. 11 - Peak collector current as a function of duty cycle and number of outputs

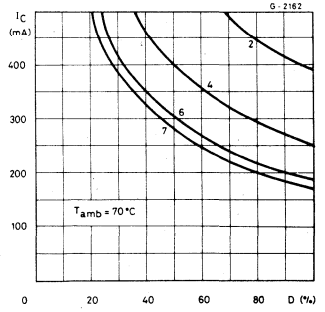


Fig. 12 - Input current vs. input voltage (for L 203 and L 204)

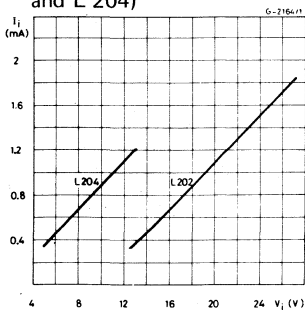


Fig. 13 - Input current vs. input voltage (L 203)

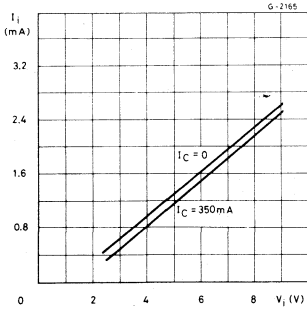
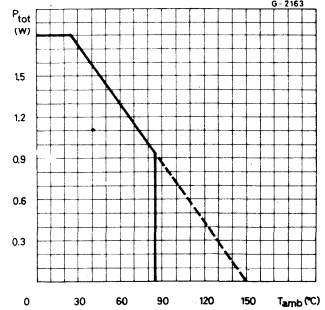


Fig. 14 - Power rating chart



L 290

LINEAR INTEGRATED CIRCUIT

PRELIMINARY DATA

TACHOMETER CONVERTER

The L290 a monolithic LSI circuit in a 16 lead dual in-line plastic package, is intended for use with the L291 and L292 which together form a complete 3-chip DC motor positioning system for applications such as carriage/daisy-wheel position control in typewriters.

The L290/1/2 system can be directly controlled by a microprocessor. The L290 integrates the following functions:

- tacho voltage generator (F/V converter)
- reference voltage generator
- position pulse generator.

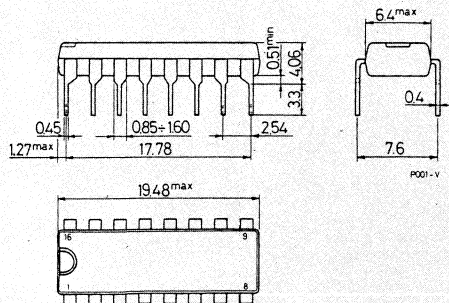
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	± 15	V
P_{tot}	Total power dissipation $T_{amb} = 70^\circ\text{C}$	1	W
T_{stg}, T_j	Storage and junction temperature	-40 to +150	$^\circ\text{C}$

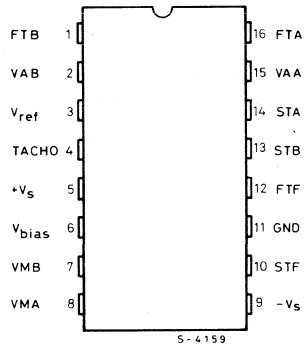
ORDERING NUMBER: L290 B

MECHANICAL DATA

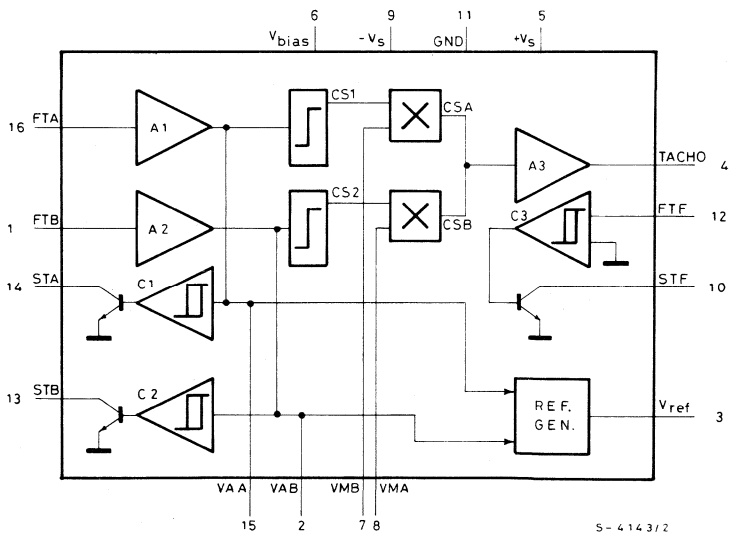
Dimensions in mm



CONNECTION DIAGRAM (top view)

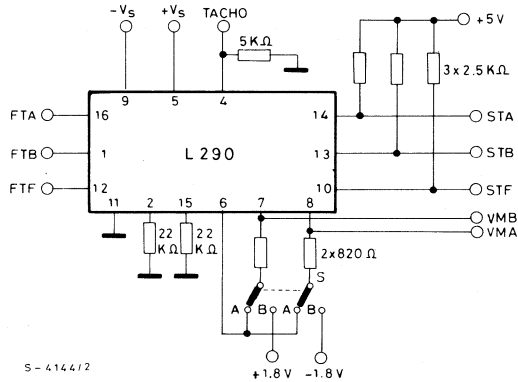


BLOCK DIAGRAM



L 290

TEST CIRCUIT



THERMAL DATA

$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	80	°C/W
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ELECTRICAL CHARACTERISTICS (Refer to the test circuit, S in (A), $V_s = \pm 12V (\pm 10\%)$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameters	Test conditions	Min.	Typ.	Max.	Unit
V_s	Supply voltage	± 10		± 15	V
I_d	Quiescent drain current		13	20	mA

INPUT AMPLIFIERS (A_1 and A_2)

FTA, FTB	Input signal from encoder	$f_{max} = 20\text{ KHz}$	± 0.4		± 0.6	V_p
V_{os}	Output offset voltage (pin 2, 15)	FTA = FTB = 0V			55	mV
G_v	Voltage gain	$f = 10\text{ KHz}$ FTA=FTB= $\pm 0.6V_p$	22	23	24	dB
V_o	Output voltage swing (pin 2, 15)	FTA= FTB= $\pm 1 V_p$	± 9.5			V

ELECTRICAL CHARACTERISTICS (continued)

Parameters	Test conditions	Min.	Typ.	Max.	Unit
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COMPARATORS WITH HYSTERESIS (C_1 , C_2 and C_3)


$V_{THP}^{(°)}$	Positive Threshold voltage	C_1 and C_2	550		850	mV
		C_3	700		900	mV
$V_{THN}^{(°°)}$	Negative Threshold voltage	C_1 and C_2	55		175	mV
		C_3	570		830	mV
V_L	Output voltage (low level) pin 10, 13, 14	$I_o = 2$ mA FTA = FTB = FTF = 0V		0.2	0.4	V
I_{leak}	(pins 10, 13, 14)	FTA = FTB = 0.5V V = 5V FTF = 1V			1	μ A

REFERENCE GENERATOR

V_{ref}	DC reference voltage (pin 3)	FTA = FTB = $\pm 0.5V_p$ (*) $I_{ref} = 1$ mA	4.5	5	5.5	V
I_{ref}	Output current (pin 3)				1.4	mA

"TACHO" AMPLIFIER (A_3)

V_{os}	Output offset voltage (pin 4)	FTA = ± 15 mV FTB = 0.5V			± 80	mV
V_o	DC output voltage (pin 4)	FTA = FTB = $\pm 0.5V_p$ (**)	5.4	6	6.6	V
		$V_{MA} = V_{MB} = \pm 1.25 V_p$ (***)	-5.4	-6	-6.6	
V_o	Output voltage swing (pin 4)	FTA = FTB = 0.5V	9			V
		S in (B) FTA = FTB = -0.5V	-9			
V_{MA} V_{MB}	Multiplier input voltage			± 1.25	± 1.7	V_p
V_{bias}	Bias voltage (pin 6)	FTA and FTB floating	-6.5		-8	V

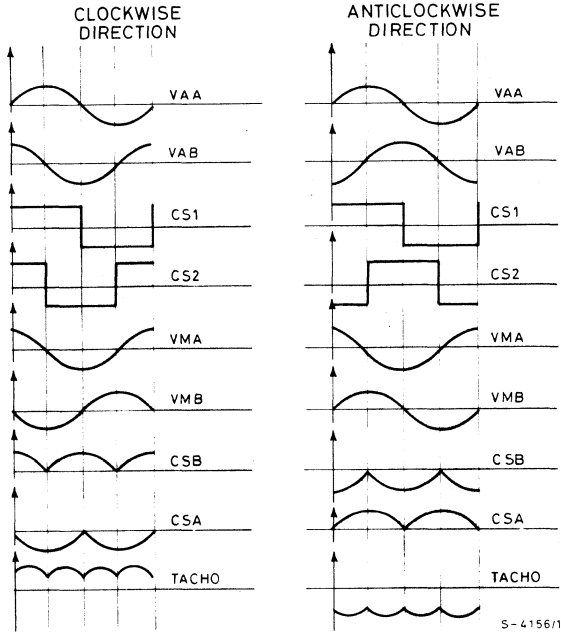
(°) : FTA = FTB = FTF =  1V (°°) : FTA = FTB = FTF =  1V

Note : Phase relationship between the signals:

- * FTA : 0° - FTB : 90°
- ** FTA : 0° - FTB : -90° - $V_{MA} = 90^\circ - V_{MB} = 0^\circ$
- *** FTA : 0° - FTB : 90° - $V_{MA} = 90^\circ - V_{MB} = 180^\circ$

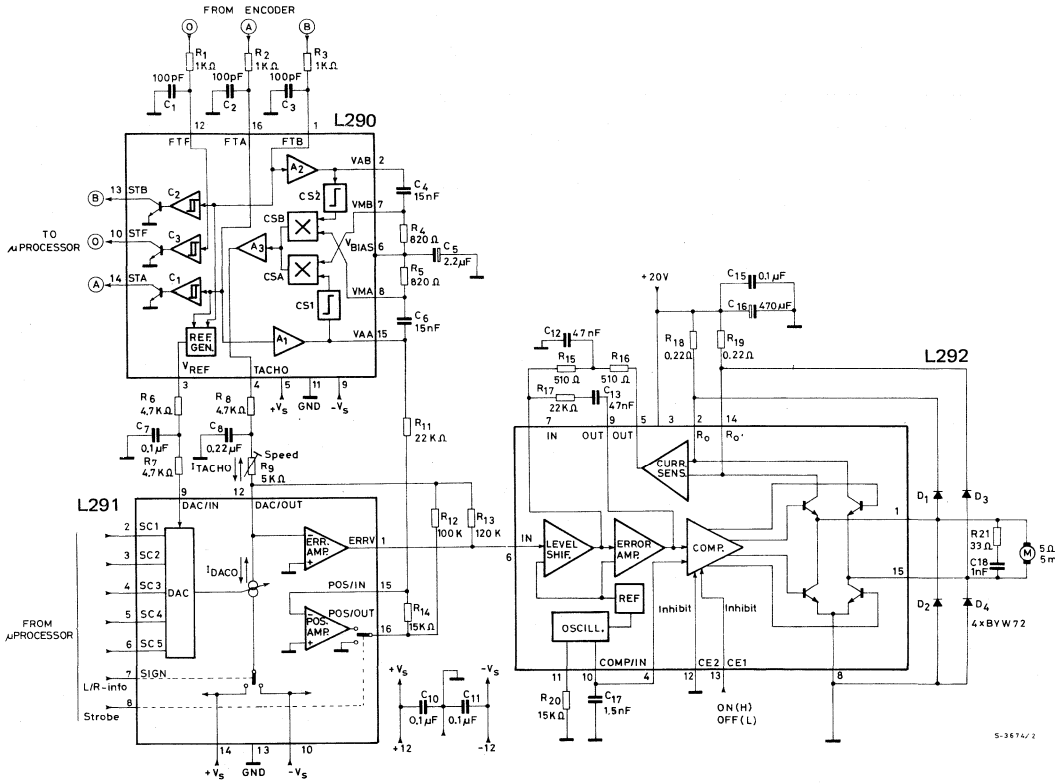
L 290

WAVEFORMS (Neglecting threshold voltage level of the comparators)



SYSTEM DESCRIPTION : refer to the L292 data sheet

Fig. 1 - Complete application circuit



5-3674/2

L 291

LINEAR INTEGRATED CIRCUIT

PRELIMINARY DATA

5 BIT - D/A CONVERTER AND POSITION AMPLIFIER

The L291, a monolithic LSI circuit in a 16 lead dual in-line plastic package, is intended for use with the L290 and L292 to form a complete 3 chip DC motor positioning system for applications such as carriage/daisy-wheel position control in typewriters.

The L290/1/2 system can be directly controlled by a microprocessor.

The L291 integrates the following functions:

- 5 bit D/A converter ($\frac{1}{2}$ LSB max linearity error)
- error amplifier
- position amplifier

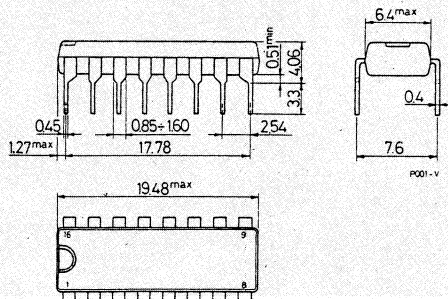
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	± 15	V
P_{tot}	Total power dissipation $T_{amb} = 70^\circ\text{C}$	1	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

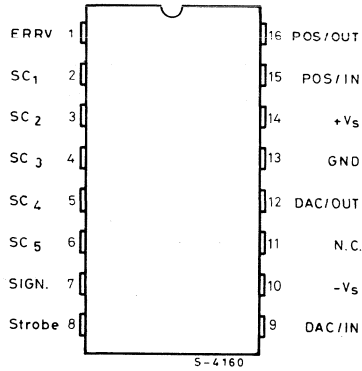
ORDERING NUMBER: L291 B

MECHANICAL DATA

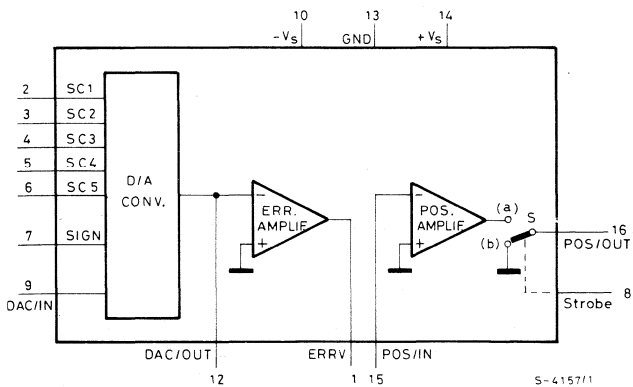
Dimensions in mm



CONNECTION DIAGRAM (top view)

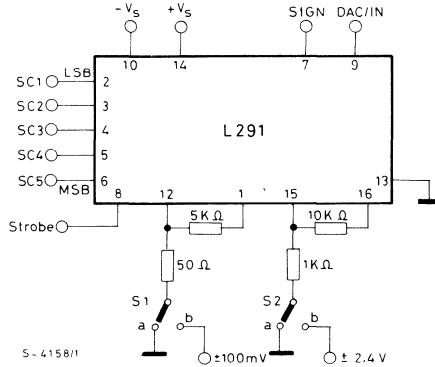


BLOCK DIAGRAM



L 291

TEST CIRCUIT



THERMAL DATA

$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	80	$^{\circ}C/W$
-----------------	-------------------------------------	-----	----	---------------

ELECTRICAL CHARACTERISTICS (Refer to the test circuit, S_1 and S_2 in (a), $V_s = \pm 12V$ ($\pm 10\%$), $T_{amb} = 25^{\circ}C$, unless otherwise specified)

Parameters	Test conditions	Min.	Typ.	Max.	Unit
V_s	Supply voltage	± 10		± 15	V
I_d	Quiescent drain current		6.5	10	mA

POSITION AMPLIFIER

V_{strobe}	Enable voltage level	V_L (S in (a)) *	0		0.8	V
		V_H (S in (b)) *	2.4		$+V_s$	V
V_{os}	Output offset voltage (pin 16)	$V_{strobe} = V_L$			± 50	mV
I_b	Input bias current (pin 15)	$V_{strobe} = V_L$			0.3	μA
V_o	Output voltage swing (pin 16)	$V_{strobe} = V_L$ S_2 in (b)	± 9			V
V_R	Residual output voltage (pin 16)	$V_{strobe} = V_H$			± 20	mV

* See block diagram.

ELECTRICAL CHARACTERISTICS (continued)

Parameters	Test conditions	Min.	Typ.	Max.	Unit
------------	-----------------	------	------	------	------

D/A CONVERTER

I_{ref}	Current reference input range (pin 9)	All inputs low	0.3		1	mA
V_{os}	Current reference offset voltage (pin 9 to GND)	$I_{ref} = 0.3$ to 1 mA All inputs high			± 20	mV
I_o	Output current range (pin 12)		0.7		1.4	mA
		$I_{ref} = 0.516$ mA all inputs low	0.98		1.02	mA
I_{os}	Output offset current (pin 12)	All inputs high			0.4	μ A
V_L	Low voltage level (digital inputs)	SC1 = LSB SC5 = MSB	0		0.8	V
V_H	High voltage level (digital inputs)		2.4		$+V_S$	V
I_L	Digital inputs current (low state)	$V_L = 0.4$ V			-50	μ A
I_H	Digital inputs current (high state)	$V_H = 5$ V			1	μ A

ERROR AMPLIFIER

V_{os}	Output offset voltage (pin 1)	$I_{ref} = 0.5$ mA; All inputs high			± 200	mV
I_o	Output current (pin 1)				5	mA
V_o	Output voltage swing (pin 1)	All inputs high S_1 in (b); $R_L = 10$ K Ω	± 7.4		± 8.4	Vp

L 291

D/A converter logic function ($I_{ref} = 0.516 \text{ mA}$)

DIGITAL WORD (From μ Processor)						Commands
$\overline{\text{SIGN}}$	$\overline{\text{SC}}_5$	$\overline{\text{SC}}_4$	$\overline{\text{SC}}_3$	$\overline{\text{SC}}_2$	$\overline{\text{SC}}_1$	
X	H	H	H	H	H	Speed = Zero
L	L	L	L	L	L	Speed = Max CK wise
L	H	H	H	H	L	Speed = Min CK wise
H	H	H	H	H	L	Speed = Min ACK wise
H	L	L	L	L	L	Speed = Max ACK wise

X = indifferent L = low H = high.

Looking from the typewriter keyboard the clockwise rotation of the motors move the carriage from left to right and the daisy clockwise.

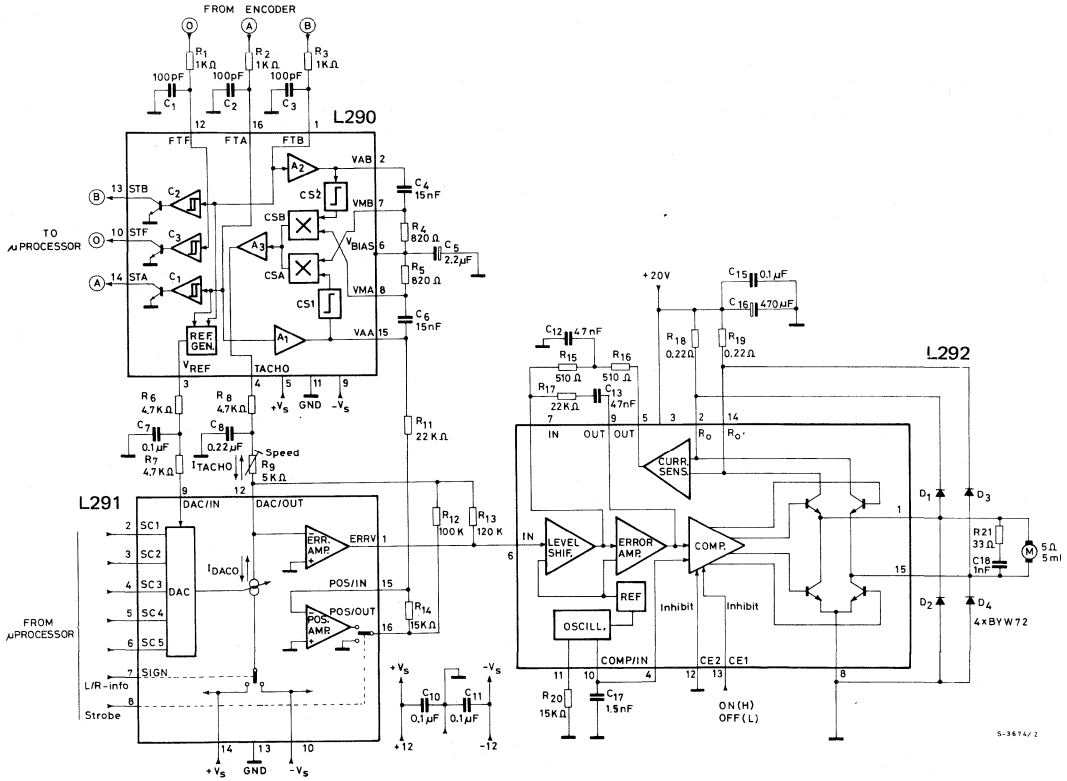
Error amplifier

In order to have a good stability, the error amplifier must work with a closed loop gain greater than 20 dB.

SYSTEM DESCRIPTION: refer to the L292 data sheet

L 291

Fig. 1 - Complete application circuit



L 292

LINEAR INTEGRATED CIRCUIT

PRELIMINARY DATA

SWITCH-MODE DRIVER FOR DC MOTORS

The L292 is a monolithic LSI circuit in 15-lead MULTIWATT[®] package. It is intended for use, together with L290 and L291, as a complete 3-chip DC motor positioning system for applications such as carriage/daisy-wheel position control in typewriters.

The L290/1/2 system can be directly controlled by a microprocessor. The outstanding characteristics of the L292 are:

- Driving capability: 2A, 36V, 30 KHz.
- 2 Logic chip enable.
- External loop gain adjustment.
- Single power supply (18 to 36V).
- Input signal symmetric to ground.
- Thermal protection.

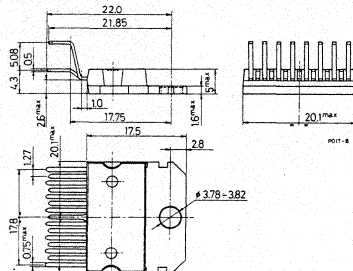
ABSOLUTE MAXIMUM RATINGS

V_s	Power supply	36	V
V_i	Input voltage	-15 to $+V_s$	V
$V_{inhibit}$	Inhibit voltage	0 to V_s	V
P_{tot}	Total power dissipation ($T_{case} = 75^\circ\text{C}$)	25	W
T_{stg}	Storage and junction temperature	-40 to +150	$^\circ\text{C}$

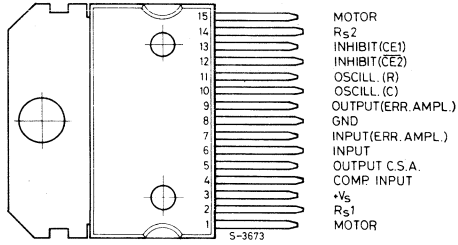
ORDERING NUMBER: L292

MECHANICAL DATA

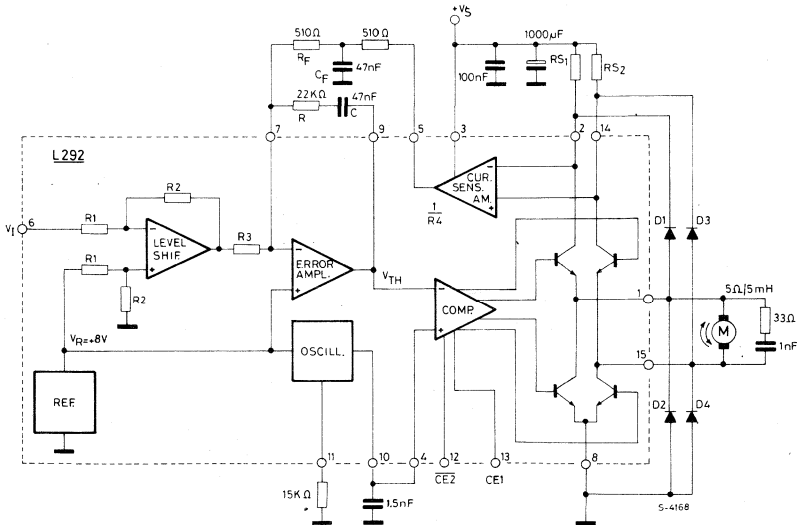
Dimension in mm



CONNECTION DIAGRAM (top view)



BLOCK DIAGRAM



$D_1 \cdot D_2 \cdot D_3 \cdot D_4 =$ High speed diodes (BYW 72 or equivalent)

L 292

THERMAL DATA

$R_{th\ j-case}$: Thermal resistance junction-case	max 3 °C/W
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ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^{\circ}C$, $f_{osc} = 20\ KHz$ unless otherwise specified)

Parameter		Test conditions	Min.	Typ.	Max.	Unit
V_s	Supply voltage		18		36	V
I_d	Quiescent drain current	$V_s = 20V$ (offset null)		30	50	mA
V_{OS}	Input offset voltage (pin 6)	$V_s = 36V$ $I_o = 0$			±350	mV
$V_{inh.}$	Inhibit low level (pin 12, 13)				2	V
	Inhibit high level (pin 12, 13)		3.2			V
$I_{inh.}$	Low voltage condition	$V_{inh.} (L) = 0.4V$			-100	μA
	High voltage conditions	$V_{inh.} (H) = 3.2V$			10	μA
I_i	Input current (pin 6)	$V_i = -8.8V$ $V_i = +8.8V$			-1.8 0.5	mA mA
V_i	Input voltage (pin 6)	$R_{s1} = R_{s2} = 0.2\Omega$	$I_o = 2A$	8.3		V
			$I_o = -2A$	-8.3		V
I_o	Output current	$V_i = \pm 8.8V$ $R_{s1} = R_{s2} = 0.2\Omega$	± 2			A
$V_{D.}$	Total drop out voltage	(including sensing resistors)	$I_o = 2A$		5	V
			$I_o = 1A$		3,5	V
V_{RS}	Sensing resistor voltage drop	$T_j = 150^{\circ}C$ $I_o = 2A$			0.44	V
$\frac{I_o}{V_i}$	Transconductance	$R_{s1} = R_{s2} = 0.2\Omega$	228	240	260	mA/V
		$R_{s1} = R_{s2} = 0.4\Omega$		120		mA/V
f_{osc}	Frequency range (pin 10)		1		30	KHz

TRUTH TABLE

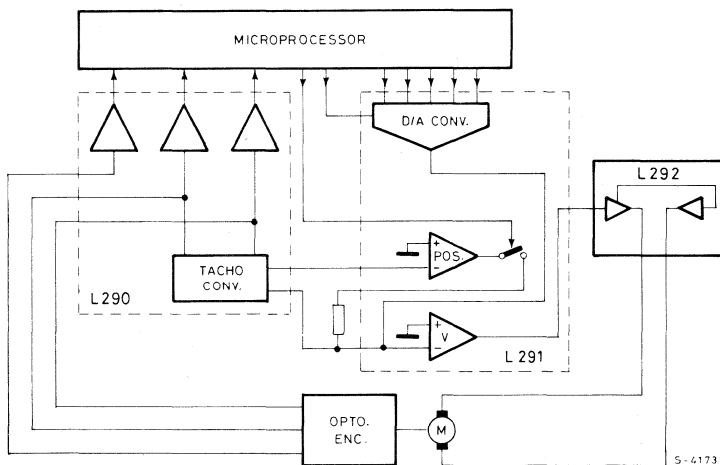
$V_{inhibit}$		Output stage condition
Pin 12	Pin 13	
L	L	Disabled
L	H	Normal operation
H	L	Disabled
H	H	Disabled

Note: The output stage is also disabled if the supply voltage falls below 18V.

SYSTEM DESCRIPTION

The L290, L291 and L292 are intended to be used as a 3-chip microprocessor controlled positioning system. These devices may be used separately - particularly the L292 motor driver - but since they will usually be used together, a description of a typical L290/1/2 system follows.

Fig. 1 - System block diagram



The system operates in two modes to achieve high-speed, high-accuracy positioning.

Speed commands for the system originate in the microprocessor. It is continuously updated on the motor position by means of pulses from the L290 tachometer chip, which in turn gets its information from the optical encoder. From this basic input, the microprocessor computes a 5-bit control word that sets the system speed dependent on the distance to travel.

When the motor is stopped and the microprocessor orders it to a new position, the system operates initially in an open-loop configuration as there is no feedback from the tachometer generator. Therefore maximum current is fed to the motor. As maximum speed is reached, the tachometer chip output backs off the processor signal thus reducing accelerating torque.

The motor continues to run at top speed but under closed-loop control.

As the target position is approached, the microprocessor lowers the value of the speed-demand word; this reduces the voltage at the main summing point, in effect braking the motor. The braking is applied progressively until the motor is running at minimum speed.

At that time, the microprocessor orders a switch to the position mode, (strobe signal at pin 8 of L291) and within 3 to 4 ms the L292 drives the motor to a null position, where it is held by electronic "detenting".

SYSTEM DESCRIPTION (continued)

The mechanical/electrical interface consists of an optical encoder which generates two sinusoidal signals 90° out of phase (leading or lagging according to the motor direction) and proportional in frequency to the speed of rotation. The optical encoder also provides an output at one position on the disk which is used to set the initial position.

The opto encoder signals, FTA and FTB are filtered by the networks $R_2 C_2$ and $R_3 C_3$ (referring to Fig. 4) and are supplied to the FTA/FTB inputs on the L290.

The main function of the L290 is to implement the following expression:

$$\text{Output signal (TACHO)} = \frac{dV_{AA}}{dt} \cdot \frac{FTB}{|FTB|} - \frac{dV_{AB}}{dt} \cdot \frac{FTA}{|FTA|}$$

Thus the mean value of TACHO is proportional to the rotation speed and its polarity indicates the direction of rotation.

The above function is performed by amplifying the input signals in A_1 and A_2 to obtain V_{AA} and V_{AB} (typ. 7 V_p). From V_{AA} and V_{AB} the external differentiator RC networks $R_5 C_6$ and $R_4 C_4$ give the signals V_{MA} and V_{MB} which are fed to the multipliers.

The second input to each multiplier consists of the sign of the first input of the other multiplier before differentiation, these are obtained using the comparators C_{S1} and C_{S2} . The multiplier outputs, C_{SA} and C_{SB} , are summed by A_3 to give the final output signal TACHO. The peak-to-peak ripple signal of the TACHO can be found from the following expression:

$$V_{\text{ripple p-p}} = \frac{\pi}{4} (\sqrt{2} - 1) \cdot V_{\text{tachoc DC}}$$

The max value of TACHO is:

$$V_{\text{tachoc max}} = \frac{\pi}{4} \sqrt{2} \cdot V_{\text{tachoc DC}}$$

Using the comparators C_1 and C_2 another two signals from V_{AA} and V_{AB} are derived - the logic signals STA and STB.

These signals are used by the microprocessor to determine the position by counting the pulses.

The L290 internal reference voltage is also derived from V_{AA} and V_{AB} :

$$V_{\text{ref}} = |V_{AA}| + |V_{AB}|$$

This reference is used by the D/A converter in the L291 to compensate for variations in input levels, temperature changes and ageing.

The "one pulse per rotation" opto encoder output is connected to pin 12 of the L290 (FTF) where it is squared to give the STF logic output for the microprocessor.

The TACHO signal and V_{ref} are sent to the L291 via filter networks $R_8 C_8 R_9$ and $R_6 C_7 R_7$ respectively. Pin 12 of this chip is the main summing point of the system where TACHO and the D/A converter output are compared.

The input to the D/A converter consists of 5 bit word plus a sign bit supplied by the microprocessor. The sign bit represents the direction of motor rotation. The (analogue) output of the D/A converter - DAC/OUT - is compared with the TACHO signal and the resulting error signal is amplified by the error amplifier, and subsequently appears on pin 1.

SYSTEM DESCRIPTION (continued)

The ERRV signal (from pin 1, L291) is fed to pin 6 of the final chip, the L292 H-bridge motor-driver. This input signal is bidirectional so it must be converted to a positive signal because the L292 uses a single supply voltage. This is accomplished by the first stage - the level shifter, which uses an internally generated 8V reference.

This same reference voltage supplies the triangle wave oscillator whose frequency is fixed by the external RC network (R_{20} , C_{17} - pins 11 and 10) where:

$$f_{osc} = \frac{1}{2RC} \quad (\text{with } R \geq 8.2 \text{ K}\Omega)$$

The oscillator determines the switching frequency of the output stage and should be in the range 1 to 30 KHz.

Motor current is regulated by an internal loop in the L292 which is performed by the resistors R_{18} , R_{19} and the differential current sense amplifier, the output of which is filtered by an external RC network and fed back to the error amplifier.

The choice of the external components in these RC network (pins 5, 7, 9) is determined by the motor type and the bandwidth requirements. The values shown in the diagram are for a 5Ω , 5 mH motor. (See L292 Transfer Function Calculation in Application Information).

The error signal obtained by the addition of the input and the current feedback signals (pin 7) is used to pulse width modulate the oscillator signal by means of the comparator. The pulse width modulated signal controls the duty cycle of the H-bridge to give an output current corresponding to the L292 input signal.

The interval between one side of the bridge switching off and the other switching on, τ , is programmed by C_{17} in conjunction with an internal resistor R_{τ} .

This can be found from:

$$\tau = R_{\tau} \cdot C_{pin\ 10} \quad (C_{17} \text{ in the diagram})$$

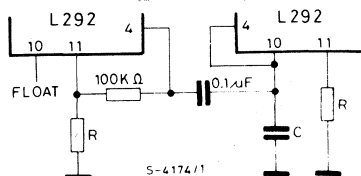
Since R_{τ} is approximately $1.5 \text{ K}\Omega$ and the recommended τ to avoid simultaneous conduction is $2.5 \mu\text{s}$ $C_{pin\ 10}$ should be around 1.5 nF .

The current sense resistors R_{18} and R_{19} should be high precision types (maximum tolerance $\pm 2\%$) and the recommended value is given by:

$$R_{max} \cdot I_{o\ max} \leq 0.44V$$

It is possible to synchronize two L292's, if desired, using the network shown in fig. 2.

Fig. 2



Finally, two enable inputs are provided on the L292 (pins 12 and 13-active low and high respectively).

L 292

SYSTEM DESCRIPTION (continued)

Thus the output stage may be inhibited by taking pin 12 high or by taking pin 13 low. The output will also be inhibited if the supply voltage falls below 18V.

The enable inputs were implemented in this way because they are intended to be driven directly by a microprocessor. Currently available microprocessors may generate spikes as high as 1.5V during power-up. These inputs may be used for a variety of applications such as motor inhibit during reset of the logical system and power-on reset (see fig. 3).

Fig. 3

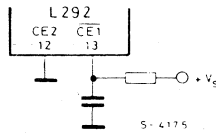
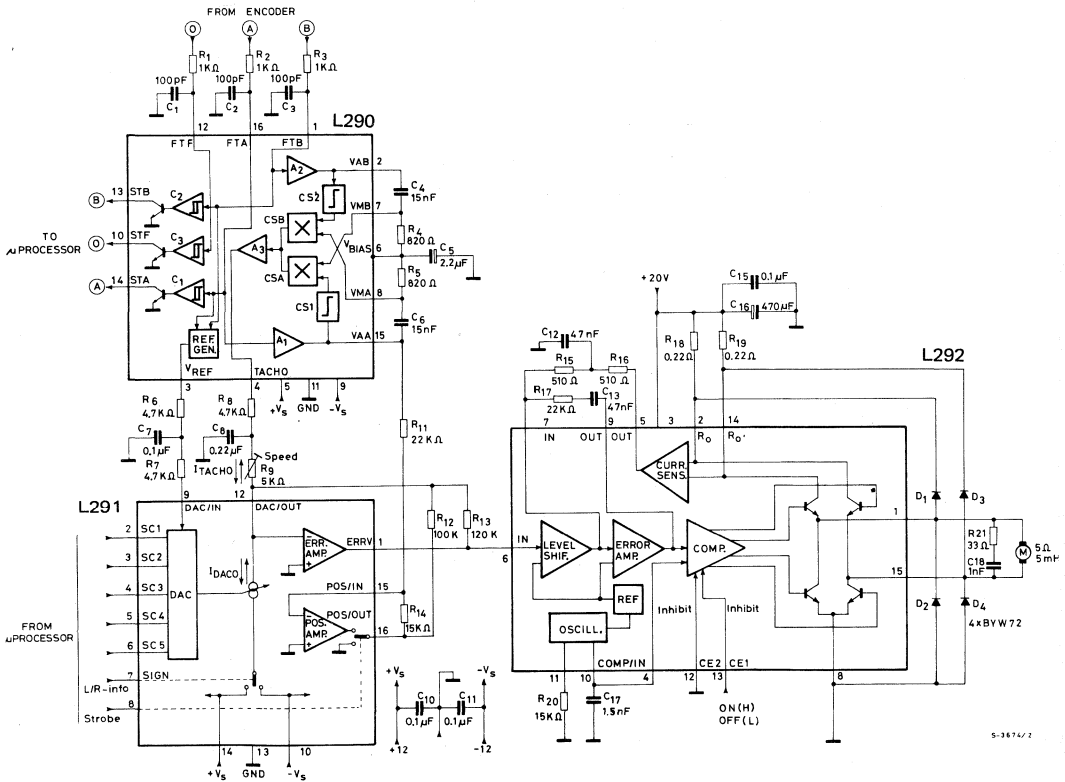


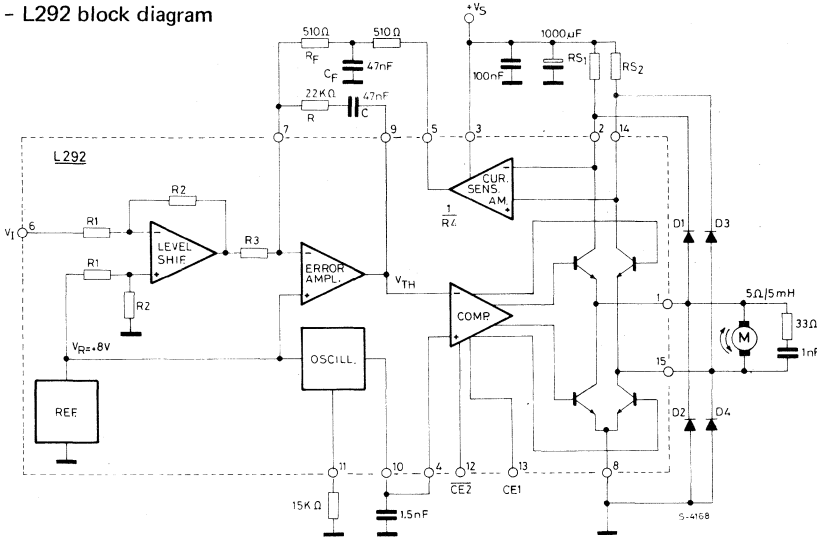
Fig. 4 - Application circuit



APPLICATION INFORMATION

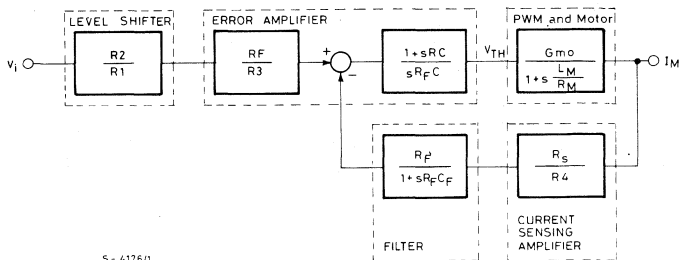
This section has been added in order to help the designer for the best choice of the values of external components.

Fig. 5 - L292 block diagram



The schematic diagram used for the Laplace analysis of the system is shown in fig. 6.

Fig. 6



S - 4176/1

$$R_{S1} = R_{S2} = R_S \text{ (sensing resistors)}$$

$$\frac{1}{R_4} = 0.005 \Omega^{-1} \text{ (current sensing amplifier transconductance)}$$

$$L_M = \text{Motor inductance}$$

$$R_M = \text{Motor resistance}$$

$$I_M = \text{Motor current}$$

$$G_{mo} = \left. \frac{I_M}{V_{TH}} \right|_{s=0} \text{ (DC transfer function from the input of the comparator (} V_{TH} \text{) to the motor current (} I_M \text{)).}$$

APPLICATION INFORMATION (continued)

Neglecting the V_{CEsat} of the bridge transistors and the V_{BE} of the diodes:

$$G_{mo} = \frac{1}{R_M} \frac{2 V_s}{V_R} \quad \text{where: } \begin{array}{l} V_s = \text{supply voltage} \\ V_R = 8V \text{ (reference voltage)} \end{array} \quad (1)$$

DC transfer function

In order to be sure that the current loop is stable the following condition is imposed:

$$1 + sRC = 1 + s \frac{L_M}{R_M} \quad \text{(pole cancellation)} \quad (2)$$

$$\text{from which } RC = \frac{L_M}{R_M} \quad \text{(Note that in practice R must be greater than } 5.6 \text{ K}\Omega)$$

The transfer function is then,

$$\frac{I_M}{V_I}(s) = \frac{R_2 R_4}{R_1 R_3} G_{mo} \frac{1 + sR_F C_F}{G_{mo} R_s + s R_4 C + s^2 R_F C_F R_4 C} \quad (3)$$

In DC condition, this is reduced to

$$\frac{I_M}{V_I}(0) = \frac{R_2 R_4}{R_1 R_3} \cdot \frac{1}{R_s} = \frac{0.048}{R_s} \left[\frac{A}{V} \right] \quad (4)$$

Open-loop gain and stability criterion

For $RC = L_M/R_M$, the open loop gain is:

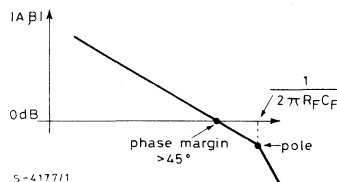
$$A\beta = \frac{1}{sR_F C} \cdot G_{mo} \frac{R_s}{R_4} \frac{R_F}{1 + sR_F C_F} = \frac{G_{mo} R_s}{R_4 C} \frac{1}{s(1 + sR_F C_F)} \quad (5)$$

In order to achieve good stability, the phase margin must be greater than 45° when $|A\beta| = 1$.

That means that, at $f_F = \frac{1}{2\pi R_F C_F}$, must be $|A\beta| < 1$ (see fig. 7), that is

$$|A\beta|_{f = \frac{1}{2\pi R_F C_F}} = \frac{G_{mo} R_s}{R_4 C} \frac{R_F C_F}{\sqrt{2}} < 1 \quad (6)$$

Fig. 7 - Open-loop frequency response



APPLICATION INFORMATION (continued)

Closed-loop system step response

a) Small-signals analysis.

The transfer function (3) can be written as follows:

$$\frac{I_M}{V_i}(s) = \frac{0.048}{R_s} \frac{1 + \frac{s}{2\xi\omega_o}}{1 + \frac{2\xi s}{\omega_o} + \frac{s^2}{\omega_o^2}} \quad (7)$$

where: $\omega_o = \sqrt{\frac{G_{mo} R_s}{R_4 C R_F C_F}}$ is the cutoff frequency

$\xi = \sqrt{\frac{R_4 C}{4 R_F C_F G_{mo} R_s}}$ is the dumping factor

By choosing the ξ value, it is possible to determine the system response to an input step signal. Examples:

1) $\xi = 1$ from which

$$I_M(t) = \frac{0.048}{R_s} \left[1 - e^{-\frac{t}{2R_F C_F}} \left(1 + \frac{t}{4R_F C_F} \right) \right] \cdot V_i$$

(where V_i is the amplitude of the input step).

2) $\xi = \frac{1}{\sqrt{2}}$ from which

$$I_M(t) = \frac{0.048}{R_s} \left(1 - \cos \frac{t}{2R_F C_F} e^{-\frac{t}{2R_F C_F}} \right) V_i$$

From fig. 9, it is possible to verify that the L292 works in "closed-loop" conditions during the entire motor current rise-time: the voltage at pin 7 (inverting input of the error amplifier) is locked to the reference voltage V_R , present at the non-inverting input of the same amplifier.

The previous linear analysis is correct for this example.

Decreasing the ξ value, the rise-time of the current decreases. But for a good stability, from relationship (6), the minimum value of ξ is:

$$\xi_{\min} = \frac{1}{2\sqrt{2}} \quad (\text{phase margin} = 45^\circ)$$

Fig. 8 - Small signal step response (normalized amplitude vs. $t/R_F C_F$)

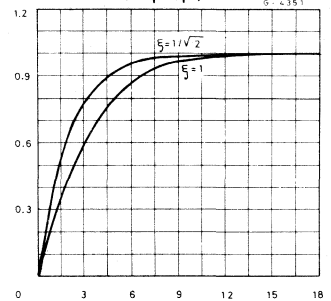
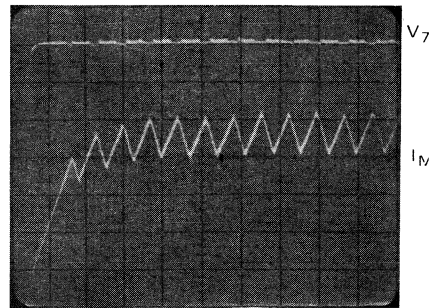


Fig. 9 - Motor current and pin 7 voltage waveforms (application of fig. 5). Small signal response



$V_7 = 200\text{mV/div.}$

$I_M = 100\text{mA/div.}$

$t = 100\mu\text{s/div.}$

with $V_i = 1.5\text{ Vp.}$

L 292

APPLICATION INFORMATION (continued)

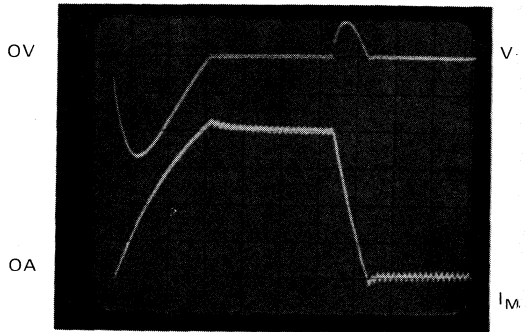
b) Large signal response

The large signal response is limited by slew-rate and inductive load.

In this case, during the rise-time of the motor current, the L292 works in open-loop condition, as can be seen from the photograph of fig. 10.

Fig. 10 - Motor current and pin 7 voltage waveforms (application of fig. 5) Large signal response.

$$\begin{aligned} V_7 &= 1\text{V/div.} \\ I_M &= 0.5\text{A/div.} \\ t &= 500\mu\text{s/div.} \end{aligned}$$



The voltage at pin 7 (inverting input of the error amplifier) departs from the reference voltage V_R present at the non-inverting input and the feedback loop is open.

The feedback loop is on when the motor current reaches its steady-state value (2A).

Closed loop system bandwidth

A good choice for ξ is the value $1/\sqrt{2}$. In this case:

$$\frac{I_M}{V_I}(s) = \frac{0.048}{R_s} \frac{1 + s R_F C_F}{1 + 2s R_F C_F + 2s^2 R_F^2 C_F^2} \quad (8)$$

The module of the transfer function is:

$$\left| \frac{I_M}{V_I} \right| = \frac{0.048}{R_s} \frac{\sqrt{2} \sqrt{1 + \omega^2 R_F^2 C_F^2}}{\sqrt{[(1 + 2\omega R_F C_F)^2 + 1]} \cdot \sqrt{[(1 - 2\omega R_F C_F)^2 + 1]}} \quad (9)$$

The cutoff frequency is derived by the expression (9) by putting $\left| \frac{I_M}{V_I} \right| = 0.707$ (-3 dB), from which:

$$\omega_T = \frac{0.9}{R_F C_F} \qquad f_T = \frac{0.9}{2\pi R_F C_F}$$

APPLICATION INFORMATION (continued)

Example:

- a) Data
- Motor characteristics : $L_M = 5 \text{ mH}$
 $R_M = 5 \Omega$
 $L_M/R_M = 1 \text{ msec}$
 - Voltage and current characteristics:
 $V_s = 20\text{V}$ $I_M = 2\text{A}$ $V_I = 8.3\text{V}$
 - Closed loop bandwidth: 6 KHz.

- b) Calculation
- From relationship (4):

$$R_s = \frac{0.048}{I_M} \quad V_I = 0.2\Omega$$

and from (1):

$$G_{mo} = \frac{2 V_s}{R_M V_R} = 1 \Omega^{-1}$$

- $RC = 1 \text{ msec}$ [from expression (2)].
- Assuming $\xi = 1/\sqrt{2}$; from (7) follows:

$$\xi^2 = \frac{1}{2} = \frac{200 C}{4 R_F C_F \cdot 0.2}$$

- The cutoff frequency is:

$$f_T = \frac{143 \cdot 10^{-3}}{R_F C_F} = 6 \text{ KHz}$$

- c) Summarising
- $RC = 1 \cdot 10^{-3} \text{ sec}$
 - $\frac{500 C}{R_F C_F} = 1$
 - $R_F C_F \cong 24 \mu\text{sec}$

}

$$C = 47 \text{ nF}$$

$$R = 22 \text{ K}\Omega$$

$$\text{For } R_F = 510 \Omega \rightarrow C_F = 47 \text{ nF.}$$

L 293

LINEAR INTEGRATED CIRCUIT

PRELIMINARY DATA

PUSH-PULL FOUR CHANNEL DRIVER

The L293 is a monolithic integrated high voltage, high current four channel driver in a 16-pin DIP package designed to accept standard DTL or TTL logic levels and drive inductive loads (such as relays solenoids, DC and stepping motors) and switching power transistors.

Two inhibit inputs are provided, which disable two channels each.

An additional supply input is provided so that the logic may be run at a lower voltage.

FEATURES

- 1 A output current capability per channel.
- 2 A peak output current (non repetitive) per channel.
- Inhibiting facility.
- Overtemperature protection.
- Logical "0" input voltage up to 1.5V (high noise immunity).

The L293 is assembled in a new 16 lead plastic package which has 4 centre pins connected together and used for heatsinking.

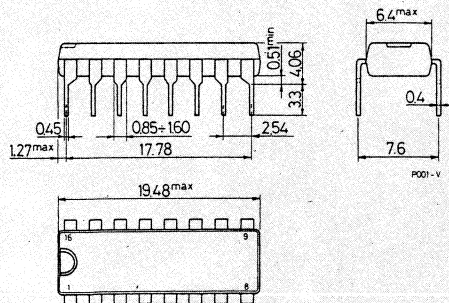
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	36	V
V_{ss}	Logic supply voltage	36	V
V_i	Input voltage	7	V
$V_{inhibit}$	Inhibit voltage	7	V
I_{out}	Peak output current (5 ms non repetitive)	2	A
P_{tot}	Total power dissipation at $T_{case} = 80^\circ\text{C}$	5	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

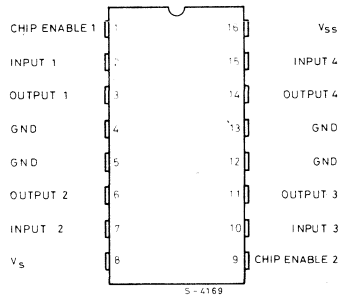
ORDERING NUMBER: L293B

MECHANICAL DATA

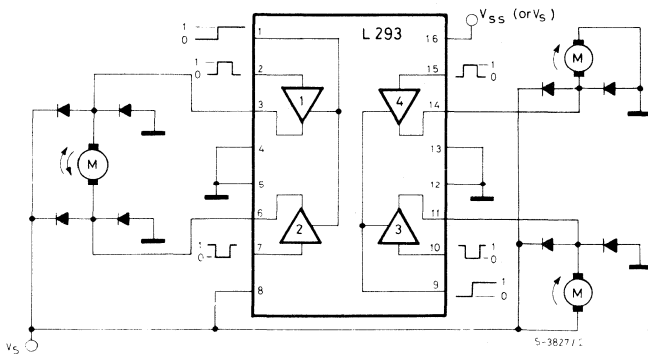
Dimensions in mm



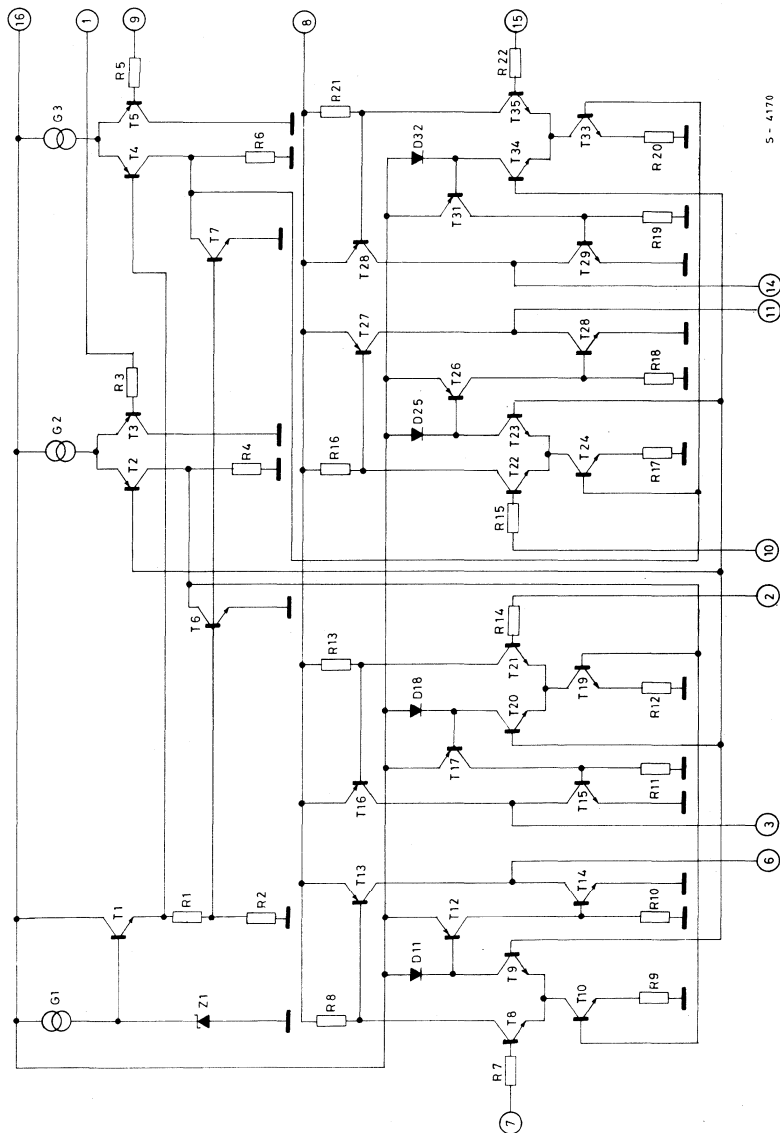
CONNECTION DIAGRAM (top view)



BLOCK DIAGRAM



SCHEMATIC DIAGRAM



THERMAL DATA

$R_{th\ j-case}$	Thermal resistance junctions-case	max	14	°C/W
$R_{th\ j-amb}$	Thermal resistance junctions-amb	max	80	°C/W

ELECTRICAL CHARACTERISTICS (for each channel, $V_s = 24V$, $V_{ss} = 5V$, $T_{amb} = 25^\circ C$)

Parameter		Test conditions	Min.	Typ.	Max.	Unit
V_s	Supply voltage (pin 8)				36	V
V_{ss}	Logic supply voltage		4.5		36	V
I_s	Quiescent supply current (pin 8)	$V_i = L$ $I_o = 0$ $V_{inh} = H$		0.5	1.5	mA
		$V_i = H$ $I_o = 0$ $V_{inh} = H$ $V_{inh} = L$		4	6 1	mA mA
I_{ss}	Quiescent current from V_{ss}	$V_i = L$ $I_o = 0$ $V_{inh} = H$		11	15	mA
		$V_i = H$ $I_o = 0$ $V_{inh} = H$ $V_{inh} = L$		4 4	5.5 6	mA mA
V_i	Input voltage	Low	-0.3		1.5	V
		High	(°)	2.3	7	V
I_i	Input current	$V_i = L$			10	μA
		$V_i = H$		30	100	μA
V_{inh} voltage (pin 1, 9)	Low		-0.3		1.5	V
		High	(°)	2.3	7	V
I_{inh} current (pin 1, 9)		$V_{inh} = L$		-30	-100	μA
		$V_{inh} = H$			± 10	μA
V_{CEsat} (H)	Source saturation voltage	$I_C = 1A$			1.8	V
V_{CEsat} (L)	Sink saturation voltage	$I_C = 1A$			1.8	V
t_r	Rise time	0.1 to 0.9 V_o (°°)		250		ns
t_f	Fall time	0.9 to 0.1 V_o (°°)		250		ns
t_{on}	Turn-on delay	0.5 V_i to 0.5 V_o (°°)		450		ns
t_{off}	Turn-off delay	0.5 V_i to 0.5 V_o (°°)		200		ns

(°) In any case, V_i and V_{inh} (High level) must be $\leq V_{ss}$.

(°°) See fig. 1.

TRUTH TABLE

V_i (each channel)	V_o	$V_{inh.} (^{\circ\circ})$
H	H	H
L	L	H
H	X ($^{\circ}$)	L
L	X ($^{\circ}$)	L

($^{\circ}$) High output impedance.

($^{\circ\circ}$) Relative to the considered channel.

Fig. 1 - Switching times

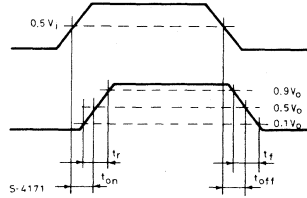


Fig. 2 - Saturation voltage vs. output current

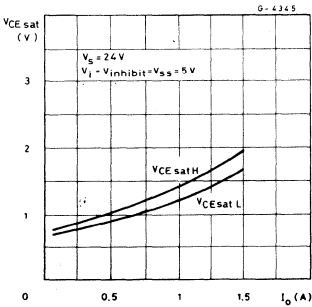


Fig. 3 - Source saturation voltage vs. ambient temperature

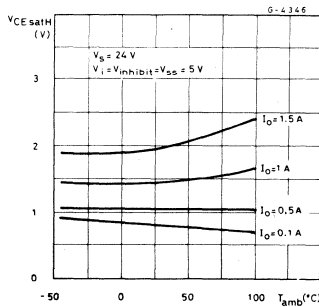


Fig. 4 - Sink saturation voltage vs. ambient temperature

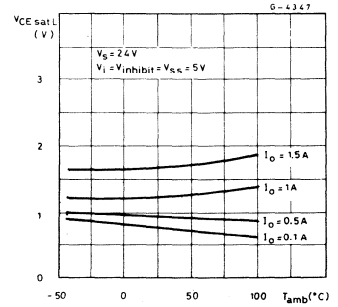


Fig. 5 - Supply current I_{SS} vs. logic supply voltage

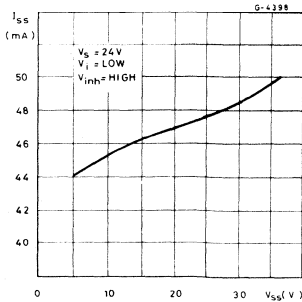


Fig. 6 - Output voltage vs. input voltage

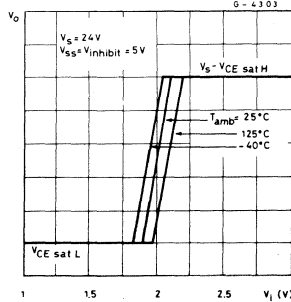
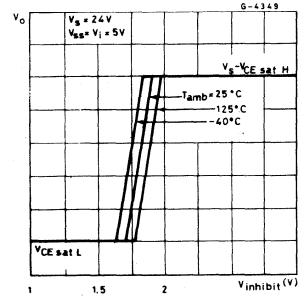
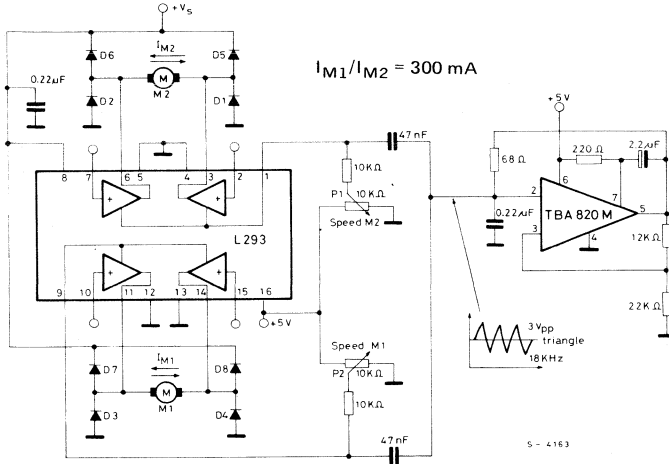


Fig. 7 - Output voltage vs. inhibit voltage



APPLICATION INFORMATION

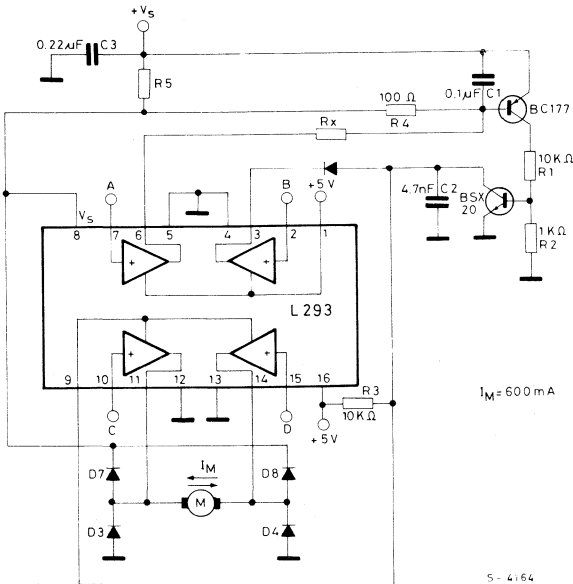
Fig. 8 - Dual DC motor bridge driver with PWM speed regulation



The inhibit is used as a comparator.

The DC level of the triangle generator, adjusted by P_1/P_2 , controls the duty-cycle of the motor current.

Fig. 9 - DC motor bridge driver with switched mode current limiting



The value of R_5 limits the maximum motor current:

$$I_{M \max} = \frac{0.6 \text{ V}}{R_5}$$

Low	High	Logic
C	D	Turn right
D	C	Turn left
	B	Current controlled only by R_5
A	A	
A	B	Current reducing by value of R_x
B	A	Free running motor stop
	D	Fast motor stop (shorted)
D	C	

L 293

APPLICATIONS INFORMATION (continued)

Fig. 10 - Bipolar stepping motor control

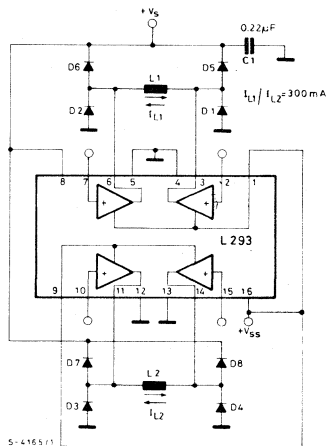
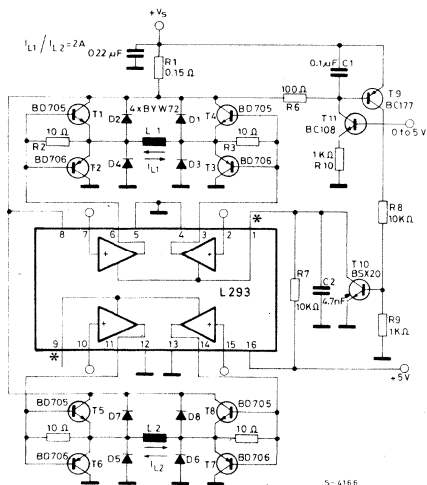


Fig. 11 - Bipolar stepping motor control with external power transistors



Note: The resistor R1 carries the sum of the currents $I_{L1} + I_{L2}$; when this current reaches a value

$$I_{sum} = \frac{V_{BE}}{R1}$$

the transistors T9 and T10 turn on and C2 is discharged. The voltage on the inhibit inputs of the IC falls below the lower threshold and the final stages are switched off.

When the coil current falls T9 and T10 are switched off, C2 recharges via R7 up to the input high threshold of the IC and the final stages are again turned-on.

When the base of T11 is connected to +5V a constant collector current flows in R6. This current is

$$I_C = \frac{5 - V_{BE}}{R10}$$

This causes a voltage drop across R6 which biases the V_{BE} junction of T9 and moves the current limiting point to a lower level, the value of which depends on R10.

(*) Pin 1 and Pin 9 are connected together.

MOUNTING INSTRUCTIONS

The $R_{thj-amb}$ of the L293 can be reduced by soldering the GND pins to a suitable copper area of the printed circuit board or to an external heatsink.

The diagram of fig. 13 shows the maximum dissippable power P_{tot} and the $R_{thj-amb}$ as a function of the side "l" of two equal square copper areas having a thickness of 35μ (see fig. 12). In addition, it is possible to use an external heatsink (see fig. 14).

During soldering the pins temperature must not exceed 260°C and the soldering time must not be longer than 12 seconds.

The external heatsink or printed circuit copper area must be connected to electrical ground.

Fig. 12 - Example of P.C. board copper area which is used as heatsink

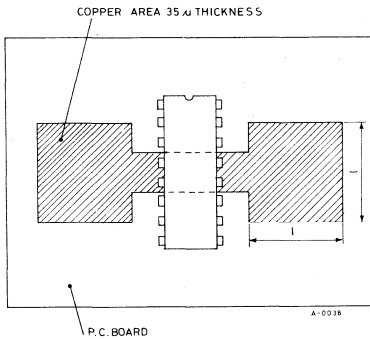


Fig. 14 - External heatsink mounting example ($R_{th} = 30^{\circ}\text{C/W}$)

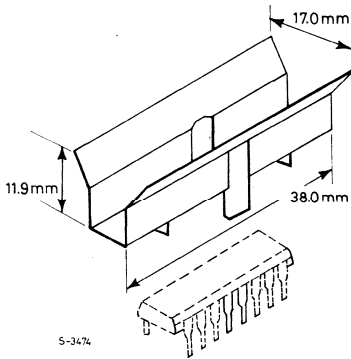


Fig. 13 - Max. dissippable power and junction to ambient thermal resistance vs. size "l"

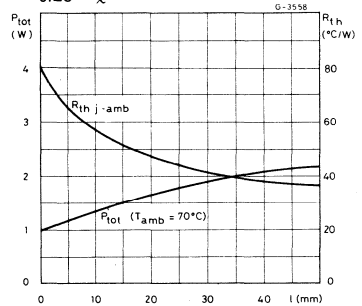
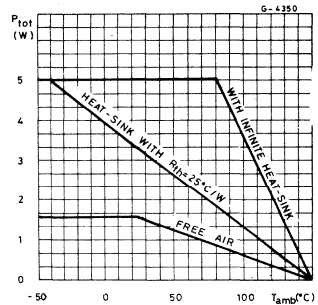


Fig. 15 - Maximum allowable power dissipation vs. ambient temperature



L 601 L 602 L 603 L 604

LINEAR INTEGRATED CIRCUITS

HIGH-VOLTAGE, HIGH-CURRENT 8 DARLINGTON ARRAYS

These high-voltage, high-current Darlington transistor arrays comprise eight silicon NPN Darlington on a common monolithic substrate. All units feature open collector outputs and integral suppression diodes for inductive loads. Peak currents of 500 mA can be withstood. They are pinned with inputs opposite outputs to facilitate circuit board layout.

- The L601 is a general-purpose array which may be used with DTL, TTL, PMOS, CMOS, etc.
- The L602 is specifically designed for use with 14 to 25V PMOS devices. Each input has a Zener diode and resistor in series in order to limit the input current to a safe value.
- The L603 has a series base resistor to each Darlington pair, and thus allows operation directly with TTL or CMOS operating at a supply voltage of 5V.
- The L604 has a series base resistor to each Darlington pair, and thus allows operation directly with PMOS or CMOS utilizing supply voltage of 6 to 15V.

In all cases, the individual Darlington collector current rating is 400 mA. However, outputs may be paralleled for higher load current capability. The devices are supplied in a 18-lead dual in-line plastic package with copper frame.

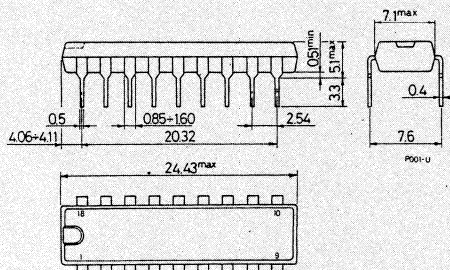
ABSOLUTE MAXIMUM RATINGS

V_{CEX}	Collector emitter voltage (input open)	90	V
I_C	Collector current	0.4	A
I_C	Collector peak current	0.5	A
V_i	Input voltage (for L602 , L603 and L604)	30	V
I_i	Input current (for L601 only)	25	mA
P_{tot}	Total power dissipation at $T_{amb} = 25^\circ\text{C}$	1.8	W
T_{op}	Operating junction temperature	-25 to 150	$^\circ\text{C}$
T_{stg}	Storage temperature	-55 to 150	$^\circ\text{C}$

ORDERING NUMBERS: L601B, L602B, L603B, L604B

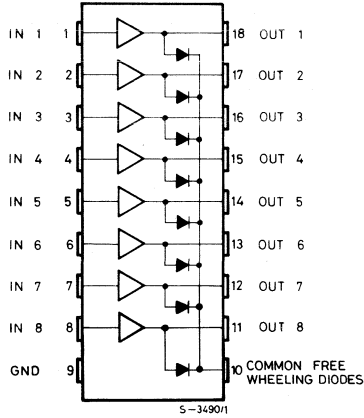
MECHANICAL DATA

Dimensions in mm



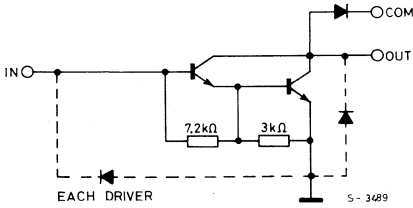
L 601 L 602 L 603 L 604

CONNECTION DIAGRAM (top view)

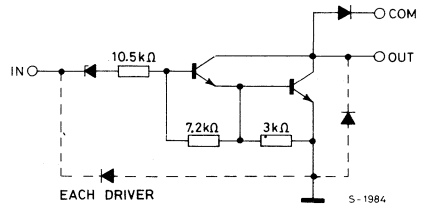


SCHEMATIC DIAGRAMS

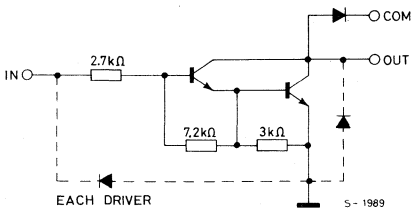
L601



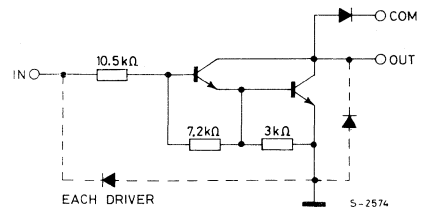
L602



L603



L604



L 601 L 602 L 603 L 604

THERMAL DATA

$R_{th\ j-amb}$ Thermal resistance junction-ambient	max 70 °C/W
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ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^{\circ}C$, unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
I_{CEX} Output leakage current	$V_{CE} = 90V$			3	μA
$V_{CE(sat)}$ Collector emitter saturation voltage	$I_C = 300\ mA$ $I_B = 500\ \mu A$ $I_C = 200\ mA$ $I_B = 350\ \mu A$ $I_C = 100\ mA$ $I_B = 250\ \mu A$			2 1.7 1.2	V V V
h_{FE} DC forward current gain (L601 only)	$V_{CE} = 3V$ $I_C = 300\ mA$	1000			—
V_i Minimum input voltage (ON condition)	$V_{CE} = 3V$ for L602 for L603 for L604 $I_C = 300\ mA$			11.5 2 2.5	V V V
V_j Maximum input voltage (OFF condition)	$V_{CE} = 90V$ for L601 for L602 for L603 for L604 $I_C = 25\ \mu A$	0.55 7 0.85 1			V V V V
I_R Clamp diode reverse current	$V_R = 90V$			50	μA
V_F Clamp diode forward voltage	$I_F = 300\ mA$		2	2.4	V
t_{on} Turn-on delay	$0.5\ V_i$ to $0.5\ V_o$		0.4		μs
t_{off} Turn-off delay	$0.5\ V_i$ to $0.5\ V_o$		0.4		μs

LINEAR INTEGRATED CIRCUIT

QUAD DARLINGTON SWITCHES

- SUSTAINING VOLTAGE: MIN. 70V
- 2A OUTPUT
- HIGH CURRENT GAIN

The L 702 is a monolithic bipolar integrated circuit for high current and high voltage switching applications.

It comprises four darlington transistors with common emitter and open collector, suitable for current sinking applications, mounted on the new **Powerdip** and **Multiwatt** packages. This circuit reduces components, sizes and costs; it can provide direct interface between low level logic and a variety of high current applications.

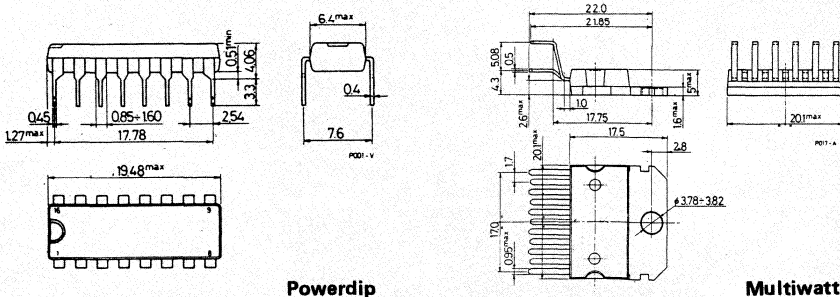
ABSOLUTE MAXIMUM RATINGS

V_{CEX}	Collector-emitter voltage (input open)	90	V	
V_i	Input voltage	30	V	
I_C	Collector current	2	A	
I_{Cp}	Collector peak current (repetitive)	3	A	
P_{tot}	Total power dissipation at $T_{pin\ 9\ to\ 16} \leq 90^\circ C$	} Powerdip	4	W
	Total power dissipation at $T_{amb} \leq 70^\circ C$		1.1	W
	Total power dissipation at $T_{case} \leq 90^\circ C$		20	W
T_{stg}	Storage temperature	-55 to 150	$^\circ C$	
T_j	Operating junction temperature	-25 to 150	$^\circ C$	

ORDERING NUMBER: L 702B - Powerdip
L 702N - Multiwatt

MECHANICAL DATA

Dimensions in mm

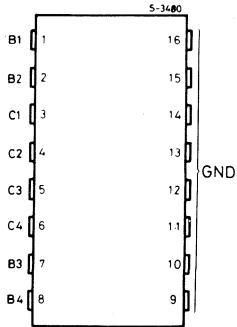


Powerdip

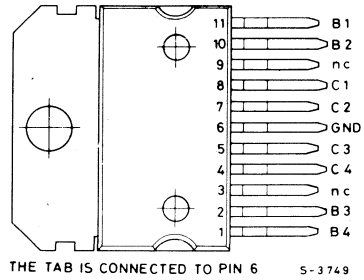
Multiwatt

L 702

CONNECTION DIAGRAMS (top view)

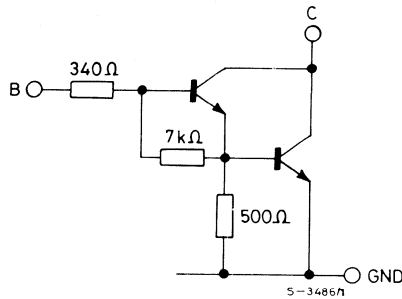


Powerdip



Multiwatt

SCHEMATIC DIAGRAM (each Darlington)



THERMAL DATA

$R_{th\ j-amb}$	Thermal resistance junction ambient	} Powerdip	max	70	$^{\circ}\text{C}/\text{W}$
$R_{th\ j-pins\ 9/16}$	Thermal resistance junction pins 9 to 16		max	14	$^{\circ}\text{C}/\text{W}$
$R_{th\ j-case}$	Thermal resistance junction-case	Multiwatt	max	3	$^{\circ}\text{C}/\text{W}$

ELECTRICAL CHARACTERISTICS ($T_{case} = 25^{\circ}C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
I_{CEX} Output leakage current	$V_{CE} = 90V$		10	50	μA
$V_{CE(sust)}$ Collector emitter ($^{\circ}$) sustaining voltage	$I_C = 100\text{ mA}$	70			V
$V_{CE(sat)}$ Collector emitter saturation voltage	$I_C = 1.25A$ $I_i = 2\text{ mA}$		1.3	1.9	V
h_{FE} DC forward current gain	$I_C = 1A$ $V_{CE} = 3V$	1700	4000		
I_i Input current	$V_i = 3.75V$ $V_i = 2.4V$ open collector		7 3	11 6	mA mA
V_i Input voltage	off condition on condition	$V_{CE} = 70V$ $V_{CE} = 3V$	$I_C \leq 0.1\text{ mA}$ $I_C \geq 1A$	0.4	V V
t_{on} Turn on time	$V_s = 12V$		0.3		μs
t_{off} Turn off time	$R_L = 10\ \Omega$		1		μs

($^{\circ}$) Pulsed: pulse duration = 300 μs , duty cycle = 1.5%.

Fig. 1 - Switching time

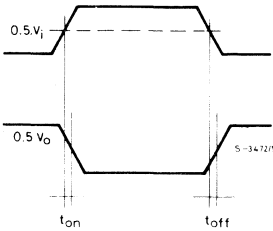


Fig. 2 - t_{on} and t_{off} test circuit

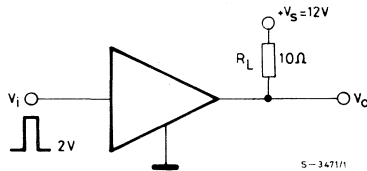
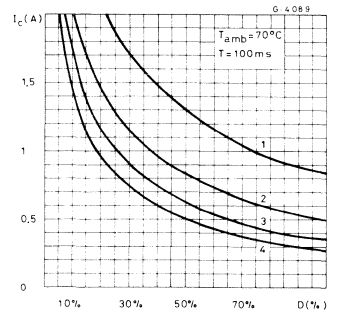


Fig. 3 - Peak collector current vs. duty cycle and number of outputs(L702B only)



L 702

Fig. 4 - Collector emitter saturation voltage vs. collector current

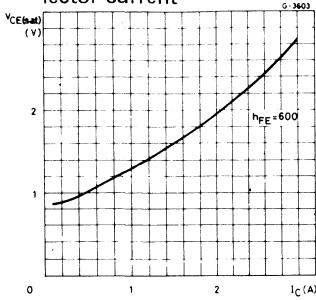


Fig. 5 - Collector current vs. input voltage

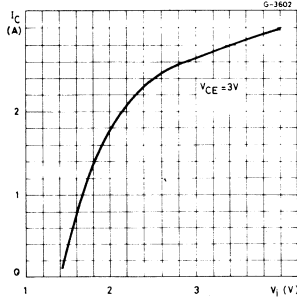


Fig. 6 - Input current vs. input voltage

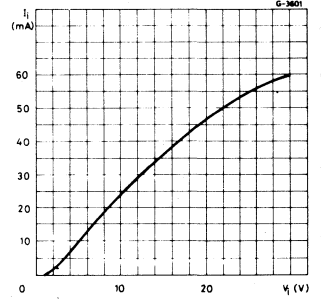


Fig. 7 - Safe operating areas (L702B)

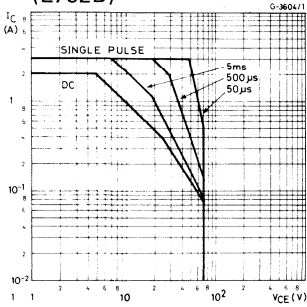


Fig. 8 - Safe operating areas (L702N)

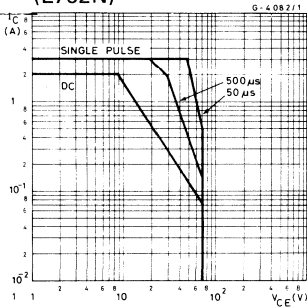
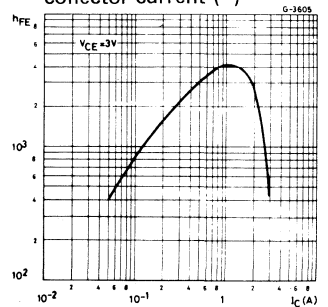


Fig. 9 - DC current gain vs. collector current (*)



(*) Pulse width = 300 μs , duty cycle 1.5%.

LINEAR INTEGRATED CIRCUITS

NOT FOR NEW DESIGN

3-TERMINAL POSITIVE VOLTAGE REGULATORS

- OUTPUT CURRENT UP TO 2A
- OUTPUT VOLTAGES OF 5; 7.5; 9; 10; 12; 15; 18; 24V
- THERMAL OVERLOAD PROTECTION
- SHORT CIRCUIT PROTECTION
- OUTPUT TRANSISTOR SOA PROTECTION

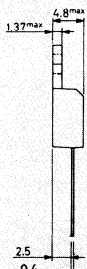
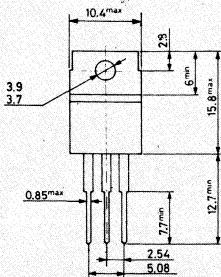
The L2000 series of three-terminal positive regulators is available in TO-220 and TO-3 packages and with several fixed output voltages, making it useful in a wide range of applications. These regulators can provide local on-card regulation, eliminating the distribution problems associated with single point regulation. Each type employs internal current limiting, thermal shut-down and safe area protection, making it essentially indestructible. If adequate heat sinking is provided, they can deliver over 2A output current. Although designed primarily as fixed voltage regulators, these devices can be used with external components to obtain adjustable voltages and currents.

ABSOLUTE MAXIMUM RATINGS

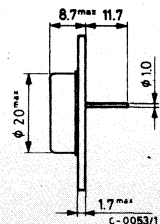
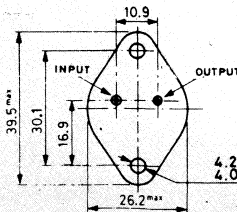
V_i	DC input voltage (for $V_o = 5$ to 18V) (for $V_o = 24V$)	35 V 40 V
I_o	Output current	internally limited
P_{tot}	Power dissipation	Internally limited
T_{stg}	Storage temperature	-65 to +150 °C
T_{op}	Operating junction temperature (for L2000) (for L2000C)	-55 to +150 °C 0 to +150 °C

MECHANICAL DATA

Dimensions in mm



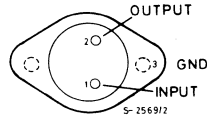
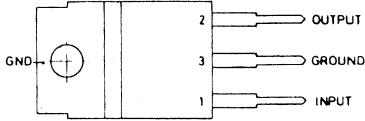
TO-220



TO-3

L 2000 Series

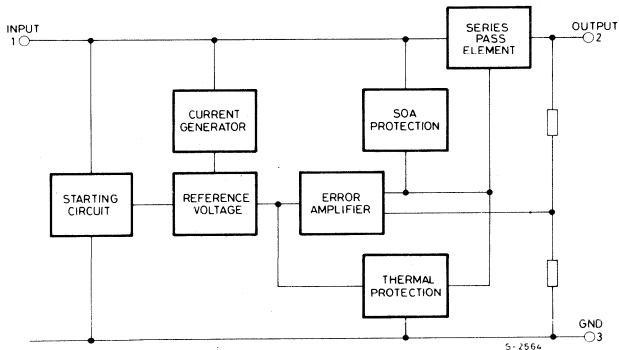
CONNECTION DIAGRAMS AND ORDERING NUMBERS (top views)



S-2566/1

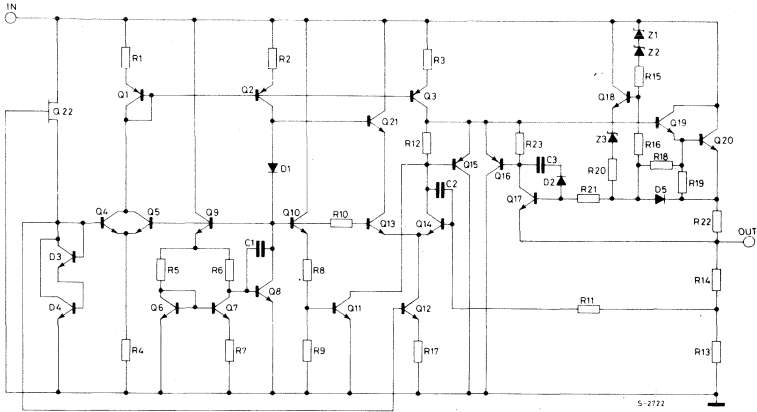
Type	TO-220	TO-3	Output voltage
L2005	—	L2005T	5V
L2005C	L2005CV	L2005CT	5V
L2075	—	L2075T	7.5V
L2075C	L2075CV	L2075CT	7.5V
L2009	—	L2009T	9V
L2009C	L2009CV	L2009CT	9V
L2010	—	L2010T	10V
L2010C	L2010CT	L2010CT	10V
L2012	—	L2012T	12V
L2012C	L2012CV	L2012CT	12V
L2015	—	L2015T	15V
L2015C	L2015CV	L2015CT	15V
L2018	—	L2018T	18V
L2018C	L2018CV	L2018CT	18V
L2024	—	L2024T	24V
L2024C	L2024CV	L2024CT	24V

BLOCK DIAGRAM



L2000 Series

SCHEMATIC DIAGRAM



TEST CIRCUITS

Fig. 1 - DC parameters

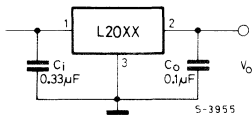


Fig. 2 - Load regulation

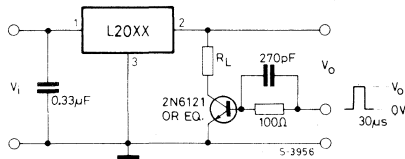
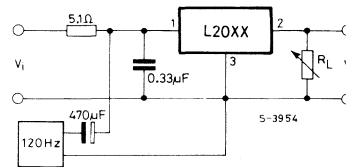


Fig. 3 - Ripple rejection



THERMAL DATA

			TO-220	TO-3
$R_{th \text{ j-case}}$	Thermal resistance junction-case	max	3 °C/W	4 °C/W
$R_{th \text{ j-amb}}$	Thermal resistance junction-ambient	max	50 °C/W	35 °C/W

L 2000 Series

ELECTRICAL CHARACTERISTICS L2000 (Refer to the test circuits, $T_j = 25^\circ\text{C}$, $I_o = 500\text{ mA}$ unless otherwise specified)

OUTPUT VOLTAGE		5			7.5			9			10			Unit
INPUT VOLTAGE (Unless otherwise specified)		10			12.5			14			15			
Parameter	Test conditions	Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	
V_o Output voltage		4.8	5	5.2	7.15	7.5	7.9	8.65	9	9.35	9.5	10	10.5	V
	$I_o = 1\text{ A}$	4.75	5	5.25 ($V_i = 7\text{V}$)	7.1	7.5	7.95 ($V_i = 9.5\text{V}$)	8.6	9	9.4 ($V_i = 11\text{V}$)	9.4	10	10.6 ($V_i = 12.5\text{V}$)	
ΔV_o Line regulation		100 ($V_i = 7$ to 25V)			120 ($V_i = 9.5$ to 25V)			130 ($V_i = 11$ to 25V)			200 ($V_i = 12.5$ to 30V)			mV
		50 ($V_i = 8$ to 12V)			60 ($V_i = 10.5$ to 20V)			65 ($V_i = 11$ to 20V)			100 ($V_i = 14$ to 22V)			
ΔV_o Load regulation	$I_o = 20\text{ mA}$ to 2 A	100			120			130			150			mV
I_d Quiescent current		8			8			8			8			mA
ΔI_d Quiescent current change	$I_o = 20\text{ mA}$ to 1 A	0.5			0.5			0.5			0.5			mA
	$I_o = 20\text{ mA}$	1.3 ($V_i = 7$ to 25V)			1.3 ($V_i = 9.5$ to 25V)			1.3 ($V_i = 11$ to 25V)			1 ($V_i = 12.5$ to 30V)			
$\frac{\Delta V_o}{\Delta T}$ Output voltage drift	$I_o = 5\text{ mA}$ $T_j = -55$ to 150°C	-1.1			-0.8			-1			-1			mV/ $^\circ\text{C}$
e_N Output noise voltage	$B = 10\text{Hz}$ to 100KHz	40			52			60			65			μV
SVR Supply voltage rejection	$f = 120\text{ Hz}$	60			54			53			53			dB
V_i Operating input voltage	$I_o \leq 1.5\text{ A}$	8			10.5			12			13			V
R_o Output resistance	$f = 1\text{ KHz}$	17			16			17			17			m Ω
I_{sc} Short circuit current	$V_i = 27\text{V}$	500			500			500			500			mA
I_{scp} Short circ. peak current		3.5			3.5			3.5			3.5			A

ELECTRICAL CHARACTERISTICS L2000 (continued)

OUTPUT VOLTAGE		12			15			18			24			Unit	
INPUT VOLTAGE (Unless otherwise specified)		19			23			26			33				
Parameter	Test conditions	Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.		
V _o	Output voltage	11.5	12	12.5	14.4	15	15.6	17.1	18	18.9	23	24	25		V
	I _o = 1A	11.4	12	12.6 (V _i = 14.5V)	14.25	15	15.75 (V _i = 17.5V)	17	18	19 (V _i = 20.5V)	22.8	24	25.2 (V _i = 27V)		
ΔV _o	Line regulation	240 (V _i = 14.5 to 30V)			300 (V _i = 17.5 to 30V)			360 (V _i = 20.5 to 30V)			480 (V _i = 27 to 38V)			mV	
		120 (V _i = 16 to 22V)			150 (V _i = 20 to 26V)			180 (V _i = 22 to 28V)			240 (V _i = 30 to 36V)				
ΔV _o	Load regulation	I _o = 20 mA to 2A			160			180			200			250	mV
I _d	Quiescent current				8			8			8			8	mA
ΔI _d	Quiescent current change	I _o = 20 mA to 1A			0.5			0.5			0.5			0.5	mA
		I _o = 20 mA			1 (V _i = 14.5 to 30V)			1 (V _i = 17.5 to 30V)			1 (V _i = 22 to 33V)			1 (V _i = 28 to 38V)	
$\frac{\Delta V_o}{\Delta T}$	Output voltage drift	I _o = 5mA T _j = -55 to 150°C			-1			-1			-1			-1.5	mV/°C
e _N	Output noise voltage	B = 10Hz to 100KHz			75			90			110			170	μV
SVR	Supply voltage rejection	f = 120 Hz			53			52			49			48	dB
V _i	Operating input voltage	I _o ≤ 1.5A			15			18			21			27	V
R _o	Output resistance	f = 1 KHz			18			19			22			23	mΩ
I _{sc}	Short circuit current	V _i = 27V			500			500			500			500	mA
I _{scp}	Short circ. peak current				3.5			3.5			3.5			3.5	A

L 2000 Series

ELECTRICAL CHARACTERISTICS L2000C (Refer to the test circuits, $T_j = 25^\circ\text{C}$, $I_o = 500\text{mA}$ unless otherwise specified)

OUTPUT VOLTAGE		5	7.5	9	10	Unit
INPUT VOLTAGE (Unless otherwise specified)		10	12.5	14	15	
Parameter	Test conditions	Min. Typ. Max.	Min. Typ. Max.	Min. Typ. Max.	Min. Typ. Max.	
V_o Output voltage		4.8 5 5.2	7.15 7.5 7.9	8.65 9 9.35	9.5 10 10.5	V
	$I_o = 1\text{A}$	4.75 5 5.25 ($V_i = 7\text{V}$)	7.1 7.5 7.95 ($V_i = 9.5\text{V}$)	8.6 9 9.4 ($V_i = 11\text{V}$)	9.4 10 10.6 ($V_i = 12.5\text{V}$)	
ΔV_o Line regulation		100 ($V_i = 7$ to 25V)	120 ($V_i = 9.5$ to 25V)	130 ($V_i = 11$ to 25V)	200 ($V_i = 12.5$ to 30V)	mV
		50 ($V_i = 8$ to 12V)	60 ($V_i = 10.5$ to 20V)	65 ($V_i = 11$ to 20V)	100 ($V_i = 14$ to 22V)	
ΔV_o Load regulation	$I_o = 20\text{mA}$ to 2A	100	140	170	240	mV
I_d Quiescent current		8	8	8	8	mA
ΔI_d Quiescent current change	$I_o = 20\text{mA}$ to 1A	0.5	0.5	0.5	0.5	mA
	$I_o = 20\text{mA}$	1.3 ($V_i = 7$ to 25V)	1.3 ($V_i = 9.5$ to 25V)	1.3 ($V_i = 11$ to 25V)	1.0 ($V_i = 12.5$ to 30V)	
$\frac{\Delta V_o}{\Delta T}$ Output voltage drift	$I_o = 5\text{mA}$ $T_{\text{amb}} = 0$ to 70°C	-1.1	-0.8	-1	-1	mV/ $^\circ\text{C}$
e_N Output noise voltage	$B = 10\text{Hz}$ to 100KHz	40	52	60	65	μV
SVR Supply voltage rejection	$f = 120\text{Hz}$	54	48	47	47	dB
V_i Operating input voltage	$I_o \leq 1.5\text{A}$	8	10.5	12	13	V
R_o Output resistance	$f = 1\text{KHz}$	17	16	17	17	$\text{m}\Omega$
I_{sc} Short circuit current	$V_i = 27\text{V}$	500	500	500	500	mA
I_{scp} Short circ. peak current		3.5	3.5	3.5	3.5	A

ELECTRICAL CHARACTERISTICS L2000C (continued)

OUTPUT VOLTAGE		12			15			18			24			Unit
INPUT VOLTAGE (Unless otherwise specified)		19			23			26			33			
Parameter	Test conditions	Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	
V _o Output voltage		11.5	12	12.5	14.4	15	15.6	17.1	18	18.9	23	24	25	V
	I _o = 1A	11.4	12	12.6 (V _i = 14.5V)	14.25	15	15.75 (V _i = 17.5V)	17	18	19 (V _i = 20.5V)	22.8	24	25.2 (V _i = 27V)	
ΔV _o Line regulation		240 (V _i = 14.5 to 30V)			300 (V _i = 17.5 to 30V)			360 (V _i = 20.5 to 30V)			480 (V _i = 27 to 38V)			mV
		120 (V _i = 16 to 22V)			150 (V _i = 20 to 26V)			180 (V _i = 22 to 28V)			240 (V _i = 30 to 36V)			
ΔV _o Load regulation	I _o = 20 mA to 2A	240			300			360			480			mV
I _d Quiescent current		8			8			8			8			mA
ΔI _d Quiescent current change	I _o = 20 mA to 1A	0.5			0.5			0.5			0.5			mA
	I _o = 20 mA	1.0 (V _i = 14.5 to 30V)			1.0 (V _i = 17.5 to 30V)			1.0 (V _i = 20.5 to 30V)			1.0 (V _i = 27 to 38V)			
$\frac{\Delta V_o}{\Delta T}$ Output voltage drift	I _o = 5mA T _{amb} = 0 to 70°C	-1			-1			-1			-1.5			mV/°C
e _N Output noise voltage	B = 10Hz to 100KHz	75			90			110			170			μV
SVR Supply voltage rejection	f = 120 Hz	47			46			43			42			dB
V _i Operating input voltage	I _o ≤ 1.5A	15			18			21			27			V
R _o Output resistance	f = 1 KHz	18			19			22			28			mΩ
I _{sc} Short circuit current	V _i = 27V	500			500			500			500			mA
I _{scp} Short circ. peak current		3.5			3.5			3.5			3.5			A

L 2600 Series

LINEAR INTEGRATED CIRCUITS

PRELIMINARY DATA

POSITIVE VOLTAGE REGULATORS FOR AUTOMOTIVE APPLICATIONS

- OUTPUT VOLTAGE OF 5, 8.5 AND 10V
- OUTPUT CURRENT UP TO 500 mA
- NO EXTERNAL COMPONENTS
- LOW DROP-OUT VOLTAGE
- LOAD DUMP VOLTAGE SURGE PROTECTION
- REVERSE VOLTAGE PROTECTION
- SHORT CIRCUIT PROTECTION
- CURRENT LIMITING
- THERMAL SHUTDOWN

The L2600 series of three terminal positive regulators is specially design to stabilize power supplies for car instrumentation in vehicles with 12V battery. They can supply an output current up to 500 mA.

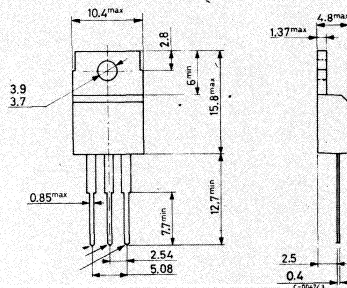
ABSOLUTE MAXIMUM RATINGS

V_i	DC input voltage	35	V
V_i	DC input reverse voltage	-28	V
V_d	Positive transient peak voltage (t = 40 ms, duty cycle = 1%)	120	V
V_d	Negative transient peak voltage (t = 30 ms, duty cycle = 1%)	-90	V
T_{op}	Operating temperature	-55 to 150	°C
T_{stg}	Storage temperature	-65 to 150	°C
P_{tot}	Power dissipation	Internally limited	

ORDERING NUMBERS: L2605V ($V_o = 5V$)
 L2685V ($V_o = 8.5V$)
 L2610V ($V_o = 10V$)

MECHANICAL DATA

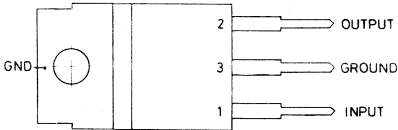
Dimensions in mm



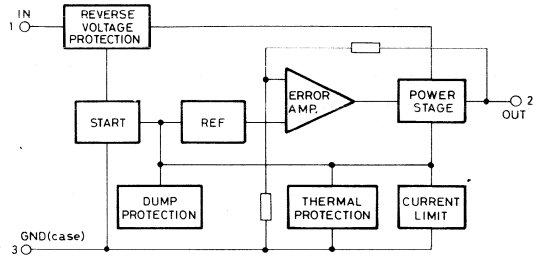
L 2600 Series

CONNECTION AND BLOCK DIAGRAMS

(top view)



S-2568/1



S-4005

THERMAL DATA

$R_{thj-case}$	Thermal resistance junction-case	max.	4 °C/W
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ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^\circ$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_o Output voltage	$I_o = 500\text{ mA}$ $V_i = 12\text{ to }16\text{ V (L2605)}$ $V_i = 12\text{ to }16\text{ V (L2685)}$ $V_i = 12\text{ to }16\text{ V (L2610)}$	4.8 8.15 9.55	5 8.5 10	5.2 8.85 10.45	V
V_i Operating input voltage	see note (°)			28	V
ΔV_o Line regulation	$I_o = 50\text{ mA}$ $V_i = 12\text{ to }16\text{ V}$		2		mV
$\frac{\Delta V_o}{V_o}$ Load regulation	$V_i = 14\text{ V}$ $I_o = 50\text{ to }500\text{ mA}$		0.3		%
ΔV_{i-o} Dropout voltage	$I_o = 500\text{ mA}$			1.8	V
$\frac{\Delta V_o}{\Delta T}$ Output voltage drift	$I_o = 50\text{ mA}$ $V_i = 14\text{ V}$ $T_{amb} = -12\text{ to }80^\circ\text{C}$		-1		mV/°C
I_{sc} Output short circuit current	$V_i = 14\text{ V}$		900		mA
SVR Supply voltage rejection	$V_i = 16\text{ V}$ $\Delta V_i = 2\text{ V}$ $f = 100\text{ Hz}$ $I_o = 500\text{ mA}$		60		dB
R_o Output resistance	$I_o = 500\text{ mA}$		0.05		Ω
e_N Output noise voltage	BW = 100Hz to 10KHz		20		μV

(°) Note: For a DC input voltage $28\text{ V} < V_i < 35\text{ V}$ the device is not operating

3-TERMINAL POSITIVE VOLTAGE REGULATORS

- OUTPUT CURRENT UP TO 1.5A
- OUTPUT VOLTAGES OF 5; 7.5; 9; 10; 12; 15; 18; 24V
- THERMAL OVERLOAD PROTECTION
- SHORT CIRCUIT PROTECTION
- OUTPUT TRANSISTOR SOA PROTECTION

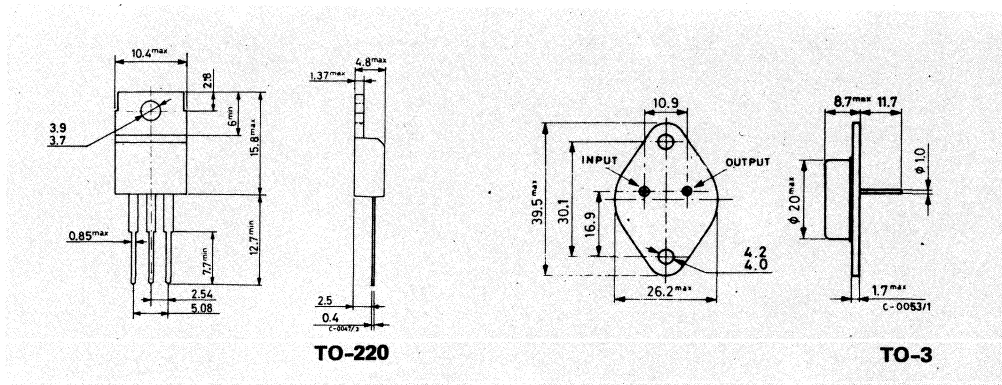
The L7800 series of three-terminal positive regulators is available in TO-220 and TO-3 packages and with several fixed output voltages, making it useful in a wide range of applications. These regulators can provide local on-card regulation, eliminating the distribution problems associated with single point regulation. Each type employs internal current limiting, thermal shut-down and safe area protection, making it essentially indestructible. If adequate heat sinking is provided, they can deliver over 1.5A output current. Although designed primarily as fixed voltage regulators, these devices can be used with external components to obtain adjustable voltages and currents.

ABSOLUTE MAXIMUM RATINGS

V_i	DC input voltage (for $V_o = 5$ to 18V) (for $V_o = 24V$)	35 V 40 V
I_o	Output current	internally limited
P_{tot}	Power dissipation	Internally limited
T_{stg}	Storage temperature	-65 to +150 °C
T_{op}	Operating junction temperature (for L7800) (for L7800C)	-55 to +150 °C 0 to +150 °C

MECHANICAL DATA

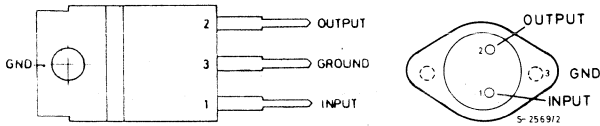
Dimensions in mm



L 7800 Series

CONNECTION DIAGRAMS AND ORDERING NUMBERS

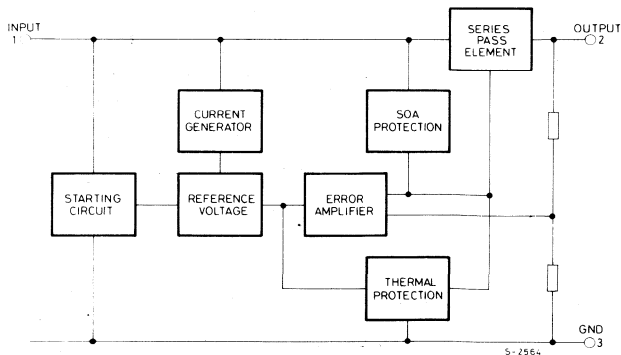
(top views)



S-2568/1

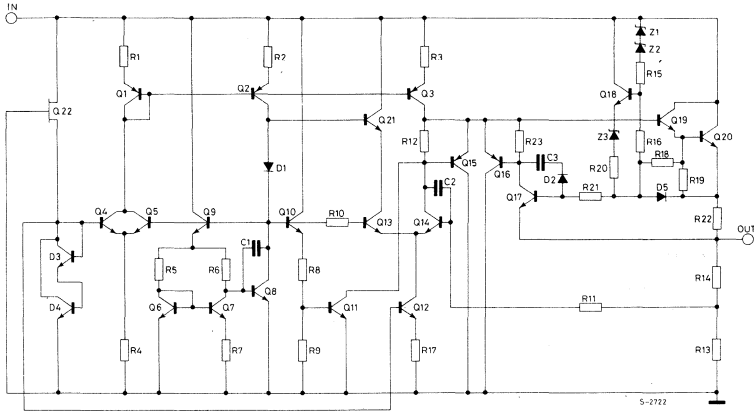
Type	TO-220	TO-3	Output voltage
L 7805	—	L 7805T	5V
L 7805C	L 7805CV	L 7805CT	5V
L 7875	—	L 7875T	7.5V
L 7875C	L 7875CV	L 7875CT	7.5V
L 7809	—	L 7809T	9V
L 7809C	L 7809CV	L 7809CT	9V
L 7810	—	L 7810T	10V
L 7810C	L 7810CV	L 7810CT	10V
L 7812	—	L 7812T	12V
L 7812C	L 7812CV	L 7812CT	12V
L 7815	—	L 7815T	15V
L 7815C	L 7815CV	L 7815CT	15V
L 7818	—	L 7818T	18V
L 7818C	L 7818CV	L 7818CT	18V
L 7824	—	L 7824T	24V
L 7824C	L 7824CV	L 7824CT	24V

BLOCK DIAGRAM



L 7800 Series

SCHEMATIC DIAGRAM



TEST CIRCUITS

Fig. 1 - DC parameters

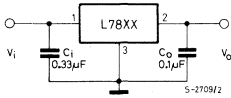


Fig. 2 - Load regulation

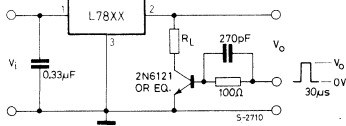
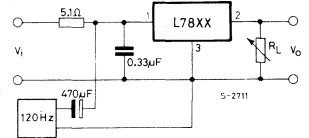


Fig. 3 - Ripple rejection



THERMAL DATA

		TO-220	TO-3
$R_{th\ j-case}$	Thermal resistance junction-case	max 3 °C/W	4 °C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max 50 °C/W	35 °C/W

L7800 Series

ELECTRICAL CHARACTERISTICS L7800 (Refer to the test circuits, $T_j = 25^\circ\text{C}$, $I_o = 500\text{ mA}$ unless otherwise specified)

OUTPUT VOLTAGE		5	7.5	9	10	Unit
INPUT VOLTAGE (Unless otherwise specified)		10	12.5	14	15	
Parameter	Test conditions	Min. Typ. Max.	Min. Typ. Max.	Min. Typ. Max.	Min. Typ. Max.	
V_o Output voltage		4.8 5 5.2	7.15 7.5 7.9	8.65 9 9.35	9.5 10 10.5	V
	$I_o = 1\text{ A}$	4.75 5 5.25 ($V_i = 7\text{V}$)	7.1 7.5 7.95 ($V_i = 9.5\text{V}$)	8.6 9 9.4 ($V_i = 11\text{V}$)	9.4 10 10.6 ($V_i = 12.5\text{V}$)	
ΔV_o Line regulation		50 ($V_i = 7$ to 25V)	60 ($V_i = 9.5$ to 25V)	80 ($V_i = 11$ to 25V)	100 ($V_i = 12.5$ to 30V)	mV
		25 ($V_i = 8$ to 12V)	30 ($V_i = 10.5$ to 20V)	40 ($V_i = 11$ to 20V)	50 ($V_i = 14$ to 22V)	
ΔV_o Load regulation	$I_o = 20\text{ mA}$ to 1.5 A	100	100	100	100	mV
I_d Quiescent current		6	6	6	6	mA
ΔI_d Quiescent current change	$I_o = 20\text{ mA}$ to 1 A	0.5	0.5	0.5	0.5	mA
	$I_o = 20\text{ mA}$	0.8 ($V_i = 8$ to 25V)	0.8 ($V_i = 9.5$ to 25V)	0.8 ($V_i = 11$ to 25V)	0.8 ($V_i = 13$ to 30V)	
$\frac{\Delta V_o}{\Delta T}$ Output voltage drift	$I_o = 5\text{ mA}$ $T_j = -55$ to 150°C	-1.1	-0.8	-1	-1	mV/ $^\circ\text{C}$
e_N Output noise voltage	$B = 10\text{ Hz}$ to 100 KHz	40	52	60	70	μV
SVR Supply voltage rejection	$f = 120\text{ Hz}$	68	62	60	60	dB
V_i Operating input voltage	$I_o \leq 1\text{ A}$	7	9.5	11	12.5	V
R_o Output resistance	$f = 1\text{ KHz}$	17	16	17	17	m Ω
I_{sc} Short circuit current	$V_i = 27\text{V}$	500	500	500	500	mA
I_{scp} Short circ. peak current		3.5	3.5	3.5	3.5	A

L7800 Series

ELECTRICAL CHARACTERISTICS L7800 (continued)

OUTPUT VOLTAGE		12			15			18			24			Unit
INPUT VOLTAGE (Unless otherwise specified)		19			23			26			33			
Parameter	Test conditions	Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	
V_o Output voltage		11.5	12	12.5	14.4	15	15.6	17.1	18	18.9	23	24	25	V
	$I_o = 1A$	11.4	12	12.6 ($V_i = 14.5V$)	14.25	15	15.75 ($V_i = 17.5V$)	17	18	19 ($V_i = 20.5V$)	22.8	24	25.2 ($V_i = 27V$)	
ΔV_o Line regulation				120			150			180			240	mV
				60 ($V_i = 16$ to $22V$)			75 ($V_i = 20$ to $26V$)			90 ($V_i = 22$ to $28V$)			120 ($V_i = 30$ to $36V$)	
ΔV_o Load regulation	$I_o = 20$ mA to $1.5A$			120			150			180			240	mV
I_d Quiescent current				6			6			6			6	mA
ΔI_d Quiescent current change	$I_o = 20$ mA to $1A$			0.5			0.5			0.5			0.5	mA
	$I_o = 20$ mA			0.8 ($V_i = 15$ to $30V$)			0.8 ($V_i = 18.5$ to $30V$)			0.8 ($V_i = 22$ to $33V$)			0.8 ($V_i = 28$ to $38V$)	
$\frac{\Delta V_o}{\Delta T}$ Output voltage drift	$I_o = 5$ mA $T_j = -55$ to $150^\circ C$			-1			-1			-1			-1.5	mV/ $^\circ C$
e_N Output noise voltage	$B = 10$ Hz to 100 KHz			75			90			110			170	μV
SVR Supply voltage rejection	$f = 120$ Hz			60			60			59			56	dB
V_i Operating input voltage	$I_o \leq 1A$			14.5			17.5			20.5			27	V
R_o Output resistance	$f = 1$ KHz			18			19			22			28	m Ω
I_{sc} Short circuit current	$V_i = 27V$			500			500			500			500	mA
I_{scp} Short circ. peak current				3.5			3.5			3.5			3.5	A

L7800 Series

ELECTRICAL CHARACTERISTICS L7800C (Refer to the test circuits, $T_j = 25^\circ\text{C}$, $I_o = 500\text{ mA}$ unless otherwise specified)

OUTPUT VOLTAGE		5	7.5	9	10	Unit
INPUT VOLTAGE (Unless otherwise specified)		10	12.5	14	15	
Parameter	Test conditions	Min. Typ. Max.	Min. Typ. Max.	Min. Typ. Max.	Min. Typ. Max.	
V_o Output voltage		4.8 5 5.2	7.15 7.5 7.9	8.65 9 9.35	9.5 10 10.5	V
	$I_o = 1\text{ A}$	4.75 5 5.25 ($V_i = 7\text{ V}$)	7.1 7.5 7.95 ($V_i = 9.5\text{ V}$)	8.6 9 9.4 ($V_i = 11\text{ V}$)	9.4 10 10.6 ($V_i = 12.5\text{ V}$)	
ΔV_o Line regulation		100 ($V_i = 7$ to 25 V)	120 ($V_i = 9.5$ to 25 V)	130 ($V_i = 11$ to 25 V)	200 ($V_i = 12.5$ to 30 V)	mV
		50 ($V_i = 8$ to 12 V)	60 ($V_i = 10.5$ to 20 V)	65 ($V_i = 11$ to 20 V)	($V_i = 14$ to 22 V)	
ΔV_o Load regulation	$I_o = 20\text{ mA}$ to 1.5 A	100	120	140	200	mV
I_d Quiescent current		8	8	8	8	mA
ΔI_d Quiescent current change	$I_o = 20\text{ mA}$ to 1 A	0.5	0.5	0.5	0.5	mA
	$I_o = 20\text{ mA}$	1.3 ($V_i = 7$ to 25 V)	1.3 ($V_i = 9.5$ to 25 V)	1.3 ($V_i = 11$ to 25 V)	1.0 ($V_i = 12.5$ to 30 V)	
$\frac{\Delta V_o}{\Delta T}$ Output voltage drift	$I_o = 5\text{ mA}$ $T_{\text{amb}} = 0$ to 70°C	-1.1	-0.8	-1	-1	mV/ $^\circ\text{C}$
e_N Output noise voltage	$B = 10\text{ Hz}$ to 100 KHz	40	52	60	65	μV
SVR Supply voltage rejection	$f = 120\text{ Hz}$	62	57	55	55	dB
V_i Operating input voltage	$I_o \leq 1\text{ A}$	7	9.5	11	12.5	V
R_o Output resistance	$f = 1\text{ KHz}$	17	16	17	17	$\text{m}\Omega$
I_{sc} Short circuit current	$V_i = 27\text{ V}$	500	500	500	500	mA
I_{scp} Short circ. peak current		3.5	3.5	3.5	3.5	A

L 7800 Series

ELECTRICAL CHARACTERISTICS L7800C (continued)

OUTPUT VOLTAGE		12			15			18			24			Unit
INPUT VOLTAGE (Unless otherwise specified)		19			23			26			33			
Parameter	Test conditions	Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	
V_o Output voltage		11.5	12	12.5	14.4	15	15.6	17.1	18	18.9	23	24	25	V
	$I_o = 1A$	11.4	12	12.6 ($V_i = 14.5V$)	14.25	15	15.75 ($V_i = 17.5V$)	17	18	19 ($V_i = 20.5V$)	22.8	24	25.2 ($V_i = 27V$)	
ΔV_o Line regulation		240 ($V_i = 14.5$ to $30V$)			300 ($V_i = 17.5$ to $30V$)			360 ($V_i = 20.5$ to $30V$)			480 ($V_i = 27$ to $38V$)			mV
		120 ($V_i = 16$ to $22V$)			150 ($V_i = 20$ to $26V$)			180 ($V_i = 22$ to $28V$)			240 ($V_i = 30$ to $36V$)			
ΔV_o Load regulation	$I_o = 20\text{ mA}$ to $1.5A$	240			300			360			480			mV
I_d Quiescent current		8			8			8			8			mA
ΔI_d Quiescent current change	$I_o = 20\text{ mA}$ to $1A$	0.5			0.5			0.5			0.5			mA
	$I_o = 20\text{ mA}$	1.0 ($V_i = 14.5$ to $30V$)			1.0 ($V_i = 17.5$ to $30V$)			1.0 ($V_i = 20.5$ to $30V$)			1.0 ($V_i = 27$ to $38V$)			
$\frac{\Delta V_o}{\Delta T}$ Output voltage drift	$I_o = 5\text{ mA}$ $T_{amb} = 0$ to 70°C	-1			-1			-1			-1.5			mV/ $^\circ\text{C}$
e_N Output noise voltage	$B = 10\text{ Hz}$ to 100 KHz	75			90			110			170			μV
SVR Supply voltage rejection	$f = 120\text{ Hz}$	55			54			53			50			dB
V_i Operating input voltage	$I_o \leq 1A$	14.5			17.5			20.5			27			V
R_o Output resistance	$f = 1\text{ KHz}$	18			19			22			28			m Ω
I_{sc} Short circuit current	$V_i = 27V$	500			500			500			500			mA
I_{scp} Short circ. peak current		3.5			3.5			3.5			3.5			A

L 7800 Series

Fig. 4 - Dropout voltage vs. junction temperature

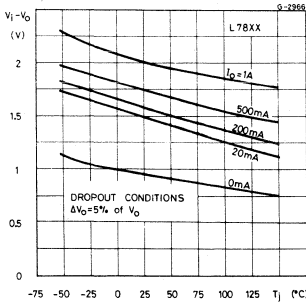


Fig. 5 - Peak output current vs. input/output differential voltage

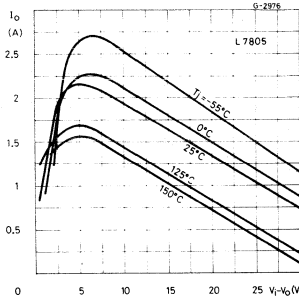


Fig. 6 - Supply voltage rejection vs. frequency

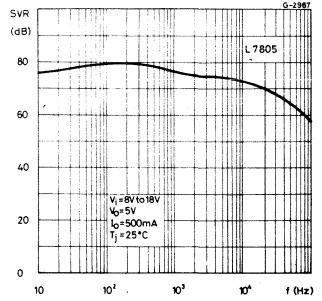


Fig. 7 - Output voltage vs. junction temperature

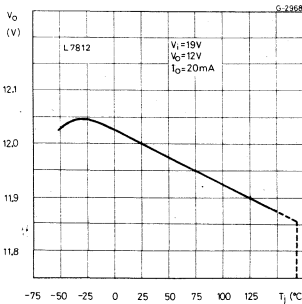


Fig. 8 - Output impedance vs. frequency

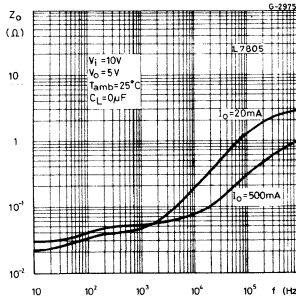


Fig. 9 - Quiescent current vs. junction temperature

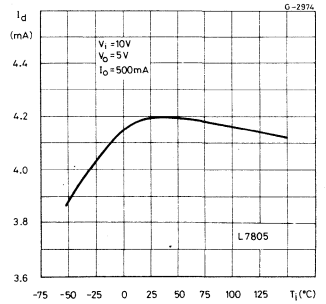


Fig. 10 - Load transient response

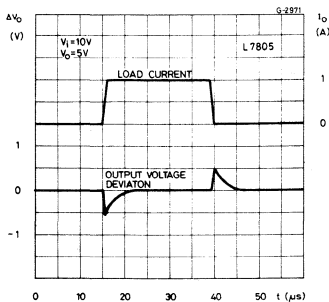


Fig. 11 - Line transient response

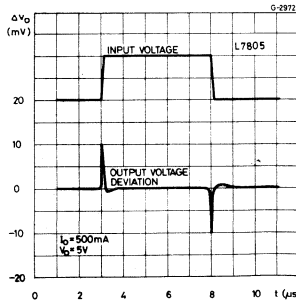
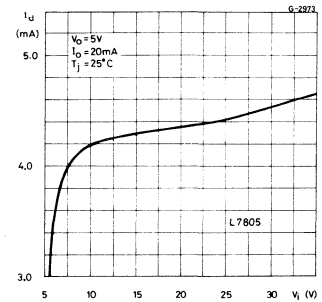


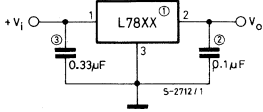
Fig. 12 - Quiescent current vs. input voltage



L7800 Series

APPLICATION INFORMATION (continued)

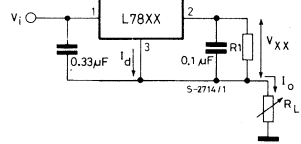
Fig. 13 - Fixed output regulator



Notes:

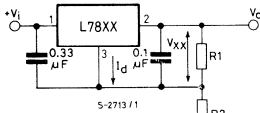
- (1) To specify an output voltage, substitute voltage value for "XX".
- (2) Although no output capacitor is needed for stability, it does improve transient response.
- (3) Required if regulator is located an appreciable distance from power supply filter.

Fig. 14 - Constant current regulator



$$I_o = \frac{V_{XX}}{R_1} + I_d$$

Fig. 15 - Circuit for increasing output voltage



$$I_{R_1} \geq 5 I_d$$

$$V_o = V_{XX} \left(1 + \frac{R_2}{R_1} \right) + I_d R_2$$

Fig. 16 - Adjustable output regulator (7 to 30V)

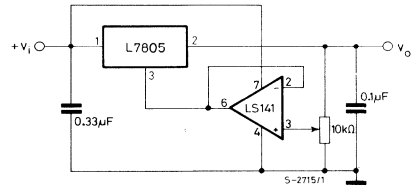
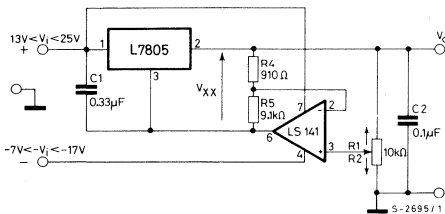
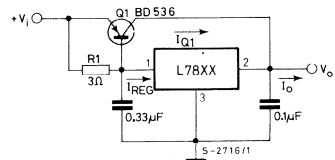


Fig. 17 - 0.5 to 10V regulator



$$V_o = V_{XX} \frac{R_4}{R_1}$$

Fig. 18 - High current voltage regulator

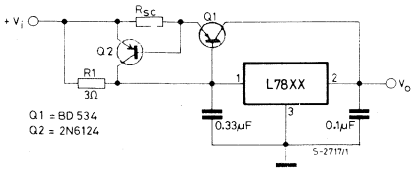


$$R_1 = \frac{V_{BEQ_1}}{I_{REG} - \frac{I_{Q_1}}{\beta_{Q_1}}}$$

$$I_o = I_{REG} + \beta_{Q_1} \left[I_{REG} - \frac{V_{BEQ_1}}{R_1} \right]$$

APPLICATION INFORMATION (continued)

Fig. 19 - High output current with short circuit protection



$$R_{SC} = \frac{V_{BEQ2}}{I_{SC}}$$

Fig. 20 - Tracking voltage regulator

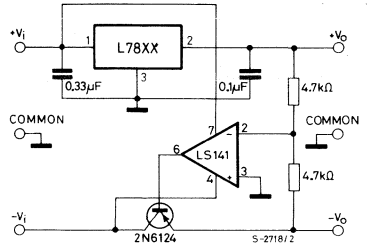
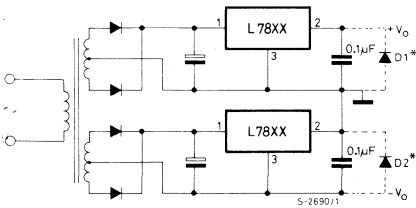


Fig. 21 - Positive and negative regulator



(*) D_1 and D_2 are necessary if the load is connected between $+V_o$ and $-V_o$

Fig. 22 - Negative output voltage circuit

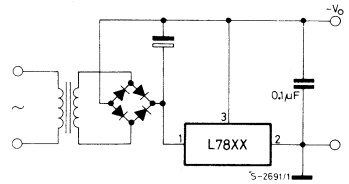


Fig. 23 - Switching regulator

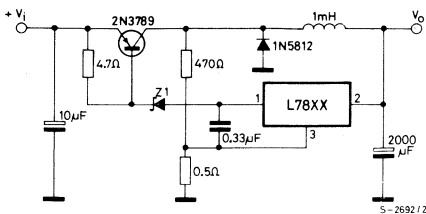
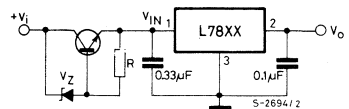


Fig. 24 - High input voltage circuit

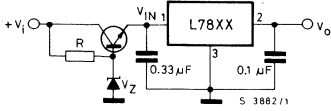


$$V_{IN} = V_i - (V_Z + V_{BE})$$

L7800 Series

APPLICATION INFORMATION (continued)

Fig. 25 - High input voltage circuit



$$V_{IN} = V_Z - V_{BE}$$

Fig. 26 - High output voltage regulator

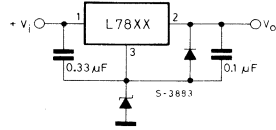
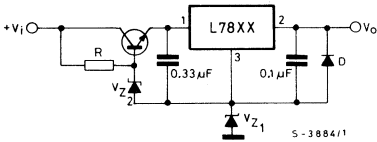
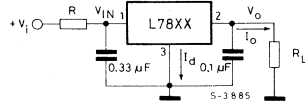


Fig. 27 - High input and output voltage



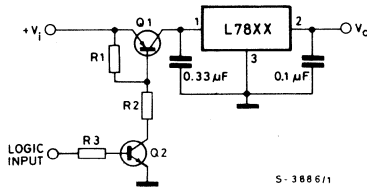
$$V_O = V_{XX} + V_{Z1}$$

Fig. 28 - Reducing power dissipation with dropping resistor



$$R = \frac{V_{i(\min)} - V_{XX} - V_{DROP(\max)}}{I_o(\max) + I_d(\max)}$$

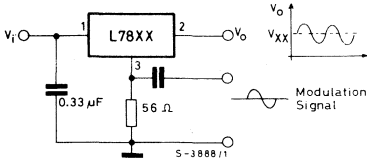
Fig. 29 - Remote shutdown



L7800 Series

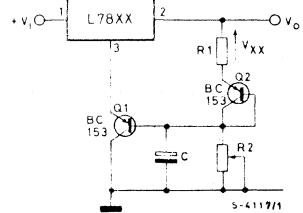
APPLICATION INFORMATION (continued)

Fig. 30 - Power AM modulator (unity voltage gain, $I_o \leq 1.5A$)



Note: The circuit performs well up to 100 KHz.

Fig. 31 - Adjustable output voltage with temperature compensation

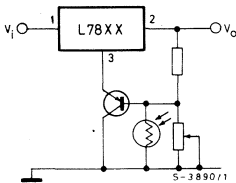


Note: Q_2 is connected as a diode in order to compensate the variation of the Q_1 V_{BE} with the temperature. C allows a slow rise-time of the V_o

$$V_o = V_{XX} \left(1 + \frac{R_2}{R_1} \right) + V_{BE}$$

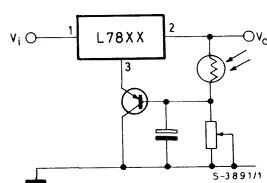
Fig. 32 - Light controllers ($V_o \min = V_{XX} + V_{BE}$)

(a)



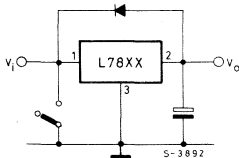
V_o falls when the light goes up

(b)



V_o rises when the light goes up

Fig. 33 - Protection against input short-circuit with high capacitance loads



Applications with high capacitance loads and an output voltage greater than 6 volts need an external diode (see fig. 33) to protect the device against input short circuit. In this case the input voltage falls rapidly while the output voltage decreases slowly. The capacitance discharges by means of the Base-Emitter junction of the series pass transistor in the regulator. If the energy is sufficiently high, the transistor may be destroyed. The external diode by-passes the current from the IC to ground.

L78S00 Series

LINEAR INTEGRATED CIRCUITS

3-TERMINAL POSITIVE VOLTAGE REGULATORS

- OUTPUT CURRENT UP TO 2A
- OUTPUT VOLTAGES OF 5; 7.5; 9; 10; 12; 15; 18; 24V
- THERMAL OVERLOAD PROTECTION
- SHORT CIRCUIT PROTECTION
- OUTPUT TRANSISTOR SOA PROTECTION

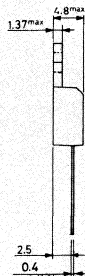
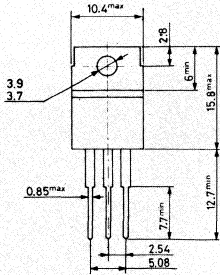
The L78S00 series of three-terminal positive regulators is available in TO-220 and TO-3 packages and with several fixed output voltages, making it useful in a wide range of applications. These regulators can provide local on-card regulation, eliminating the distribution problems associated with single point regulation. Each type employs internal current limiting, thermal shut-down and safe area protection, making it essentially indestructible. If adequate heat sinking is provided, they can deliver over 2A output current. Although designed primarily as fixed voltage regulators, these devices can be used with external components to obtain adjustable voltages and currents.

ABSOLUTE MAXIMUM RATINGS

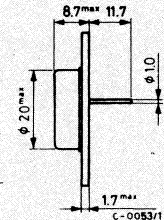
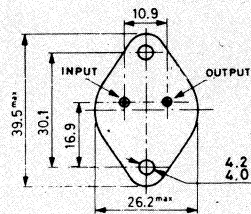
V_i	DC input voltage (for $V_o = 5$ to 18V) (for $V_o = 24V$)	35 V 40 V
I_o	Output current	internally limited
P_{tot}	Power dissipation	Internally limited
T_{stg}	Storage temperature	-65 to +150 °C
T_{op}	Operating junction temperature (for L78S00) (for L78S00C)	-55 to +150 °C 0 to +150 °C

MECHANICAL DATA

Dimensions in mm



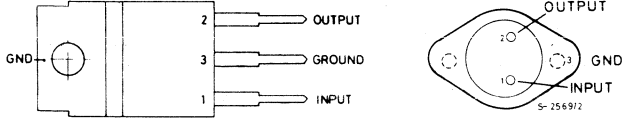
TO-220



TO-3

L 78S00 Series

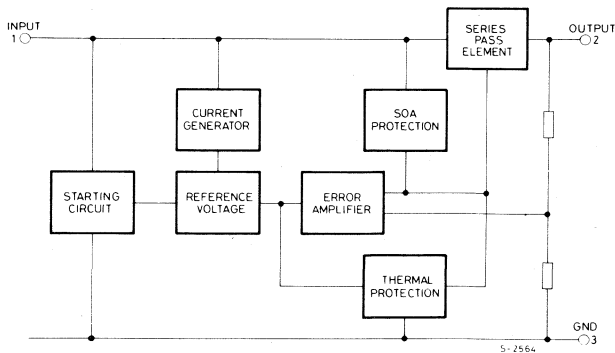
CONNECTION DIAGRAMS AND ORDERING NUMBERS (top views)



5-2568/1

Type	TO-220	TO-3	Output voltage
L 78S05	—	L 78S05T	5V
L 78S05C	L 78S05CV	L 78S05CT	5V
L 78S75	—	L 78S75T	7.5V
L 78S75C	L 78S75CV	L 78S75CT	7.5V
L 78S09	—	L 78S09T	9V
L 78S09C	L 78S09CV	L 78S09CT	9V
L 78S10	—	L 78S10T	10V
L 78S10C	L 78S10CT	L 78S10CT	10V
L 78S12	—	L 78S12T	12V
L 78S12C	L 78S12CV	L 78S12CT	12V
L 78S15	—	L 78S15T	15V
L 78S15C	L 78S15CV	L 78S15CT	15V
L 78S18	—	L 78S18T	18V
L 78S18C	L 78S18CV	L 78S18CT	18V
L 78S24	—	L 78S24T	24V
L 78S24C	L 78S24CV	L 78S24CT	24V

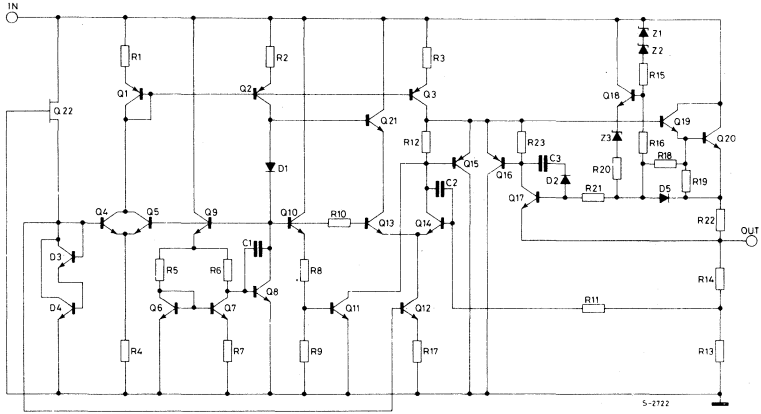
BLOCK DIAGRAM



5-2564

L78S00 Series

SCHEMATIC DIAGRAM



TEST CIRCUITS

Fig. 1 - DC parameters

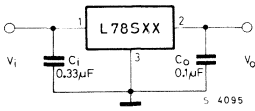


Fig. 2 - Load regulation

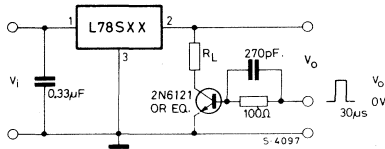
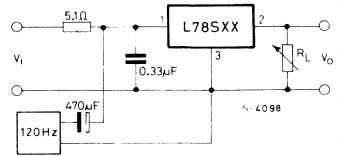


Fig. 3 - Ripple rejection



THERMAL DATA

			TO-220	TO-3
$R_{th\ j-case}$	Thermal resistance junction-case	max	3 °C/W	4 °C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	50 °C/W	35 °C/W

L78S00 Series

ELECTRICAL CHARACTERISTICS L78S00 (Refer to the test circuits, $T_j = 25^\circ\text{C}$, $I_o = 500\text{ mA}$ unless otherwise specified)

OUTPUT VOLTAGE		5	7.5	9	10	Unit
INPUT VOLTAGE (Unless otherwise specified)		10	12.5	14	15	
Parameter	Test conditions	Min. Typ. Max.	Min. Typ. Max.	Min. Typ. Max.	Min. Typ. Max.	
V_o Output voltage		4.8 5 5.2	7.15 7.5 7.9	8.65 9 9.35	9.5 10 10.5	V
	$I_o = 1\text{ A}$	4.75 5 5.25 ($V_i = 7\text{V}$)	7.1 7.5 7.95 ($V_i = 9.5\text{V}$)	8.6 9 9.4 ($V_i = 11\text{V}$)	9.4 10 10.6 ($V_i = 12.5\text{V}$)	
ΔV_o Line regulation		100 ($V_i = 7$ to 25V)	120 ($V_i = 9.5$ to 25V)	130 ($V_i = 11$ to 25V)	200 ($V_i = 12.5$ to 30V)	mV
		50 ($V_i = 8$ to 12V)	60 ($V_i = 10.5$ to 20V)	65 ($V_i = 11$ to 20V)	100 ($V_i = 14$ to 22V)	
ΔV_o Load regulation	$I_o = 20\text{ mA}$ to 2 A	100	120	130	150	mV
I_d Quiescent current		8	8	8	8	mA
ΔI_d Quiescent current change	$I_o = 20\text{ mA}$ to 1 A	0.5	0.5	0.5	0.5	mA
	$I_o = 20\text{ mA}$	1.3 ($V_i = 7$ to 25V)	1.3 ($V_i = 9.5$ to 25V)	1.3 ($V_i = 11$ to 25V)	1 ($V_i = 12.5$ to 30V)	
$\frac{\Delta V_o}{\Delta T}$ Output voltage drift	$I_o = 5\text{ mA}$ $T_j = -55$ to 150°C	-1.1	-0.8	-1	-1	mV/ $^\circ\text{C}$
e_N Output noise voltage	$B = 10\text{ Hz}$ to 100 KHz	40	52	60	65	μV
SVR Supply voltage rejection	$f = 120\text{ Hz}$	60	54	53	53	dB
V_i Operating input voltage	$I_o \leq 1.5\text{ A}$	8	10.5	12	13	V
R_o Output resistance	$f = 1\text{ KHz}$	17	16	17	17	m Ω
I_{sc} Short circuit current	$V_i = 27\text{V}$	500	500	500	500	mA
I_{scp} Short circ. peak current		3.5	3.5	3.5	3.5	A

L78S00 Series

ELECTRICAL CHARACTERISTICS L78S00 (continued)

OUTPUT VOLTAGE		12			15			18			24			Unit
INPUT VOLTAGE (Unless otherwise specified)		19			23			26			33			
Parameter	Test conditions	Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	
V_o Output voltage		11.5	12	12.5	14.4	15	15.6	17.1	18	18.9	23	24	25	V
	$I_o = 1A$	11.4	12	12.6 ($V_i = 14.5V$)	14.25	15	15.75 ($V_i = 17.5V$)	17	18	19 ($V_i = 20.5V$)	22.8	24	25.2 ($V_i = 27V$)	
ΔV_o Line regulation		240 ($V_i = 14.5$ to $30V$)			300 ($V_i = 17.5$ to $30V$)			360 ($V_i = 20.5$ to $30V$)			480 ($V_i = 27$ to $38V$)			mV
		120 ($V_i = 16$ to $22V$)			150 ($V_i = 20$ to $26V$)			180 ($V_i = 22$ to $28V$)			240 ($V_i = 30$ to $36V$)			
ΔV_o Load regulation	$I_o = 20mA$ to $2A$	160			180			200			250			mV
I_d Quiescent current		8			8			8			8			mA
ΔI_d Quiescent current change	$I_o = 20mA$ to $1A$	0.5			0.5			0.5			0.5			mA
	$I_o = 20mA$	1 ($V_i = 14.5$ to $30V$)			1 ($V_i = 17.5$ to $30V$)			1 ($V_i = 22$ to $33V$)			1 ($V_i = 28$ to $38V$)			
$\frac{\Delta V_o}{\Delta T}$ Output voltage drift	$I_o = 5mA$ $T_{amb} = 0$ to $70^\circ C$	-1			-1			-1			-1.5			mV/ $^\circ C$
e_N Output noise voltage	$B = 10Hz$ to $100KHz$	75			90			110			170			μV
SVR Supply voltage rejection	$f = 120Hz$	53			52			49			48			dB
V_i Operating input voltage	$I_o \leq 1.5A$	15			18			21			27			V
R_o Output resistance	$f = 1KHz$	18			19			22			23			m Ω
I_{sc} Short circuit current	$V_i = 27V$	500			500			500			500			mA
I_{scp} Short circ. peak current		3.5			3.5			3.5			3.5			A

L78S00 Series

ELECTRICAL CHARACTERISTICS L78S00C (Refer to the test circuits, $T_j = 25^\circ\text{C}$, $I_o = 500\text{mA}$ unless otherwise specified)

OUTPUT VOLTAGE		5	7.5	9	10	Unit
INPUT VOLTAGE (Unless otherwise specified)		10	12.5	14	15	
Parameter	Test conditions	Min. Typ. Max.	Min. Typ. Max.	Min. Typ. Max.	Min. Typ. Max.	
V_o Output voltage		4.8 5 5.2	7.15 7.5 7.9	8.65 9 9.35	9.5 10 10.5	V
	$I_o = 1\text{A}$	4.75 5 5.25 ($V_i = 7\text{V}$)	7.1 7.5 7.95 ($V_i = 9.5\text{V}$)	8.6 9 9.4 ($V_i = 11\text{V}$)	9.4 10 10.6 ($V_i = 12.5\text{V}$)	
ΔV_o Line regulation		100 ($V_i = 7$ to 25V)	120 ($V_i = 9.5$ to 25V)	130 ($V_i = 11$ to 25V)	200 ($V_i = 12.5$ to 30V)	mV
		50 ($V_i = 8$ to 12V)	60 ($V_i = 10.5$ to 20V)	65 ($V_i = 11$ to 20V)	100 ($V_i = 14$ to 22V)	
ΔV_o Load regulation	$I_o = 20\text{mA}$ to 2A	100	140	170	240	mV
I_d Quiescent current		8	8	8	8	mA
ΔI_d Quiescent current change	$I_o = 20\text{mA}$ to 1A	0.5	0.5	0.5	0.5	mA
	$I_o = 20\text{mA}$	1.3 ($V_i = 7$ to 25V)	1.3 ($V_i = 9.5$ to 25V)	1.3 ($V_i = 11$ to 25V)	1.0 ($V_i = 12.5$ to 30V)	
$\frac{\Delta V_o}{\Delta T}$ Output voltage drift	$I_o = 5\text{mA}$ $T_{\text{amb}} = 0$ to 70°C	-1.1	-0.8	-1	-1	mV/ $^\circ\text{C}$
e_N Output noise voltage	$B = 10\text{Hz}$ to 100KHz	40	52	60	65	μV
SVR Supply voltage rejection	$f = 120\text{Hz}$	54	48	47	47	dB
V_i Operating input voltage	$I_o \leq 1.5\text{A}$	8	10.5	12	13	V
R_o Output resistance	$f = 1\text{KHz}$	17	16	17	17	$\text{m}\Omega$
I_{sc} Short circuit current	$V_i = 27\text{V}$	500	500	500	500	mA
I_{scp} Short circ. peak current		3.5	3.5	3.5	3.5	A

L78S00 Series

ELECTRICAL CHARACTERISTICS L78S00C (continued)

OUTPUT VOLTAGE		12			15			18			24			Unit
INPUT VOLTAGE (Unless otherwise specified)		19			23			26			33			
Parameter	Test conditions	Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	
V_o Output voltage		11.5	12	12.5	14.4	15	15.6	17.1	18	18.9	23	24	25	V
	$I_o = 1A$	11.4	12	12.6 ($V_i = 14.5V$)	14.25	15	15.75 ($V_i = 17.5V$)	17	18	19 ($V_i = 20.5V$)	22.8	24	25.2 ($V_i = 27V$)	
ΔV_o Line regulation		240 ($V_i = 14.5$ to $30V$)			300 ($V_i = 17.5$ to $30V$)			360 ($V_i = 20.5$ to $30V$)			480 ($V_i = 27$ to $38V$)			mV
		120 ($V_i = 16$ to $22V$)			150 ($V_i = 20$ to $26V$)			180 ($V_i = 22$ to $28V$)			240 ($V_i = 30$ to $36V$)			
ΔV_o Load regulation	$I_o = 20mA$ to $2A$	240			300			360			480			mV
I_d Quiescent current		8			8			8			8			mA
ΔI_d Quiescent current change	$I_o = 20mA$ to $1A$	0.5			0.5			0.5			0.5			mA
	$I_o = 20mA$	1.0 ($V_i = 14.5$ to $30V$)			1.0 ($V_i = 17.5$ to $30V$)			1.0 ($V_i = 20.5$ to $30V$)			1.0 ($V_i = 27$ to $38V$)			
$\frac{\Delta V_o}{\Delta T}$ Output voltage drift	$I_o = 5mA$ $T_{amb} = 0$ to $70^\circ C$	-1			-1			-1			-1.5			mV/ $^\circ C$
e_N Output noise voltage	$B = 10Hz$ to $100KHz$	75			90			110			170			μV
SVR Supply voltage rejection	$f = 120Hz$	47			46			43			42			dB
V_i Operating input voltage	$I_o \leq 1.5A$	15			18			21			27			V
R_o Output resistance	$f = 1KHz$	18			19			22			28			m Ω
I_{sc} Short circuit current	$V_i = 27V$	500			500			500			500			mA
I_{scp} Short circ. peak current		3.5			3.5			3.5			3.5			A

L78S00 Series

Fig. 4 - Dropout voltage vs. junction temperature

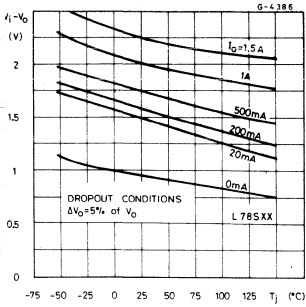


Fig. 5 - Peak output current vs. input/output differential voltage

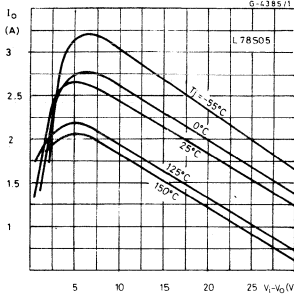


Fig. 6 - Supply voltage rejection vs. frequency

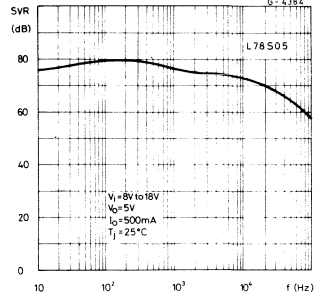


Fig. 7 - Output voltage vs. junction temperature

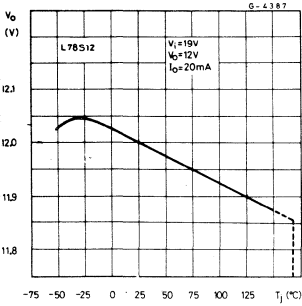


Fig. 8 - Output impedance vs. frequency

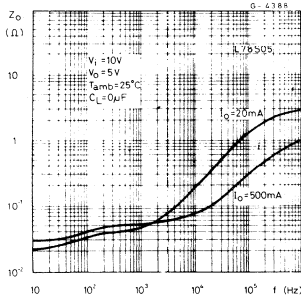


Fig. 9 - Quiescent current vs. junction temperature

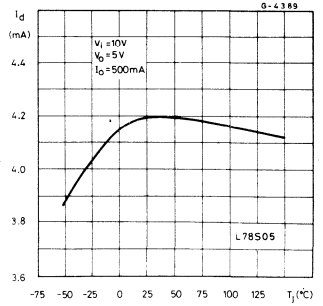


Fig. 10 - Load transient response

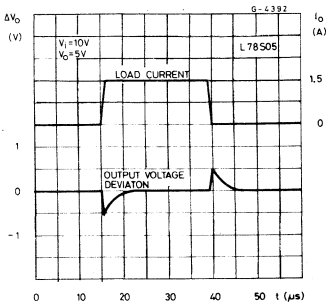


Fig. 11 - Line transient response

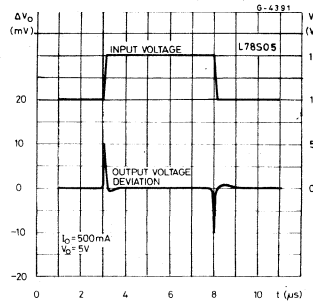
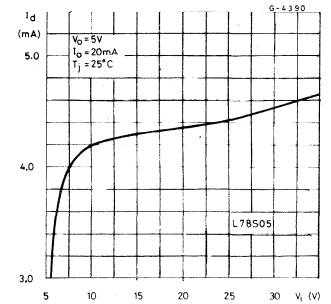


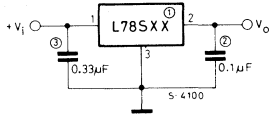
Fig. 12 - Quiescent current vs. input voltage



L78S00 Series

APPLICATION INFORMATION (continued)

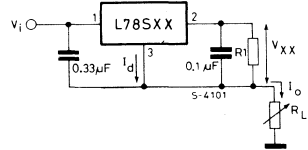
Fig. 13 - Fixed output regulator



Notes:

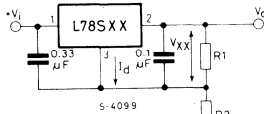
- (1) To specify an output voltage, substitute voltage value for "XX".
- (2) Although no output capacitor is needed for stability, it does improve transient response.
- (3) Required if regulator is located an appreciable distance from power supply filter.

Fig. 14 - Constant current regulator



$$I_o = \frac{V_{XX}}{R_1} + I_d$$

Fig. 15 - Circuit for increasing output voltage



$$I_{R1} \geq 5 I_d$$

$$V_o = V_{XX} \left(1 + \frac{R_2}{R_1} \right) + I_d R_2$$

Fig. 16 - Adjustable output regulator (7 to 30V)

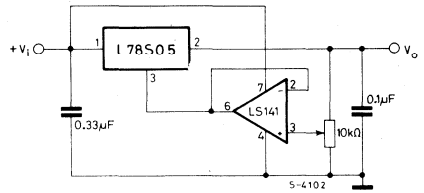
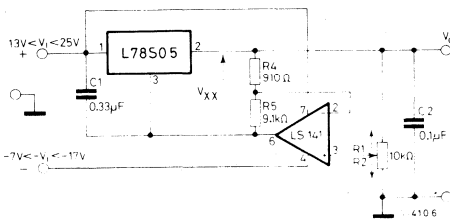
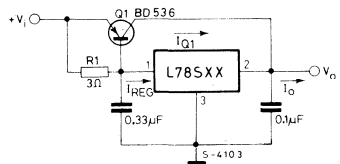


Fig. 17 - 0.5 to 10V regulator



$$V_o = V_{XX} \frac{R_4}{R_1}$$

Fig. 18 - High current voltage regulator



$$R_1 = \frac{V_{BEQ1}}{I_{REG} - \frac{I_{Q1}}{\beta_{Q1}}}$$

$$I_o = I_{REG} + \beta_{Q1} \left[I_{REG} - \frac{V_{BEQ1}}{R_1} \right]$$

L78S00 Series

APPLICATION INFORMATION (continued)

Fig. 19 - High output current with short circuit protection

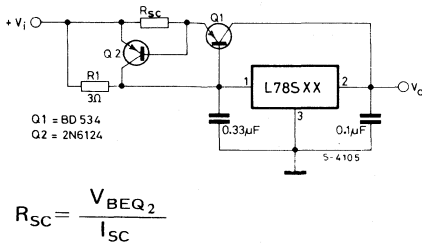
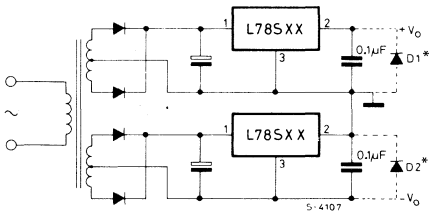


Fig. 21 - Positive and negative regulator



(*)D₁ and D₂ are necessary if the load is connected between +V_O and -V_O

Fig. 23 - Switching regulator

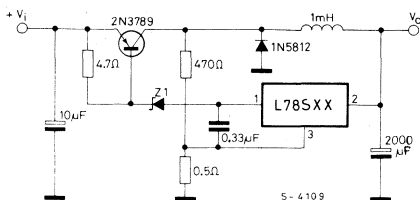


Fig. 20 - Tracking voltage regulator

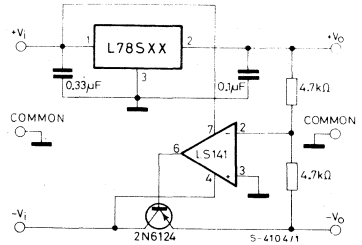


Fig. 22 - Negative output voltage circuit

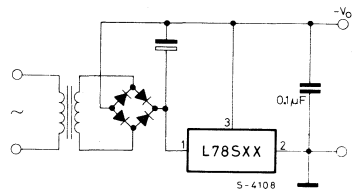
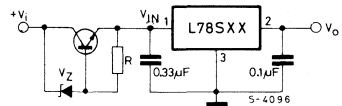


Fig. 24 - High input voltage circuit

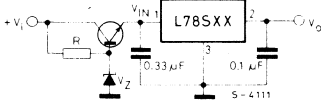


$$V_{IN} = V_i - (V_Z + V_{BE})$$

L78S00 Series

APPLICATION INFORMATION (continued)

Fig. 25 - High input voltage circuit



$$V_{IN} = V_Z - V_{BE}$$

Fig. 26 - High output voltage regulator

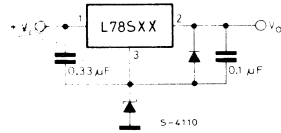
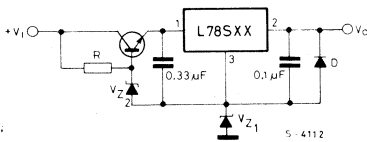
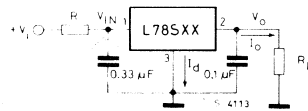


Fig. 27 - High input and output voltage



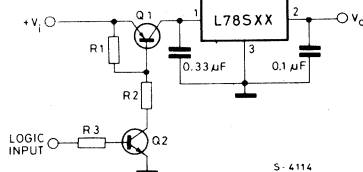
$$V_O = V_{XX} + V_{Z1}$$

Fig. 28 - Reducing power dissipation with dropping resistor



$$R = \frac{V_{i(\min)} - V_{XX} - V_{DROP(\max)}}{I_o(\max) + I_d(\max)}$$

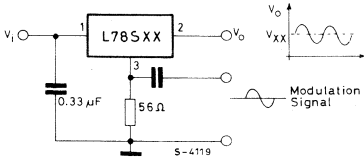
Fig. 29 - Remote shutdown



L78S00 Series

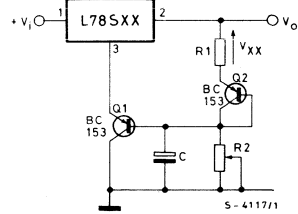
APPLICATION INFORMATION (continued)

Fig. 30 - Power AM modulator oscillator (unity voltage gain, $I_o \leq 1.5A$)



Note: The circuit performs well up to 100 KHz.

Fig. 31 - Adjustable output voltage with temperature compensation

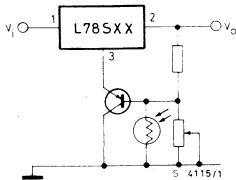


Note: Q₂ is connected as a diode in order to compensate the variation of the Q₁ V_{BE} with the temperature. C allows a slow rise-time of the V_o

$$V_o = V_{XX} \left(1 + \frac{R_2}{R_1} \right) + V_{BE}$$

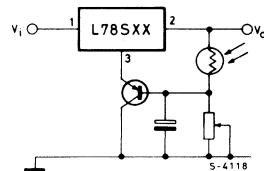
Fig. 32 - Light controllers ($V_o \min = V_{XX} + V_{BE}$)

(a)



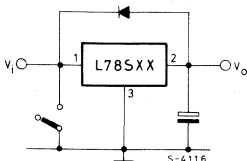
V_o falls when the light goes up

(b)



V_o rises when the light goes up

Fig. 33 - Protection against input short-circuit with high capacitance loads



Applications with high capacitance loads and an output voltage greater than 6 volts need an external diode (see fig. 33) to protect the device against input short circuit. In this case the input voltage falls rapidly while the output voltage decreases slowly. The capacitance discharges by means of the Base-Emitter junction of the series pass transistor in the regulator. If the energy is sufficiently high, the transistor may be destroyed. The external diode by-passes the current from the IC to ground.

LS 025

LINEAR INTEGRATED CIRCUIT

BALANCED MODULATOR

- SINGLE OR DUAL SUPPLY OPERATION
- LOW POWER CONSUMPTION
- LOW CARRIER LEAKAGE
- LOW DISTORTION
- LOW NOISE

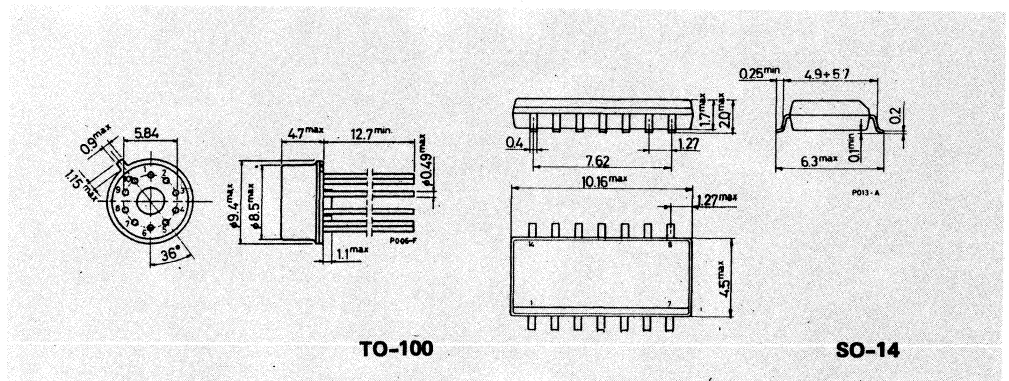
The LS025 is a low noise linear integrated circuit, intended for use as a channel modulator and demodulator in FDM telephone equipments and as analogue AC and DC multiplier in industrial and professional applications. It features low quiescent power consumption, low distortion and intermodulation. It shows a typical carrier leakage better than 85 dB throughout the audio bandwidth. The LS025 is available in TO-100 metal case, while the hermetic gold chip (8000 series) is available in SO-14 (14-lead plastic micropackage). This last version is particularly suitable for professional and telecom applications wherever very high MTBF are required.

ABSOLUTE MAXIMUM RATINGS

		TO-100	μ package
V_s	Supply voltage	30 V	
ΔV_i	Differential input voltage	± 5 V	
T_{op}	Operating temperature	-25 to 85 °C	
P_{tot}	Power dissipation at $T_{amb} = 70$ °C	520 mW	400 mW
T_{stg}	Storage temperature	-65 to 150 °C	-55 to 150 °C

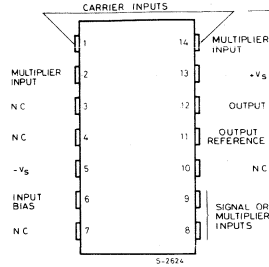
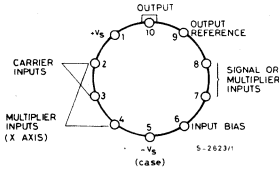
MECHANICAL DATA

Dimensions in mm



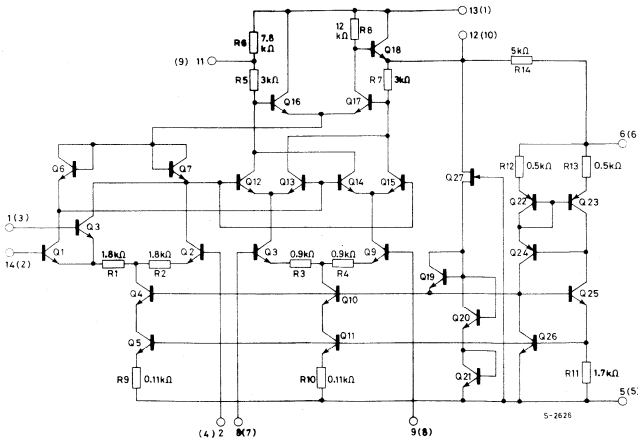
LS 025

CONNECTION DIAGRAMS AND ORDERING NUMBERS (top views)



Type	TO-100	SO-14
LS 025	LS 025T	LS025M
LS 8025		LS 8025M

SCHEMATIC DIAGRAM (The pin numbers refer to the μ package version, while the numbers in brackets refer to the TO-100 version)



THERMAL DATA

		TO-100	SO-14
$R_{th \text{ j-amb}}$	Thermal resistance junction ambient	max	155 °C/W
			200* °C/W

* The thermal resistance is measured with the device mounted on a ceramic substrate (25 x 16 x 0.6 mm).

LS 025

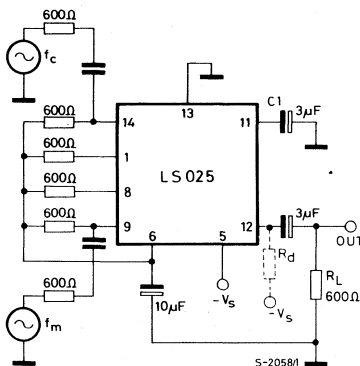
ELECTRICAL CHARACTERISTICS (Referred to the circuit of fig. 1; $T_{amb} = 25^{\circ}\text{C}$ unless otherwise specified. The pins correspond to the μ package version)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s	Supply voltage range	-12		-30	V
I_s	Supply current		2	2.5	mA
I_b	Input bias current	Pins 14-1 Pins 14-2 Pins 8-9	0.7 0.7 1.4	2 2 4	μA μA μA
ΔI	Input offset current	Pins 14-1 Pins 14-2 Pins 8-9	50 70 100		nA nA nA
	Positive input common mode voltage		4.5		V
	Negative input common mode voltage		-8		V
V_o	DC output voltage (pin 12)	-3.2	-3.8	-4.6	V
ΔV_o	Differential output voltage (pins 11-12)		25	100	mV
V_{ref}	Input biasing reference voltage (pin 6)		-7.5		V
R_i	Input resistance	Pins 14-1 Pins 14-2 Pins 8-9	30 300 150		$\text{k}\Omega$ $\text{k}\Omega$ $\text{k}\Omega$
R_o	Output resistance	$f = 1 \text{ kHz}$	3	10	Ω
V_o	Output voltage swing	1	1.3		Vpp
CMR	Common mode rejection	CM signal (pins 14-1) $V = 700 \text{ mVrms}$ $f_1 = 10 \text{ kHz}$ Diff. signal (pins 8-9) $V = 350 \text{ mVrms}$ $f_2 = 40 \text{ kHz}$	98		dB
		CM signal (pins 14-2) $V = 700 \text{ mVrms}$ $f_1 = 10 \text{ kHz}$ Diff. signal (pins 8-9) $V = 350 \text{ mVrms}$ $f_2 = 40 \text{ kHz}$	86		dB
		CM signal (pins 8-9) $V = 350 \text{ mVrms}$ $f_1 = 10 \text{ kHz}$ Diff. signal (pins 14-1) $V = 175 \text{ mVrms}$ $f_2 = 40 \text{ kHz}$	80		dB
SVR	Positive supply voltage rejection	$f = 1 \text{ kHz}$	33		dB
SVR	Negative supply voltage rejection		80		dB

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
K	Scale factor		3.2		V ⁻¹
G _c	Conversion gain	4.5	5	5.5	dB
ΔG _c	Conversion gain change	T _{amb} = 10 to 50°C		± 0.1	dB
	Carrier leakage	V _m = 0		-35	dBv
$\frac{V_{f_m}}{V_{(f_c \pm f_m)}}$	Modulating signal leakage	-35	-50		dBmo
$\frac{V_{(2f_m)}}{V_{(f_c \pm f_m)}}$	2nd harmonic modulating signal leakage		-75		dBmo
$\frac{V_{(f_c \pm 2f_m)}}{V_{(f_c \pm f_m)}}$	2nd harmonic distortion	-60	-75		dBmo
$\frac{V_{2(f_c \pm f_m)}}{V_{(f_c \pm f_m)}}$	2nd harmonic distortion	-55	-80		dBmo
$\frac{V_{(f_c \pm 3f_m)}}{V_{(f_c \pm f_m)}}$	3rd harmonic distortion	-60	-79		dBmo
Low frequency thermal noise	V _m = 0 B = 100 Hz f = 1 kHz	-115	-125		dBv
High frequency thermal noise	V _m = 0 B = 100 Hz f = 30 kHz		-127		dBv

Fig. 1 – Test and application circuit of modulator with single supply voltage



Working conditions

$V_s = -20V$
 $f_c = 130 \text{ kHz}$
 $f_m = 25 \text{ kHz}$
 $V_o = -15 \text{ dBv } (f_c \pm f_m)$
 $V_c = -13 \text{ dBv}$
 $R_L \equiv 600 \Omega$

LS 025

Fig. 2 - Carrier leakage vs. modulation signal input offset

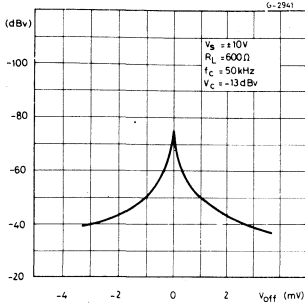


Fig. 3 - Conversion gain vs. frequency

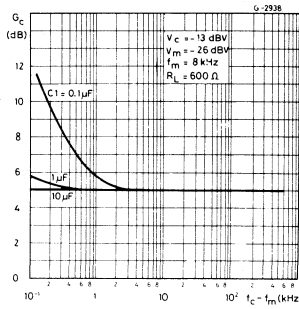


Fig. 4 - Distortion vs. output level

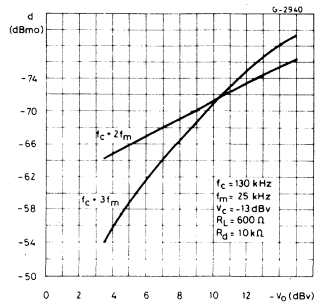


Fig. 5 - Carrier leakage adjustment circuit for system with two supply voltages

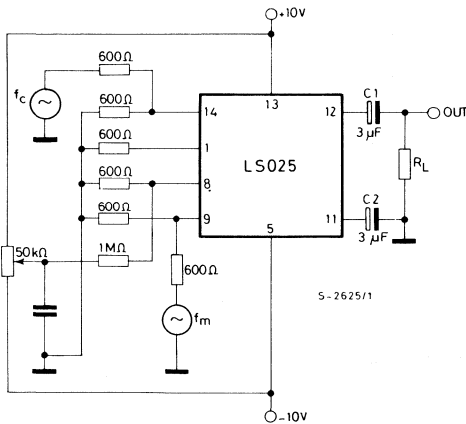
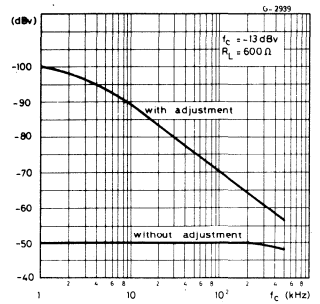
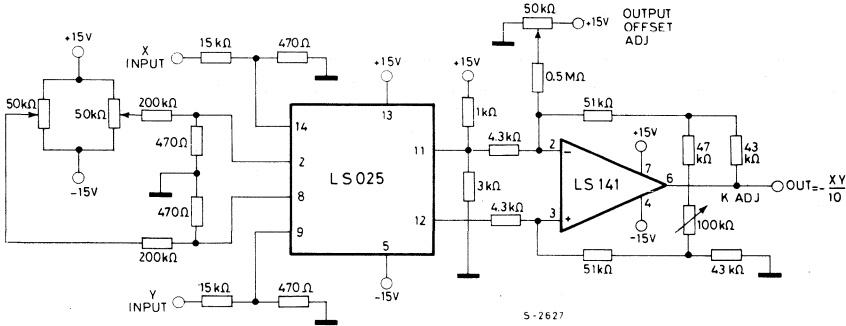


Fig. 6 - Carrier leakage vs. frequency



APPLICATION INFORMATION

Fig. 7 - DC multiplier



Application diagram of DC multiplier, have a scale factor $K = 0.1$. Typical linearity and leakage errors are less than 1%.
The input voltage range is $\pm 10V$.

Definition of units

dBm : power level ($10 \lg \frac{P_2}{P_1}$) is expressed in dBm when P_1 is 1 mW, therefore 0 dBm = 1 mW.

dBm_o : the power is expressed in dBm_o when referred to an established power level in the circuit, generally the output signal level.

e.g.: if the output level is -15 dBm and this level is chosen as reference, then 0 dBm_o = -15 dBm; if another signal, i.e. the distortion measured at the same point of the circuit, is -90 dBm, then the distortion is -75 dBm_o.

dBv : $20 \lg \frac{V_2}{V_1}$ when $V_1 = 775 \text{ mVrms}$.

Definition of terms

Common mode rejection ratio : $CMR = 20 \lg \frac{V_{CM} G}{V_o}$

with G = Conversion gain with specified circuit conditions
 V_{CM} = Common mode signal level
 V_o = Output signal level at frequency = $f_2 \pm f_1$

Scale factor : $K = \frac{V_o}{V_x \cdot V_y}$

with V_x = voltage input (pins 14 - 2)
 V_y = voltage input (pins 8 - 9)

LS 025

APPLICATION INFORMATION (continued)

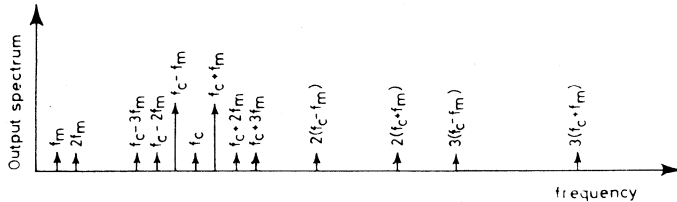
Conversion gain : $G_c = 20 \lg \frac{V_o (f_c \pm f_m)}{V_i (f_m)}$

Carrier leakage : is defined as the output voltage at carrier frequency with only the carrier applied to the input (modulating voltage = 0)

Modulating signal leakage: is defined as the output voltage, at modulating frequency, referred to fundamental carrier sidebands

$$\text{M.S.L.} = 20 \lg \frac{V_o (f_m)}{V_o (f_c \pm f_m)}$$

Output spectrum vs. frequency



- f_c = carrier fundamental (leakage)
- f_m = mod. sig. (leakage)
- nf_m = harmonic modulating signal (leakage)
- $f_c \pm f_m$ = fundamental carrier sidebands
- $f_c \pm nf_m$ = fundamental carrier sideband harmonics
- $n (f_c \pm f_m)$ = carrier harmonic sidebands

LINEAR INTEGRATED CIRCUIT

CHANNEL AMPLIFIER

The LS 045 is a monolithic integrated circuit intended for use as channel amplifier in FDM and PCM telephone equipment. It features low quiescent power consumption, low distortion, high gain. The LS 045 is available in TO-99 metal case, while the hermetic gold chip (8000 series) is available in SO-8 (8-lead plastic micropackage). This last version is particularly suitable for professional and telecom applications wherever very high MTTF are required.

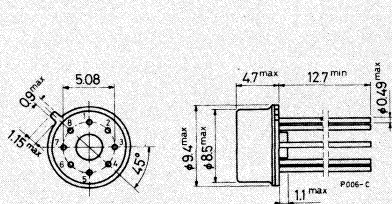
ABSOLUTE MAXIMUM RATINGS

		TO-99	μ package
V_s	Supply voltage	± 18 V	
$V_{i(1)}$	Input voltage	± 12 V	
ΔV_i	Differential input voltage	± 30 V	
T_{op}	Operating temperature	-25 to 85 °C	
	Output short circuit duration (2)	indefinite	
P_{tot}	Power dissipation at $T_{amb} = 70^\circ\text{C}$	520 mW	400 mW
T_{stg}	Storage temperature	-65 to 150 °C	-55 to 150 °C

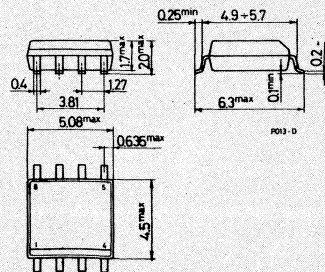
- (1) For supply voltages less than ± 12 V, input voltage is equal to supply voltage.
 (2) The short circuit duration is limited by thermal dissipation.

MECHANICAL DATA

Dimensions in mm



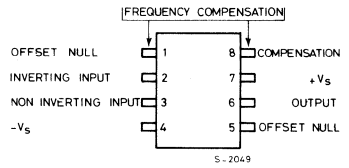
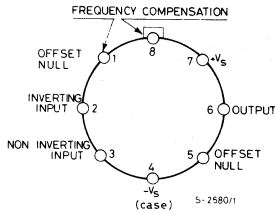
TO-99



SO-8

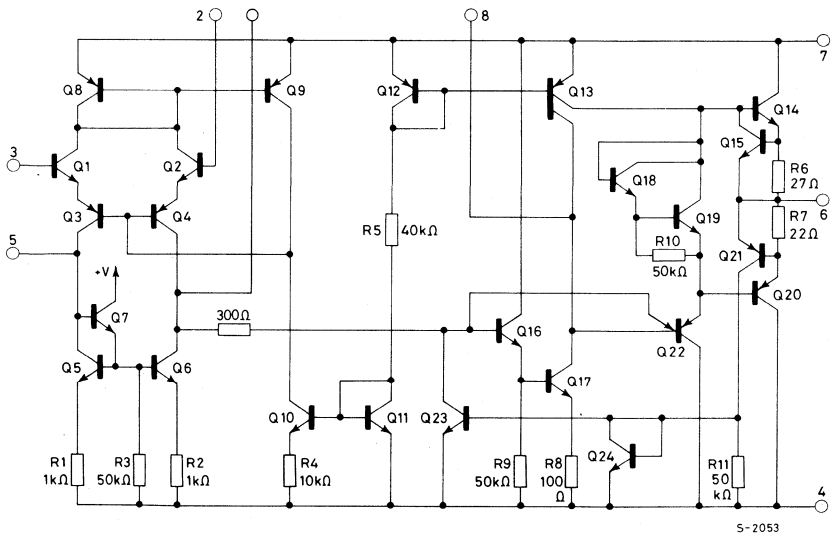
LS 045

CONNECTION DIAGRAMS AND ORDERING NUMBERS (top views)



Type	TO-99	SO-8
LS 045	LS 045T	LS045M
LS 8045		LS 8045M

SCHEMATIC DIAGRAM



THERMAL DATA

		TO-99	SO-8
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	max
		155 °C/W	200* °C/W

* The thermal resistance is measured with the device mounted on a ceramic substrate (25x16x0.6 mm).

ELECTRICAL CHARACTERISTICS ($V_s = -20V$, $V_{bal} = -10V$, $T_{amb} = 25^\circ C$ unless otherwise specified. For V_{bal} see fig. 7)

Parameter		Test conditions	Min.	Typ.	Max.	Unit
V_{OS}	Input offset voltage	$R_g = 10\text{ k}\Omega$		± 1.5	± 10	mV
I_b	Input bias current			100	750	nA
R_i	Input resistance	Open loop		2		M Ω
R_o	Output resistance			75		Ω
G_V	Open loop voltage gain	$R_L = 2\text{ k}\Omega$ $f = 10\text{ Hz}$	83	105		dB
d	Distortion	$f = 1\text{ kHz}$ $G_V = 40\text{ dB}$ $Z_{Leq} = 470\Omega$ $P_o = -5\text{ dBm}$ $P_o = 8\text{ dBm}$		0.15 0.15	0.3 0.3	% %
P_{tot}	Quiescent power dissipation	$P_o = 0$		20	30	mW
P_o	Maximum output power	$d = 1\%$ $Z_{Leq} = 470\Omega$ $G_V = 40\text{ dB}$	14	16		dBm
P_n	Noise power referred to input	$R_g \leq 1.5\text{ k}\Omega$ $f = 1\text{ kHz}$ $G_V = 40\text{ dB}$ $B = 100\text{ Hz}$			-120.5	dBm
SVR	Supply voltage rejection referred to output	$f = 1\text{ kHz}$ $G_V = 40\text{ dB}$	30	36		dB

THE FOLLOWING SPECIFICATION APPLY FOR $T_{amb} = -25$ to $85^\circ C$

V_{OS}	Input offset voltage	$R_g = 10\text{ k}\Omega$			± 15	mV
I_b	Input bias current				1.5	μA
G_V	Open loop voltage gain	$R_L = 2\text{ k}\Omega$	78			dB

Fig. 1 - Quiescent power dissipation vs. ambient temperature

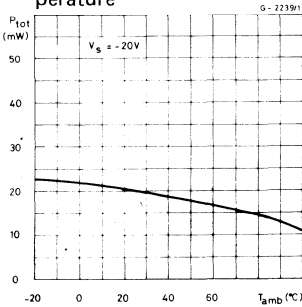


Fig. 2 - Quiescent power dissipation vs. supply voltage

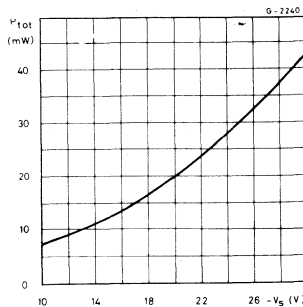
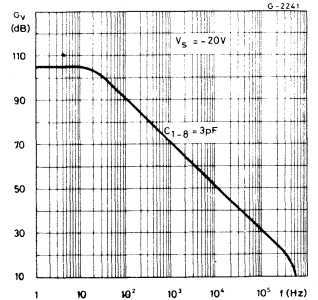


Fig. 3 - Voltage gain (open loop) vs. frequency



LS 045

Fig. 4 - Maximum output power vs. load resistance

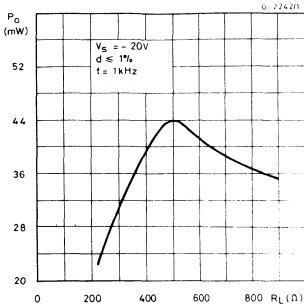


Fig. 5 - Distortion vs. output power

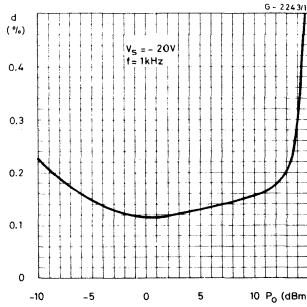
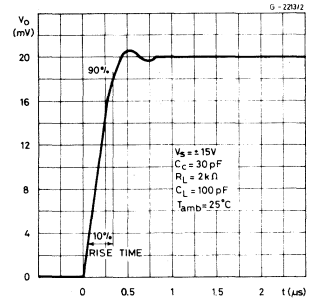


Fig. 6 - Transient response (unity gain)



APPLICATION INFORMATION

Fig. 7 - Channel amplifier circuit

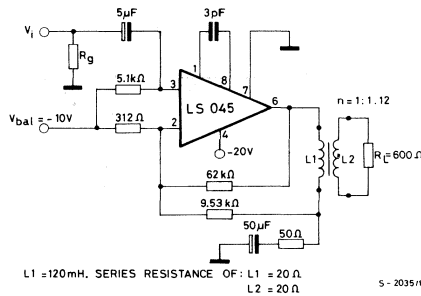


Fig. 8 - Return loss vs. frequency

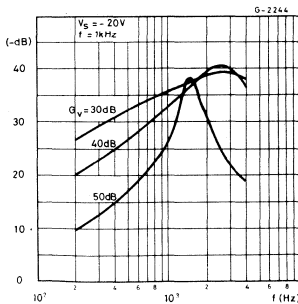
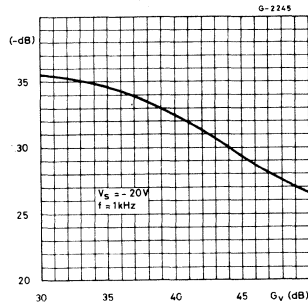


Fig. 9 - Return loss vs. voltage gain



LINEAR INTEGRATED CIRCUITS

HIGH PERFORMANCE OPERATIONAL AMPLIFIERS

- GUARANTEED DRIFT CHARACTERISTICS
- SLEW RATE OF $10V/\mu s$ AS A SUMMING AMPLIFIER
- UNITY GAIN PHASE COMPENSATION WITH A SINGLE 30 pF CAPACITOR
- 3 mV MAX OFFSET VOLTAGE OVER TEMPERATURE RANGE
- 100 nA MAX INPUT BIAS CURRENT OVER TEMPERATURE RANGE

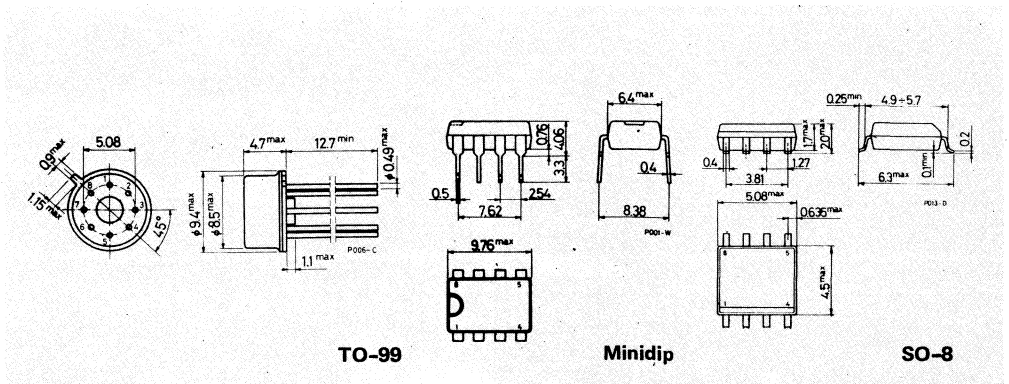
The LS 101 series consists of high performance operational amplifiers, intended for a wide range of analog applications, where tailoring of frequency characteristics is desirable. The LS 101 series is short circuit protected and has the same pin configuration as the LS 141 and LS 148. Absence of latch-up and high common mode voltage range make the LS 101 series ideal for use as voltage followers. In addition, the LS 101 series provides better accuracy and lower noise in high impedance circuitry: the low input current also makes it particularly well suited for long interval integrators, timers, sample and hold circuits and low frequency generators. The LS 101 series is also available with hermetic gold chip (8000 series), particularly suitable for professional and telecom applications, wherever very high MTBF are required.

ABSOLUTE MAXIMUM RATINGS		TO-99	Minidip	μ package
V_s	Supply voltage for LS 101/101A/201/201A for LS 301A		± 22 V ± 18 V	
V_i (1)	Input voltage		± 15 V	
ΔV_i	Differential input voltage		± 30 V	
T_{op}	Operating temperature for LS 101/LS 101A for LS 201A for LS 201/LS 301A		-55 to 125 °C -25 to 85 °C 0 to 70 °C	
	Output short circuit duration (2)		indefinite	
P_{tot}	Power dissipation at $T_{amb} = 70$ °C	520 mW	665 mW	400 mW
T_{stg}	Storage temperature	-65 to 150 °C	-55 to 150 °C	-55 to 150 °C

- (1) For supply voltage less than $\pm 15V$, input voltage is equal to the supply voltage.
 (2) The short circuit duration is limited by thermal dissipation.

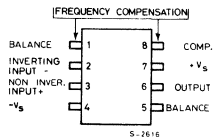
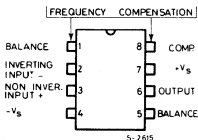
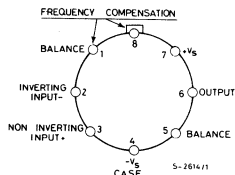
MECHANICAL DATA

Dimensions in mm



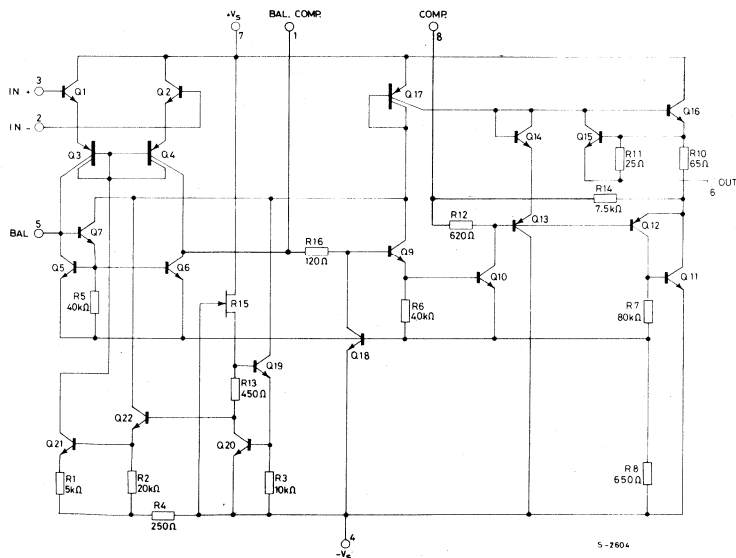
LS 101 LS 201 LS 301

CONNECTION DIAGRAMS AND ORDERING NUMBERS (top views)



Type	TO-99	Minidip	SO-8
LS 101	LS 101T	—	—
LS 101A	LS 101AT	—	—
LS 201	LS 201T	LS 201B	LS 201M
LS 201A	LS 201AT	—	—
LS 301A	LS 301AT	LS 301AB	LS 301AM
LS 8101	—	—	LS 8101M
LS 8101A	—	—	LS 8101AM
LS 8201	—	—	LS 8201M
LS 8201A	—	—	LS 8201AM
LS 8301A	—	—	LS 8301AM

SCHEMATIC DIAGRAM



THERMAL DATA

			TO-99	Minidip	SO-8
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	155 °C/W	120 °C/W	200* °C/W

* Measured with the device mounted on a ceramic substrate (25x16x0.6 mm)

ELECTRICAL CHARACTERISTICS* for LS 101 and LS 201

Parameter	Test conditions	LS 101			LS 201			Unit
		Min.	Typ.	Max.	Min.	Typ.	Max.	
V_{os} Input offset voltage	$R_g \leq 10\ k\Omega$ $R_g \leq 10\ k\Omega$ $T_{amb} = 25^\circ C$		1	6 5		2	10 7.5	mV mV
$\frac{\Delta V_{os}}{\Delta T}$ Average temperat. coefficient of input offset voltage	$R_g \leq 10\ k\Omega$ $R_g \leq 50\ k\Omega$		6 3			10 6		$\mu V/^\circ C$ $\mu V/^\circ C$
I_{os} Input offset current	$T_{amb} = 25^\circ C$ $T_{amb} = T_{max}$ $T_{amb} = T_{min}$		40 10 100	200 200 500		100 50 150	500 400 750	nA nA nA
I_b Input bias current	$T_{amb} = 25^\circ C$		0.12	1.5 0.5		0.25	2 1.5	μA μA
R_i Input resistance	$T_{amb} = 25^\circ C$	0.3	0.8		0.1	0.4		M Ω
V_i Input voltage range	$V_s = \pm 15V$	± 12			± 12			V
G_v Large signal voltage gain	$V_s = \pm 15V$ $V_o = \pm 10V$ $R_L \geq 2\ k\Omega$	88			83			dB
	$V_s = \pm 15V$ $V_o = \pm 10V$ $R_L \geq 2\ k\Omega$ $T_{amb} = 25^\circ C$	94	104		86	103		dB
CMR Common mode rejection	$R_g \leq 10\ k\Omega$	70	90		65	90		dB
SVR Supply voltage rejection	$R_g \leq 10\ k\Omega$	70	90		70	90		dB
V_o Output voltage swing	$V_s = \pm 15V$ $R_L = 10\ k\Omega$ $R_L = 2\ k\Omega$	± 12 ± 10	± 14 ± 13		± 12 ± 10	± 14 ± 13		V V
	$V_s \pm 20V$		1.8	3		1.8	3	mA

* These specifications, unless otherwise specified, apply for $C_1 = 30\ pF$, $V_s = \pm 5$ to $\pm 20V$ and $T_{amb} = -55$ to $125^\circ C$ (LS 101/LS 101A), $T_{amb} = -25$ to $85^\circ C$ (LS 201A) and $T_{amb} = 0$ to $70^\circ C$ (LS 201); $V_s = \pm 5$ to $\pm 15V$ and $T_{amb} = 0$ to $70^\circ C$ (LS 301A).

LS 101 LS 201 LS 301

ELECTRICAL CHARACTERISTICS* for LS 101A, LS 201A and LS 301A

Parameter	Test conditions	LS 101A/LS 201A			LS 301A			Unit
		Min.	Typ.	Max.	Min.	Typ.	Max.	
V_{OS} Input offset voltage	$R_g \leq 50 \text{ k}\Omega$ $R_g \leq 50 \text{ k}\Omega$ $T_{amb} = 25^\circ\text{C}$		0.7	3 2		2	10 7.5	mV mV
$\frac{\Delta V_{OS}}{\Delta T}$ Average temperat. coefficient of input offset voltage	$R_g \leq 50 \text{ k}\Omega$		3	15		6	30	$\mu\text{V}/^\circ\text{C}$
I_{OS} Input offset current	$T_{amb} = 25^\circ\text{C}$		1.5	20 10		3	70 50	nA nA
$\frac{\Delta I_{OS}}{\Delta T}$ Average temperat. coefficient of input offset current	$T_{amb} = 25^\circ\text{C}$ to T_{max} $T_{amb} = T_{min}$ to 25°C		0.01 0.02	0.1 0.2		0.01 0.02	0.3 0.6	nA/ $^\circ\text{C}$ nA/ $^\circ\text{C}$
I_b Input bias current	$T_{amb} = 25^\circ\text{C}$		30	0.1 75		70	0.3 250	μA nA
R_i Input resistance	$T_{amb} = 25^\circ\text{C}$	1.5	4		0.5	2		M Ω
V_i Input voltage range	$V_s = \pm 20\text{V}$ $V_s = \pm 15\text{V}$	± 15			± 12			V V
G_v Large signal voltage gain	$V_s = \pm 15\text{V}$ $V_o = \pm 10\text{V}$ $R_L \geq 2 \text{ k}\Omega$	88			83			dB
	$V_s = \pm 15\text{V}$ $V_o = \pm 10\text{V}$ $R_L \geq 2 \text{ k}\Omega$ $T_{amb} = 25^\circ\text{C}$	94	104		86	104		dB
CMR Common mode rejection	$R_g \leq 50 \text{ k}\Omega$	80	96		70	90		dB
SVR Supply voltage rejection	$R_g \leq 50 \text{ k}\Omega$	80	96		70	96		dB
V_o Output voltage swing	$V_s = \pm 15\text{V}$ $R_L = 10 \text{ k}\Omega$ $R_L = 2 \text{ k}\Omega$	± 12 ± 10	± 14 ± 13		± 12 ± 10	± 14 ± 13		V V
I_s Supply current	$V_s = \pm 20\text{V}$ $T_{amb} = T_{max}$ $T_{amb} = 25^\circ\text{C}$		1.2	2.5				μA
	$V_s = \pm 20\text{V}$ $V_s = \pm 15\text{V}$		1.8	3		1.8	3	mA mA

* These specifications, unless otherwise specified, apply for $C_1 = 30 \text{ pF}$, $V_s = \pm 5$ to $\pm 20\text{V}$ and $T_{amb} = -55$ to 125°C (LS 101/LS 101A), $T_{amb} = -25$ to 85°C (LS 201A) and $T_{amb} = 0$ to 70°C (LS 201); $V_s = \pm 5$ to $\pm 15\text{V}$ and $T_{amb} = 0$ to 70°C (LS 301A).

Guaranteed characteristics (LS 101/LS 201)

Fig. 1 - Input voltage range vs. supply voltage

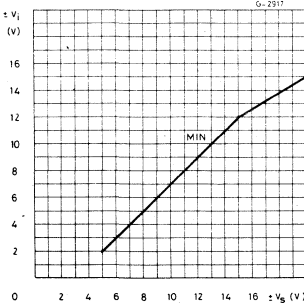


Fig. 2 - Output voltage swing vs. supply voltage

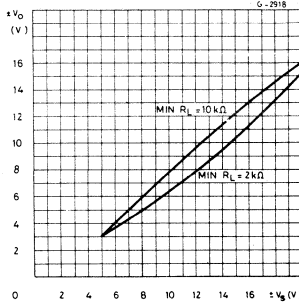
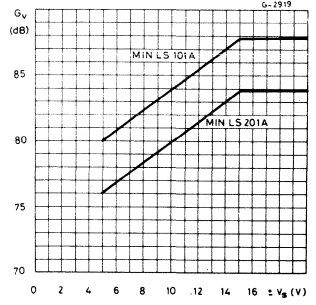


Fig. 3 - Voltage gain vs. supply voltage



Guaranteed characteristics (LS 101A/LS 201A)

Fig. 4 - Input voltage range vs. supply voltage

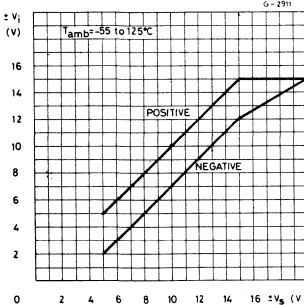


Fig. 5 - Output voltage swing vs. supply voltage

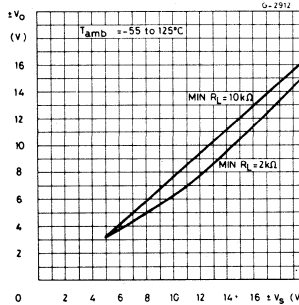
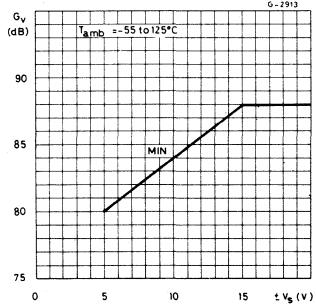


Fig. 6 - Voltage gain vs. supply voltage



Guaranteed characteristics (LS 301A)

Fig. 7 - Input voltage range vs. supply voltage

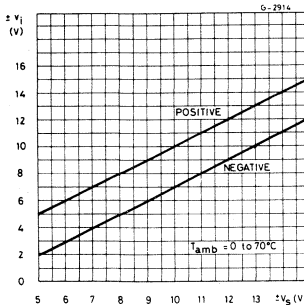


Fig. 8 - Output voltage swing vs. supply voltage

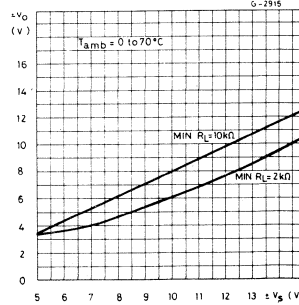
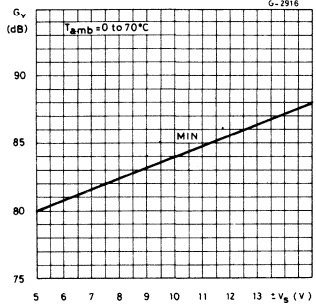


Fig. 9 - Voltage gain vs. supply voltage



LS 101 LS 201 LS 301

Fig. 10 - Input bias current vs. ambient temperature (for LS 101A/201A/301A)

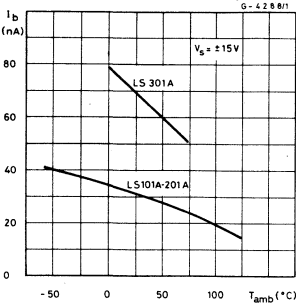


Fig. 11 - Input offset current vs. ambient temperature (for LS 101A/201A/301A)

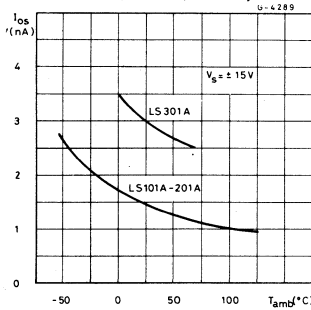


Fig. 12 - Input bias current vs. ambient temperature (for LS 101/201)

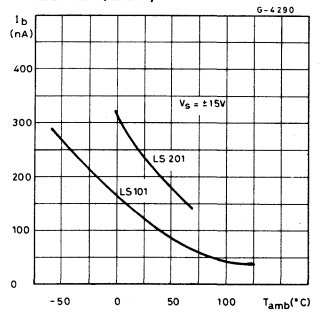


Fig. 13 - Input offset current vs. ambient temperature (for LS 101/201)

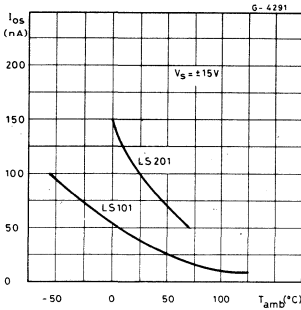


Fig. 14 - Supply current vs. supply voltage

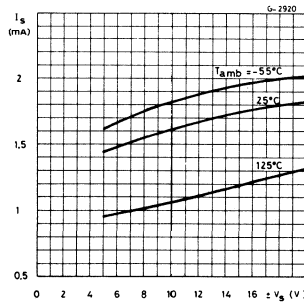


Fig. 15 - Voltage gain vs. supply voltage

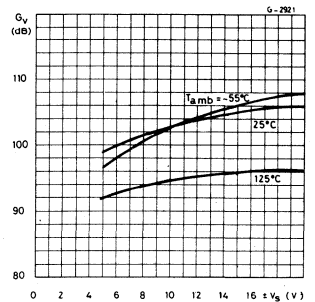


Fig. 16 - Output voltage swing vs. output current

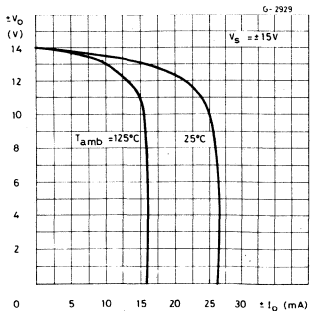


Fig. 17 - Input noise voltage vs. frequency

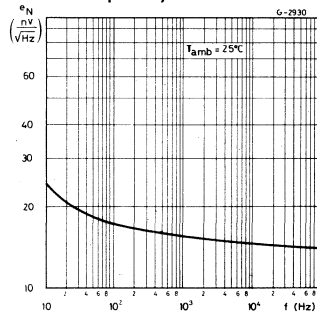
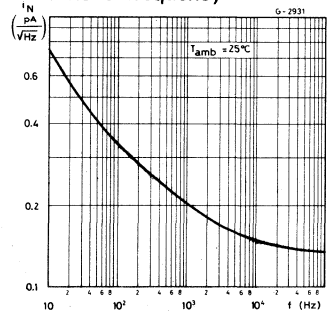


Fig. 18 - Input noise current vs. frequency



OPERATIONAL AMPLIFIER COMPENSATION

SINGLE POLE

Fig. 19

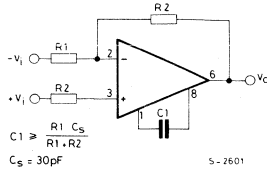


Fig. 20 - Open loop frequency response

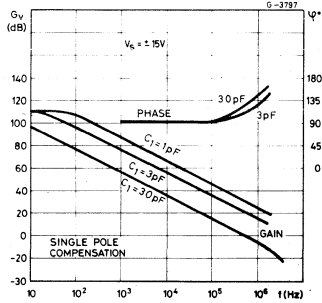
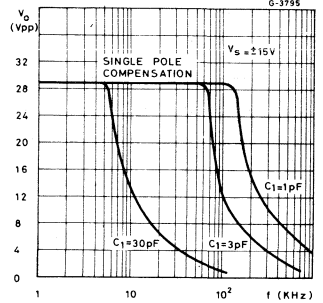


Fig. 21 - Large signal frequency response



TWO POLE

Fig. 22

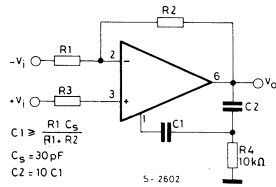


Fig. 23 - Open loop frequency response

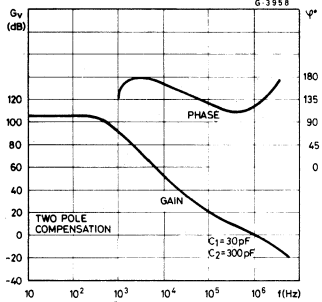
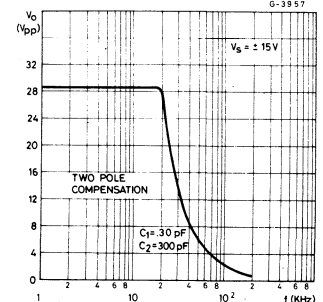


Fig. 24 - Large signal frequency response



FEED FORWARD

Fig. 25

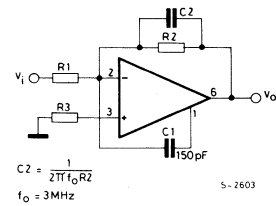


Fig. 26 - Open loop frequency response

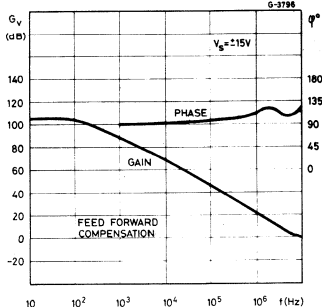
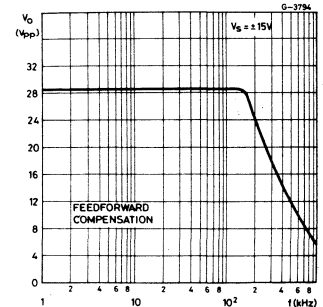


Fig. 27 - Large signal frequency response



LS 101 LS 201 LS 301

Fig. 28 - Single pole compensation pulse response

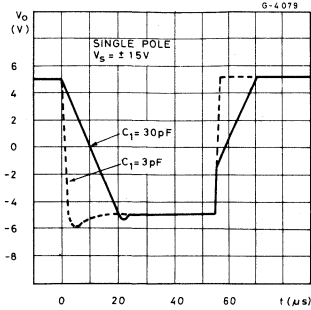


Fig. 29 - Two pole compensation pulse response

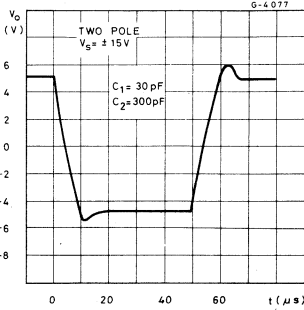
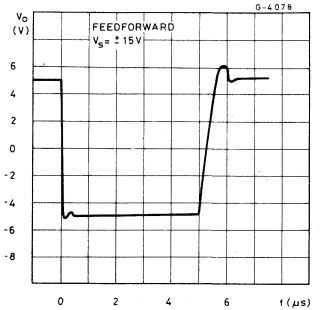


Fig. 30 - Feed forward pulse response



TYPICAL APPLICATIONS

Fig. 31 - Inverting amplifier with balancing circuit

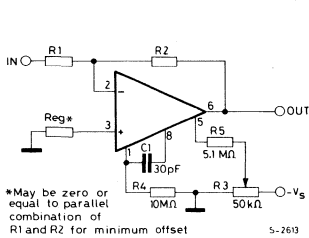


Fig. 32 - Integrator with bias current compensation

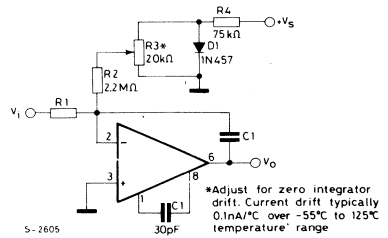


Fig. 33 - Standard compensation and offset balancing circuit

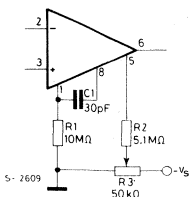
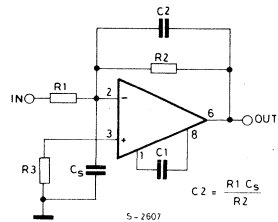


Fig. 34 - Compensation for stray input capacitances or large feedback resistor



TYPICAL APPLICATIONS (continued)

Fig. 35 - Protecting against gross fault conditions

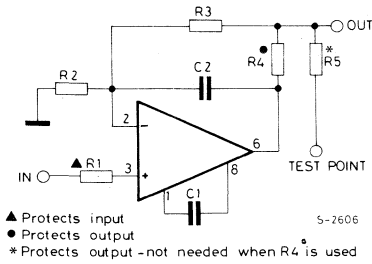


Fig. 36 - Bilateral current source

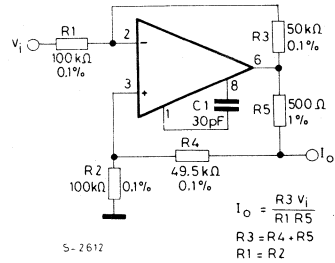
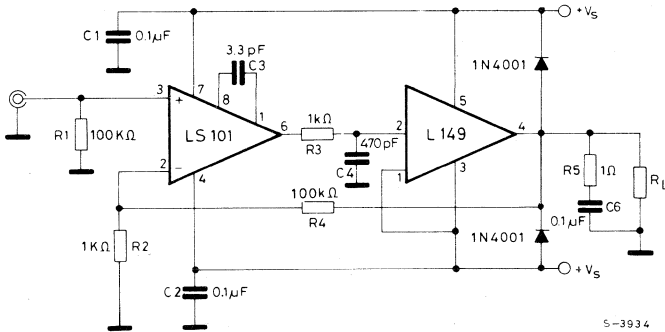
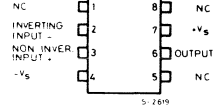
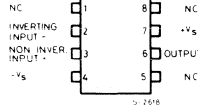
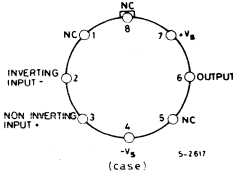


Fig. 37 - Power operational amplifier



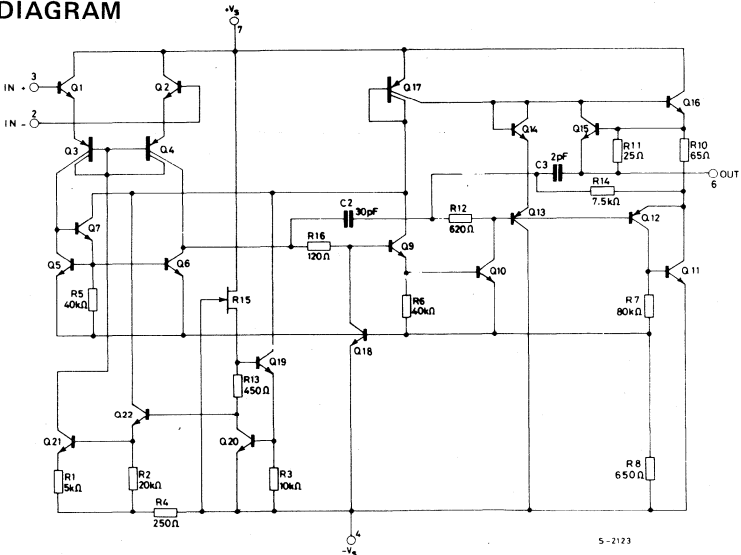
LS 107 LS 207 LS 307

CONNECTION DIAGRAMS AND ORDERING NUMBERS (top views)



Type	TO-99	Minidip	SO-8
LS 107	LS 107T	—	—
LS 207	LS 207T	—	—
LS 307	LS 307T	LS 307B	LS 307M
LS 8107	—	—	LS 8107M
LS 8207	—	—	LS 8207M
LS 8307	—	—	LS 8307M

SCHEMATIC DIAGRAM



THERMAL DATA

	TO-99	Minidip	SO-8	
$R_{th j-amb}$ Thermal resistance junction-ambient	max	155 °C/W	120 °C/W	200 °C/W

* Measured with the device mounted on a ceramic substrate (25x16x0.6 mm)

LS 107 LS 207 LS 307

ELECTRICAL CHARACTERISTICS (see note)

Parameter	Test conditions	LS 107/LS 207			LS 307			Unit	
		Min.	Typ.	Max.	Min.	Typ.	Max.		
V_{os}	Input offset voltage	$R_g \leq 50 \text{ k}\Omega$ $R_g \leq 50 \text{ k}\Omega$	$T_{amb} = 25^\circ\text{C}$		3 0.7	2	10 7.5	mV mV	
$\frac{\Delta V_{os}}{\Delta T}$	Average temperature coefficient of input offset voltage				3	15	6	30	$\mu\text{V}/^\circ\text{C}$
I_{os}	Input offset current		$T_{amb} = 25^\circ\text{C}$		1.5	20 10	3	70 50	nA nA
$\frac{\Delta I_{os}}{\Delta T}$	Average temperature coefficient of input offset current		$T_{amb} = 25^\circ\text{C}$ to T_{max} $T_{amb} = T_{min}$ to 25°C		0.01 0.02	0.1 0.2	0.01 0.02	0.3 0.6	$\text{nA}/^\circ\text{C}$ $\text{nA}/^\circ\text{C}$
I_b	Input bias current		$T_{amb} = 25^\circ\text{C}$		30	100 75	70	300 250	nA nA
R_i	Input resistance		$T_{amb} = 25^\circ\text{C}$	1.5	4		0.5	2	$\text{M}\Omega$
G_v	Large signal voltage gain	$V_s = \pm 15\text{V}$ $R_L \geq 2 \text{ k}\Omega$	$V_o = \pm 10\text{V}$						
		$V_s = \pm 15\text{V}$ $R_L \geq 2 \text{ k}\Omega$	$V_o = \pm 10\text{V}$ $T_{amb} = 25^\circ\text{C}$	88			84		
				94	104		88	104	dB
V_i	Input voltage range	$V_s = \pm 20\text{V}$ $V_s = \pm 15\text{V}$		± 15			± 12		V V
V_o	Output voltage swing	$V_s = \pm 15\text{V}$	$R_L = 10 \text{ k}\Omega$	± 12	± 14		± 12	± 14	V V
		$V_s = \pm 15\text{V}$	$R_L = 2 \text{ k}\Omega$	± 10	± 13		± 10	± 13	
CMR	Common mode rejection	$R_g \leq 50 \text{ k}\Omega$		80	96		70	90	dB
SVR	Supply voltage rejection	$R_g \leq 50 \text{ k}\Omega$		80	96		70	96	dB
I_s	Supply current	$V_s = \pm 20\text{V}$ $T_{amb} = 25^\circ\text{C}$			1.8	3			mA mA
		$V_s = \pm 15\text{V}$ $T_{amb} = 25^\circ\text{C}$			1.2	2.5		1.8	3

Note: These specifications, unless otherwise specified, apply for $V_s = \pm 5\text{V}$ to $\pm 20\text{V}$ and $T_{amb} = -55$ to 125°C for LS 107; $V_s = \pm 5\text{V}$ to $\pm 20\text{V}$ and $T_{amb} = -25$ to 85°C for LS 207; $V_s = \pm 5\text{V}$ to $\pm 15\text{V}$ and $T_{amb} = 0$ to 70°C for LS 307.

Fig. 1 - Supply current vs. supply voltage

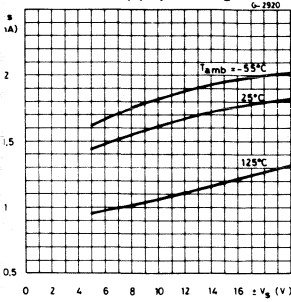


Fig. 2 - Voltage gain vs. supply voltage

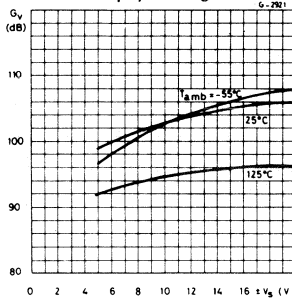


Fig. 3 - Input current vs. ambient temp.

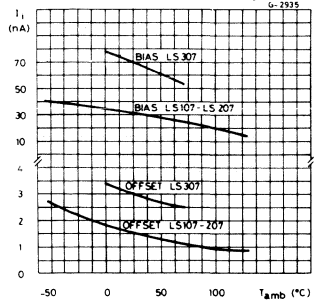


Fig. 4 - Current limiting vs. output current

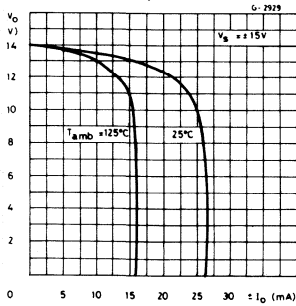


Fig. 5 - Input noise voltage vs. frequency

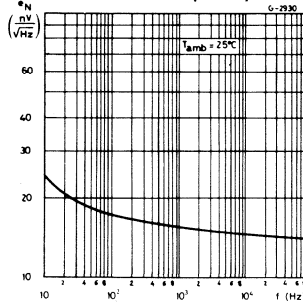


Fig. 6 - Input noise current vs. frequency

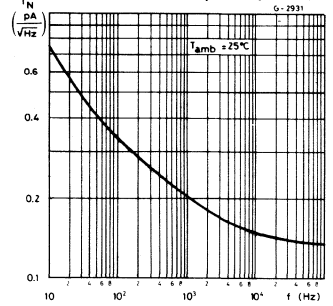


Fig. 7 - Open loop frequency response

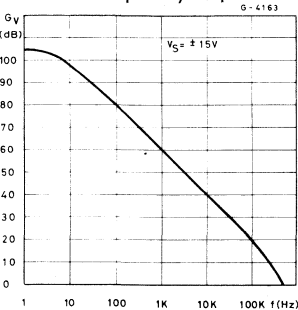


Fig. 8 - Large signal frequency response

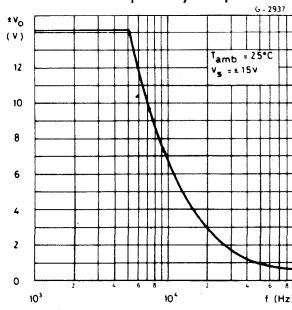
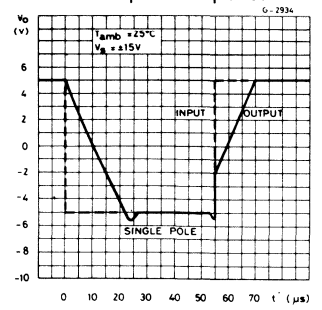


Fig. 9 - Voltage follower pulse response



LS 107 LS 207 LS 307

Guaranteed performance characteristics (LS 107/LS 207)

Fig. 10 - Input voltage range vs. supply voltage

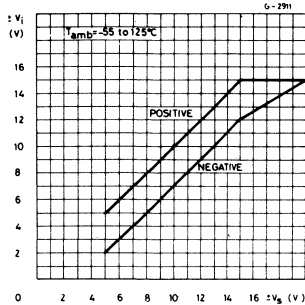


Fig. 11 - Output voltage swing vs. supply voltage

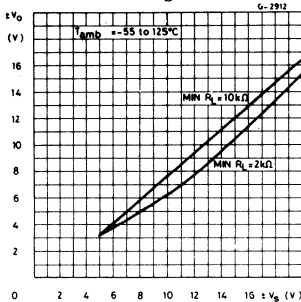
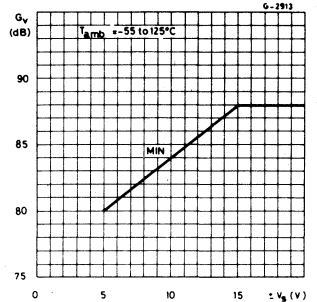


Fig. 12 - Voltage gain vs. supply voltage



Guaranteed performance characteristics (LS 307)

Fig. 13 - Input voltage range vs. supply voltage

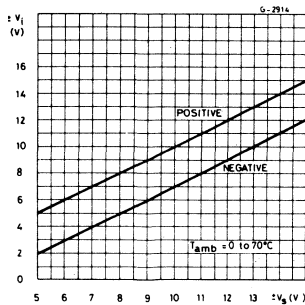


Fig. 14 - Output voltage swing vs. supply voltage

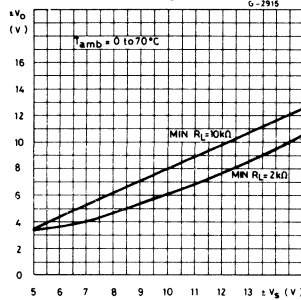
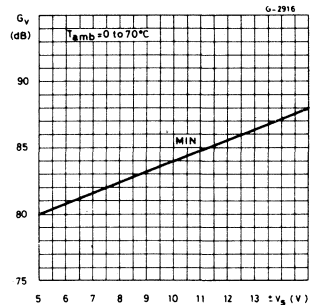


Fig. 15 - Voltage gain vs. supply voltage



TYPICAL APPLICATIONS

Fig. 16 - Inverting amplifier

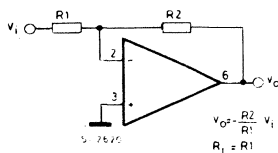


Fig. 17 - Non-inverting AC amplifier

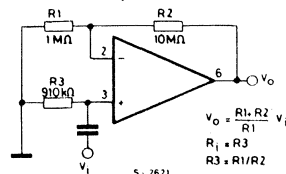
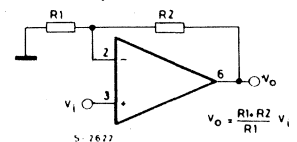


Fig. 18 - Non-inverting amplifier



LINEAR INTEGRATED CIRCUITS

FREQUENCY COMPENSATED OPERATIONAL AMPLIFIERS

- NO FREQUENCY COMPENSATION REQUIRED
- SHORT CIRCUIT PROTECTION
- OFFSET VOLTAGE NULL CAPABILITY
- LARGE COMMON MODE AND DIFFERENTIAL VOLTAGE RANGE
- NO LATCH-UP

The LS 141 series consists of general purpose operational amplifiers, intended for a wide range of analog applications. High common mode voltage range and absence of "latch-up" tendencies make the LS 141 series ideal for use as a voltage follower. The high gain and wide range of operating voltage provide superior performance in integrators, summing amplifiers, and general feedback applications. The LS 141 series is available with hermetic gold chip (8000 series). This is particularly suitable for professional and telecom applications, wherever very high MTBF are required.

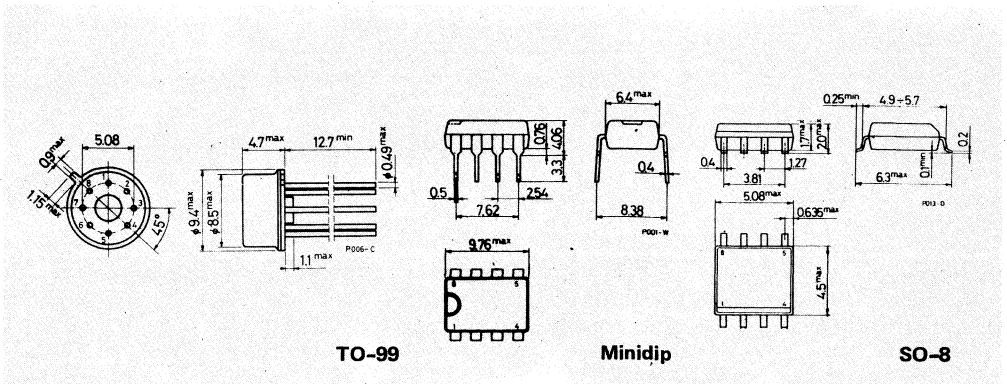
ABSOLUTE MAXIMUM RATINGS

		TO-99	Minidip	μpackage
V_s	Supply voltage for LS 141/LS 141A for LS 141C		± 22V ± 18V ± 15V ± 30V	
V_i (1)	Input voltage			
ΔV_i	Differential input voltage			
T_{op}	Operating temperature for LS 141/LS 141A for LS 141C		-55 to 125°C 0 to 70°C	
	Output short circuit duration(2)		indefinite	
P_{tot}	Power dissipation at $T_{amb} = 70^\circ\text{C}$	520 mW	665 mW	400 mW
T_{stg}	Storage temperature	-65 to 150°C	-55 to 150°C	-55 to 150°C
	Lead soldering temperature	300°C (10s)	260°C (12s)	260°C (5s) 235°C (11s)

- 1) For supply voltage less than ± 15V, input voltage is equal to the supply voltage
- 2) The short circuit duration is limited by thermal dissipation

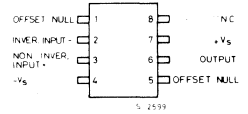
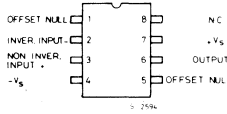
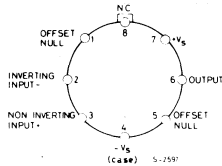
MECHANICAL DATA

Dimensions in mm



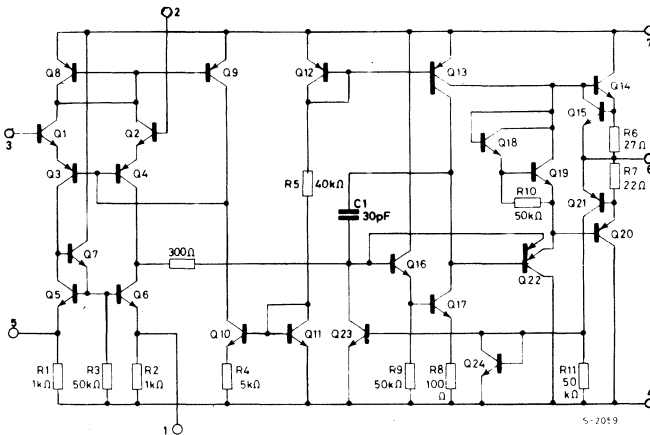
LS141 LS141A LS141C

CONNECTION DIAGRAMS AND ORDERING NUMBERS



Type	TO-99	Minidip	SO-8
LS 141	LS 141T	—	—
LS 141A	LS 141 AT	—	—
LS 141C	LS 141 CT	LS 141 CB	LS 141 CM
LS 8141	—	—	LS 8141M
LS 8141A	—	—	LS 8141 AM
LS 8141C	—	—	LS 8141 CM

SCHEMATIC DIAGRAM



THERMAL DATA

		TO-99	Minidip	SO-8	
$R_{th J-amb}$	Thermal resistance junction ambient	max	155 °C/W	120 °C/W	200* °C/W

* Measured with the device mounted on a ceramic substrate (25 x 16 x 0.6 mm)

ELECTRICAL CHARACTERISTICS (see note)

Parameter	Test conditions	LS 141			LS 141A			LS 141C			Unit
		Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	
V _{os} Input offset voltage	T _{amb} = 25°C R _g ≤ 10 kΩ R _g ≤ 50 Ω		1	5		0.8	3		2	6	mV mV
	T _{amb} = T _{min} to T _{max} R _g ≤ 10 kΩ R _g ≤ 50 Ω			6			4			7.5	mV mV
ΔV _{os} Input offset voltage adjust. range	V _s = ± 20V V _s = ± 15V T _{amb} = 25°C		±15			±10			±15		mV mV
$\frac{\Delta V_{os}}{\Delta T}$ Average input offset voltage drift							15				$\frac{\mu V}{^\circ C}$
I _{os} Input offset current	T _{amb} = 25°C		20	200		3	30		20	200	nA nA
	T _{amb} = T _{min} to T _{max}		85	500			70		300		
$\frac{\Delta I_{os}}{\Delta T}$ Average input offset current drift							0.5				$\frac{nA}{^\circ C}$
I _b Input bias current	T _{amb} = 25°C		80	500		30	80		80	500	nA μA
	T _{amb} = T _{min} to T _{max}			1.5		0.21			0.8		
R _i Input resistance	T _{amb} = 25°C	0.3	2		1	6		0.3	2		MΩ MΩ
	T _{amb} = T _{min} to T _{max}				0.5						
V _i Input voltage range	T _{amb} = T _{min} to T _{max}	±12	±13		±12	±13		±12	±13		V
G _v Large signal voltage gain	T _{amb} = 25°C R _L ≥ 2 kΩ V _s = ±15V V _o = ±10V	94	106		94			86	106		dB
	T _{amb} = T _{min} to T _{max} R _L ≥ 2 kΩ V _s = ±15V V _o = ±10V V _s = ±5V V _o = ±2V	88			90 80			84			dB
V _o Output voltage swing	V _s = ±15V R _L ≥ 10 kΩ R _L ≥ 2 kΩ	±12 ±10	±14 ±13		±12 ±10	±14 ±13		±12 ±10	±14 ±13		V V
	T _{amb} = 25°C T _{amb} = T _{min} to T _{max}		25		10 10	25	35 40		25		mA mA
CMR Common mode rejection	V _s = ±20V R _g ≤ 10 kΩ V _{CM} = ±12V	70	90		80	95		70	90		dB
SVR Supply voltage rejection	R _g ≤ 50Ω V _s = ±5 to ±20V R _g ≤ 10kΩ V _s = ±5 to ±15V	77	96		86	96		77	96		dB dB

LS141 LS141A LS141C

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	LS 141			LS 141A			LS 141C			Unit	
		Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.		
Transient respon. (unity gain) Rise time Overshoot	$T_{amb} = 25^\circ\text{C}$		0.3 5			0.25 6	0.8 20		0.3 5		μs %	
B	Bandwidth	$T_{amb} = 25^\circ\text{C}$			0.437	1.5					MHz	
SR	Slew rate	$T_{amb} = 25^\circ\text{C}$		0.5		0.3	0.7		0.5		V/ μs	
I_s	Supply current	$T_{amb} = 25^\circ\text{C}$		1.7	2.8				1.7	2.8	mA	
P_{tot}	Power consumption	$T_{amb} = 25^\circ\text{C}$ $V_s = \pm 20\text{V}$ $V_s = \pm 15\text{V}$		50	85		80	150		50	85	mW mW
		$V_s = \pm 20\text{V}$ $T_{amb} = T_{min}$ $T_{amb} = T_{max}$						165 135				mW mW
		$V_s = \pm 15\text{V}$ $T_{amb} = T_{min}$ $T_{amb} = T_{max}$		60 45	100 75							mW mW

Note: These specifications, unless otherwise specified, apply for $V_s = \pm 15\text{V}$ and $T_{amb} = -55$ to 125°C for LS 141 and LS 141A. For the LS 141C these specifications apply for $T_{amb} = 0$ to 70°C

Fig. 1 - Open loop voltage gain vs. supply voltage

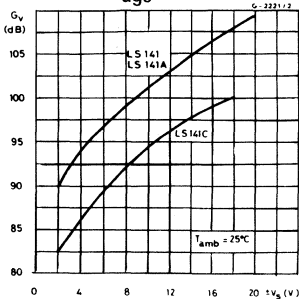


Fig. 2 - Output voltage swing vs. supply voltage

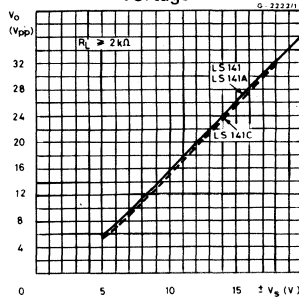


Fig. 3 - Power consumption vs. supply voltage

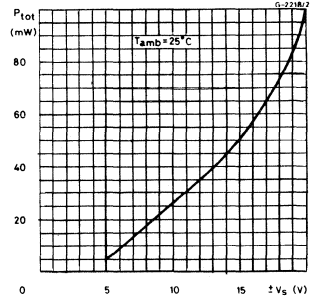


Fig. 4 - Open loop voltage gain vs. frequency

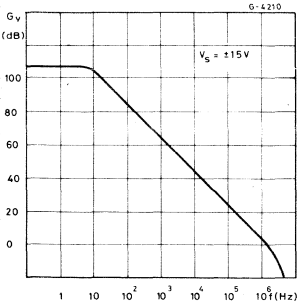


Fig. 5 - Open loop phase response vs. frequency

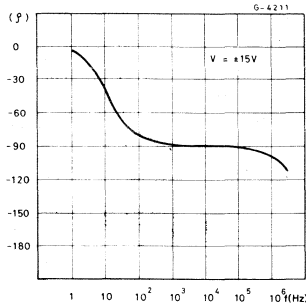


Fig. 6 - Input offset current vs. supply voltage (for LS 141 and LS 141C)

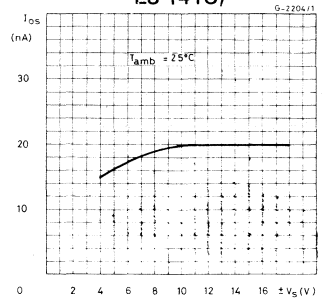


Fig. 7 - Input resistance and capacitance vs. frequency (for LS 141 and LS 141C)

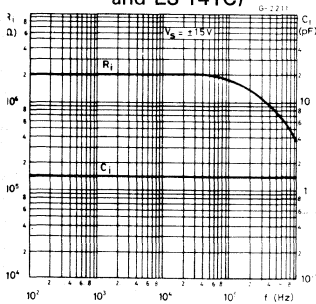


Fig. 8 - Output resistance vs. frequency

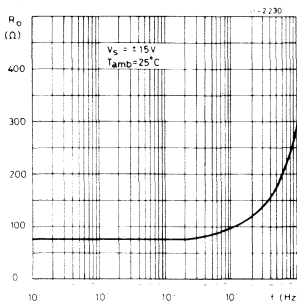


Fig. 9 - Output voltage swing vs. load resistance

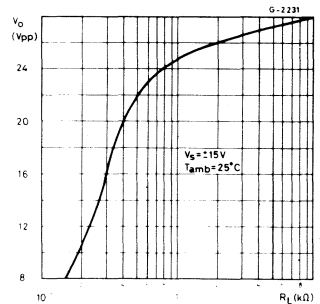


Fig. 10 - Output voltage swing vs. frequency

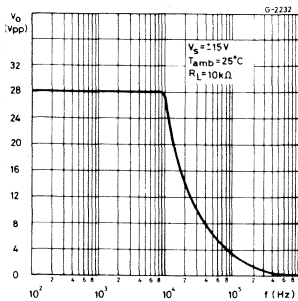


Fig. 11 - Input noise voltage vs. frequency

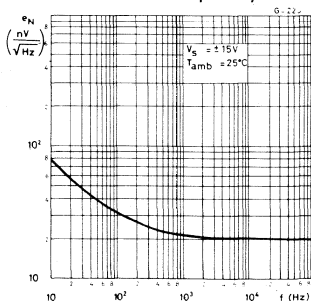
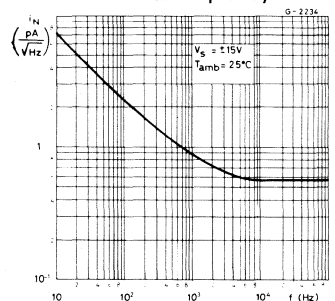


Fig. 12 - Input noise current vs. frequency



LS141 LS141A LS141C

Fig. 13 - Transient response

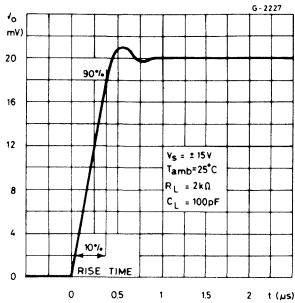


Fig. 14 - Common mode rejection ratio vs. frequency

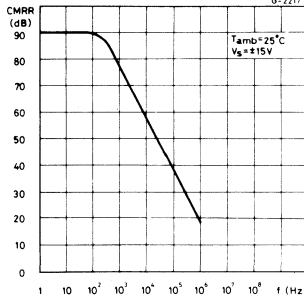
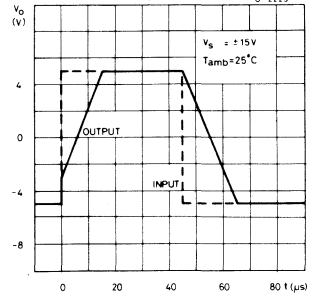


Fig. 15 - Voltage follower large signal pulse response



Typical performance curves for LS 141 and LS 141A

Fig. 16 - Input bias current vs. ambient temperature

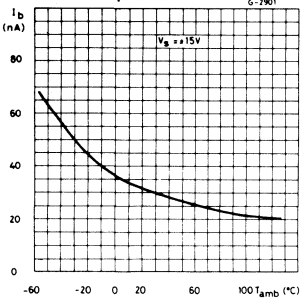


Fig. 17 - Input resistance vs. ambient temperature

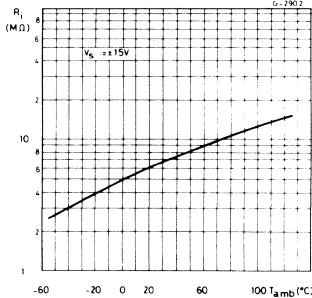


Fig. 18 - Input offset current vs. ambient temperature

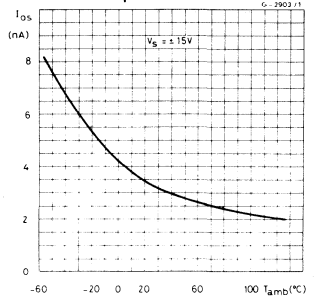


Fig. 19 - Output short-circuit current vs. ambient temperature

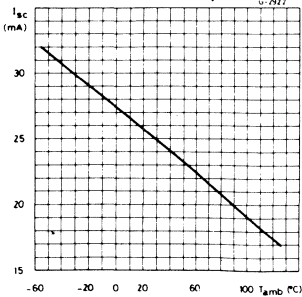


Fig. 20 - Power consumption vs. ambient temperature

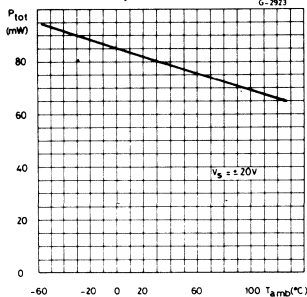
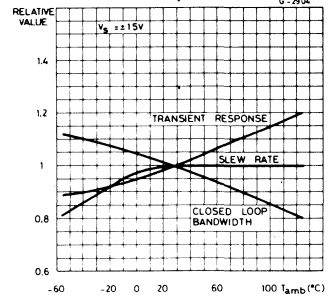


Fig. 21 - Frequency characteristics vs. ambient temperature



LS141 LS141A LS141C

Typical performance curves for LS 141C

Fig. 22 - Input bias current vs. ambient temperature

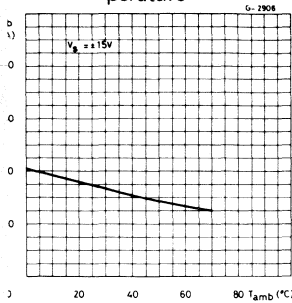


Fig. 23 - Input resistance vs. ambient temperature

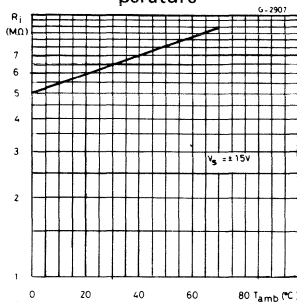


Fig. 24 - Input offset current vs. ambient temperature

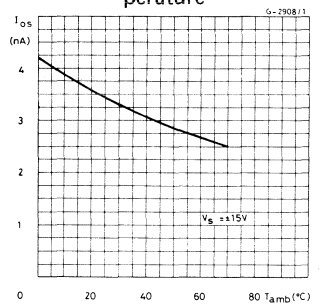


Fig. 25 - Output short circuit current vs. ambient temperature

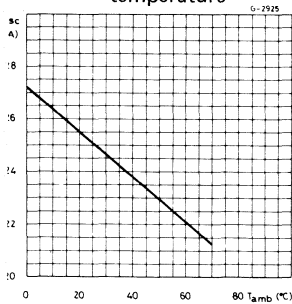


Fig. 26 - Power consumption vs. ambient temperature

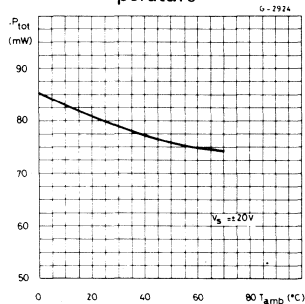
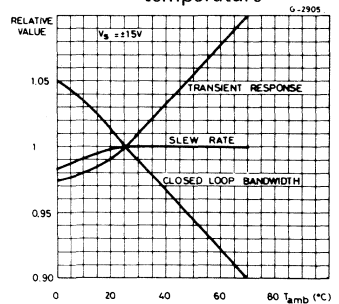


Fig. 27 - Frequency characteristics vs. ambient temperature



TYPICAL APPLICATIONS

Fig. 28 - Clipping amplifier

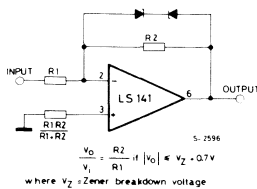


Fig. 29 - Simple integrator

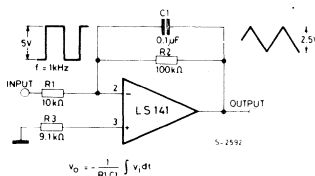
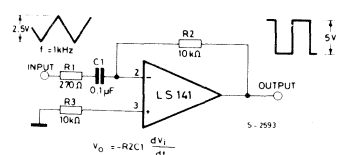


Fig. 30 - Simple differentiator



LS141 LS141A LS141C

TYPICAL APPLICATIONS (continued)

Fig. 31 – Speed control of DC motor

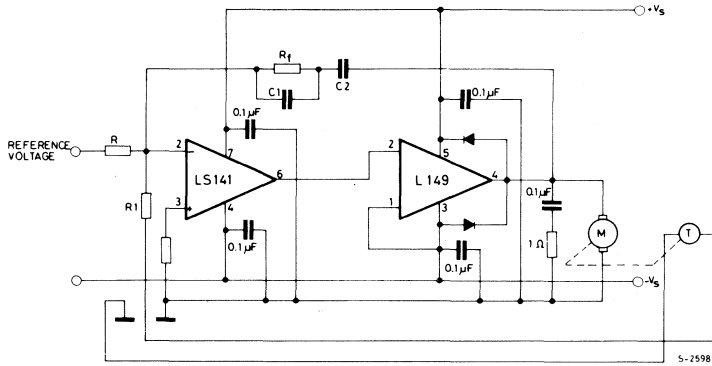


Fig. 32 – Notch filter using the LS 141 as a gyrator

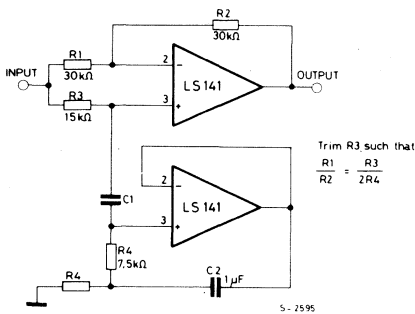
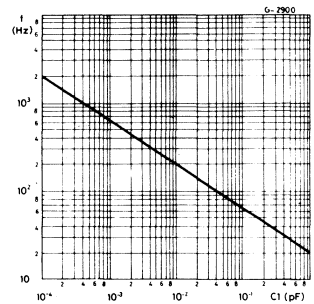


Fig. 33 – Notch frequency vs. C1



LINEAR INTEGRATED CIRCUITS

OPERATIONAL AMPLIFIERS

- SHORT CIRCUIT PROTECTION
- OFFSET VOLTAGE NULL CAPABILITY
- LARGE COMMON MODE AND DIFFERENTIAL VOLTAGE RANGE
- NO LATCH-UP
- SLEW-RATE = $5.5V/\mu s$ ($G_v = 10$, $C_C = 3.5 pF$)

The LS 148 series consists of general purpose operational amplifiers, intended for a wide range of analog applications where tailoring of frequency characteristics is desirable. High common mode voltage range and absence of "Latch-up" tendencies make the LS 148 series ideal for use as a voltage follower. The high gain and wide range of operating voltage provide superior performance in integrators, summing amplifiers and general feedback applications. Unity gain frequency compensation is achieved by means of a single 30 pF capacitor. The LS 148 series is available with hermetic gold chip (8000 series). This is particularly suitable for professional and telecom applications, wherever very high MTBF are required.

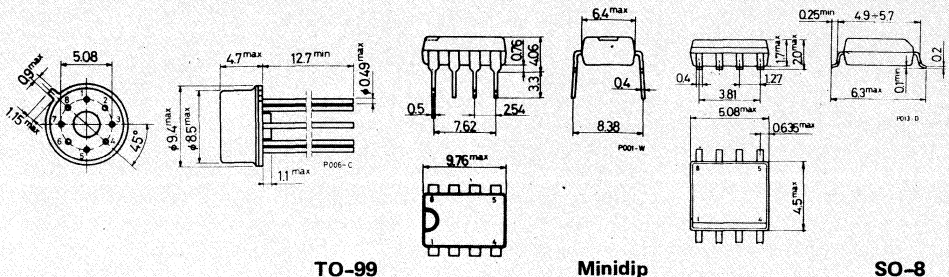
ABSOLUTE MAXIMUM RATINGS

	TO-99	Minidip	μ package
V_s Supply voltage		$\pm 22V$	
V_i (1) Input voltage		$\pm 15V$	
ΔV_i Differential input voltage		$\pm 30V$	
T_{op} Operating temperature		-55 to 125 °C	
		0 to 70 °C	
		indefinite	
P_{tot} Output short circuit duration (2)	520 mW	665 mW	400 mW
T_{stg} Power dissipation at $T_{amb} = 70^\circ C$	-65 to 150 °C	-55 to 150 °C	-55 to 150 °C

- 1) For supply voltage less than $\pm 15V$, input voltage is equal to the supply voltage
- 2) The short circuit duration is limited by thermal dissipation.

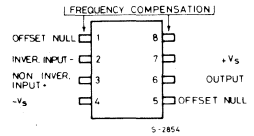
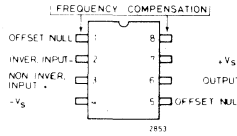
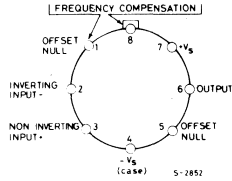
MECHANICAL DATA

Dimensions in mm



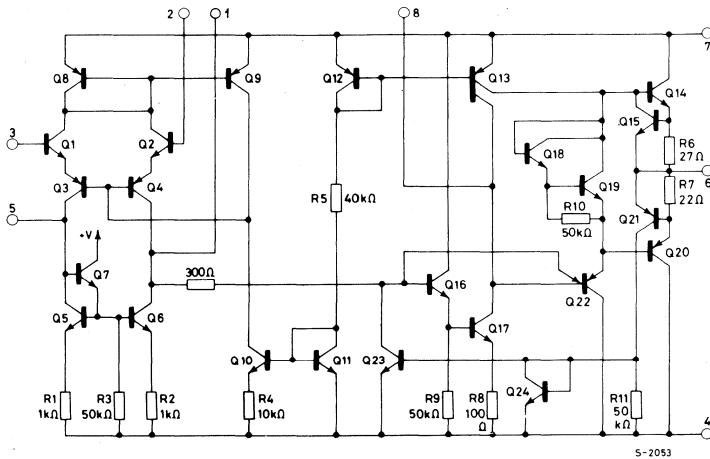
LS 148 LS 148 A LS 148 C

CONNECTION DIAGRAMS AND ORDERING NUMBERS (top views)



Type	TO-99	Minidip	SO-8
LS 148	LS 148T	—	—
LS 148A	LS 148 AT	—	—
LS 148C	LS 148 CT	LS 148 CB	LS 148 CM
LS 8148	—	—	LS 8148M
LS 8148A	—	—	LS 8148 AM
LS 8148C	—	—	LS 8148 CM

SCHEMATIC DIAGRAM



THERMAL DATA

	TO-99	Minidip	SO-8
$R_{th\ j-amb}$ Thermal resistance junction-ambient	max	155 °C/W	120 °C/W
		200* °C/W	

* Measured with the device mounted on a ceramic substrate (25 x 16 x 0.6 mm)

ELECTRICAL CHARACTERISTICS (see note)

Parameter	Test conditions	LS 148			LS 148A			LS 148C			Unit
		Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	
V _{os} Input offset voltage	T _{amb} = 25°C R _g ≤ 10 kΩ R _g ≤ 50 kΩ		1	5		0.5	2		2	6	mV mV
	T _{amb} = T _{min} to T _{max} R _g ≤ 10 kΩ R _g ≤ 50 kΩ		1	6		0.5	3			7.5	mV mV
ΔV _{os} Input offset voltage adjust. range	T _{amb} = 25°C		±15			±25			±15		mV
$\frac{\Delta V_{os}}{\Delta T}$ Average input offset voltage drift	R _g ≤ 50 kΩ					2.5	15				$\frac{\mu V}{^\circ C}$
I _{os} Input offset current	T _{amb} = 25°C		20	200		2	10		20	200	nA nA
	T _{amb} = T _{min} to T _{max}		50	500			25			300	
$\frac{\Delta I_{os}}{\Delta T}$ Average input offset current drift							0.15				$\frac{nA}{^\circ C}$
I _b Input bias current	T _{amb} = 25°C		80	500		20	75		80	500	nA μA
	T _{amb} = T _{min} to T _{max}			1.5			0.1			0.8	
R _i Input resistance	T _{amb} = 25°C	0.3	2		2	10		0.3	2		MΩ
V _i Input voltage range		±12	±13		±12	±13		±12	±13		V
G _v Large signal voltage gain	T _{amb} = 25°C R _L ≥ 2 kΩ V _s = ±15V V _o = ±10V	94	104		94	108		86	104		dB
	T _{amb} = T _{min} to T _{max} R _L ≥ 2 kΩ V _s = ±15V V _o = ±10V	88			88			84			dB
V _o Output voltage swing	V _s = ±15V R _L ≥ 10 kΩ R _L ≥ 2 kΩ	±12 ±10	±14 ±13		±12 ±10	±14 ±13		±12 ±10	±14 ±13		V V
I _{sc} Output short circuit current			25			25			25		mA
CMR Common mode rejection	R _g ≤ 10 kΩ V _{CM} = ±12V	70	90		80	95		70	90		dB
SVR Supply voltage rejection	V _s = ±5 to ±20V R _g ≤ 10 kΩ	76	90		80	97		76	90		dB
SR Slew rate	T _{amb} = 25°C R _L ≥ 2 kΩ	G _v = 1			0.5		0.5		0.5		V/μs
		G _v = 10*			5.5		5.5		5.5		V/μs

* C_C = 3.5 pF

LS 148 LS 148A LS 148C

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	LS 148			LS 148A			LS 148C			Unit
		Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.	
Transient respon. (unity gain) Rise time Overshoot	$T_{amb} = 25^{\circ}C$ $V_i = 20\text{ mV}$ $C_c = 30\text{ pF}$ $R_L = 2\text{ k}\Omega$ $C_L \leq 100\text{ pF}$		0.2 5			0.2 5			0.2 5		μs %
I_S Supply current	$T_{amb} = 25^{\circ}C$		1.9 2.8		1.9 2.8			1.9 2.8			mA
P_S Power consumption	$T_{amb} = 25^{\circ}C$ $V_S = \pm 20V$ $V_S = \pm 15V$		60 85		60 85			60 85			mW mW
	$V_S = \pm 15V$ $T_{amb} = T_{min}$ $T_{amb} = T_{max}$		60 45	100 75		60 40	100 75		60 100		mW mW

Note: These specifications, unless otherwise specified, apply for $V_S = \pm 15V$ and $T_{amb} = -55$ to $125^{\circ}C$ for LS 148 and LS 148A. For LS 148C these specifications apply for $T_{amb} = 0$ to $70^{\circ}C$ ($C_c = 30\text{ pF}$).

Fig. 1 - Voltage offset null circuit

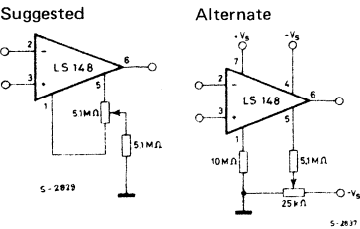
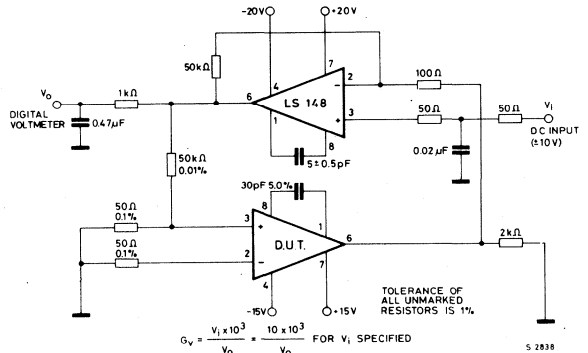


Fig. 2 - Gain test circuit



Typical performance curves for LS 148

Fig. 3 - Input bias current vs. ambient temperature

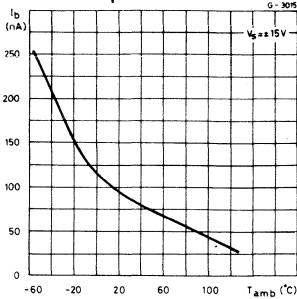


Fig. 4 - Input resistance vs. ambient temperature

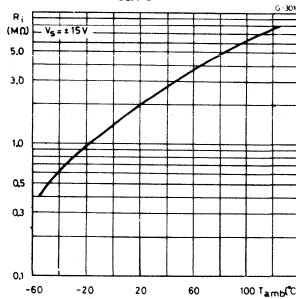


Fig. 5 - Output short-circuit current vs. ambient temperature

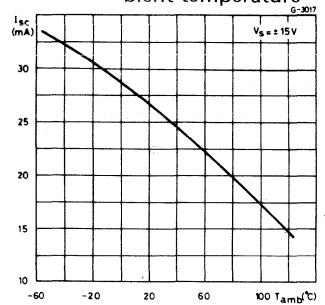


Fig. 6 - Input offset current vs. ambient temperature

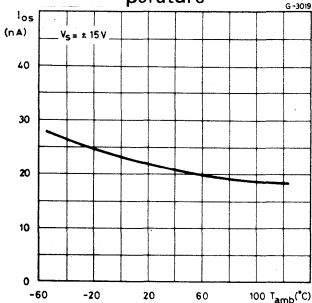


Fig. 7 - Power consumption vs. ambient temperature

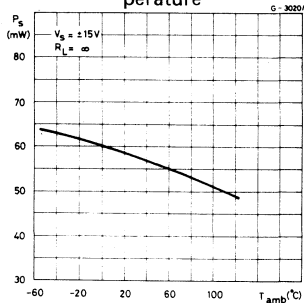
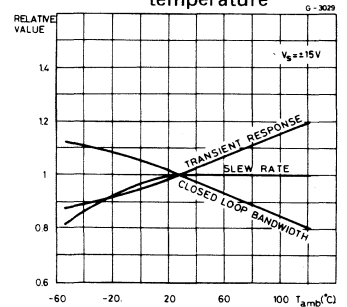


Fig. 8 - Frequency characteristics vs. ambient temperature



Typical performance curves for LS 148C

Fig. 9 - Input bias current vs. ambient temperature

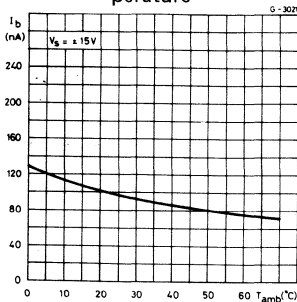


Fig. 10 - Input resistance vs. ambient temperature

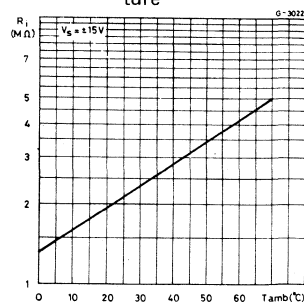
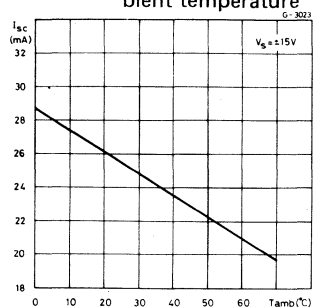


Fig. 11 - Output short-circuit current vs. ambient temperature



LS 148 LS 148 A LS 148 C

Fig. 12 - Input offset current vs. ambient temperature

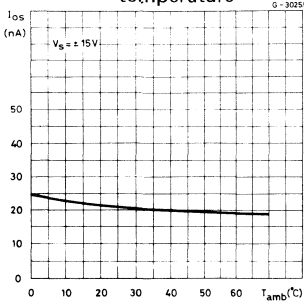


Fig. 13 - Power consumption vs. ambient temperature

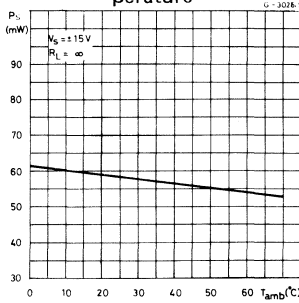
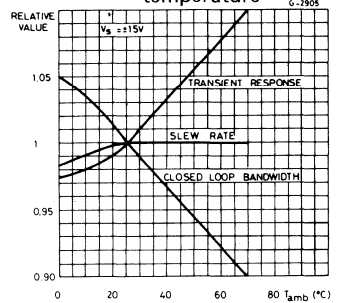


Fig. 14 - Frequency characteristics vs. ambient temperature



Typical performance curves for LS 148 and LS 148C

Fig. 15 - Open loop voltage gain vs. supply voltage

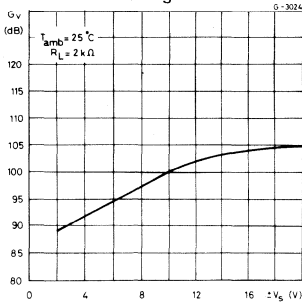


Fig. 16 - Output voltage swing vs. supply voltage

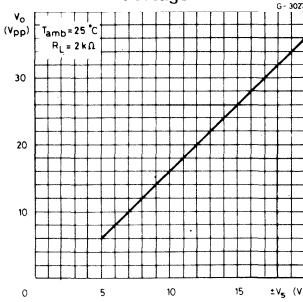


Fig. 17 - Power consumption vs. supply voltage

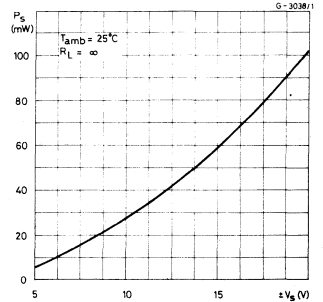


Fig. 18 - Output voltage swing vs. load resistance

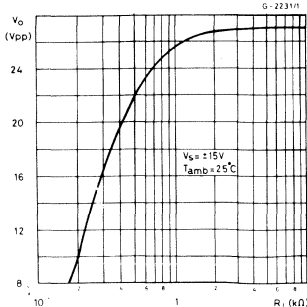


Fig. 19 - Input offset current vs. supply voltage

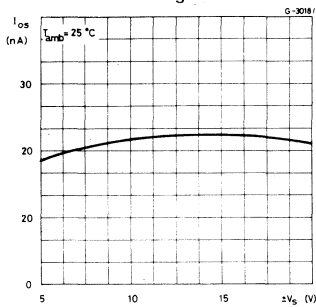
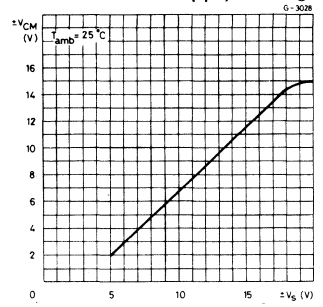


Fig. 20 - Input common mode voltage range vs. supply voltage



LS 148 LS 148 A LS 148 C

Fig. 21 - Input noise voltage vs. frequency

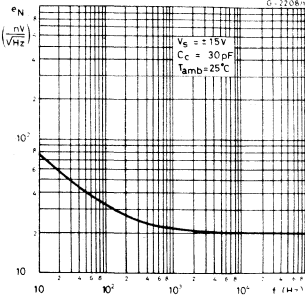


Fig. 22 - Input noise current vs. frequency

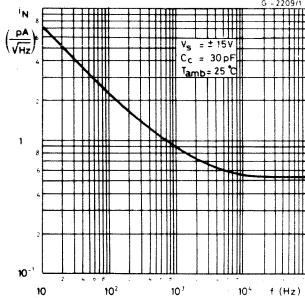


Fig. 23 - Broadband noise for various bandwidths

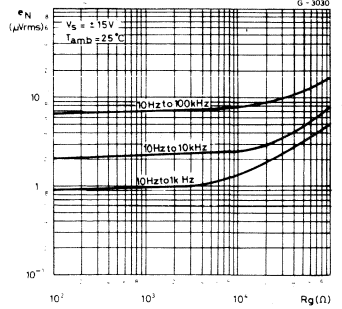


Fig. 24 - Open loop frequency and phase response vs. frequency

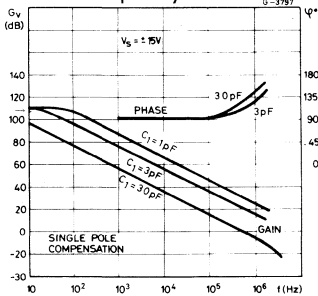


Fig. 25 - Output voltage swing vs. frequency

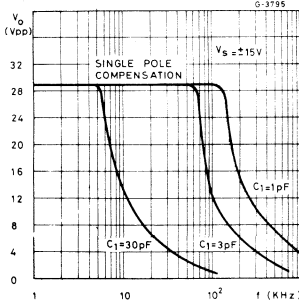


Fig. 26 - Slew-rate

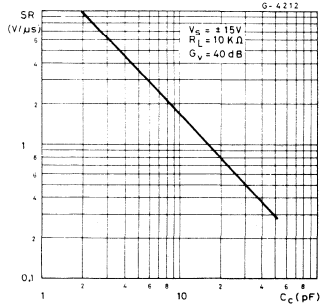


Fig. 27 - Compensation capacitance vs. closed loop voltage gain

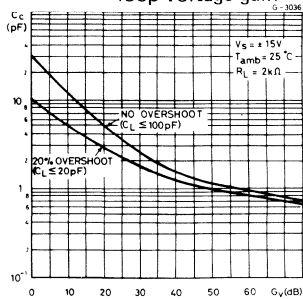


Fig. 28 - Input resistance and input capacitance vs. frequency

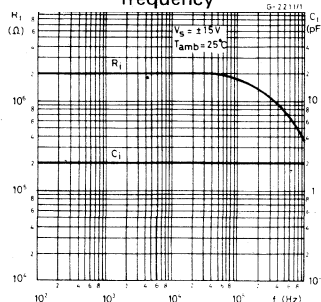
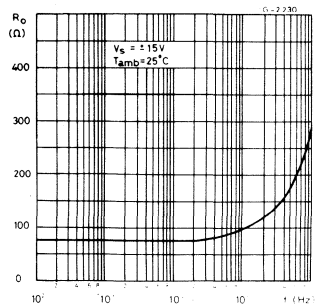


Fig. 29 - Output resistance vs. frequency



LS 148 LS 148 A LS 148 C

Fig. 30 - Frequency characteristics vs. supply voltage

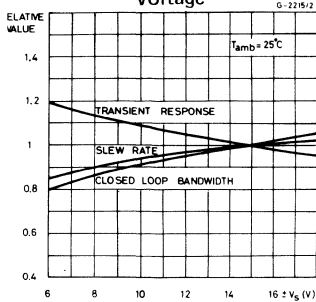


Fig. 31 - Voltage follower transient response (unity gain)

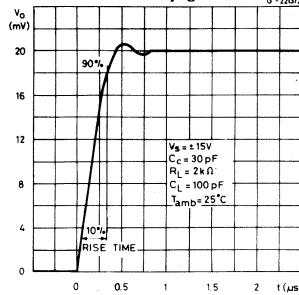


Fig. 32 - Transient response test circuit

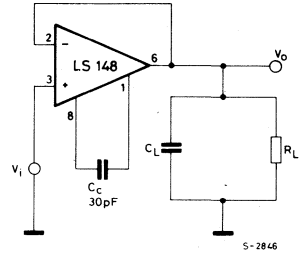


Fig. 33 - Voltage follower large-signal pulse response

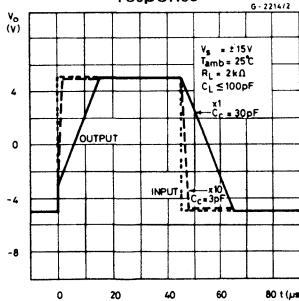


Fig. 34 - Feed forward compensation

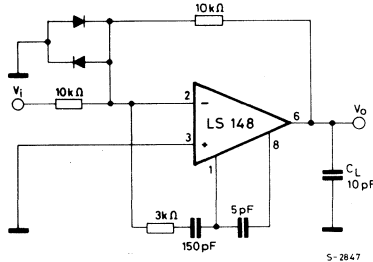
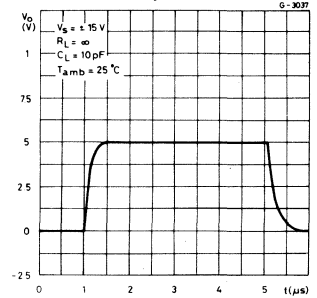
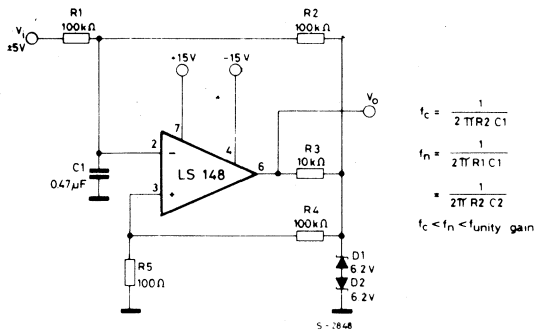


Fig. 35 - Large signal feed forward transient response



TYPICAL APPLICATIONS

Fig. 36 - Pulse width modulator



TYPICAL APPLICATION (continued)

Fig. 37 - Differentiator circuit

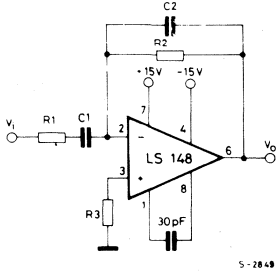


Fig. 38 - Single supply circuit

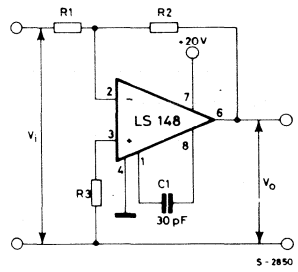


Fig. 39 - High power amplifier with split power supply ($G_v = 30$ dB)

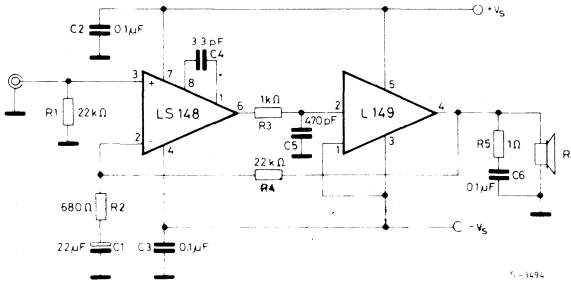
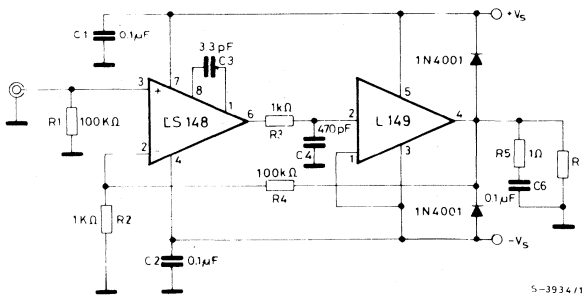


Fig. 40 - High slew-rate power operational amplifier.



LS 150

LINEAR INTEGRATED CIRCUIT

HIGH PERFORMANCE 80 dB COMPANDOR

The LS150 is a monolithic integrated circuit in 14-lead dual in-line ceramic and plastic packages; it performs signal level expansion in an 80-dB range [with an overall accuracy of ± 0.2 dB in a 60 dB range] and, when used in the feedback path of an operational amplifier, it performs complementary signal compression. The LS150 has been designed to improve audio channel signal-to-noise ratio according to CCITT recommendations which require an unaffected reference level of -14 dBm across 600 Ω . The device can also be used to reduce crosstalk and may be converted into a unity gain amplifier for data transmission links by means of a simple switch without affecting output and input impedance levels. Another possible application is as a **noise reducer and dynamic range expander** in cassette tape recorders and intercoms.

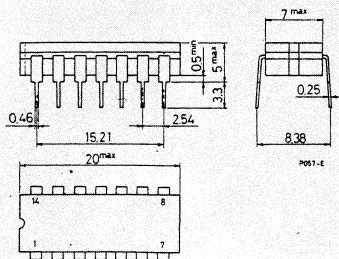
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	24	V
I_{5-6}	Differential current between pins 5 and 6	20	mA
V_i	Common mode input voltage	V_s	
T_{stg}, T_j	Storage and junction temperature	-65 to 150	$^{\circ}$ C
T_{op}	Operating temperature	-20 to 85	$^{\circ}$ C

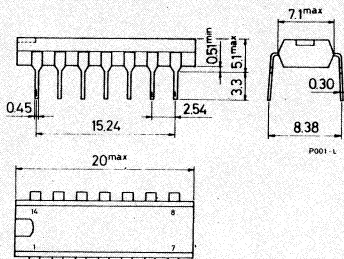
ORDERING NUMBERS: LS150 CD (Ceramic package)
LS150 CB (Plastic package)

MECHANICAL DATA

Dimensions in mm

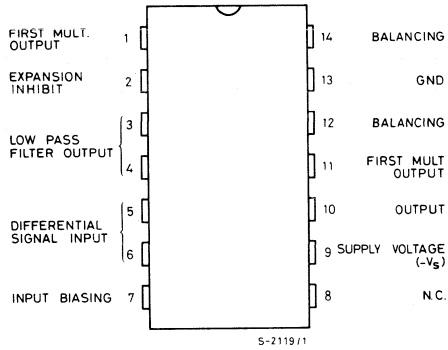


LS 150 CD

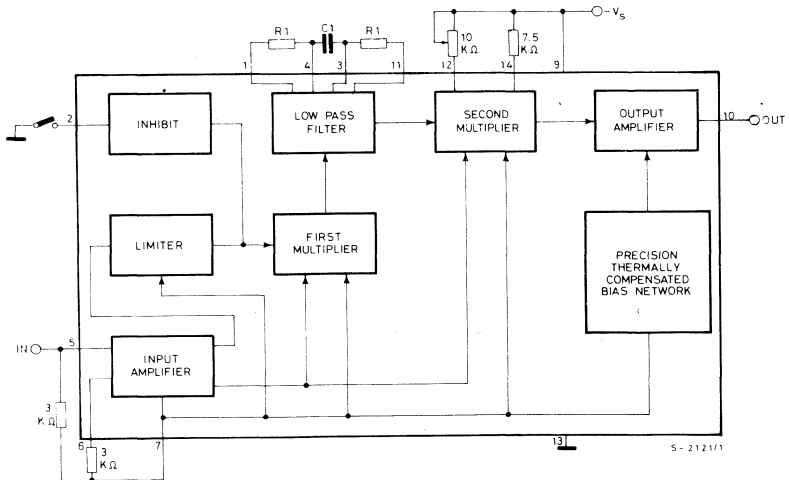


LS 150 CB

CONNECTION DIAGRAM (top view)

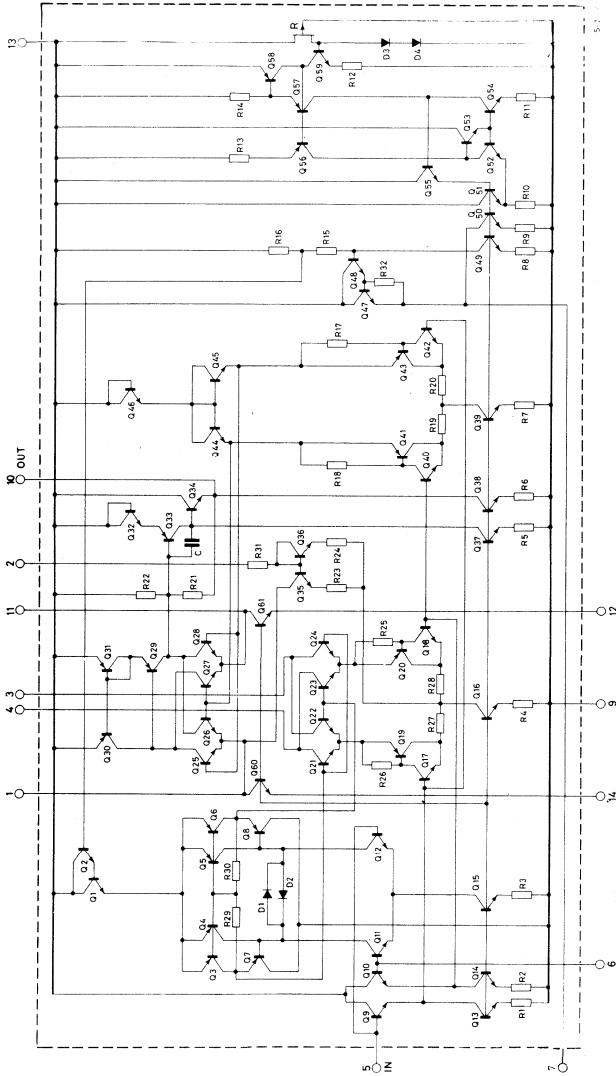


BLOCK DIAGRAM



LS 150

SCHEMATIC DIAGRAM



LS 150

THERMAL DATA

		Plastic	Ceramic	
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	100 °C/W	120 °C/W

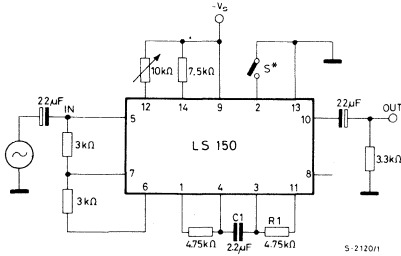
ELECTRICAL CHARACTERISTICS (Refer to the test circuit of fig. 1, $-V_s = -12V$; $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit		
I_s	Supply current		5	8	mA		
R_7	Input dynamic biasing resistance (pin 7)	$L_i = -14\text{ dBv}$ $f = 800\text{ Hz}$ External time constant $2 R_1 \cdot C_1 = 20\text{ ms}$		60	90	Ω	
G_v	Gain	-1	0	+1	dB		
ΔG_v	Gain variation		$T_{amb} = 5\text{ to }55^\circ C$ $\Delta V_s = \pm 2\%$	± 0.2 ± 0.03	dB dB		
B	Bandwidth (-3 dB)		500		KHz		
R_o	Output resistance		25	60	Ω		
R_{i_1}	Input resistance (pin 5)	$L_i = -14\text{ dBv}$ $f = 800\text{ Hz}$		100	K Ω		
d	Distortion		0.7		%		
d_3	Two-tone third order intermodulation	$f_1 = 900\text{ Hz}$ $f_2 = 1020\text{ Hz}$ $V_1 = V_2 = 88\text{ mV}$		0.5	%		
e_N	Output noise in psophometric band		-100		dBm		
$\Delta G $	Expansion accuracy after balancing	$L_i = -40\text{ to }-10\text{ dBv}$, $f = 800\text{ Hz}$ $T_{amb} = 5\text{ to }55^\circ C$, $f = 800\text{ Hz}$		0.1 0.2	0.2 0.3	dB dB	
I_{off}	Inhibit current consumption (pin 2)		0.3	1	mA		
G	Amplifier gain	Inhibit ON (pin 2 grounded) $f = 800\text{ Hz}$		-1.5	0	+1.5	dB

LS 150

TEST AND APPLICATION CIRCUITS

Fig. 1 - Expander circuit



(*) S closed : unity gain amplifier.
S open : expander.

Fig. 2 - Compressor circuit

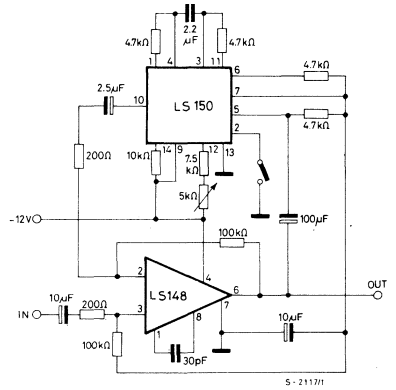


Fig. 3 - Compander Characteristics

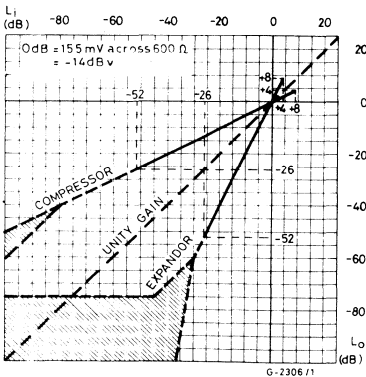


Fig. 4 - Comparison between LS150 performance (curve A) and limits from CCITT recommendation (curve B) - Green Book - Geneva 1972 - G162.

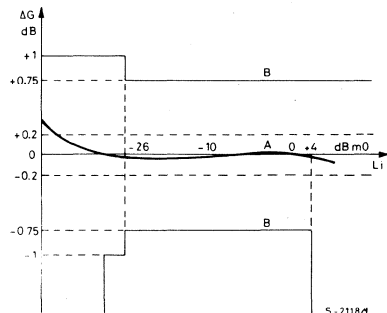


Fig. 5 - Expander gain vs. temperature

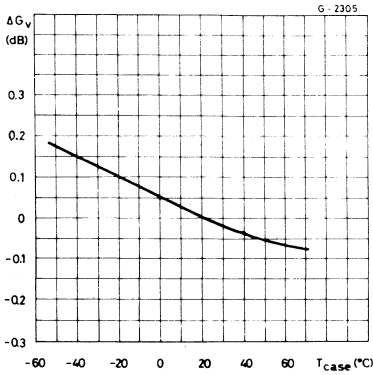
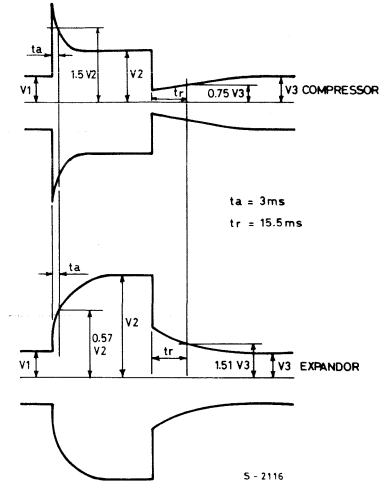


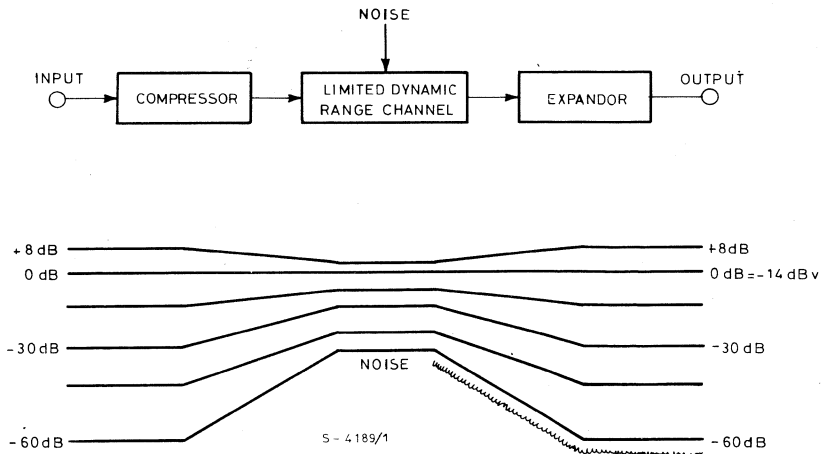
Fig. 6 - Transient response



APPLICATION INFORMATION

The fig. 7 shows the basic configuration (with relative signal levels) of a compandorized system. It is clear the action against the line noise: the system using a compressor in sending and an expander in receiving can improve very much the signal-to-noise ratio, especially with very high noise lines. By using the LS150 it is possible to built both the compressor and the expander blocks.

Fig. 7 - Compandorized system.

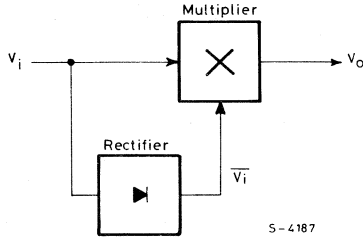


LS 150

APPLICATION INFORMATION (continued)

The basic block diagram of an expander is shown in fig. 8. The product of the input voltage V_i and its mean value \overline{V}_i (obtained from the rectifier with time constant τ) is supplied at the output of an "ideal" multiplier.

Fig. 8 - Basic expander circuit.



S-4187

The output voltage V_o is proportional to the product of V_i and \overline{V}_i :

$$V_o = KV_i \times \overline{V}_i$$

where K is a factor that defines a level for unity gain.

For a constant input level,

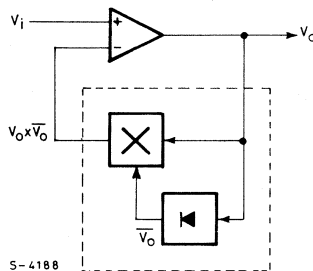
$$\overline{V}_o = K\overline{V}_i \times \overline{V}_i = K\overline{V}_i^2$$

Expressing all levels in decibels relative to a reference level:

$$\overline{V}_o \text{ (dB)} = 20 \log_{10} \overline{V}_i^2 = 2 \overline{V}_i \text{ (dB)}.$$

Signals with an input level equal to the reference level are unaffected by the expander while higher levels are raised and lower levels attenuated. It is recommended by CCITT, and practically advantageous, that the unaffected level be -14 dBv, a voltage corresponding to -14 dBm across 600Ω . A time constant for the average rectifier of 20 ms is also recommended, giving "syllabic" operation of the compandor.

Fig. 9 - Basic compressor circuit.



S-4188

A compressor can easily be implemented with an expander in the feedback path of an operational amplifier (Fig. 9). Assuming infinite gain for the amplifier:

$$V_i = KV_o \times \overline{V}_o$$

and for a constant input level

$$\overline{V}_o = \sqrt{\frac{\overline{V}_i}{K}}$$

In decibels, with respect to the unaffected level,

$$\overline{V}_o \text{ (dB)} = 20 \log_{10} (\overline{V}_i)^{\frac{1}{2}} = \frac{1}{2} \overline{V}_i \text{ (dB)}.$$

APPLICATION INFORMATION (continued)

Design Constraints

There are several constraints on the design of a compandor to be used in telecommunication equipment.

Level: The reference (or unity gain) level is -14 dBv, i.e. 155 mV rms. For application in high-quality multiplexer transmission systems between exchanges, and expansion accuracy better than 0.2 dB in the same range ($+40$ to -25 dBmo) considered by CCITT for all operating conditions is required. These parameters had to be compatible with mass production manufacturing techniques. Particularly when taking into account the low signal levels, this requirement is very demanding. It was the main target in designing the device and had a strong influence on the fabrication process, circuit configurations, and layout.

Power Supply: The circuit has to operate with a single 12V negative supply, unregulated, and with relatively high noise.

Input Impedance: This has to be precisely defined by an external resistor, which is the passive termination of an LC filter before the expander. Thus the input impedance of the IC must be very high. A differential input stage is preferable to reduce ground loop noise.

Gain: The expander (or compressor) shall not modify the level diagram of existing channel modems, already optimized for crosstalk and noise. This means that the gain at the unaffected level shall be 0 dB, with small spread.

Inhibition: It must be possible to inhibit the operation of the compandor for testing and maintenance purpose, and to allow the transmission of telegraph channels.

Definition of units

dBmo : power level ($10 \log \frac{P_2}{P_1}$) is expressed in dBm when P_1 is 1 mW, therefore 0 dBm = 1 mW.

dBm : the power is expressed in dBmo when referred to an established power level in the circuit, generally the output signal level.

e.g.: if the output level is -15 dBm and this level is chosen as reference, then 0 dBmo = -15 dBm; if another signal, i.e. the distortion measured at the same point of the circuit, is -90 dBm, then the distortion is -75 dBmo.

dBv : $20 \log \frac{V_2}{V_1}$ when $V_1 = 775$ mVrms.

LS 159

LINEAR INTEGRATED CIRCUIT

HIGH RELIABILITY TRANSISTOR ARRAY

The LS159 is an array of 5 NPN transistors on a common monolithic substrate in an SO-14 (14-lead plastic micropackage). This package is easily mounted on thick and thin film hybrid circuits. Two transistors are internally connected to form a differential amplifier. The transistors of the LS159 are well suited to low noise general purposes and to a wide variety of applications in low power systems in the DC through VHF range. They may be used as discrete components in conventional circuits; in addition they provide the very significant inherent integrated circuit advantages of close electrical and thermal matching. The device is also available with a hermetic goldchip (LS8159M) that is particularly suitable for professional and telecom applications, wherever very high MTBF are required. This performance is guaranteed by silicon nitride sealing of chip surface and Ti-Pt-Au metallization, protected with a double passivated layer, providing resistance against contamination, electrolytic corrosion and electromigration.

ABSOLUTE MAXIMUM RATINGS

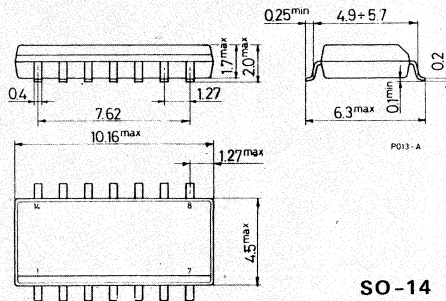
		Each transistor	Total package
V_{CBO}	Collector-base voltage ($I_E = 0$)	20 V	—
V_{CEO}	Collector-emitter voltage ($I_B = 0$)	15 V	—
V_{CSS} *	Collector-substrate voltage	20 V	—
V_{EBO}	Emitter-base voltage ($I_C = 0$)	5 V	—
I_C	Collector current	50 mA	—
P_{tot}	Total power dissipation at $T_{amb} = 25^\circ\text{C}$	250 mW	500 mW
T_{stg}, T_j	Storage, and junction temperature	-55 to 150 °C	
	Soldering dip or wave at 5 s	260 °C	
		11 s	
		235 °C	

*) The collector of each transistor of the LS159 is isolated from the substrate by an integrated diode. The substrate (pin 13) must be connected to the most negative point in the external circuit to maintain isolation between transistors and to provide for normal transistor action.

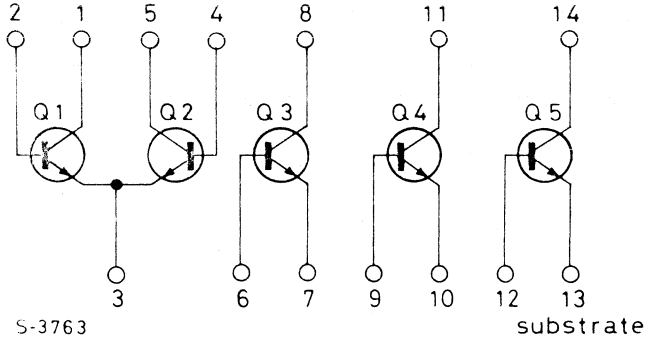
ORDERING NUMBERS: LS 159M — LS 8159M

MECHANICAL DATA

Dimensions in mm



SCHEMATIC DIAGRAM



THERMAL DATA

$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	250	$^{\circ}C/W$
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ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^{\circ}C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig.
I_{CBO}	Collector cutoff current ($I_E = 0$)		0.002	40	nA	1
I_{CEO}	Collector cutoff current ($I_B = 0$)		see curve	0.5	μA	2
$ I_{B1} - I_{B2} $	Input offset current	$I_C = 1\text{ mA}$	$V_{CE} = 3V$	0.3	μA	7
V_{CBO}	Collector-base voltage ($I_E = 0$)	20	60		V	—
V_{CEO}	Collector-emitter voltage ($I_B = 0$)	15	24		V	—
V_{CSS}	Collector-substrate voltage ($I_{CSS} = 0$)	20	60		V	—
$V_{CE(sat)}$	Collector-emitter saturation voltage	$I_C = 10\text{ mA}$	$I_B = 1\text{ mA}$	0.23	V	—

LS 159

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig.		
V_{EBO}	Emitter-base voltage ($I_C = 0$)	$I_E = 10 \mu A$	5	7		V	—	
V_{BE}	Base-emitter voltage	$I_E = 1 \text{ mA}$ $I_E = 10 \text{ mA}$	$V_{CE} = 3 \text{ V}$ $V_{CE} = 3 \text{ V}$	0.71 0.8		V V	4	
$ V_{BE1} - V_{BE2} $	Input offset voltage	$I_C = 1 \text{ mA}$	$V_{CE} = 3 \text{ V}$	0.45	5	mV	4-6	
$ V_{BE3} - V_{BE4} $	Input offset voltage							
$ V_{BE4} - V_{BE5} $	Input offset voltage							
$ V_{BE5} - V_{BE4} $	Input offset voltage							
$\frac{\Delta V_{BE}}{\Delta T}$	Base-emitter voltage temperature coefficient	$I_C = 1 \text{ mA}$	$V_{CE} = 3 \text{ V}$	-1.9		mV/°C	5	
$\frac{ V_{BE1} - V_{BE2} }{\Delta T}$	Input offset voltage temperature coefficient	$I_C = 1 \text{ mA}$	$V_{CE} = 3 \text{ V}$	1.1		$\mu\text{V}/^\circ\text{C}$	6	
h_{FE}	DC current gain	$I_C = 10 \text{ mA}$ $I_C = 1 \text{ mA}$ $I_C = 10 \mu A$	$V_{CE} = 3 \text{ V}$ $V_{CE} = 3 \text{ V}$ $V_{CE} = 3 \text{ V}$	40	100 100 54	— — —	3	
f_T	Transition frequency	$I_C = 3 \text{ mA}$	$V_{CE} = 3 \text{ V}$	300	550		MHz	14
NF	Noise figure	$I_C = 100 \mu A$ $R_g = 1 \text{ k}\Omega$	$V_{CE} = 3 \text{ V}$ $f = 1 \text{ kHz}$		3.25		dB	8
h_{ie}	Input impedance	$I_C = 1 \text{ mA}$	$V_{CE} = 3 \text{ V}$ $f = 1 \text{ KHz}$		3.5	k Ω	9	
h_{fe}	Forward current transfer ratio							
h_{re}	Reverse voltage transfer ratio							
h_{oe}	Output admittance							
h_{re}	Reverse voltage transfer ratio				1.8x10 ⁻⁴	—		
h_{oe}	Output admittance				15.6	μS		
Y_{ie}	Input admittance	$I_C = 1 \text{ mA}$	$V_{CE} = 3 \text{ V}$ $f = 1 \text{ MHz}$		0.3+j0.04	mS	11	
Y_{fe}	Forward transadmittance							
Y_{re}	Reverse transadmittance							
Y_{oe}	Output admittance							
Y_{fe}	Forward transadmittance				31-j1.5	mS	10	
Y_{re}	Reverse transadmittance				see curve	mS	13	
Y_{oe}	Output admittance				0.001+j0.03	mS	12	
C_{EBO}	Emitter-base capacitance	$I_C = 0$	$V_{EB} = 3 \text{ V}$		0.6		pF	—
C_{CBO}	Collector-base capacitance	$I_E = 0$	$V_{CB} = 3 \text{ V}$		0.58		pF	—
C_{CSS}	Collector-substrate capacitance	$I_C = 0$	$V_{CSS} = 3 \text{ V}$		2.8		pF	—

Fig. 1 - Collector cutoff current vs. ambient temperature

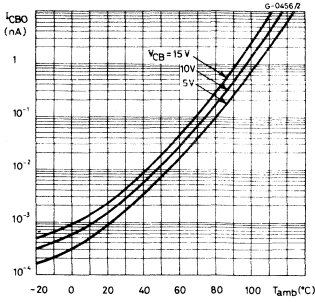


Fig. 2 - Collector cutoff current vs. ambient temperature

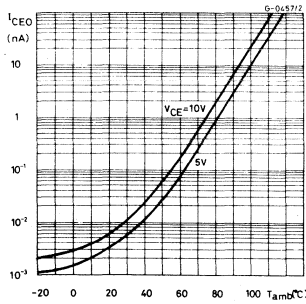


Fig. 3 - DC current gain

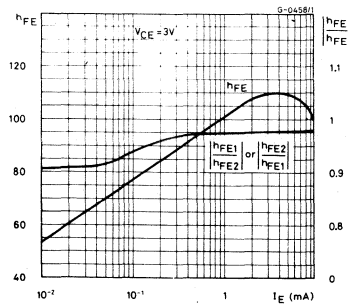


Fig. 4 - Input voltage and input offset voltage vs. emitter current

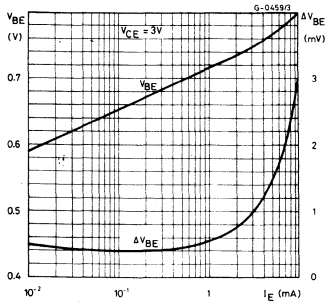


Fig. 5 - Input characteristics for each transistor

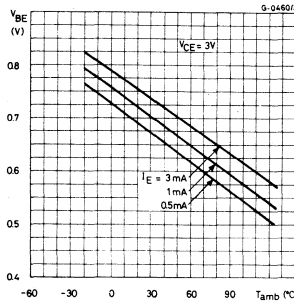


Fig. 6 - Input offset voltage vs. ambient temperature

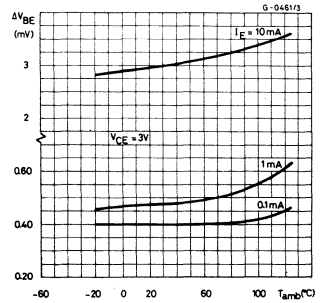


Fig. 7 - Input offset current for matched transistor pair

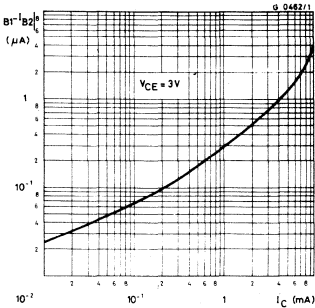


Fig. 8 - Noise figure vs. collector current

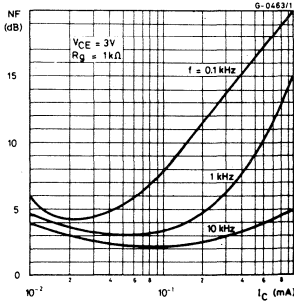
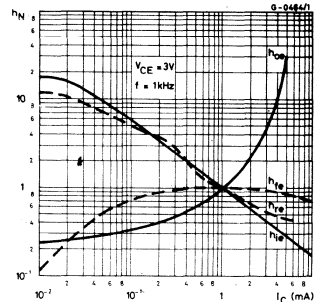


Fig. 9 - Normalized h parameters vs. collector current



LS 159

Fig. 10 - Forward admittance vs. frequency

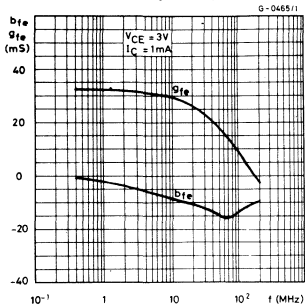


Fig. 11 - Input admittance vs. frequency

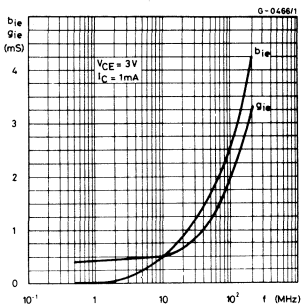


Fig. 12 - Output admittance vs. frequency

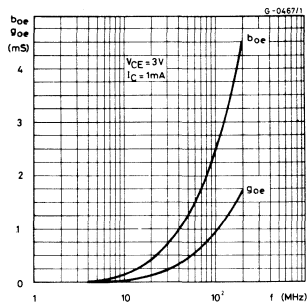


Fig. 13 - Reverse admittance vs. frequency

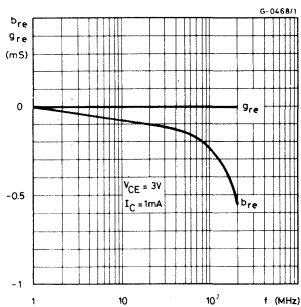
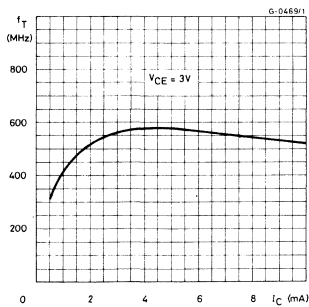


Fig. 14 - Transition frequency vs. collector current



LINEAR INTEGRATED CIRCUITS

HIGH PERFORMANCE DUAL OPERATIONAL AMPLIFIERS

- SINGLE OR SPLIT SUPPLY OPERATION
- LOW POWER CONSUMPTION
- SHORT CIRCUIT PROTECTION
- LOW DISTORTION, LOW NOISE
- HIGH GAIN-BANDWIDTH PRODUCT
- HIGH CHANNEL SEPARATION

The LS 204 is a high performance dual operational amplifier with frequency and phase compensation built into the chip. The internal phase compensation allows stable operation as voltage follower in spite of its high gain-bandwidth products. The circuit presents very stable electrical characteristics over the entire supply voltage range, and it is particularly intended for professional and telecom applications (active filters, etc.). The LS 204 series is available with hermetic gold chip (8000 series).

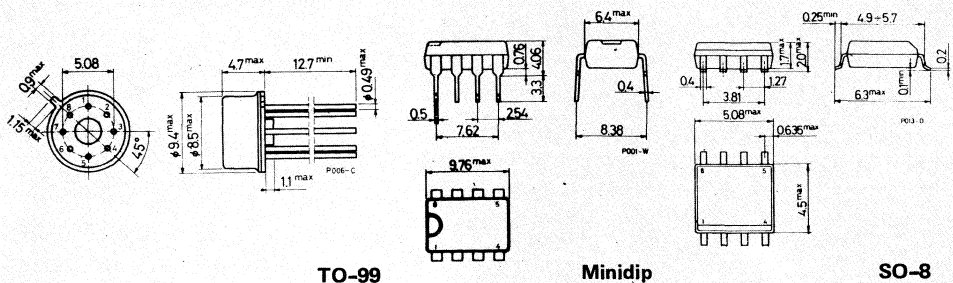
ABSOLUTE MAXIMUM RATINGS		Each transistor	Total package
V_{CBO}	Collector-base voltage ($I_E = 0$)	20 V	—
V_{CEO}	Collector-emitter voltage ($I_B = 0$)	15 V	—
V_{CSS}^*	Collector-substrate voltage	20 V	—
V_{EBO}	Emitter-base voltage ($I_C = 0$)	5 V	—
I_C	Collector current	50 mA	—
P_{tot}	Total power dissipation at $T_{amb} = 25^\circ\text{C}$	250 mW	500 mW
T_{stg}, T_j	Storage, and junction temperature	-55 to 150 °C	
	Soldering dip or wave at 5 s	260 °C	
	11 s	235 °C	

*) The collector of each transistor of the LS159 is isolated from the substrate by an integrated diode. The substrate (pin 13) must be connected to the most negative point in the external circuit to maintain isolation between transistors and to provide for normal transistor action.

ORDERING NUMBERS: LS 159M – LS 8159M

MECHANICAL DATA

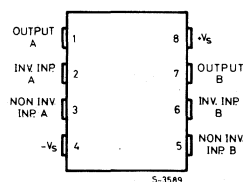
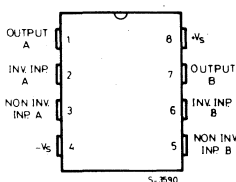
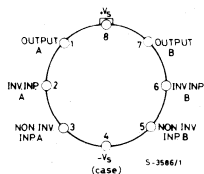
Dimensions in mm



LS 204 LS 204A LS 204C

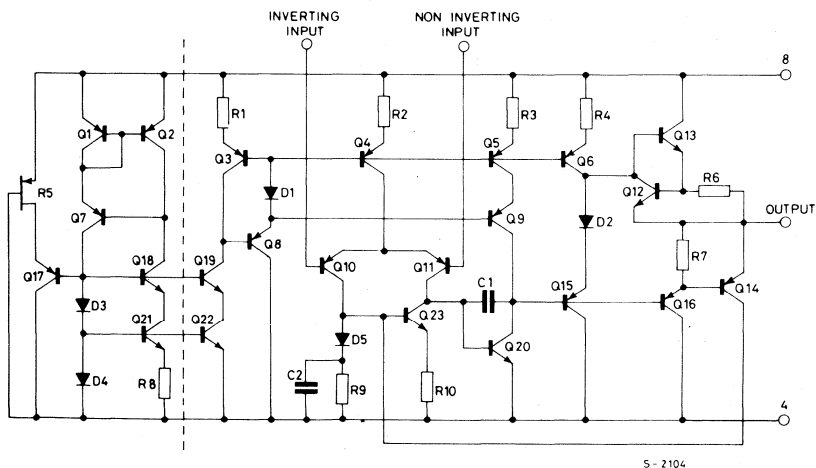
CONNECTION DIAGRAMS AND ORDERING NUMBERS

(top views)



Type	TO-99	Minidip	SO-8
LS 204	LS 204 T	—	LS 204 M
LS 204 A	LS 204 AT	—	—
LS 204 C	LS 204 CT	LS 204 CB	LS 204 CM
LS 8204	—	—	LS 8204 M
LS 8204 A	—	—	LS 8204 AM
LS 8204 C	—	—	LS 8204 CM

SCHEMATIC DIAGRAM (one section)



THERMAL DATA

	TO-99	Minidip	SO-8
$R_{th\ j-amb}$ Thermal resistance junction-ambient max	155 °C/W	120 °C/W	200 °C/W

* Measured with the device mounted on a ceramic substrate (25x16x96 mm)

LS 204 LS 204A LS 204C

ELECTRICAL CHARACTERISTICS ($V_s = \pm 15V$, $T_{amb} = 25^\circ C$, unless otherwise specified)

Parameter	Test conditions	LS 204/LS204A			LS 204C			Unit
		Min.	Typ.	Max.	Min.	Typ.	Max.	
I_s Supply current			0.7	1		0.8	1.5	mA
I_b Input bias current			50	150		100	300	nA
	$T_{min} < T_{op} < T_{max}$			300			700	nA
R_i Input resistance	$f = 1 \text{ KHz}$		1			0.5		M Ω
V_{os} Input offset voltage	$R_g \leq 10 \text{ K}\Omega$		0.5	2.5		0.5	3.5	mV
	$R_g \leq 10 \text{ K}\Omega$ $T_{min} < T_{op} < T_{max}$			3.5			5	mV
$\frac{\Delta V_{os}}{\Delta T}$ Input offset voltage drift	$R_g = 10 \text{ K}\Omega$ $T_{min} < T_{op} < T_{max}$		5			5		$\mu V/^\circ C$
I_{os} Input offset current			5	20		12	50	nA
	$T_{min} < T_{op} < T_{max}$			40			100	nA
$\frac{\Delta I_{os}}{\Delta T}$ Input offset current drift	$T_{min} < T_{op} < T_{max}$		0.08			0.1		$\frac{nA}{^\circ C}$
I_{sc} Output short circuit current			23			23		mA
G_v Large signal open loop voltage gain	$T_{min} < T_{op} < T_{max}$ $R_L = 2 \text{ K}\Omega$ $V_s = \pm 15V$ $V_s = \pm 4V$	90	100 95		86	100 95		dB
B Gain-bandwidth product	$f = 20 \text{ KHz}$	1.8	3		1.5	2.5		MHz
e_N Total input noise voltage	$f = 1 \text{ KHz}$ $R_g = 50\Omega$ $R_g = 1 \text{ K}\Omega$ $R_g = 10 \text{ K}\Omega$		8 10 18	15		10 12 20		$\frac{nV}{\sqrt{Hz}}$
d Distortion	$G_v = 20 \text{ dB}$ $R_L = 2 \text{ K}\Omega$ $V_o = 2 V_{pp}$ $f = 1 \text{ KHz}$		0.03	0.1		0.03	0.1	%
V_o DC output voltage swing	$R_L = 2 \text{ K}\Omega$ $V_s = \pm 15V$ $V_s = \pm 4V$	± 13	± 3		± 13	± 3		V
V_o Large signal voltage swing	$R_L = 10 \text{ K}\Omega$ $f = 10 \text{ KHz}$		28			28		V _{pp}
SR Slew rate	unity gain $R_L = 2 \text{ K}\Omega$	0.8	1.5			1		V/ μs
CMR Common mode rejection	$V_i = 10V$ $T_{min} < T_{op} < T_{max}$	90			86			dB
SVR Supply voltage rejection	$V_i = 1V$ $f = 100 \text{ Hz}$ $T_{min} < T_{op} < T_{max}$	90			86			dB
CS Channel separation	$f = 1 \text{ KHz}$	100	120			120		dB

Note:	LS 204	LS 204A	LS 204C
$T_{min.}$	$-25^\circ C$	$-55^\circ C$	$0^\circ C$
$T_{max.}$	$+85^\circ C$	$+125^\circ C$	$+70^\circ C$

LS 204 LS 204 A LS 204 C

Fig. 1 - Supply current vs. supply voltage

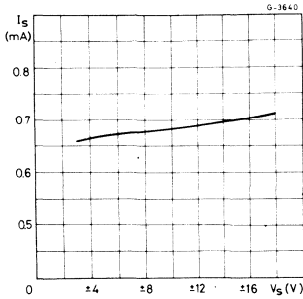


Fig. 2 - Supply current vs. ambient temperature

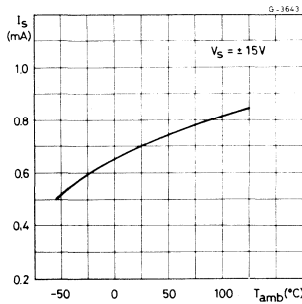


Fig. 3 - Output short circuit current vs. ambient temperature

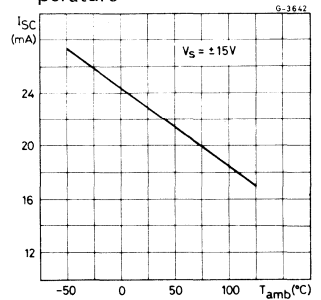


Fig. 4 - Open loop frequency and phase response

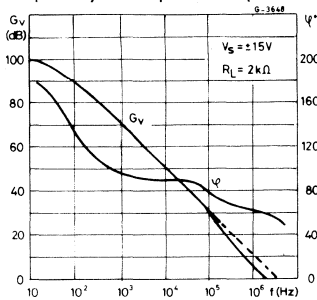


Fig. 5 - Open loop gain vs. ambient temperature

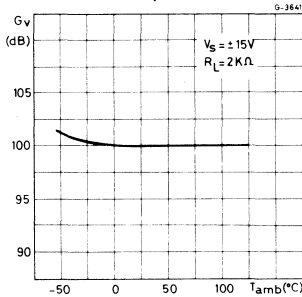


Fig. 6 - Supply voltage rejection vs. frequency

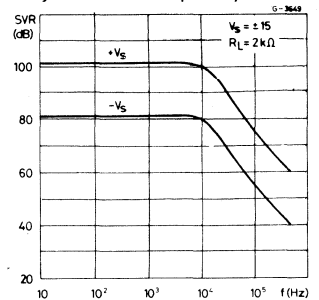


Fig. 7 - Large signal frequency response

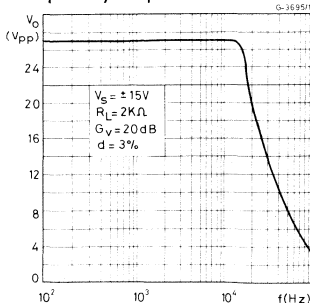


Fig. 8 - Output voltage swing vs. load resistance

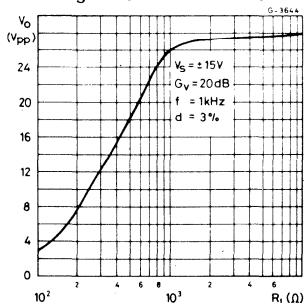
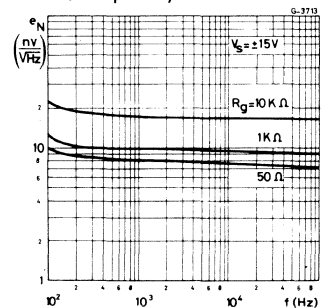


Fig. 9 - Total input noise vs. frequency



APPLICATION INFORMATION

Active low-pass filter:

BUTTERWORTH

The Butterworth is a "maximally flat" amplitude response filter. Butterworth filters are used for filtering signals in data acquisition systems to prevent aliasing errors in sampled data applications and for general purpose low-pass filtering.

The cutoff frequency, f_c , is the frequency at which the amplitude response is down 3 dB. The attenuation rate beyond the cutoff frequency is -n6 dB per octave of frequency where n is the order (number of poles) of the filter.

Other characteristics:

- Flattest possible amplitude response.
- Excellent gain accuracy at low frequency end of passband.

BESSEL

The Bessel is a type of "linear phase" filter. Because of their linear phase characteristics, these filters approximate a constant time delay over a limited frequency range. Bessel filters pass transient waveforms with a minimum of distortion. They are also used to provide time delays for low pass filtering of modulated waveforms and as a "running average" type filter.

The maximum phase shift is $\frac{-n\pi}{2}$ radians where n is the order (number of poles) of the filter. The cutoff frequency, f_c , is defined as the frequency at which the phase shift is one half of this value. For accurate delay, the cutoff frequency should be twice the maximum signal frequency. The following table can be used to obtain the -3 dB frequency of the filter.

	2 pole	4 pole	6 pole	8 pole
-3 dB frequency	0.77 f_c	0.67 f_c	0.57 f_c	0.50 f_c

Other characteristics:

- Selectivity not as great as Chebyshev or Butterworth.
- Very little overshoot response to step inputs
- Fast rise time.

CHEBYSHEV

Chebyshev filters have greater selectivity than either Bessel or Butterworth at the expense of ripple in the passband.

Chebyshev filters are normally designed with peak-to-peak ripple values from ± 0.2 dB to ± 2 dB.

Increased ripple in the passband allows increased attenuation above the cutoff frequency.

The cutoff frequency is defined as the frequency at which the amplitude response passes through the specified maximum ripple band and enters the stop band.

Other characteristics:

- Greater selectivity
- Very nonlinear phase response
- High overshoot response to step inputs

Fig. 10 - Amplitude response

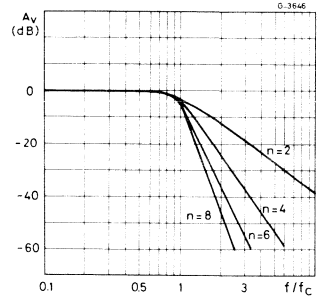


Fig. 11 - Amplitude response

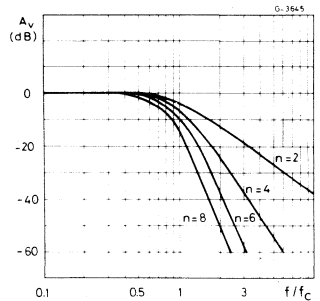
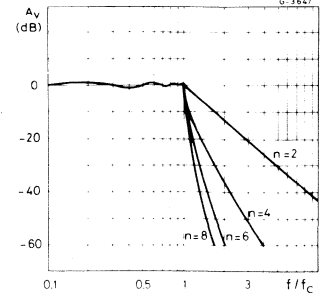


Fig. 12 - Amplitude response (± 1 dB ripple)



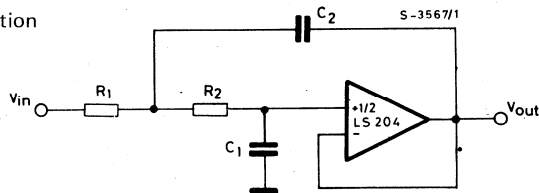
APPLICATION INFORMATION (continued)

The table below shows the typical overshoot and settling time response of the low pass filters to a step input.

	NUMBER OF POLES	PEAK OVERSHOOT	SETTLING TIME (% of final value)		
		% Overshoot	± 1%	± 0.1%	± 0.01%
BUTTERWORTH	2	4	$1.1/f_c$ sec.	$1.7/f_c$ sec.	$1.9/f_c$ sec.
	4	11	$1.7/f_c$	$2.8/f_c$	$3.8/f_c$
	6	14	$2.4/f_c$	$3.9/f_c$	$5.0/f_c$
	8	16	$3.1/f_c$	$5.1/f_c$	$7.1/f_c$
BESSEL	2	0.4	$0.8/f_c$	$1.4/f_c$	$1.7/f_c$
	4	0.8	$1.0/f_c$	$1.8/f_c$	$2.4/f_c$
	6	0.6	$1.3/f_c$	$2.1/f_c$	$2.7/f_c$
	8	0.3	$1.6/f_c$	$2.3/f_c$	$3.2/f_c$
CHEBYSCHEV (RIPPLE ± 0.25 dB)	2	11	$1.1/f_c$	$1.6/f_c$	-
	4	18	$3.0/f_c$	$5.4/f_c$	-
	6	21	$5.9/f_c$	$10.4/f_c$	-
	8	23	$8.4/f_c$	$16.4/f_c$	-
CHEBYSCHEV (RIPPLE ± 1 dB)	2	21	$1.6/f_c$	$2.7/f_c$	-
	4	28	$4.8/f_c$	$8.4/f_c$	-
	6	32	$8.2/f_c$	$16.3/f_c$	-
	8	34	$11.6/f_c$	$24.8/f_c$	-

Design of 2nd order active low pass filter (Sallen and Key configuration unity gain op-amp)

Fig. 13 - Filter configuration



$$\frac{V_o}{V_i} = \frac{1}{1 + 2\xi \frac{S}{\omega_c} + \frac{S^2}{\omega_c^2}}$$

where:

$$\omega_c = 2\pi f_c \quad \text{with } f_c = \text{cutoff frequency}$$

ξ = damping factor.

APPLICATION INFORMATION (continued)

Three parameters are needed to characterise the frequency and phase response of a 2nd order active filter: the gain (G_V), the damping factor (ξ) or the Q-factor ($Q = (2\xi)^{-1}$), and the cutoff frequency (f_c).

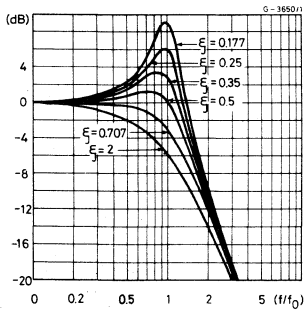
The higher order responses are obtained with a series of 2nd order sections. A simple RC section is introduced when an odd filter is required.

The choice of ' ξ ' (or Q-factor) determines the filter response (see table).

Tab. I

Filter response	ξ	Q	Cutoff frequency f_c
Bessel	$\frac{\sqrt{3}}{2}$	$\frac{1}{\sqrt{3}}$	Frequency at which phase shift is -90°
Butterworth	$\frac{\sqrt{2}}{2}$	$\frac{1}{\sqrt{2}}$	Frequency at which $G_V = -3$ dB
Chebyshev	$< \frac{\sqrt{2}}{2}$	$> \frac{1}{\sqrt{2}}$	Frequency at which the amplitude response passes through specified max. ripple band and enters the stop band

Fig. 14 - Filter response vs. damping factor



Fixed $R = R_1 = R_2$, we have (see fig. 13)

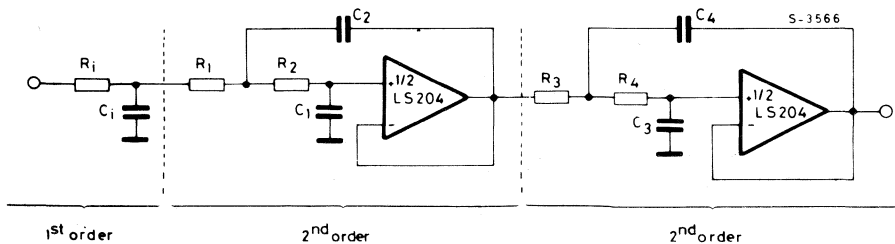
$$C_1 = \frac{1}{R} \frac{\xi}{\omega_c}$$

$$C_2 = \frac{1}{R} \frac{1}{\xi \omega_c}$$

The diagram of fig. 14 shows the amplitude response for different values of damping factor ξ in 2nd order filters.

EXAMPLE:

Fig. 15 - 5th order low pass filter (Butterworth) with unity gain configuration.



LS 204 LS 204A LS 204C

APPLICATION INFORMATION (continued)

In the circuit of fig. 15, for $f_c = 3.4$ KHz and $R_1 = R_2 = R_3 = R_4 = 10$ K Ω , we obtain:

$$C_1 = 1.354 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 6.33 \text{ nF}$$

$$C_1 = 0.421 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 1.97 \text{ nF}$$

$$C_2 = 1.753 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 8.20 \text{ nF}$$

$$C_3 = 0.309 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 1.45 \text{ nF}$$

$$C_4 = 3.325 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 15.14 \text{ nF}$$

The attenuation of the filter is 30 dB at 6.8 KHz and better than 60 dB at 15 KHz.

The same method, referring to Tab. II and fig. 16, is used to design high-pass filter. In this case the damping factor is found by taking the reciprocal of the numbers in Tab. II. For $f_c = 5$ KHz and $C_1 = C_2 = C_3 = C_4 = 1$ nF we obtain:

$$R_1 = \frac{1}{1.354} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 23.5 \text{ K}\Omega$$

$$R_1 = \frac{1}{0.421} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 75.6 \text{ K}\Omega$$

$$R_2 = \frac{1}{1.753} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 18.2 \text{ K}\Omega$$

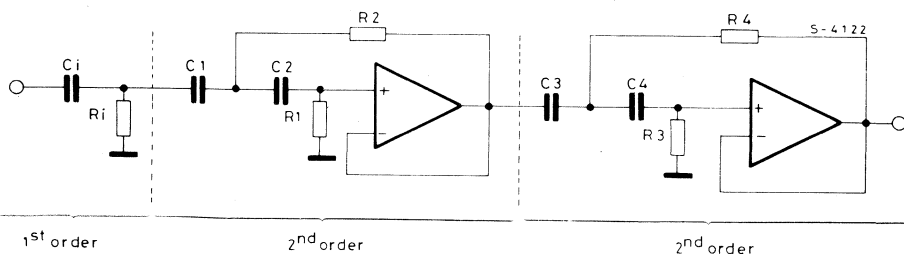
$$R_3 = \frac{1}{0.309} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 103 \text{ K}\Omega$$

$$R_4 = \frac{1}{3.325} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 9.6 \text{ K}\Omega$$

Tab. II
Damping factor for low-pass Butterworth filters

Order	C ₁	C ₁	C ₂	C ₃	C ₄	C ₅	C ₆	C ₇	C ₈
2		0.707	1.41						
3	1.392	0.202	3.54						
4		0.92	1.08	0.38	2.61				
5	1.354	0.421	1.75	0.309	3.235				
6		0.966	1.035	0.707	1.414	0.259	3.86		
7	1.336	0.488	1.53	0.623	1.604	0.222	4.49		
8		0.98	1.02	0.83	1.20	0.556	1.80	0.195	5.125

Fig. 16 - 5th order high-pass filter (Butterworth) with unity gain configuration.



LINEAR INTEGRATED CIRCUITS

TELEPHONE SPEECH CIRCUITS

The LS285 and LS285A are monolithic integrated circuits for replacement of the hybrid (2-4 line interface) in conventional telephones, interfacing the two transducers to the line and providing a controlled amount of sidetone.

The same type of transducer can be used for both transmitter and receiver, usually a 350Ω dynamic type.

By sensing the line current, LS285 and LS285A adjust the gain in both directions to compensate for line attenuation.

Output impedance can be matched to the line, independent of transducer impedance.

The LS285 and LS285A are packaged in a 14 lead dual in-line plastic package.

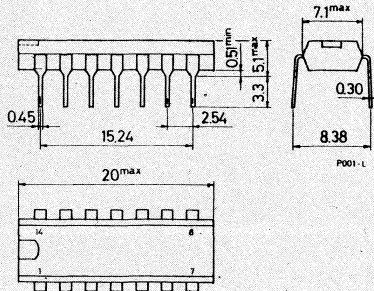
ABSOLUTE MAXIMUM RATINGS

V_L	Line voltage (3 ms pulse duration)	22	V
I_L	Forward current	120	mA
I_{Lr}	Reverse current	-150	mA
T_{stg}	Storage and junction temperature	-55 to 150	$^{\circ}\text{C}$
T_{op}	Operating temperature	-40 to 70	$^{\circ}\text{C}$

ORDERING NUMBERS: LS285 B
LS285 AB

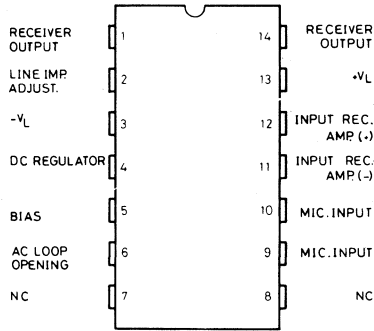
MECHANICAL DATA

Dimensions in mm



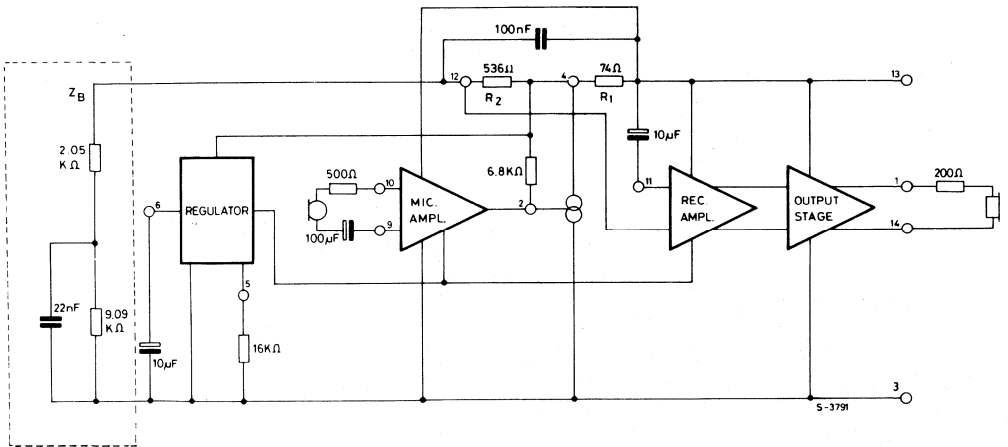
LS 285 LS 285 A

CONNECTION DIAGRAM (top view)



5-4029

BLOCK DIAGRAM



5-3791

LS 285 LS 285A

DESCRIPTION

The LS285 and the LS285A are based on a bridge configuration. They contain a regulator block, a sending amplifier and a receiver amplifier.

The regulator monitors the line current and adjusts the amplifier gain to compensate for the line length. It provides DC characteristics in line with CEPT standards.

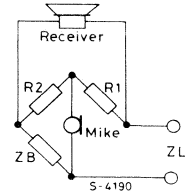
The transmit/receiver amplifiers are connected to the line via an external bridge to provide sidetone attenuation.

The line current compensation ensures that when the subscriber is talking, the signal delivered to the line is increased in according to line length. When he is hearing, the signal level on the receiver capsule is constant.

The amplifiers can also be matched to different transducers simply by varying external components. Gain variation over the operating temperature range is less than ± 1 dB.

The impedance to the line can be adjusted—without any change in circuit parameters—by changing an external resistor (6.8 K Ω at pin 2).

Basic circuit configuration



THERMAL DATA

$R_{th\ j-amb}$	Thermal resistance junction ambient	max	80	$^{\circ}\text{C/W}$
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ELECTRICAL CHARACTERISTICS (Refer to the test circuits, $T_{amb} = -15$ to $+45$ $^{\circ}\text{C}$; $f = 200$ to 3400 Hz unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig.
V_L Terminal voltage	$I_L = 80$ mA $I_L = 20$ mA $I_L = 10$ mA	10 5 3.8		11.5 5.8 4.6	V V V	1
G_S Sending gain	$f = 1$ KHz $T_{amb} = 25^{\circ}\text{C}$ $R_L = 0$ LS285 $R_L = 800$ Ω $R_L = 2.2$ K Ω $I_L = 80$ mA	41		43	dB	2
		46.5		48.5	dB	
		46.5		49.5	dB	
		40		43	dB	
	$R_L = 0$ LS285A $R_L = 800$ Ω $R_L = 2.2$ K Ω $I_L = 80$ mA	40.7		44.1	dB	2
		45.4		49.5	dB	
		46.5		50.5	dB	
		40		43.3	dB	
ΔG_S Sending gain variation	Refer to the value at $T_{amb} = 25^{\circ}\text{C}$			± 1	dB	2

LS 285 LS 285A

ELECTRICAL CHARACTERISTICS (continued)

Parameter		Test conditions	Min.	Typ.	Max.	Unit	Fig.
G _R	Receiving gain	f = 1 KHz T _{amb} = 25°C R _L = 0 LS285 R _L = 800 Ω R _L = 2.2 KΩ I _L = 80 mA	-18		-16	dB	3
			-13		-11	dB	
			-13		-10	dB	
			-19		-16	dB	
		LS285A R _L = 0 R _L = 800 Ω R _L = 2.2 KΩ I _L = 80 mA	-18		-14.9	dB	3
			-13.6		-10.6	dB	
			-13		-9.9	dB	
			-19		-16	dB	
ΔG _R	Receiving gain variation	Refer to the value at T _{amb} = 25°C			± 1	dB	3
	Side tone	f = 1 KHz T _{amb} = 25°C R _L = 0 R _L = 800 Ω		-7 -28		dB dB	2-4
	G _{IS01} -(G _{S1} + G _{R1}) G _{IS02} -(G _{S2} + G _{R2})						
	Sending noise	R _L = 0 E ₁ = 0 psophometric			-67	dB	2
	Receiving noise	R _L = 0 E ₂ = 0			-80	dB	3
	Sending gain flatness	R _L = 0 f _{ref} = 1KHz	-0.5		+0.5	dB	2
	Receiving gain flatness	R _L = 0 f _{ref} = 1KHz	-0.5		+0.5	dB	3
	Sending distortion	I _L = 10 to 15 mA V ₁ = 0.7 Vp I _L = 15 to 80 mA V ₁ = 1.5 Vp			2 2	% %	2
	Receiving distortion	I _L = 10 to 15 mA V ₂ = 350 mVp I _L = 15 to 80 mA (LS285) V ₂ = 600 mVp			2 2	% %	3
		I _L = 15 to 80 mA V ₂ = 500 mVp (LS285A)			2	%	
	Max sending output (°)	I _L = 10 to 80 mA E ₁ = 1V			3	Vp	2
	Max receiving output (°)	I _L = 10 to 80 mA E ₂ = 10V			0.8	Vp	3
Z _L	Output impedance	I _L = 10 to 80 mA f = 1 KHz	540		740	Ω	5
Z _{MIC}	Microphone amplifier input impedance	R _L = 0	R ₆ +R ₇ +45		R ₆ +R ₇ +85	Ω	1-6
Z _{RE}	Receiver amplifier output impedance	R _L = 0	R ₉ +R ₁₀ +60		R ₉ +R ₁₀ +100	Ω	1-7

(°) These outputs are limited to allow for input overvoltage.

LS 285 LS 285A

Fig. 1 - Application and test circuit.

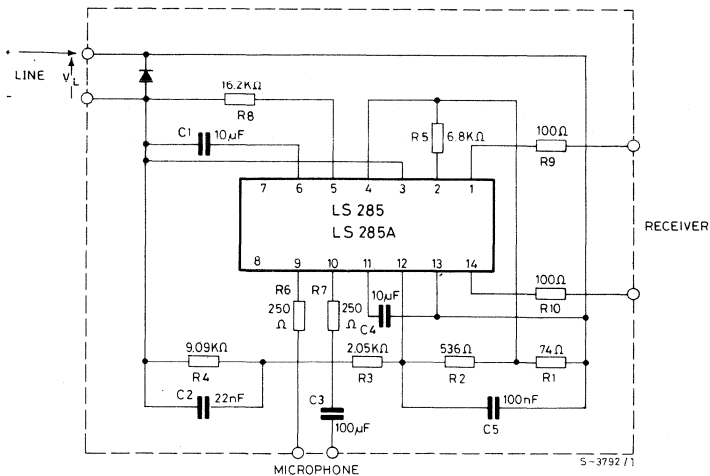


Fig. 2 - Sending gain test

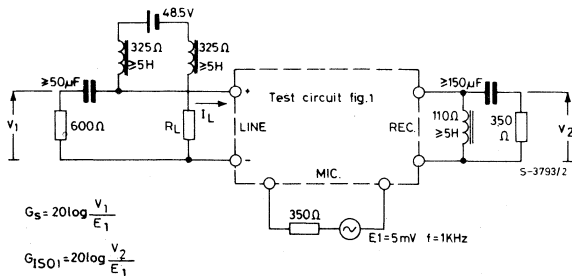
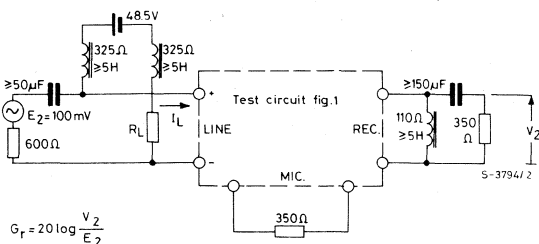


Fig. 3 - Receiving test



LS 285 LS 285A

Fig. 4 - Sidetone test

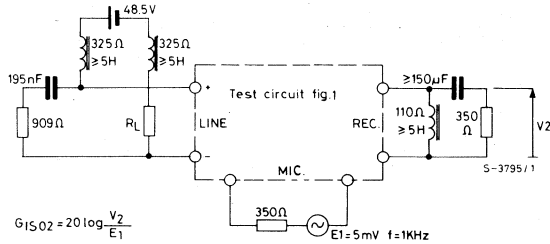


Fig. 5 - Output impedance test

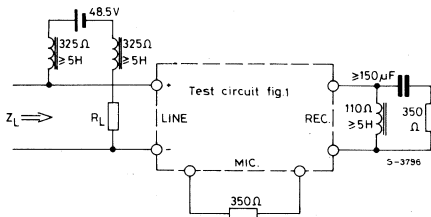


Fig. 6 - Input impedance test

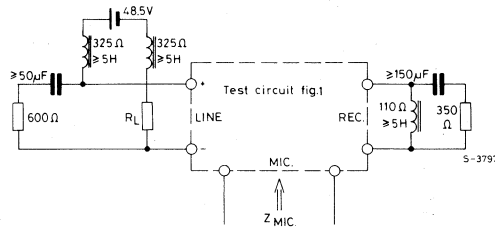


Fig. 7 - Receiving output impedance test

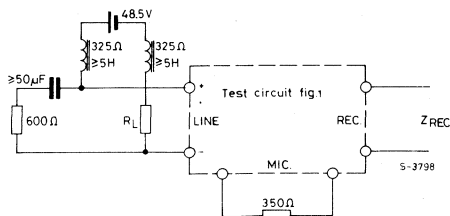
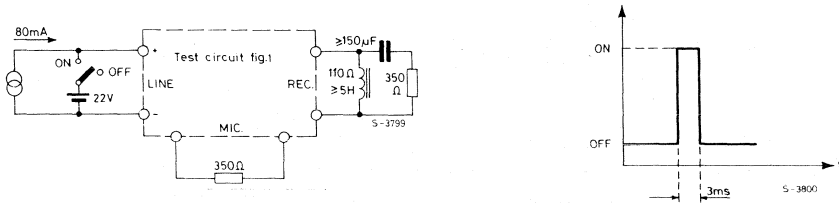


Fig. 8 - Electric transient test



APPLICATION INFORMATION

The table shows the recommended values for the typical application circuit (fig. 1)

Component	Recommended value	Purpose	Note
R1	74 Ω	Bridge resistors	The ratio R2/R1 fixes the amount of signal delivered to the line.
R2	536 Ω		
R3	2.05 KΩ	Balance network (see block diagram)	In order to optimize the sidetone it is possible to change R3 and R4 values. In any case: $\frac{Z_B}{Z_L} = \frac{R2}{R1}$ where $Z_B = R3 + R4 // C2$.
R4	9.09 KΩ		
R5	6.8 KΩ	Line impedance adjustment	$Z_L = \left[\frac{R5}{11} // (R2 + Z_B) \right] + R1$ This approximates to: $Z_L \cong \frac{R5}{11}$.
R6 and R7	250 Ω	Microphone impedance matching	R6 and R7 must be equal; 250 Ω is a typical value for dynamic microphones (°).
R8	16.2 KΩ	Bias resistor (see fig. 9)	Changing R8 value it is possible to shift the gain characteristics. The value can be chosen from 15 KΩ to 20 KΩ. The recommended value assures the maximum output swing.
R9 and R10	100 Ω	Receiver impedance matching	R9 and R10 must be equal; 100 Ω is a typical value for dynamic receivers (°).
C1	10 μF	AC loop opening	Ensures a high regulator impedance for AC signals ($\cong 20$ KΩ). This capacitor should not be higher than 10 μF in order to have a short response time of the system.

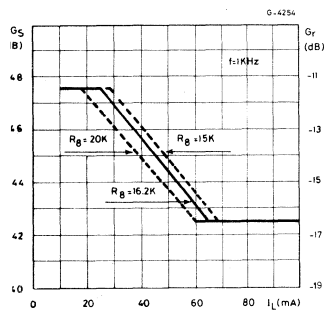
(°) The dynamic microphone and receiver capsules can have an impedance in a range of $\pm 20\%$ of this nominal value. The resistors R6/R7 and R9/R10 should be modified to match the capsule employed.

LS 285 LS 285A

APPLICATION INFORMATION (continued)

Component	Recommended value	Purpose	Note
C2	22 nF	Balance network	See note for R3 and R4.
C3	100 μ F	DC decoupling for mike input	
C4	10 μ F	DC decoupling for receiving input.	
C5	100 nF	RF filter.	

Fig. 9 - Sending and receiving gain vs. line current



LINEAR INTEGRATED CIRCUIT

MULTIFREQUENCY TO TELEPHONE LINE INTERFACE CIRCUIT

The LS342 is a monolithic integrated circuit in dual in-line minidip plastic package. It interfaces the multifrequency tone dialler M751 to the line in telephone sets, performing the following functions:

- Adjustment of the DC current/voltage characteristic and AC input line impedance by means of an external resistor (R_E).
- Sending to the line of the multifrequency signal.
- Adjustment of the signal level by means of an external resistor (R_T).
- Stabilized supply voltage to the M751.

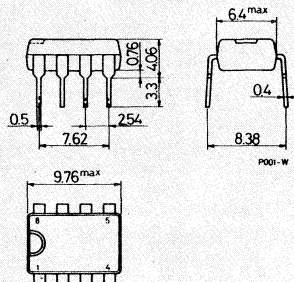
ABSOLUTE MAXIMUM RATINGS

V_L	Maximum line voltage (pulse duration ≤ 10 ms)	22	V
I_L	Maximum forward current	155	mA
I_L	Maximum reverse current	-150	mA
T_{op}	Operating temperature	-40 to 70	$^{\circ}C$
T_{stg}, T_j	Storage and junction temperature	-55 to 150	$^{\circ}C$

ORDERING NUMBER: LS342B

MECHANICAL DATA

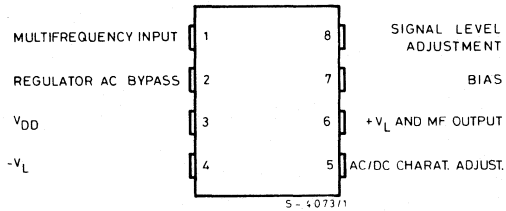
Dimension in mm



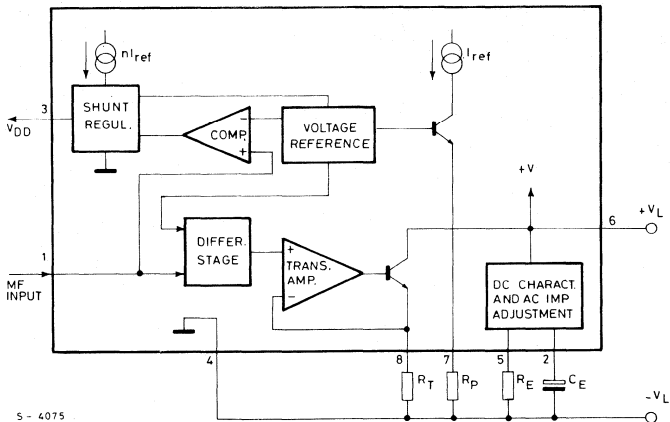
LS 342

CONNECTION DIAGRAM

(Top view)



BLOCK DIAGRAM



DESCRIPTION

The LS342 interfaces the M751 with the telephone line. Power is only applied to the system when the handset is lifted and a key pressed. At this time, S1 is also switched (see fig. 1) disconnecting the speech circuit from the line and connecting the dialling circuit.

In the dialling condition the LS342 performs 3 functions:

- 1) D.C. and A.C. line termination
- 2) M751 power supply
- 3) Amplification and transmission of tone pairs.

In the initial stage of switch-on the supply voltage V_{DD} is regulated at $\cong 4$ volt. This overdrives the M751 oscillator causing a rapid start-up and therefore rapid generation of output tones. When the system reaches its normal operating point the supply voltage V_{DD} is stabilized at $2.5V \pm 4\%$.

LS 342

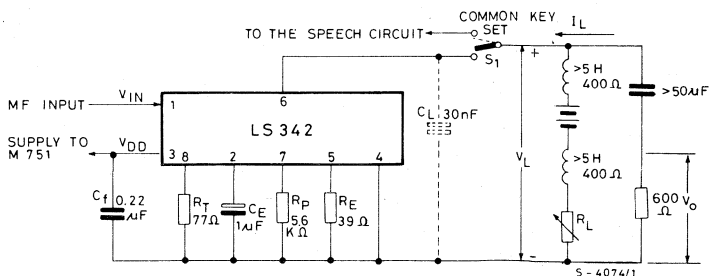
THERMAL DATA

$R_{thj-amb}$	Thermal resistance junction-ambient	max 100 °C/W
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ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $T_{amb} = -15$ to $+45^{\circ}\text{C}$; $f = 300$ to 3400 Hz, unless otherwise specified).

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_L Line voltage (pins 6-4)	$R_E = 39\ \Omega$ $I_L = 8\text{mA}$ $I_L = 17\text{mA}$ $I_L = 60\text{mA}$ $I_L = 150\text{mA}$		4.2 4.6 6.4 10.2	4.5 5 7 11.5	V V V V
Max output level (pins 6-4)	$I_L = 8$ to 17mA $f = 1$ KHz $d < 1.5\%$	1.7			V _{pp}
	$I_L = 17$ to 150mA $f = 1$ KHz $d < 1.5\%$	3.2			V _{pp}
V_{DD} Output voltage (pin 3)	$I_L = 8$ to 150mA	2.4			V
Z_o Output impedance (pins 6, 4)	$I_L = 8$ to 150mA $C_E = 1\ \mu\text{F}$ $R_E = 39\ \Omega$		900		Ω
Z_i Input impedance (pin 1)	$I_L = 8$ to 150mA		5		M Ω
Multifrequency output level (pin 6)	$R_T = 77\ \Omega$	Low tones	770		mV _{pp}
		High tones	980		mV _{pp}
I_{DD} Supply current from V_{DD} (pin 3)	$I_L \geq 8\ \text{mA}$ $V_{3-4} = 2.5\text{V}$	2			mA

Fig. 1 - Test circuit



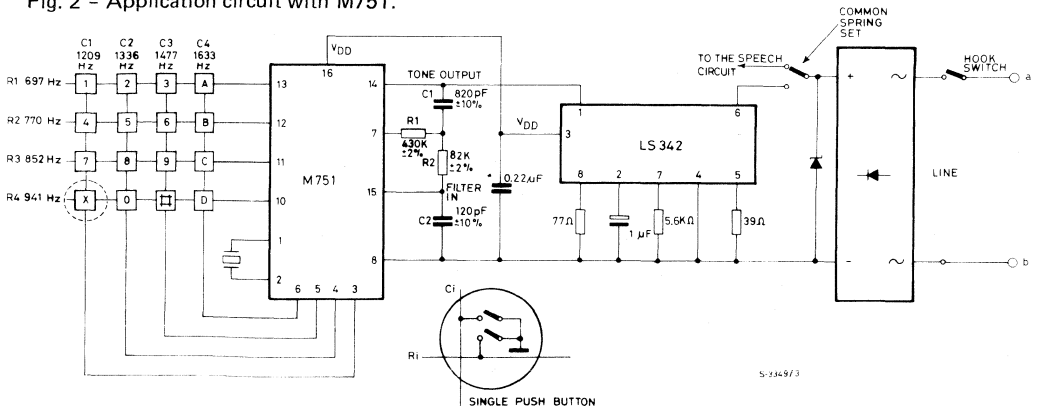
LS 342

APPLICATION INFORMATION

The table shows the recommended values for the circuit of fig. 1.

Component	Recomm. value	Purpose	Note
R_E	39 Ω	DC characteristic AC impedance adjustment	The relationships involving R_E are: <ul style="list-style-type: none"> $V_L = (I_L - I_o) R_E + V_o$ where $I_o \cong 6 \text{ mA}$ $V_o \cong 4 \text{ V}$ $Z_o = 23R_E$ ($f = 1 \text{ KHz}$) R_E must be greater than 27 Ω
R_p	5.6 K Ω	Bias resistor	R_p can be reduced in order to increase the output current from pin 3 (V_{DD}). In this case, the total current consumption is increased.
R_T	77 Ω	Signal level adjustment	The gain is: $G_{MF} = (Z_L/Z_o)/R_T$ R_T can have a range of $\pm 20\%$. At the lower values, the line current is increased of about 0.6 mA.
C_E	1 μF	Regulator AC bypass	A value greater than 1 μF gives a system start time too high when line current is between 8 mA and 17 mA. A value less than 1 μF gives an alteration of the AC line impedance because its reactance is not negligible at low frequencies.
C_f	0.22 μF	DC filtering	The C_f range is from 0.1 μF to 0.47 μF . The lowest values is ripple limited, the higher values is starting up time limited.
C_L	30 nF	Matching to a capacitive line	This is needed with a capacitive line because the output impedance of the LS342 is essentially resistive. The range of C_L is between 30 and 60 nF.

Fig. 2 - Application circuit with M751.



S-2469/3

LINEAR INTEGRATED CIRCUITS

LS 404 LS 404C

HIGH PERFORMANCE QUAD OPERATIONAL AMPLIFIER

- SINGLE OR SPLIT SUPPLY OPERATION
- VERY LOW POWER CONSUMPTION
- SHORT CIRCUIT PROTECTION
- LOW DISTORTION, LOW NOISE
- HIGH GAIN-BANDWIDTH PRODUCT
- HIGH CHANNEL SEPARATION

The LS 404 is a high performance quad operational amplifier with frequency and phase compensation built into the chip. The internal phase compensation allows stable operation as voltage follower in spite of its high gain-bandwidth product. The circuit presents very stable electrical characteristics over the entire supply voltage range, and it is particularly intended for professional and telecom applications (active filters, etc.).

The patented input stage circuit allows small input signal swings below the negative supply voltage and prevents phase inversion when the input is over driven.

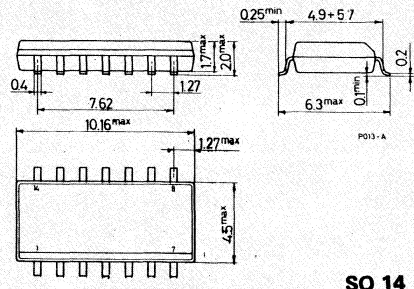
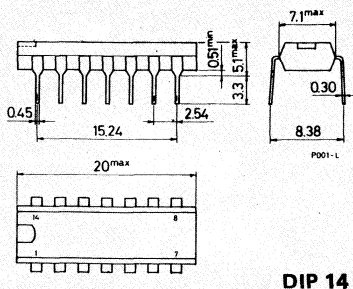
The LS 404 is available with hermetic gold chip (8000 series).

ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage		± 18	V
V_i	Input voltage	(positive)	$+ V_s$	
		(negative)	$-V_s - 0.5$	V
V_i	Differential input voltage		$\pm (V_s - 1)$	
T_{op}	Operating temperature	LS 404	-25 to + 85	°C
		LS 404C	0 to + 70	°C
P_{tot}	Power dissipation	($T_{amb} = 70^\circ\text{C}$)	400	mW
T_{stg}	Storage temperature		-55 to + 150	°C

MECHANICAL DATA

Dimensions in mm

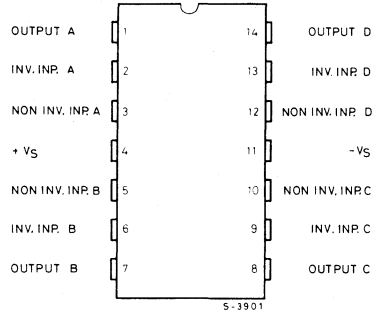


LS 404 LS 404C

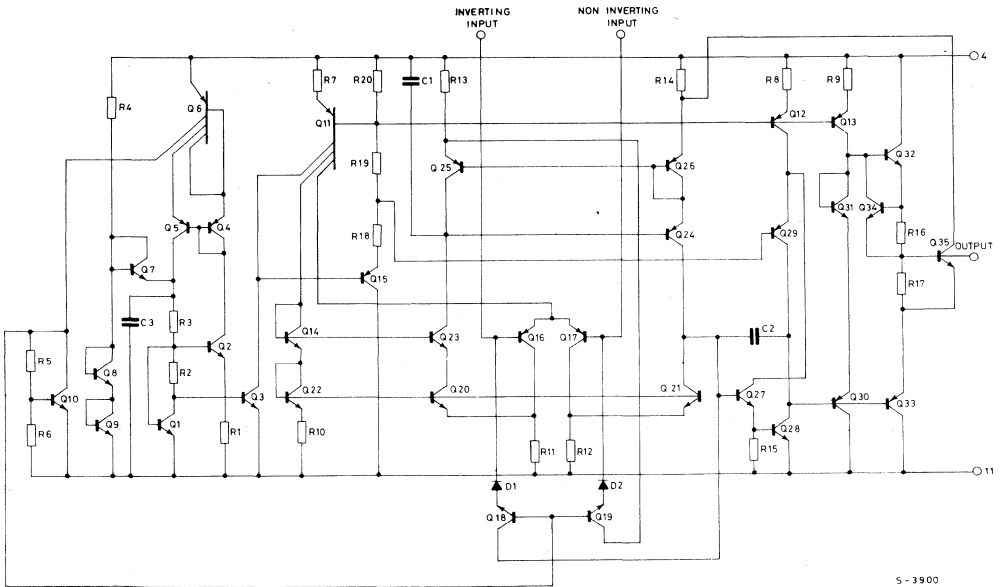
CONNECTION DIAGRAM AND ORDERING NUMBERS

(top view)

Type	DIP 14	SO-14
LS 404 LS 404C	— LS 404CB	LS 404M LS 404CM
LS 8404 LS 8404C	— —	LS 8404M LS 8404CM



SCHEMATIC DIAGRAM (one section)



THERMAL DATA

			DIP 14	SO-14
$R_{thj-amb}$	Thermal resistance junction-ambient	max	200°C/W	200°C/W*

(*) Measured with the device mounted on a ceramic substrate (25 x 16 x 0.6 mm.)

ELECTRICAL CHARACTERISTICS $(V_s = \pm 12V, T_{amb} = 25^\circ C, \text{ unless otherwise specified})$

Parameter	Test conditions	LS 404			LS 404C			Unit
		Min.	Typ.	Max.	Min.	Typ.	Max.	
I_s	Supply current		1.3	2		1.5	3	mA
I_b	Input bias current		50	200		100		nA
R_i	Input resistance	$f = 1\text{KHz}$	0.7			0.5		M Ω
V_{os}	Input offset voltage	$R_g = 10\text{K}\Omega$	1			1		mV
$\frac{\Delta V_{os}}{\Delta T}$	Input offset voltage drift	$R_g = 10\text{K}\Omega$ $T_{min} < T_{op} < T_{max}$	5			5		$\mu\text{V}/^\circ\text{C}$
I_{os}	Input offset current		10	40		20		nA
$\frac{\Delta I_{os}}{\Delta T}$	Input offset current drift	$T_{min} < T_{op} < T_{max}$	0.08			0.1		$\frac{\text{nA}}{^\circ\text{C}}$
I_{sc}	Output short circuit current		23			23		mA
G_v	Large signal open loop voltage gain	$R_L = 2\text{K}\Omega$ $V_s = \pm 12\text{V}$ $V_s = \pm 4\text{V}$	90	100 95		86	100 95	dB
B	Gain-bandwidth product	$f = 20\text{KHz}$	1.8	3		1.5	2.5	MHz
e_N	Total input noise voltage	$f = 1\text{KHz}$ $R_g = 50\Omega$ $R_g = 1\text{K}\Omega$ $R_g = 10\text{K}\Omega$		8 10 18	15		10 12 20	$\frac{\text{nV}}{\sqrt{\text{Hz}}}$
d	Distortion	unity gain $R_L = 2\text{K}\Omega$ $V_o = 2\text{Vpp}$	$f = 1\text{KHz}$ $f = 20\text{KHz}$	0.01 0.03	0.04		0.01 0.03	%
V_o	DC output voltage swing	$R_L = 2\text{K}\Omega$	$V_s = \pm 12\text{V}$ $V_s = \pm 4\text{V}$	± 10 ± 3		± 10	± 3	V
V_o	Large signal voltage swing	$f = 10\text{KHz}$	$R_L = 10\text{K}\Omega$ $R_L = 1\text{K}\Omega$	22 20			22 20	Vpp
SR	Slew rate	unity gain $R_L = 2\text{K}\Omega$		0.8	1.5		1	V/ μs
CMR	Comm. mode rejection	$V_i = 10\text{V}$		94			90	dB
SVR	Supply voltage rejection	$V_i = 1\text{V}$ $f = 100\text{Hz}$		94			90	dB
CS	Channel separation	$f = 1\text{KHz}$		100	120		120	dB

LS 404 LS 404C

Fig. 1 - Supply current vs. supply voltage

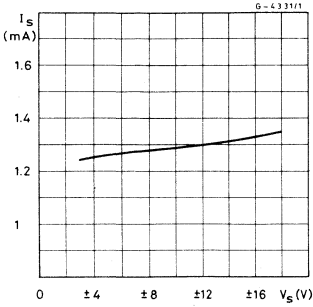


Fig. 2 - Supply current vs. ambient temperature

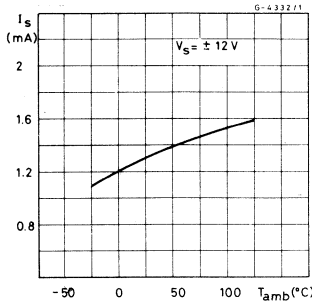


Fig. 3 - Output short circuit current vs. ambient temperature

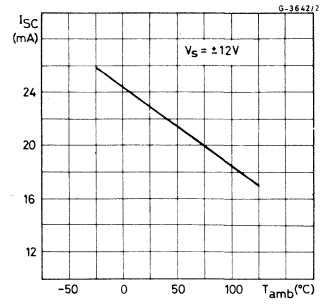


Fig. 4 - Open loop frequency and phase response

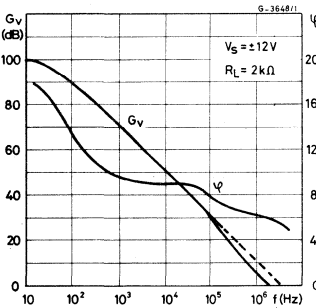


Fig. 5 - Open loop gain vs. ambient temperature

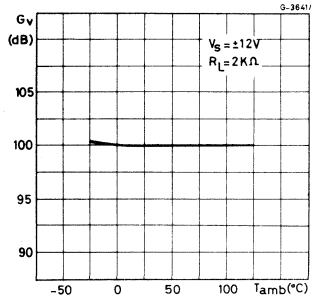


Fig. 6 - Supply voltage rejection vs. frequency

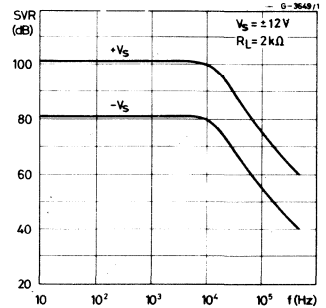


Fig. 7 - Large signal frequency response

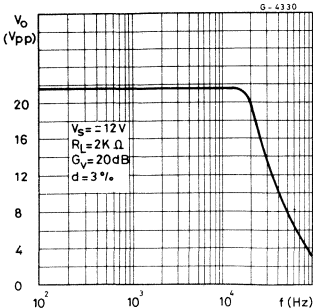


Fig. 8 - Output voltage swing vs. load resistance

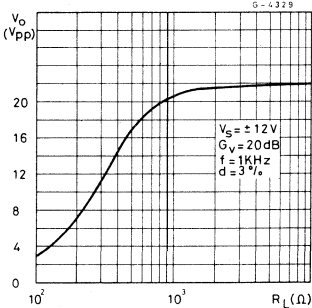
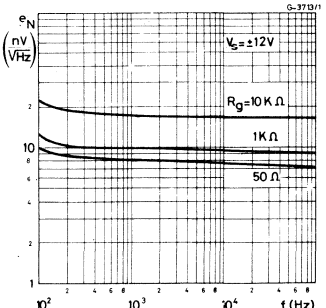


Fig. 9 - Total input noise vs. frequency



APPLICATION INFORMATION

Active low-pass filter:

BUTTERWORTH

The Butterworth is a "maximally flat" amplitude response filter. Butterworth filters are used for filtering signals in data acquisition systems to prevent aliasing errors in sampled-data applications and for general purpose low-pass filtering.

The cutoff frequency, f_c , is the frequency at which the amplitude response is down 3 dB. The attenuation rate beyond the cutoff frequency is -6 dB per octave of frequency where n is the order (number of poles) of the filter.

Other characteristics:

- Flattest possible amplitude response.
- Excellent gain accuracy at low frequency end of passband.

BESSEL

The Bessel is a type of "linear phase" filter. Because of their linear phase characteristics, these filters approximate a constant time delay over a limited frequency range. Bessel filters pass transient waveforms with a minimum of distortion. They are also used to provide time delays for low pass filtering of modulated waveforms and as a "running average" type filter.

The maximum phase shift is $\frac{-n\pi}{2}$ radians where n is the order (number of poles) of the filter. The cutoff frequency, f_c , is defined as the frequency at which the phase shift is one half to this value. For accurate delay, the cutoff frequency should be twice the maximum signal frequency. The following table can be used to obtain the -3 dB frequency of the filter.

	2 pole	4 pole	6 pole	8 pole
-3 dB frequency	$0.77 f_c$	$0.67 f_c$	$0.57 f_c$	$0.50 f_c$

Other characteristics:

- Selectivity not as great as Chebyshev or Butterworth.
- Very small overshoot response to step inputs
- Fast rise time.

CHEBYSHEV

Chebyshev filters have greater selectivity than either Bessel or Butterworth at the expense of ripple in the passband.

Chebyshev filters are normally designed with peak-to-peak ripple values from 0.2 dB to 2 dB.

Increased ripple in the passband allows increased attenuation above the cutoff frequency.

The cutoff frequency is defined as the frequency at which the amplitude response passes through the specified maximum ripple band and enters the stop band.

Other characteristics:

- Greater selectivity
- Very nonlinear phase response
- High overshoot response to step inputs.

Fig. 10 - Amplitude response

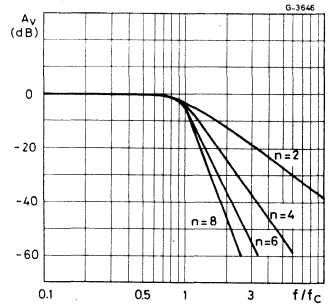


Fig. 11 - Amplitude response

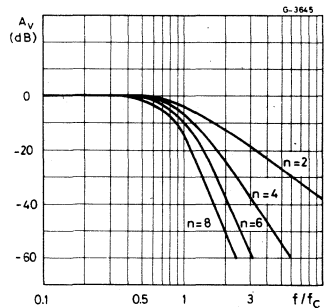
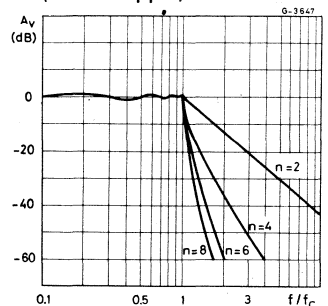


Fig. 12 - Amplitude response (± 1 dB ripple)



LS 404 LS 404C

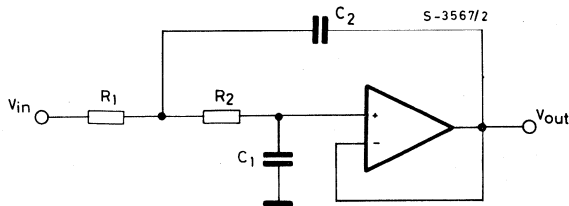
APPLICATION INFORMATION (continued)

The table below shows the typical overshoot and settling time response of the low pass filter to a step input.

	NUMBER OF POLES	PEAK OVERSHOOT	SETTLING TIME (% of final value)		
		% Overshoot	± 1%	± 0.1%	± 0.01%
BUTTERWORTH	2	4	$1.1/f_c$ sec.	$1.7/f_c$ sec.	$1.9/f_c$ sec.
	4	11	$1.7/f_c$	$2.8/f_c$	$3.8/f_c$
	6	14	$2.4/f_c$	$3.9/f_c$	$5.0/f_c$
	8	16	$3.1/f_c$	$5.1/f_c$	$7.1/f_c$
BESSEL	2	0.4	$0.8/f_c$	$1.4/f_c$	$1.7/f_c$
	4	0.8	$1.0/f_c$	$1.8/f_c$	$2.4/f_c$
	6	0.6	$1.3/f_c$	$2.1/f_c$	$2.7/f_c$
	8	0.3	$1.6/f_c$	$2.3/f_c$	$3.2/f_c$
CHEBYSCHEV (RIPPLE ± 0.25 dB)	2	11	$1.1/f_c$	$1.6/f_c$	—
	4	18	$3.0/f_c$	$5.4/f_c$	—
	6	21	$5.9/f_c$	$10.4/f_c$	—
	8	23	$8.4/f_c$	$16.4/f_c$	—
CHEBYSCHEV (RIPPLE ± 1 dB)	2	21	$1.6/f_c$	$2.7/f_c$	—
	4	28	$4.8/f_c$	$8.4/f_c$	—
	6	32	$8.2/f_c$	$16.3/f_c$	—
	8	34	$11.6/f_c$	$24.8/f_c$	—

Design of 2nd order active low pass filter (Sallen and Key configuration unity gain op-amp)

Fig. 13 - Filter configuration



$$\frac{V_o}{V_i} = \frac{1}{1 + 2\xi \frac{S}{\omega_c} + \frac{S^2}{\omega_c^2}}$$

where:

$$\omega_c = 2\pi f_c \quad \text{with } f_c = \text{cutoff frequency}$$

ξ = damping factor.

APPLICATION INFORMATION (continued)

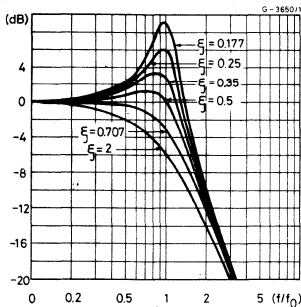
Three parameters are needed to characterize the frequency and phase response of a 2nd order active filter: the gain (G_V), the damping factor (ξ) or the Q-factor ($Q = (2\xi)^{-1}$), and the cutoff frequency (f_c).

The higher order responses are obtained with a series of 2nd order sections. A simple RC section is introduced when an odd filter is required. The choice of ' ξ ' (or Q-factor) determines the filter response (see table).

TAB. 1

Filter response	ξ	Q	Cutoff frequency f_c
Bessel	$\frac{\sqrt{3}}{2}$	$\frac{1}{\sqrt{3}}$	Frequency at which phase shift is -90°
Butterworth	$\frac{\sqrt{2}}{2}$	$\frac{1}{\sqrt{2}}$	Frequency at which $G_V = -3$ dB
Chebyshev	$\left\langle \frac{\sqrt{2}}{2} \right\rangle$	$\left\langle \frac{1}{\sqrt{2}} \right\rangle$	Frequency at which the amplitude response passes through specified max. ripple band and enters the stop band

Fig. 14 - Filter response vs. damping factor



Fixed $R = R_1 = R_2$, we have (see fig. 13)

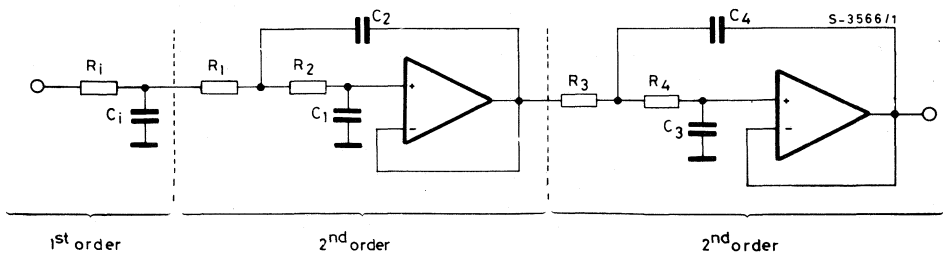
$$C_1 = \frac{1}{R} \frac{\xi}{\omega_c}$$

$$C_2 = \frac{1}{R} \frac{1}{\xi \omega_c}$$

The diagram of fig. 14 shows the amplitude response for different values of damping factor ξ in 2nd order filters.

EXAMPLE:

Fig. 15 - 5th order low pass filter (Butterworth) with unity gain configuration.



LS 404 LS 404C

APPLICATION INFORMATION (continued)

In the circuit of fig. 15, for $f_c = 3.4$ KHz and $R_i = R_1 = R_2 = R_3 = R_4 = 10$ K Ω , we obtain:

$$C_i = 1.354 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 6.33 \text{ nF}$$

$$C_1 = 0.421 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 1.97 \text{ nF}$$

$$C_2 = 1.753 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 8.20 \text{ nF}$$

$$C_3 = 0.309 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 1.45 \text{ nF}$$

$$C_4 = 3.325 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 15.14 \text{ nF}$$

The attenuation of the filter is 30 dB at 6.8 KHz and better than 60 dB at 15 KHz.

The same method, referring to Tab. II and fig. 16, is used to design high-pass filter. In this case the damping factor is found by taking the reciprocal of the numbers in Tab. II. For $f_c = 5$ KHz and $C_i = C_1 = C_2 = C_3 = C_4 = 1$ nF we obtain:

$$R_i = \frac{1}{1.354} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 23.5 \text{ K}\Omega$$

Tab. II
Damping factor for low-pass Butterworth filters

Order	C _i	C ₁	C ₂	C ₃	C ₄	C ₅	C ₆	C ₇	C ₈
2		0.707	1.41						
3	1.392	0.202	3.54						
4		0.92	1.08	0.38	2.61				
5	1.354	0.421	1.75	0.309	3.235				
6		0.966	1.035	0.707	1.414	0.259	3.86		
7	1.336	0.488	1.53	0.623	1.604	0.222	4.49		
8		0.98	1.02	0.83	1.20	0.556	1.80	0.195	5.125

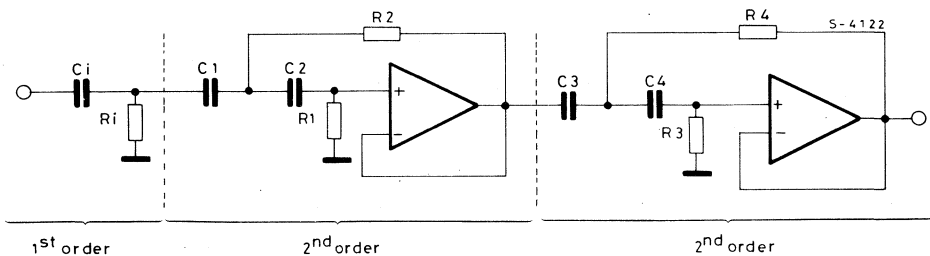
$$R_1 = \frac{1}{0.421} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 75.6 \text{ K}\Omega$$

$$R_2 = \frac{1}{1.753} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 18.2 \text{ K}\Omega$$

$$R_3 = \frac{1}{0.309} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 103 \text{ K}\Omega$$

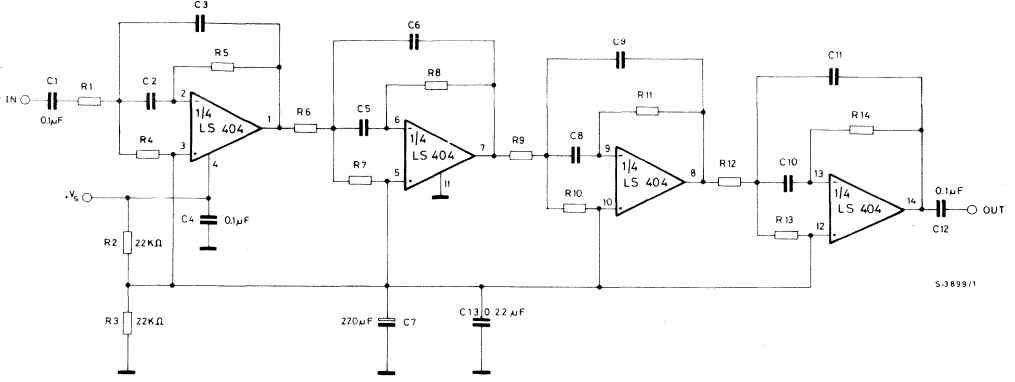
$$R_4 = \frac{1}{3.325} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 9.6 \text{ K}\Omega$$

Fig. 16 - 5th order high-pass filter (Butterworth) with unity gain configuration.



APPLICATION INFORMATION (continued)

Fig. 17 - Multiple feedback 8-pole bandpass filter.



$f_c = 1.180\text{Hz}$; $A = 1$; $C_2 = C_3 = C_5 = C_6 = C_8 = C_9 = C_{10} = C_{11} = 3.300\text{ pF}$;
 $R_1 = R_6 = R_9 = R_{12} = 160\text{ K}\Omega$; $R_5 = R_8 = R_{11} = R_{14} = 330\text{K}\Omega$; $R_4 = R_7 = R_{10} = R_{13} = 5.3\text{K}\Omega$

Fig. 18 - Frequency response of band-pass filter

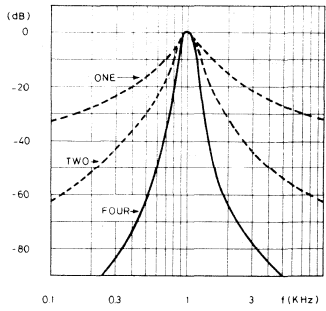
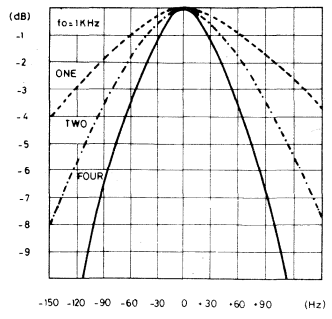


Fig. 19 - Bandwidth of band-pass filter



OPERATIONAL AMPLIFIERS

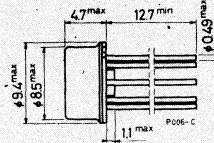
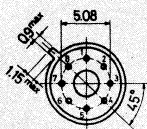
The LS 709 series features low offset, high input impedance, large input common mode range, high output voltage swing. The amplifier is intended for use in D.C. servosystems, high impedance analog computer, low level instrumentation applications, and for the generation of special linear and non linear transfer functions.

ABSOLUTE MAXIMUM RATINGS		TO-99	DIP
V_s	Supply voltage	± 18 V	
V_i (1)	Input voltage	± 10 V	
ΔV_i	Differential input voltage	± 5 V	
T_{op}	Operating temperature for LS 709/LS 709A for LS 709C	-55 to 125 °C 0 to 70 °C	
P_{tot}	Power dissipation at $T_{amb} = 70$ °C	520 mW	400 mW
T_{stg}	Storage temperature	-65 to 150 °C	-55 to 150 °C

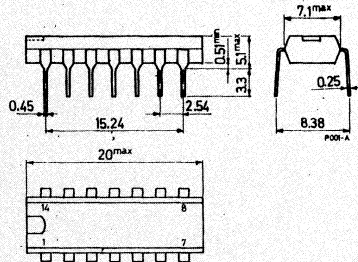
1) For supply voltages less than ± 10 V maximum input voltage is equal to the supply voltage.

MECHANICAL DATA

Dimensions in mm



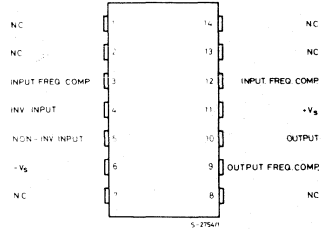
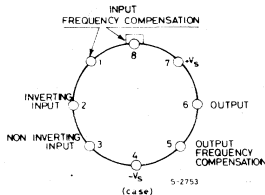
TO-99



DIP

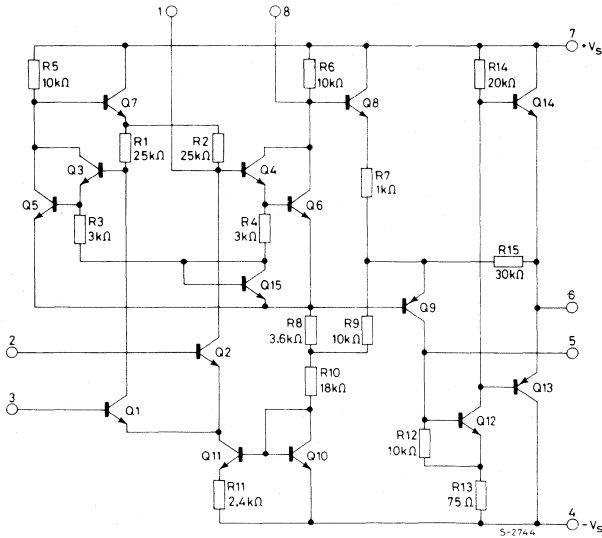
LS 709 LS 709A LS 709C

CONNECTION DIAGRAMS AND ORDERING NUMBERS (top views)



Type	TO-99	DIP
LS 709	LS 709T	—
LS 709A	LS 709 AT	—
LS 709C	LS 709 CT	LS 709 CB

SCHEMATIC DIAGRAM (pin numbers are referred to the TO-99 version)



THERMAL DATA

	TO-99	DIP
$R_{th j-amb}$ Thermal resistance junction-ambient	max	max
	155 °C/W	200 °C/W

LS 709 LS 709A LS 709C

ELECTRICAL CHARACTERISTICS (see note)

Parameter	Test conditions	LS 709A			LS 709			LS 709C			Unit	
		Min.	Typ.	Max.	Min.	Typ.	Max.	Min.	Typ.	Max.		
V_{os}	Input offset voltage	$R_g \leq 10 \text{ k}\Omega$ $R_g \leq 10 \text{ k}\Omega$ $T_{amb}=25^\circ\text{C}$		3 2		6 5		10 7.5		mV mV		
I_b	Input bias current	$T_{amb} = T_{min}$ $T_{amb} = 25^\circ\text{C}$		0.3 100	0.6 200	0.5 200	1.5 500	0.36 300	2 1500	μA nA		
I_{os}	Input offset current	$T_{amb} = T_{max}$ $T_{amb} = T_{min}$ $T_{amb} = 25^\circ\text{C}$		3.5 40 10	50 250 50	20 100 50	200 500 200	75 125 100	400 750 500	nA nA nA		
R_i	Input resistance	$T_{amb} = T_{min}$ $T_{amb} = 25^\circ\text{C}$		85 350	170 700	40 150	100 400	50 50	250 250	k Ω k Ω		
R_o	Output resistance	$T_{amb} = 25^\circ\text{C}$		150		150		150		Ω		
I_s	Supply current	$V_s = \pm 15\text{V}$ $T_{amb}=25^\circ\text{C}$		2.5	3.6	2.6	5.5	2.6	6.6	mA		
	Transient response Risetime Overshoot	$V_i = 20 \text{ mV}$ $C_L \leq 100 \text{ pF}$ $T_{amb} = 25^\circ\text{C}$			1.5 30	0.3 10	1 30	0.3 10	1 30	μs %		
SR	Slew rate	$T_{amb} = 25^\circ\text{C}$		0.25		0.25		0.25		V/ μs		
$\frac{\Delta V_{os}}{\Delta T}$	Average temperature coefficient of input offset voltage	$R_g = 50\Omega$ $T_{amb} = 25^\circ\text{C}$ to T_{max} $T_{amb} = 25^\circ\text{C}$ to T_{min} $R_g = 10 \text{ k}\Omega$ $T_{amb} = 25^\circ\text{C}$ to T_{max} $T_{amb} = 25^\circ\text{C}$ to T_{min}		1.8 1.8	10 10		3 6	6 12		$\mu\text{V}/^\circ\text{C}$ $\mu\text{V}/^\circ\text{C}$ $\mu\text{V}/^\circ\text{C}$ $\mu\text{V}/^\circ\text{C}$		
G_v	Large signal voltage gain	$V_s = \pm 15\text{V}$ $R_L \geq 2 \text{ k}\Omega$ $V_o = \pm 10\text{V}$		88	93	97	88	93	97	83	93	dB
V_o	Output voltage swing	$V_s = \pm 15\text{V}$ $R_L = 10 \text{ k}\Omega$ $V_s = \pm 15\text{V}$ $R_L = 2 \text{ k}\Omega$		± 12 ± 10	± 14 ± 13		± 12 ± 10	± 14 ± 13		± 12 ± 10	± 14 ± 13	V V
V_i	Input voltage range	$V_s = \pm 15\text{V}$		± 8		± 8	± 10	± 8	± 10			V
CMR	Common mode rejection	$R_g \leq 10 \text{ k}\Omega$		80	110	70	90	65	90			dB
SVR	Supply voltage rejection	$R_g \leq 10 \text{ k}\Omega$		80	88	76	92	74	92			dB

Note: These specifications, unless otherwise specified, apply for $T_{amb} = -55$ to 125°C for LS 709/LS 709A and $T_{amb} = 0$ to 70°C for LS 709C with the following conditions: $V_s = +9\text{V}$ to $+15\text{V}$, $C_1 = 5000 \text{ pF}$, $R_1 = 1.5 \text{ k}\Omega$, $C_2 = 200 \text{ pF}$ and $R_2 = 51\Omega$. (See fig. 8 and fig. 17).

Fig. 1 – Voltage gain vs. supply voltage (for 709A)

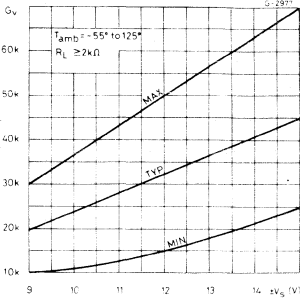


Fig. 2 – Output voltage swing vs. supply voltage (for 709A)

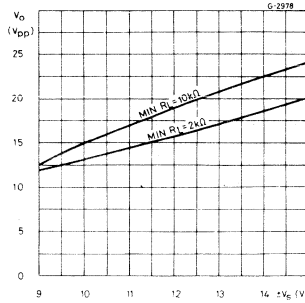


Fig. 3 – Input common mode voltage range vs. supply voltage (for 709A)

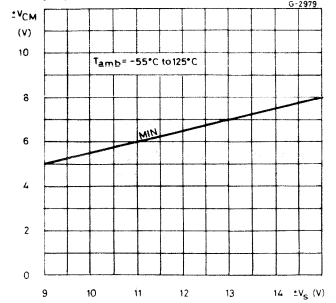


Fig. 4 – Power consumption vs. supply voltage (for 709A)

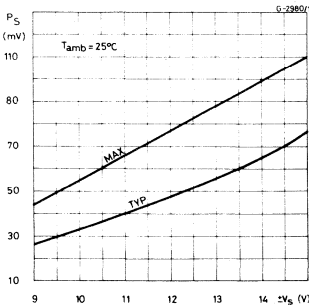


Fig. 5 – Output voltage swing vs. load resistance (for 709A)

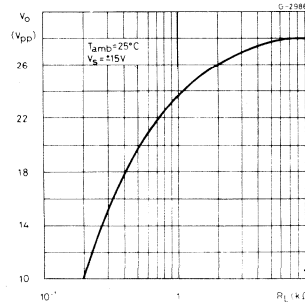


Fig. 6 – Input bias current vs. ambient temperature (for 709A)

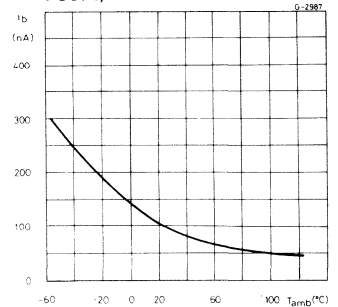


Fig. 7 – Input offset current vs. ambient temperature (for 709A)

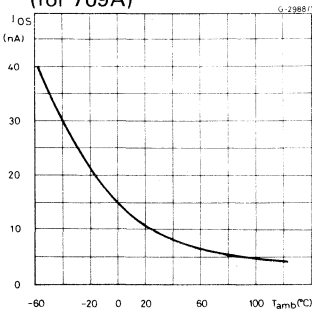


Fig. 8 – Transient response test circuit

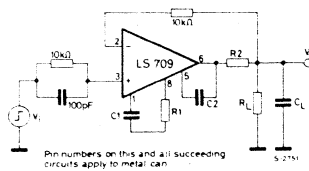
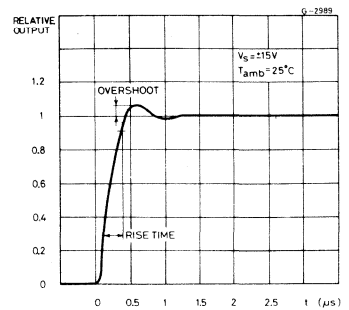


Fig. 9 – Transient response (for 709A)



LS 709 LS 709A LS 709C

Fig. 10 – Slew rate vs. closed loop gain using recommended compensation networks (for 709A)

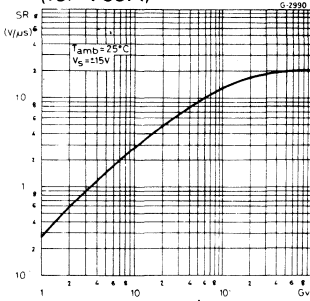


Fig. 11 – Voltage gain vs. supply voltage (for 709)

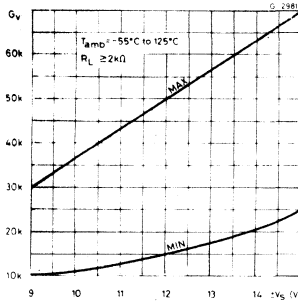


Fig. 12 – Output voltage swing vs. supply voltage (for 709 and 709C)

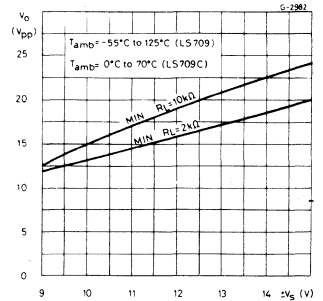


Fig. 13 – Voltage gain vs. supply voltage (for 709C)

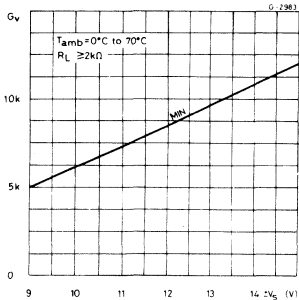


Fig. 14 – Input bias current vs. ambient temperature (for 709C)

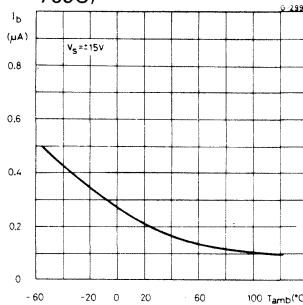
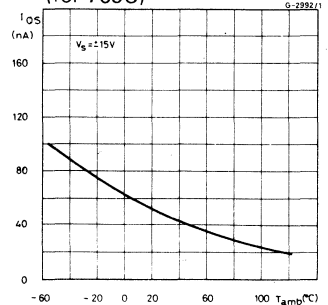


Fig. 15 – Input offset current vs. ambient temperature (for 709C)



Frequency compensation for all types

Fig. 16 – Open loop frequency response for various values of compensation

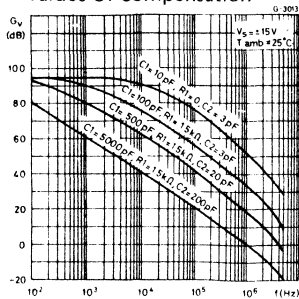


Fig. 17 – Frequency compensation circuit

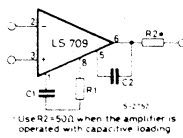
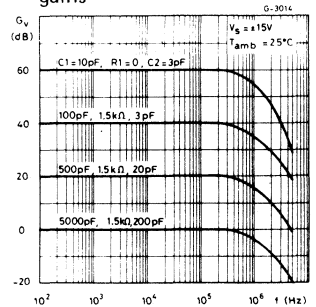


Fig. 18 – Frequency response for various closed loop gains



PROTECTION CIRCUITS

Fig. 19 - Output short circuit protection

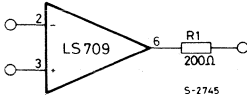


Fig. 20 - Input breakdown protection

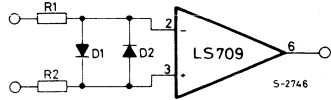


Fig. 21 - Latch up protection

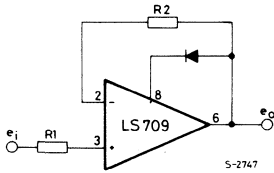
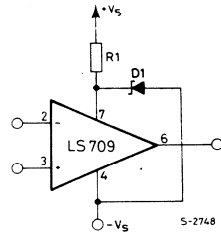


Fig. 22 - Supply overvoltage protection



LS 776 LS 776C

LINEAR INTEGRATED CIRCUITS

PROGRAMMABLE OPERATIONAL AMPLIFIER

- MICROPOWER CONSUMPTION
- INTERNALLY FREQUENCY COMPENSATION
- OFFSET NULL CAPABILITY
- SHORT CIRCUIT PROTECTION
- LOW INPUT BIAS CURRENTS
- LOW NOISE

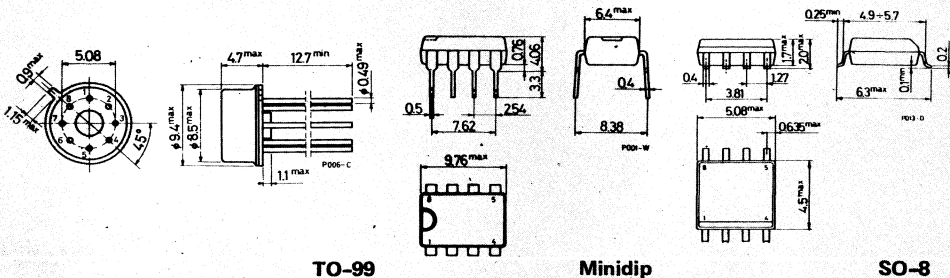
The LS 776 is a programmable operational amplifier available in three different packages (TO-99, Minidip and SO-8 micropackage). High input impedance, low supply currents and low input noise over a wide range of operating supply voltages coupled with programmable electrical characteristics, make it an extremely versatile amplifier for use in high accuracy, low power consumption analog applications. Input noise voltage and current, power consumption and input current can be optimized by a single resistor r_{cf} current source that sets the quiescent current for nanowatt power consumption or for characteristics similar to the LS 141. Internal frequency compensation, absence of "latch-up", high slew rate and short circuit current protection assure ease of use in long interval integrators, active filters and sample and hold circuits. The LS 776 is available with hermetic gold chip (8000 Series).

ABSOLUTE MAXIMUM RATINGS		TO-99	Minidip	μ package
V_s	Supply voltage		$\pm 18V$	
V_i (1)	Input voltage		$\pm 15V$	
ΔV_i	Differential input voltage		$\pm 30V$	
V_{SET}	Maximum voltage to ground at I_{SET}		$V_s - 2V$ to V_s	
I_{SET}	Maximum current at I_{SET}		$500 \mu A$	
T_{op}	Operating temperature for LS 776 for LS 776 C		-55 to $125^\circ C$ 0 to $70^\circ C$	
	Output short circuit duration (2)		indefinite	
P_{tot}	Power dissipation at $T_{amb} = 70^\circ C$	$520 mW$	$665 mW$	$400 mW$
T_{sta}, T_j	Storage and junction temperature	-65 to $150^\circ C$	-55 to $150^\circ C$	-55 to $150^\circ C$

- 1) For supply voltage less than $\pm 15V$, input voltage is equal to the supply voltage
- 2) The short circuit duration is limited by thermal dissipation

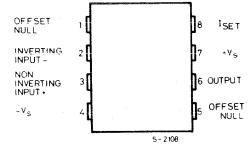
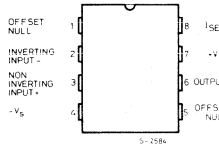
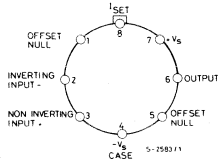
MECHANICAL DATA

Dimensions in mm



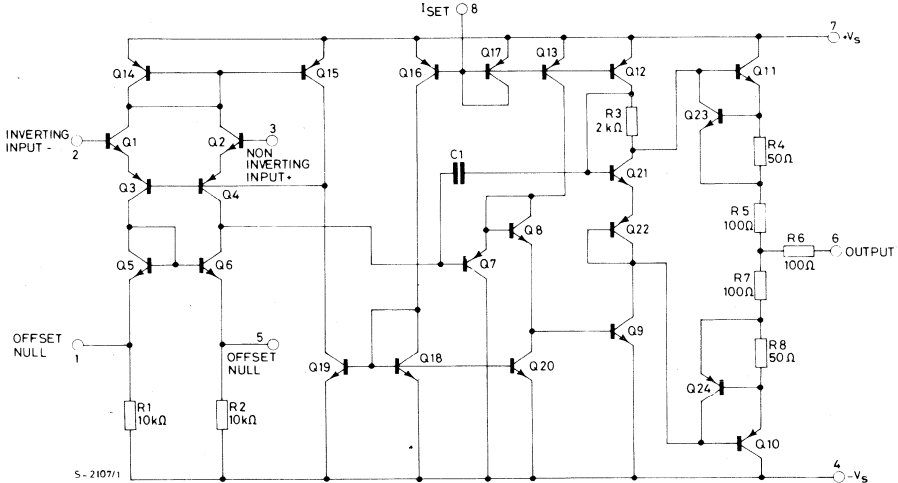
LS 776 LS 776C

CONNECTION DIAGRAMS AND ORDERING NUMBERS (top views)



Type	TO-99	Minidip	SO-8
LS 776	LS 776T	—	—
LS 776C	LS 776CT	LS 776 CB	LS 776CM
LS 8776	—	—	LS 8776M
LS 8776C	—	—	LS 8776CM

SCHEMATIC DIAGRAM



THERMAL DATA

	TO-99	Minidip	SO-8
$R_{th j-amb}$ Thermal resistance junction-ambient max.	155 °C/W	120 °C/W	200* °C/W

* The thermal resistance is measured with device mounted on a ceramic substrate (25 x 16 x 0.6 mm)

LS 776 LS 776C

ELECTRICAL CHARACTERISTICS for LS 776

($V_S = \pm 15V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter	Test conditions	$I_{SET} = 1.5 \mu A$			$I_{SET} = 15 \mu A$			Unit
		Min.	Typ.	Max.	Min.	Typ.	Max.	
V_{OS} Input offset voltage	$R_g \leq 10 \text{ k}\Omega$		2	5		2	5	mV
I_{OS} Input offset current	$R_g \leq 10 \text{ k}\Omega$		0.7	3		2	15	nA
I_b Input bias current			2	7.5		15	50	nA
R_i Input resistance			50			5		M Ω
C_i Input capacitance			2			2		pF
ΔV_{OS} Input offset voltage adjustment range			9			18		mV
G_v Large signal voltage gain	$R_L \geq 75 \text{ k}\Omega$ $V_o = \pm 10 V$	106	112					dB
	$R_L \geq 5 \text{ k}\Omega$ $V_o = \pm 10 V$				100	112		dB
R_o Output resistance			5			1		k Ω
I_{sc} Output short-circuit current			3			12		mA
I_s Supply current			20	25		160	180	μA
P_S Power consumption				0.75			5.4	mW
Transient response (unity gain) Rise time t_r Overshoot ΔV_o	$V_i = 20 \text{ mV}$ $R_L \geq 5 \text{ k}\Omega$ $C_L = 100 \text{ pF}$		1.6			0.35		μs
			0			10		%
SR Slew rate	$R_L \geq 5 \text{ k}\Omega$		0.1			0.8		V/ μs
V_o Output voltage swing	$R_L \geq 75 \text{ k}\Omega$	± 12	± 14					V
	$R_L \geq 5 \text{ k}\Omega$				± 10	± 13		V

The following specifications apply for $T_{amb} = -55$ to $125^\circ C$

V_{OS} Input offset voltage	$R_g \leq 10 \text{ k}\Omega$			6			6	mV
I_{OS} Input offset current	$T_{amb} = 125^\circ C$			5			15	nA
	$T_{amb} = -55^\circ C$			10			40	nA
I_b Input bias current	$T_{amb} = 125^\circ C$			7.5			50	nA
	$T_{amb} = -55^\circ C$			20			120	nA
V_i Input voltage range		± 10				± 10		V
CMR Common mode rejection	$R_g \leq 10 \text{ k}\Omega$	70	90		70	90		dB
SVR Supply voltage rejection	$R_g \leq 10 \text{ k}\Omega$	76	92		76	92		dB
G_v Large signal voltage gain	$R_L \geq 75 \text{ k}\Omega$ $V_o = \pm 10V$	100			98			dB
V_o Output voltage swing	$R_L \geq 75 \text{ k}\Omega$	± 10			± 10			V
I_s Supply current				30			200	μA
P_S Power consumption				0.9			6	mW

LS 776 LS 776C

ELECTRICAL CHARACTERISTICS for LS 776

($V_S = \pm 3V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter	Test conditions	$I_{SET} = 1.5 \mu A$			$I_{SET} = 15 \mu A$			Unit
		Min.	Typ.	Max.	Min.	Typ.	Max.	
V_{OS} Input offset voltage	$R_g \leq 10 k\Omega$		2	5		2	5	mV
I_{OS} Input offset current			0.7	3		2	15	nA
I_b Input bias current			2	7.5		15	50	nA
R_i Input resistance			50			5		M Ω
C_i Input capacitance			2			2		pF
ΔV_{OS} Input offset voltage adjustment range			9			18		mV
G_v Large signal voltage gain	$R_L \geq 75 k\Omega$ $V_o = \pm 1V$	94	106					dB
	$R_L \geq 5 k\Omega$ $V_o = \pm 1V$				94	106		dB
R_o Output resistance			5			1		k Ω
I_{sc} Output short-circuit current			3			5		mA
I_s Supply current			13	20		130	160	μA
P_S Power consumption			78	120		780	960	μW
Transient response (unity gain) Rise time t_r Overshoot ΔV_o	$V_i = 20 mV$ $R_L \geq 5 k\Omega$ $C_L \leq 100 pF$		3			0.6		μs
			0			5		%
SR Slew rate	$R_L \geq 5 k\Omega$		0.03			0.35		V/ μs

The following specifications apply for $T_{amb} = -55$ to $125^\circ C$

V_{OS} Input offset voltage	$R_g \leq 10 k\Omega$			6			6	mV
I_{OS} Input offset current	$T_{amb} = 125^\circ C$			5			15	nA
	$T_{amb} = -55^\circ C$			10			40	nA
I_b Input bias current	$T_{amb} = 125^\circ C$			7.5			50	nA
	$T_{amb} = -55^\circ C$			20			120	nA
V_i Input voltage range		± 1				± 1		V
CMR Common mode rejection	$R_g \leq 10 k\Omega$	70	86		70	86		dB
SVR Supply voltage rejection	$R_g \leq 10 k\Omega$	76	92		76	92		dB
G_v Large signal voltage gain	$R_L \geq 75 k\Omega$ $V_o = \pm 1V$	88						dB
	$R_L \geq 5 k\Omega$ $V_o = \pm 1V$				88			dB
V_o Output voltage swing	$R_L \geq 75 k\Omega$	± 2	± 2.4					V
	$R_L \geq 5 k\Omega$				± 1.9	± 2.1		V
I_s Supply current				25			180	μA
P_S Power consumption				150			1080	μW

LS 776

LS 776C

ELECTRICAL CHARACTERISTICS for LS 776C

($V_s = \pm 3V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter	Test conditions	$I_{SET} = 1.5 \mu A$			$I_{SET} = 15 \mu A$			Unit
		Min.	Typ.	Max.	Min.	Typ.	Max.	
V_{OS} Input offset voltage	$R_g \leq 10 \text{ k}\Omega$		2	6		2	6	mV
I_{OS} Input offset current			0.7	6		2	25	nA
I_b Input bias current			2	10		15	50	nA
R_i Input resistance			50			5		M Ω
C_i Input capacitance			2			2		pF
ΔV_{OS} Input offset voltage adjustment range			9			18		mV
G_v Large signal voltage gain	$R_L \geq 75 \text{ k}\Omega$ $V_o = \pm 1V$	88	106					dB
	$R_L \geq 5 \text{ k}\Omega$ $V_o = \pm 1V$				88	106		dB
R_o Output resistance			5			1		k Ω
I_{sc} Output short-circuit current			3			5		mA
I_s Supply current			13	20		130	170	μA
P_s Power consumption			78	120		780	1020	μW
Transient response (unity gain) Rise time t_r Overshoot ΔV_o	$V_i = 20 \text{ mV}$ $R_L \geq 5 \text{ k}\Omega$ $C_L \leq 100 \text{ pF}$		3			0.6		μs
			0			5		%
SR Slew rate	$R_L \geq 5 \text{ k}\Omega$		0.03			0.35		V/ μs

The following specifications apply for $T_{amb} = 0$ to $70^\circ C$

V_{OS} Input offset voltage	$R_g \leq 10 \text{ k}\Omega$			7.5			7.5	mV
I_{OS} Input offset current	$T_{amb} = 70^\circ C$			6			25	nA
	$T_{amb} = 0^\circ C$			10			40	nA
I_b Input bias current	$T_{amb} = 70^\circ C$			10			50	nA
	$T_{amb} = 0^\circ C$			20			100	nA
V_i Input voltage range		± 1			± 1			V
CMR Common mode rejection	$R_g \leq 10 \text{ k}\Omega$	70	86		70	86		dB
SVR Supply voltage rejection	$R_g \leq 10 \text{ k}\Omega$	74	92		74	92		dB
G_v Large signal voltage gain	$R_L \geq 75 \text{ k}\Omega$ $V_o = \pm 1V$	88						dB
	$R_L \geq 5 \text{ k}\Omega$ $V_o = \pm 1V$				88			dB
V_o Output voltage swing	$R_L \geq 75 \text{ k}\Omega$	± 2	± 2.4					V
	$R_L \geq 5 \text{ k}\Omega$				± 2	± 2.1		V
I_s Supply current				25			180	μA
P_s Power consumption				150			1080	μW

LS 776 LS 776C

ELECTRICAL CHARACTERISTICS for LS 776C

($V_s = \pm 15V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter	Test conditions	$I_{SET} = 1.5 \mu A$			$I_{SET} = 15 \mu A$			Unit
		Min.	Typ.	Max.	Min.	Typ.	Max.	
V_{OS} Input offset voltage	$R_g \leq 10 \text{ k}\Omega$		2	6		2	6	mV
I_{OS} Input offset current			0.7	6		2	25	nA
I_b Input bias current			2	10		15	50	nA
R_i Input resistance			50			5		M Ω
C_i Input capacitance			2			2		pF
ΔV_{OS} Input offset voltage adjustment range			9			18		mV
G_v Large signal voltage gain	$R_L \geq 75 \text{ k}\Omega$ $V_o = \pm 10V$	94	112					dB
	$R_L \geq 5 \text{ k}\Omega$ $V_o = \pm 10V$				94	112		dB
R_o Output resistance			5			1		k Ω
I_{sc} Output short-circuit current			3			12		mA
I_s Supply current			20	30		160	190	μA
P_s Power consumption				0.9			5.7	mW
Transient response (unity gain) Rise time t_r Overshoot ΔV_o	$V_i = 20 \text{ mV}$ $R_L \geq 5 \text{ k}\Omega$ $C_L \leq 100 \text{ pF}$		1.6			0.35		μs
			0			10		%
SR Slew rate	$R_L \geq 5 \text{ k}\Omega$		0.1			0.8		V/ μs
V_o Output voltage swing	$R_L \geq 75 \text{ k}\Omega$	± 12	± 14					V
	$R_L \geq 5 \text{ k}\Omega$				± 10	± 13		V

The following specifications apply for $T_{amb} = 0$ to $70^\circ C$

V_{OS} Input offset voltage	$R_g \leq 10 \text{ k}\Omega$			7.5			7.5	mV
I_{OS} Input offset current	$T_{amb} = 70^\circ C$			6			25	nA
	$T_{amb} = 0^\circ C$			10			40	nA
I_b Input bias current	$T_{amb} = 70^\circ C$			10			50	nA
	$T_{amb} = 0^\circ C$			20			100	nA
V_i Input voltage range		± 10			± 10			V
CMR Common mode rejection	$R_g \leq 10 \text{ k}\Omega$	70	90		70	90		dB
SVR Supply voltage rejection	$R_g \leq 10 \text{ k}\Omega$	74	92		74	92		dB
G_v Large signal voltage gain	$R_L \geq 75 \text{ k}\Omega$ $V_o = \pm 10V$	94			94			dB
V_o Output voltage swing	$R_L \geq 75 \text{ k}\Omega$	± 10			± 10			V
I_s Supply current				35			200	μA
P_s Power consumption				1.05			6	mW

LS 776 LS 776C

Fig. 1 - Input bias current vs. set current

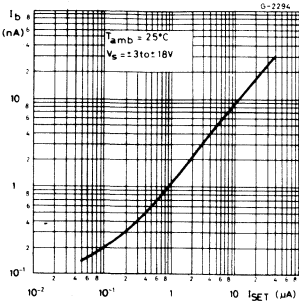


Fig. 2 - Input bias current vs. ambient temperature

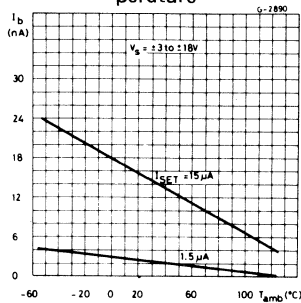


Fig. 3 - Input offset current vs. ambient temperature

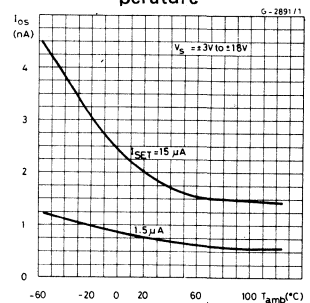


Fig. 4 - Change in input offset voltage vs. set current

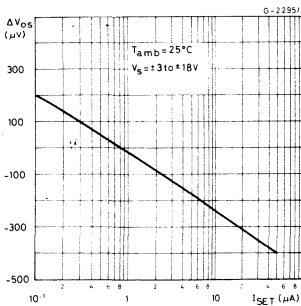


Fig. 5 - Change in input offset voltage vs. ambient temperature (unnull)

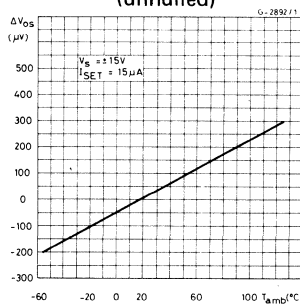


Fig. 6 - Input noise voltage vs. set current

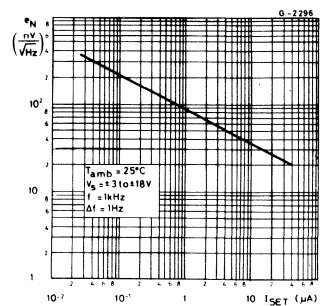


Fig. 7 - Input noise voltage and current vs. frequency

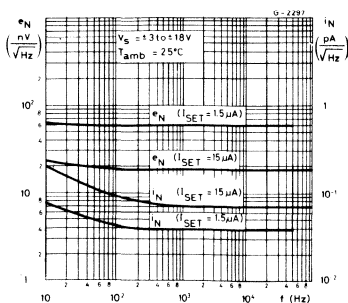


Fig. 8 - Input noise current vs. set current

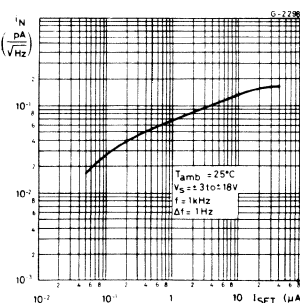
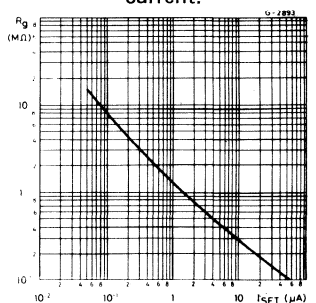


Fig. 9 - Optimum source resistance for minimum noise vs. set current.



LS 776 LS 776C

Fig. 10 - Output voltage swing vs. load resistance

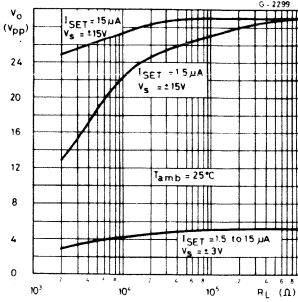


Fig. 11 - Output voltage swing vs. supply voltage

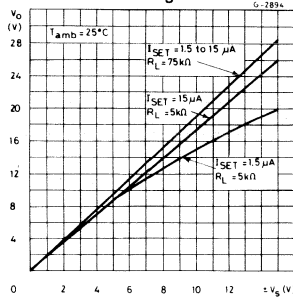


Fig. 12 - Gain bandwidth product vs. set current

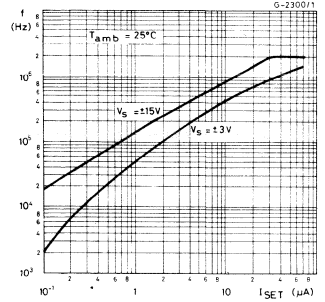


Fig. 13 - Open loop voltage gain vs. ambient temperature

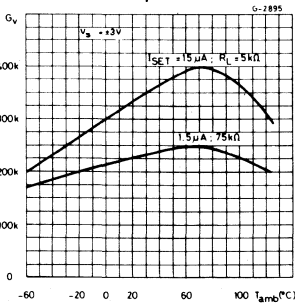


Fig. 14 - Open loop voltage gain vs. ambient temperature

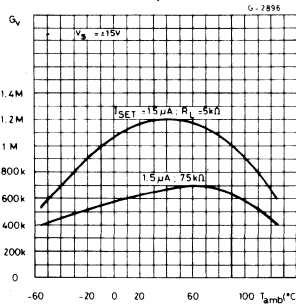


Fig. 15 - Open loop voltage gain vs. set current

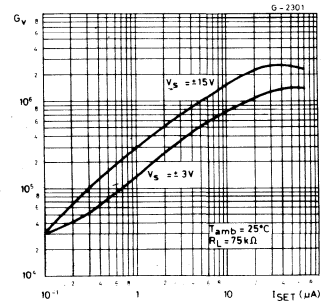


Fig. 16 - Common mode rejection vs. set current

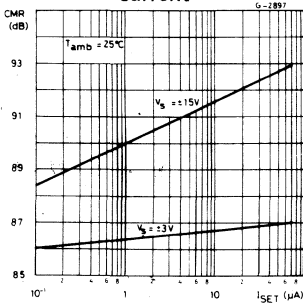


Fig. 17 - Supply voltage rejection vs. set current

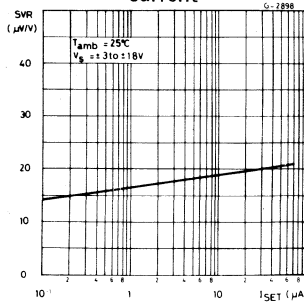
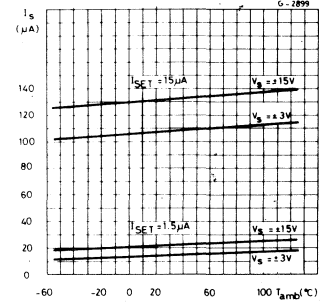


Fig. 18 - Supply current vs. ambient temperature



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Fig. 19 - Standby supply current vs. set current

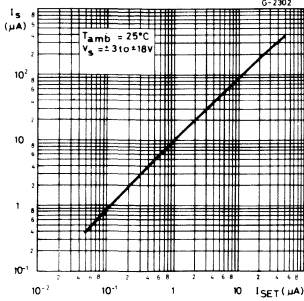


Fig. 20 - Slew rate vs. set current

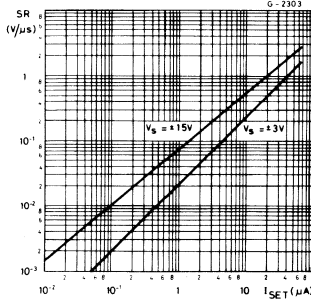
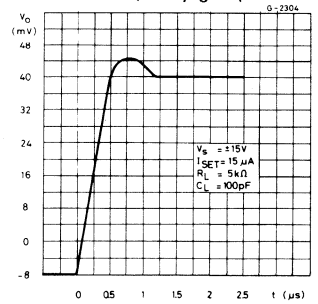


Fig. 21 - Voltage follower transient response (unity gain)



TYPICAL APPLICATIONS

Fig. 22 - High accuracy sample and hold

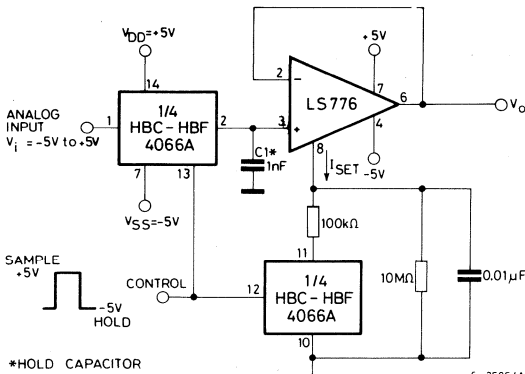


Fig. 23 - Nanowatt amplifier

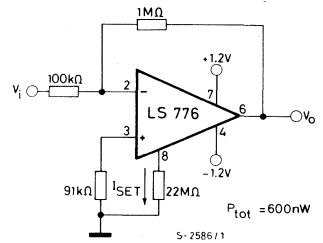
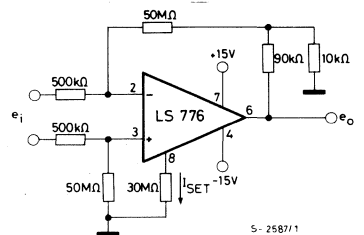
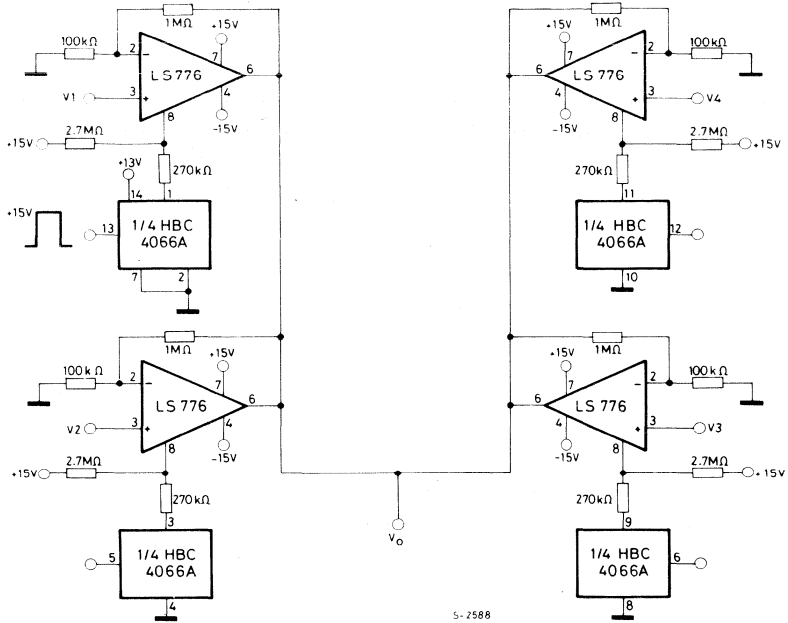


Fig. 24 - High input impedance amplifier



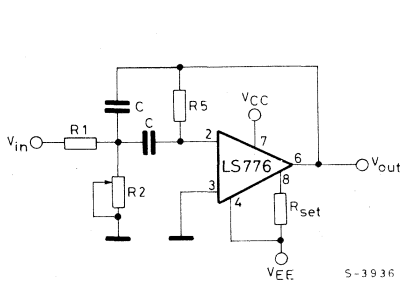
TYPICAL APPLICATIONS (continued)

Fig. 25 - Multiplexing and signal conditioning



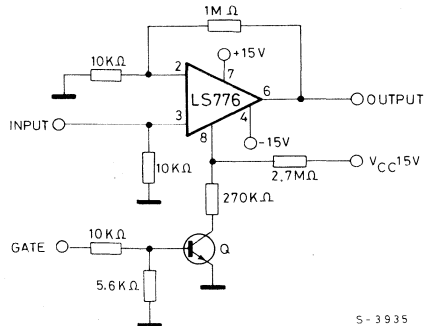
5-2588

Fig. 26 - Multiple feedback bandpass filter



5-3936

Fig. 27 - Gated amplifier



5-3935

TAA 550 TBA 271

LINEAR INTEGRATED CIRCUITS

VOLTAGE STABILIZER

- LOW TEMPERATURE COEFFICIENT
- LOW ZENER RESISTANCE

The TAA 550/TBA 271 are monolithic integrated voltage stabilizers in a TO-18 two pins metal case. They are especially designed as voltage supplies for varicap diodes in television tuners. The TAA 550/TBA 271 are supplied in 3 groups of stabilized voltage identified by a letter after the code.

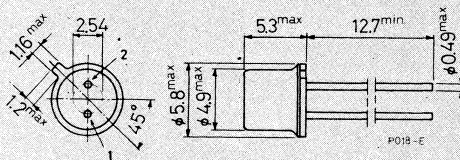
ABSOLUTE MAXIMUM RATINGS

I_z	Zener current at $T_{case} \leq 70^\circ$	15	mA
T_{stg}	Storage temperature	-20 to 150	$^\circ\text{C}$
T_{op}	Operating junction temperature	0 to 150	$^\circ\text{C}$

ORDERING NUMBERS: TAA 550 A or TBA 271 A (for V_z range - : 30-32V)
TAA 550 B or TBA 271 B (for V_z range : 32-34V)
TAA 550 C or TBA 271 C (for V_z range : 34-36V)

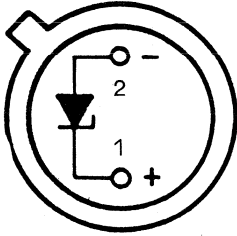
MECHANICAL DATA

Dimensions in mm



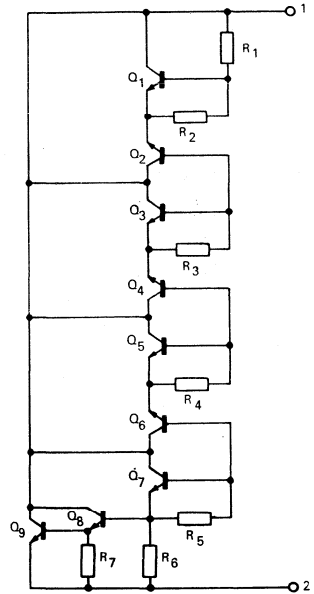
CONNECTION DIAGRAM

(bottom view)



SS 0036

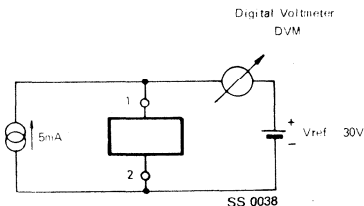
SCHEMATIC DIAGRAM



SS 0037

TEST CIRCUITS

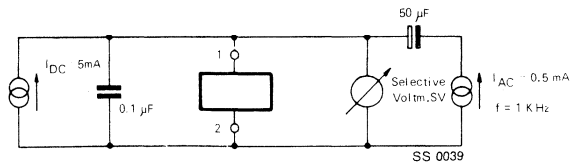
Circuit No. 1 (for V_z measurement)



SS 0038

$$V_z = V_{ref} \cdot V_{DVM}$$

Circuit No. 2 (for r_z measurement)



SS 0039

$$r_z = \frac{V_{sv}}{0.5 \text{ mA}}$$

TAA 550 TBA 271

THERMAL DATA

$R_{th\ j-case}$	Thermal resistance junction-case	max	150 °C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	400 °C/W

ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^{\circ}C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_z	Zener voltage	$I_z = 5\text{ mA}$ (circuit No. 1) for TAA 550 A/TBA 271 A for TAA 550 B/TBA 271 B for TAA 550 C/TBA 271 C			30 V 32 V 34 V
r_z	Zener dynamic resistance	$I_z = 5\text{ mA}$ $I_{AC} = 0.5\text{ mA}$ $f = 1\text{ kHz}$ (circuit No. 2)			10 Ω to 25 Ω
$\frac{\Delta V_z}{\Delta T_{amb}}$	Temperature coefficient	$I_z = 5\text{ mA}$ $\Delta T_{amb} = 0\text{ to }50^{\circ}C$			-3.2 to +1.6 mV/°C

Fig. 1 - Zener dynamic resistance vs. current

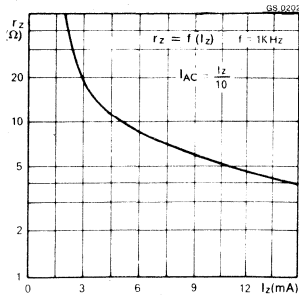


Fig. 2 - Temperature coefficient vs. current

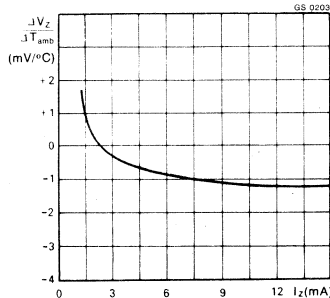
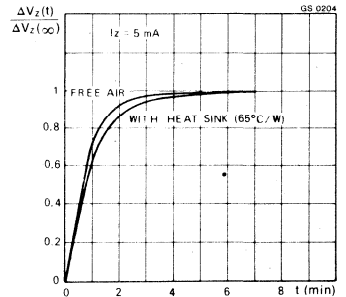


Fig. 3 - $\frac{\Delta V_z(t)}{\Delta V_z(\infty)}$ vs time



LINEAR INTEGRATED CIRCUIT

1.8W AUDIO AMPLIFIER

- LOW DISTORTION
- LOW QUIESCENT CURRENT
- SELF CENTERING BIAS
- HIGH INPUT IMPEDANCE

The TAA 611A is a monolithic integrated circuit in a 14-lead quad in-line plastic package or in a TO-100 metal case.

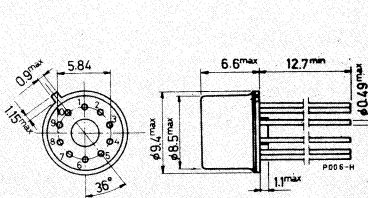
It is particularly designed for use in radio receivers and record-players as audio amplifier. The usable range of supply voltage varies from 6V to 12V and the circuit requires a minimum number of external components.

ABSOLUTE MAXIMUM RATINGS		TAA 611 A12	TAA 611 A55
V_s	DC supply voltage	12 V	
V_i	Input voltage	V_s	
I_o	Output peak current (repetitive)	1 A	
P_{tot}	Power dissipation at $T_{amb} = 25^\circ\text{C}$ at $T_{case} = 70^\circ\text{C}$	1.35 W 3.1 W	0.57 W 1.6 W
T_{stg}, T_j	Storage and junction temperature	-40 to 150 °C	

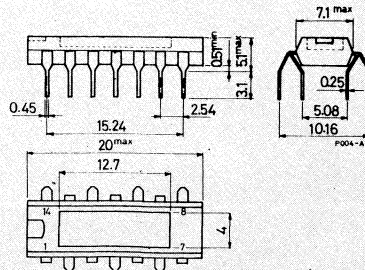
ORDERING NUMBERS: TAA 611 A55 (for TO-100 metal case)
TAA 611 A12 (for quad in-line plastic package)

MECHANICAL DATA

Dimensions in mm



TAA 611 A55

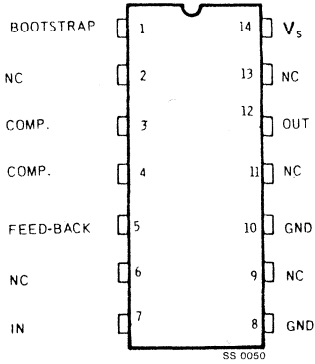


TAA 611 A12

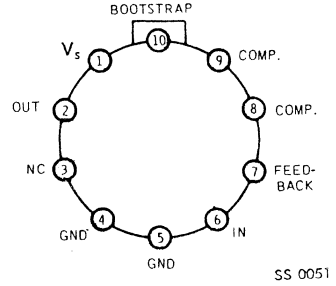
TAA 611A

CONNECTION DIAGRAMS (top view)

For TAA 611 A12

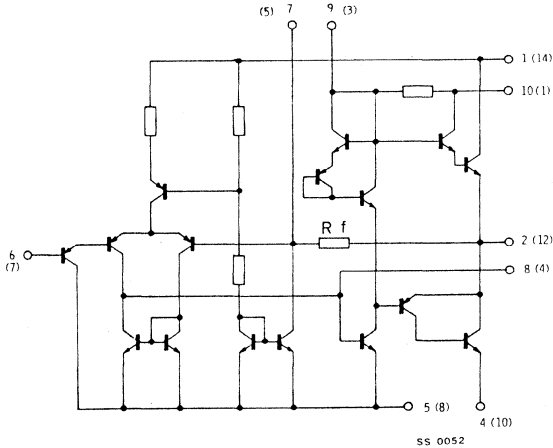


For TAA 611 A55



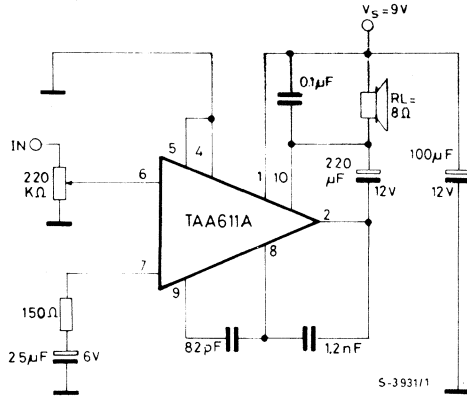
SCHEMATIC DIAGRAM

(Pin numbers in brackets are referred to the plastic package).

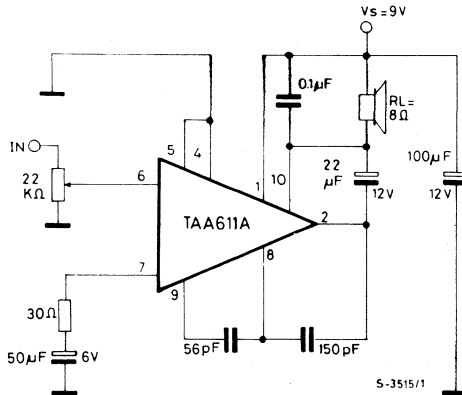


TEST AND APPLICATION CIRCUITS

Circuit 1 – Audio amplifier for record-player ($G_v = 34$ dB)



Circuit 2 – Audio amplifier for radio ($G_v = 48$ dB)



The pin numbers refer to TAA 611 A12 (plastic package)

THERMAL DATA

			TAA 611 A12	TAA 611 A55
$R_{th\ j-case}$	Thermal resistance junction-case	max	16 °C/W	50 °C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	93 °C/W	220 °C/W

TAA 611A

ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^{\circ}\text{C}$, $V_s = 9\text{V}$, refer to the application circuit no. 2 unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_o	Quiescent output voltage		4.8		V
I_d	Total quiescent drain current		3		mA
I_d	Quiescent drain current of output transistors		1		mA
I_d	Drain current	$P_o = 1.15\text{W}$ $R_L = 8\Omega$	170		mA
I_b	Input bias current		0.1	0.8	μA
P_o^*	Output power	$d = 2\%$ $f = 1\text{ kHz}$ $V_s = 6\text{V}$ $R_L = 4\Omega$ $R_L = 8\Omega$ $V_s = 9\text{V}$ $R_L = 4\Omega$ $R_L = 8\Omega$	0.50 0.35 1.4 0.9		W W W W
		$d = 10\%$ $f = 1\text{ kHz}$ $V_s = 6\text{V}$ $R_L = 4\Omega$ $R_L = 8\Omega$ $V_s = 9\text{V}$ $R_L = 4\Omega$ $R_L = 8\Omega$	0.65 0.45 1.8 1.15		W W W W
R_f	Internal feedback resistance (see schematic diagram)		7.5		k Ω
Z_i	Input impedance (open loop)		5		M Ω
d	Distortion	Application circuit 1 $P_o = 50\text{ mW}$ $R_L = 8\Omega$ $f = 1\text{ kHz}$ $P_o = 0.5\text{W}$ $R_L = 8\Omega$	0.4 0.3		% %
		Application circuit 2 $P_o = 50\text{ mW}$ $R_L = 8\Omega$ $f = 1\text{ kHz}$ $P_o = 0.5\text{W}$ $V_s = 9\text{V}$ $R_L = 8\Omega$ $f = 1\text{ kHz}$	1.7 1.2		% %
G_v	Voltage gain (open loop)	$R_L = 8\Omega$	68		dB

* External heatsink not required except for TAA 611 A55 at $V_s = 9\text{V}$, $R_L = 4\Omega$.

Fig. 1 - Output power vs. load resistance

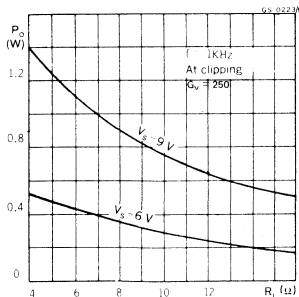
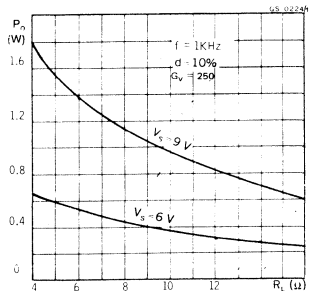


Fig. 2 - Output power vs. load resistance



LINEAR INTEGRATED CIRCUIT

2W AUDIO AMPLIFIER

- LOW DISTORTION
- LOW QUIESCENT CURRENT
- SELF CENTERING BIAS
- HIGH INPUT IMPEDANCE

The TAA 611 B is a monolithic integrated circuit in a 14-lead quad in-line plastic package. It is particularly designed for use in radio receivers and record-players as audio amplifier. The usable range of supply voltage varies from 6V to 15V and the circuit requires a minimum number of external components.

ABSOLUTE MAXIMUM RATING

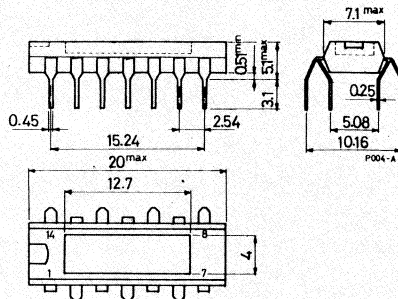
V_s	DC Supply voltage	15	V
V_i^*	Input voltage	-0.5 to 15	V
I_o	Output peak current (repetitive)	1	A
P_{tot}	Power dissipation at $T_{amb} = 25^\circ\text{C}$	1.35	W
	at $T_{case} = 70^\circ\text{C}$	3.1	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

* For $V_s < 15\text{V}$, $V_{i\ max} = V_s$.

ORDERING NUMBER: TAA 611 B12

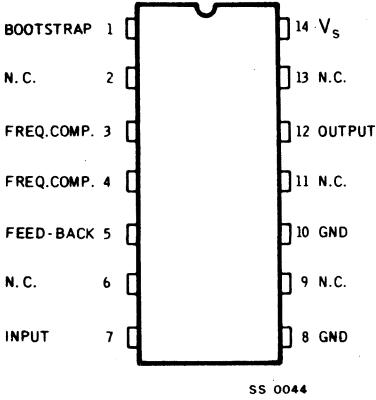
MECHANICAL DATA

Dimensions in mm

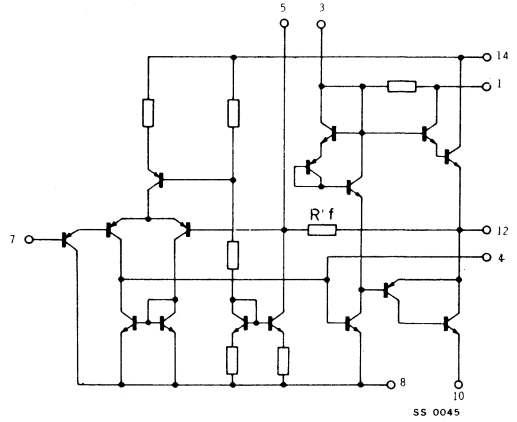


TAA 611B

CONNECTION DIAGRAM
(top view)

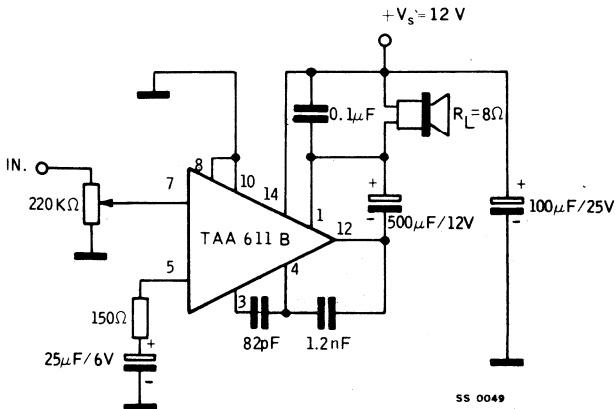


SCHEMATIC DIAGRAM



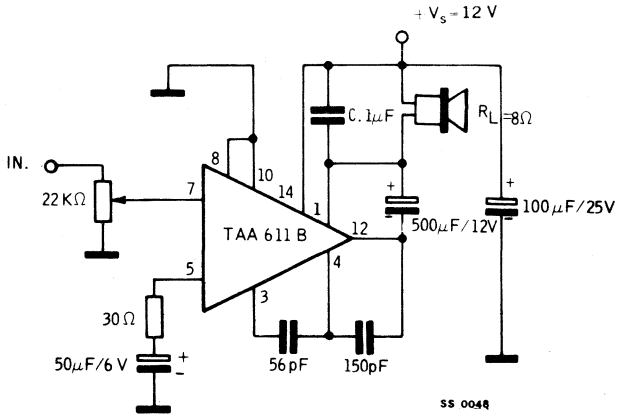
TEST AND APPLICATION CIRCUITS

Circuit 1 - Audio amplifier for record-player ($G_v = 34$ dB)



TEST AND APPLICATION CIRCUITS (continued)

Circuit 2 Audio amplifier for radio ($G_V = 48 \text{ dB}$)



THERMAL DATA

$R_{th \text{ j-case}}$	Thermal resistance junction-case	max	16	$^{\circ}\text{C/W}$
$R_{th \text{ j-amb}}$	Thermal resistance junction-ambient	max	93	$^{\circ}\text{C/W}$

ELECTRICAL CHARACTERISTICS

($T_{amb} = 25^{\circ}\text{C}$, refer to the application circuit no. 2 unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_o	Quiescent output voltage		4.8 6.3		V V
I_d	Total quiescent drain current		3 3.5		mA mA
I_d	Quiescent drain current of output transistors		1 1.2		mA mA
I_d	Drain current	$R_L = 8\Omega$ $P_o = 1.15 \text{ W}$ $P_o = 2.1 \text{ W}$	$V_s = 9 \text{ V}$ $V_s = 12 \text{ V}$		170 235 mA mA
I_b	Input bias current		60 0.1	1	nA μA

TAA 611B

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
P_o Output power	$d = 2\%$ $f = 1 \text{ kHz}$ $V_s = 9 \text{ V}$ $R_L = 8 \Omega$ $V_s = 12 \text{ V}$ $R_L = 8 \Omega$		0.9 1.7		W W
	$d = 10\%$ $f = 1 \text{ kHz}$ $V_s = 9 \text{ V}$ $R_L = 8 \Omega$ $V_s = 12 \text{ V}$ $R_L = 8 \Omega$	1.5	1.15 2.1		W W
R_f Internal feedback resistance (see schematic diagram)			7.5		$k\Omega$
Z_i Input impedance	open loop		5		$M\Omega$
d Distortion	Applic. Circuit 1 $R_L = 8 \Omega$ $f = 1 \text{ kHz}$ $P_o = 50 \text{ mW}$ $V_s = 9 \text{ V}$ $P_o = 50 \text{ mW}$ $V_s = 12 \text{ V}$ $P_o = 0.5 \text{ W}$ $V_s = 9 \text{ V}$ $P_o = 1 \text{ W}$ $V_s = 12 \text{ V}$		0.4 0.3 0.3 0.2		% % % %
	Applic. Circuit 2 $R_L = 8 \Omega$ $f = 1 \text{ kHz}$ $P_o = 50 \text{ mW}$ $V_s = 9 \text{ V}$ $P_o = 50 \text{ mW}$ $V_s = 12 \text{ V}$ $P_o = 0.5 \text{ W}$ $V_s = 9 \text{ V}$ $P_o = 1 \text{ W}$ $V_s = 12 \text{ V}$		1.7 1.5 1.2 1		% % % %
G_v Voltage gain (open loop)	$R_L = 8 \Omega$ $V_s = 12 \text{ V}$		70		dB

Fig. 1 - Output power vs load resistance

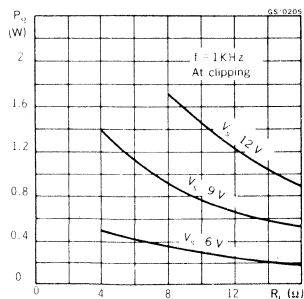
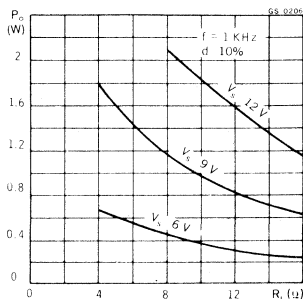


Fig. 2 - Output power vs load resistance



LINEAR INTEGRATED CIRCUIT

3.3W AUDIO AMPLIFIER

- LOW DISTORTION
- LOW QUIESCENT CURRENT
- SELF CENTERING BIAS
- HIGH INPUT IMPEDANCE

The TAA 611C is a monolithic integrated circuit in a 14-lead quad in-line power plastic package. It is particularly designed for use as audio amplifier in radio receivers, record players and portable TV sets. The usable range of supply voltage varies from 6 to 18V, and the circuit requires a minimum number of external components.

The package has very low thermal resistance. To decrease the thermal resistance further an external heatsink can easily be mounted by means of ordinary hardware.

ABSOLUTE MAXIMUM RATINGS

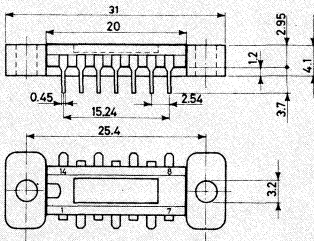
V_s	Supply voltage	22	V
V_s^*	Operating supply voltage	18	V
V_i^*	Input voltage	-0.5 to 20	V
I_o	Output peak current (repetitive)	1	A
P_{tot}	Power dissipation at $T_{amb} = 25^\circ\text{C}$	2	W
	at $T_{case} = 100^\circ\text{C}$	3.1	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

* For $V_s < 20\text{V}$, $V_{i\ max} = V_s$.

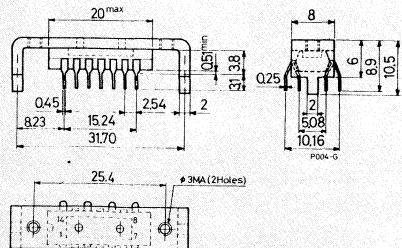
ORDERING NUMBERS: TAA 611 C72 (for quad in-line plastic package with spacer)
TAA 611 C11 (for quad in-line plastic package with inverted external bar)

MECHANICAL DATA

Dimensions in mm



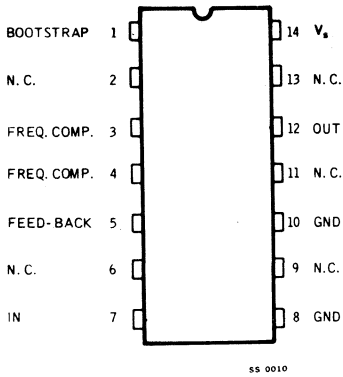
TAA 611 C72



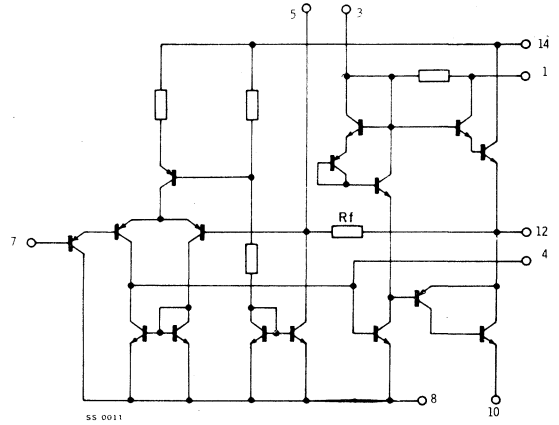
TAA 611 C11

TAA 611C

CONNECTION DIAGRAM (top view)

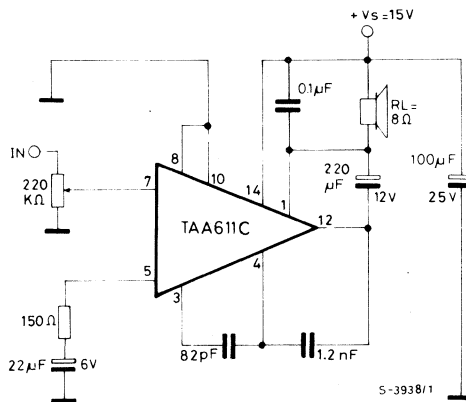


SCHEMATIC DIAGRAM



TEST AND APPLICATION CIRCUITS

Fig. 1 - Audio amplifier for record player



TAA 611C

THERMAL DATA

			TAA 611 CT2	TAA 611 C11
$R_{th\ j-case}$	Thermal resistance junction-case	max	16 °C/W	16 °C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	93 °C/W	63 °C/W

ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^{\circ}C$, refer to the application circuit of fig. 1 unless otherwise specified)

Parameter		Test conditions		Min.	Typ.	Max.	Unit		
V_o	Quiescent output voltage	$V_s = 12\ V$ $V_s = 15\ V$			6.3 7.9		V V		
I_d	Total quiescent drain current	$V_s = 12\ V$ $V_s = 15\ V$			3.5 4		mA mA		
I_d	Quiescent drain current of output transistors	$V_s = 12\ V$ $V_s = 15\ V$			1.2 1.8		mA mA		
I_d	Drain current	$V_s = 12\ V$	$P_o = 2.1\ W$		235		mA		
		$V_s = 15\ V$	$P_o = 3.3\ W$		300		mA		
I_b	Input bias current	$V_s = 12\ V$ $V_s = 15\ V$			75 0.1	1	nA μA		
P_o^*	Output power	$d = 2\%$ $V_s = 9\ V$	$f = 1\ kHz$ $R_L = 4\ \Omega$ $R_L = 8\ \Omega$		1.4 0.9		W W		
			$V_s = 12\ V$	$R_L = 8\ \Omega$		1.7		W	
		$V_s = 15\ V$	$R_L = 8\ \Omega$ $R_L = 16\ \Omega$		2.8 1.6		W W		
			$d = 10\%$ $V_s = 9\ V$	$f = 1\ kHz$ $R_L = 4\ \Omega$ $R_L = 8\ \Omega$		1.8 1.15		W W	
		$V_s = 12\ V$		$R_L = 8\ \Omega$		2.1		W	
		$V_s = 15\ V$	$R_L = 8\ \Omega$ $R_L = 16\ \Omega$	2.5	3.3 1.9		W		
		R_f	Internal feedback resistance (see schematic diagram)				7.5		K Ω
		Z_i	Input impedance	open loop			5		M Ω
d	Distortion	$R_L = 8\ \Omega$ $V_s = 12\ V$ $V_s = 15\ V$	$f = 1\ kHz$ $P_o = 50\ mW$		0.3		%		
			$P_o = 50\ mW$		0.3		%		
		$V_s = 12\ V$ $V_s = 15\ V$	$P_o = 1\ W$ $P_o = 1\ W$		0.2 0.2		% %		
		G_v	Voltage gain (open loop)	$V_s = 15\ V$	$R_L = 8\ \Omega$		72		dB

* External heatsink not required except for the conditions $V_s = 15\ V$, $R_L = 8\ \Omega$

TAA 621

LINEAR INTEGRATED CIRCUIT

NOT FOR NEW DESIGNS

4W AUDIO AMPLIFIER

- SELF CENTERING BIAS
- LOW QUIESCENT OUTPUT CURRENT
- NO CROSS OVER DISTORTION
- HIGH EFFICIENCY

The TAA 621 is a monolithic integrated circuit in a 14-lead quad in-line plastic package with or without external bar. It is particularly designed for use in television sets as audio amplifier.

Special features of the circuit include:

- Self centering bias for any supply voltage from 6 to 24V.
- Direct coupled high impedance input and high supply voltage rejection.

The package has very low thermal resistance. To decrease the thermal resistance further, an external heatsink can easily be mounted by means of ordinary hardware.

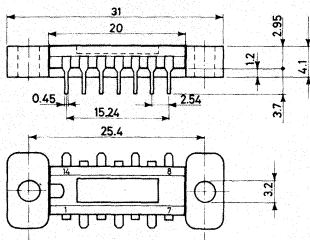
ABSOLUTE MAXIMUM RATINGS

V_s	DC supply voltage	27	V
V_i	Input voltage	V_s	
I_o	Output peak current (repetitive)	1	A
P_{tot}	Power dissipation at $T_{amb} = 25^\circ\text{C}$	2	W
	at $T_{case} = 70^\circ\text{C}$	4.5	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

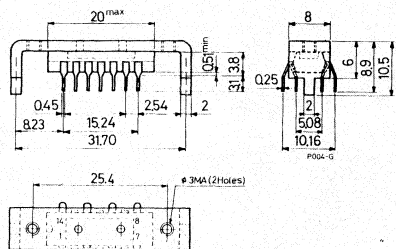
ORDERING NUMBERS: TAA 621 A72 (for quad in-line plastic package with spacer)
TAA 621 A11 (for quad in-line plastic package with inverted external bar)

MECHANICAL DATA

Dimensions in mm



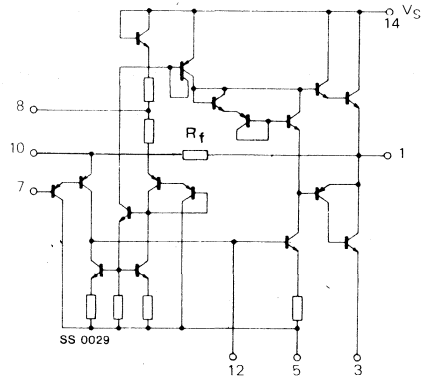
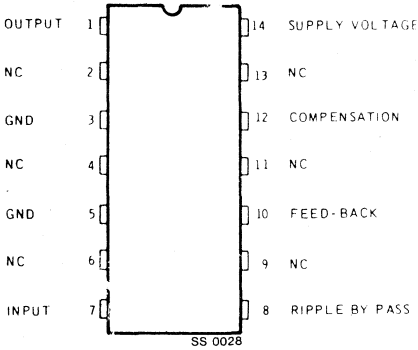
TAA 621 A72



TAA 621 A11

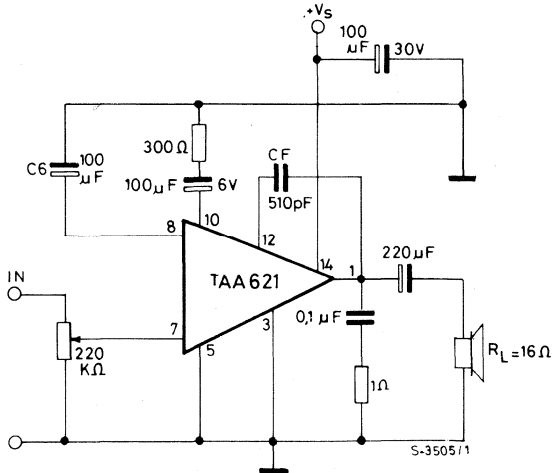
TAA 621

CONNECTION AND SCHEMATIC DIAGRAMS (top view)



The heatsink is connected to the substrate (pin 5)

TEST AND APPLICATION CIRCUIT ($G_v = 34$ dB)



TAA 621

THERMAL DATA

$R_{th\ j-case}$	Thermal resistance junction-case	max	17	°C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	63	°C/W

ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $T_{amb} = 25^{\circ}\text{C}$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
I_{d1}	Total quiescent drain current	$V_s = 18\text{V}$ $V_s = 24\text{V}$	6.2 7.5		mA mA
I_d	Quiescent drain current of output transistors	$V_s = 18\text{V}$ $V_s = 24\text{V}$	2.5 3		mA mA
I_s	Drain current	$d = 10\%$ $R_L = 16\Omega$ $P_o = 2.2\text{W}$ $V_s = 18\text{V}$ $P_o = 4\text{W}$ $V_s = 24\text{V}$	175 220		mA mA
I_b	Input bias current	$V_s = 18\text{V}$ $V_s = 24\text{V}$	180 250		nA nA
P_o^*	Output power	$d = 2\%$ $R_L = 16\Omega$ $V_s = 18\text{V}$ $R_L = 16\Omega$ $V_s = 24\text{V}$	1.7 2.7		W W
		$d = 10\%$ $R_L = 16\Omega$ $V_s = 18\text{V}$ $R_L = 16\Omega$ $V_s = 24\text{V}$	3	2.2 4	W W
R_f	Internal feedback resistance (see schematic diagram)		15		k Ω
Z_i	Input impedance	$V_s = 18\text{V}$ $f = 1\text{ KHz}$ $V_s = 24\text{V}$	150 110		k Ω k Ω
d	Distortion	$P_o = 50\text{ mW}$ $f = 1\text{ kHz}$ $R_L = 16\Omega$ $V_s = 18\text{V}$ $V_s = 24\text{V}$	0.1 0.1		% %
G_v	Voltage gain (open loop)	$R_L = 16\Omega$ $V_s = 18\text{V}$ $V_s = 24\text{V}$	72 74		dB dB
SVR	Supply voltage rejection	$R_L = 16\Omega$ $V_s = 24\text{V}$ $f_{(ripple)} = 100\text{ Hz}$ $C_6 = 100\ \mu\text{f}$ $C_6 = 50\ \mu\text{F}$	52 46		dB dB

* External heatsink not required except for the conditions $V_s = 24\text{V}$, $R_L = 16\Omega$.

LINEAR INTEGRATED CIRCUIT

DUAL AUDIO PREAMPLIFIER

- SINGLE OR DUAL SUPPLY OPERATION
- LOW NOISE FIGURE
- HIGH GAIN
- LARGE INPUT VOLTAGE RANGE
- EXCELLENT GAIN STABILITY VERSUS SUPPLY VOLTAGE
- NO LATCH UP
- OUTPUT SHORT CIRCUIT PROTECTED

The TBA 231A is a monolithic integrated dual operational amplifier in a 14-lead dual in-line plastic package.

These low-noise, high-gain amplifiers show extremely stable operating characteristics over a wide range of supply voltage and temperatures.

The device is intended for a variety of applications requiring two high performance operational amplifiers, such as phono and tape stereo preamplifier, TV remote control receiver, etc.

ABSOLUTE MAXIMUM RATINGS

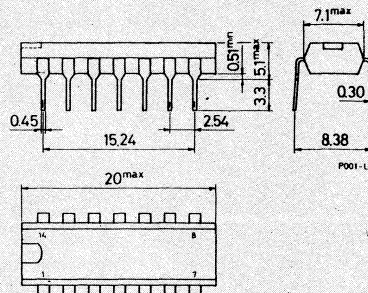
V_s	Supply voltage	± 18	V
V_i	Differential input voltage	± 5	V
V_{CM}	* Common mode input voltage	± 15	V
P_{tot}	Power dissipation at $T_{amb} \leq 60^\circ\text{C}$	500	mW
T_{stg}	Storage temperature	-40 to 150	$^\circ\text{C}$
T_{op}	Operating temperature	0 to 70	$^\circ\text{C}$

* For $V_s \leq \pm 15\text{V}$, $V_{CM\ max} = V_s$.

ORDERING NUMBER: TBA 231A

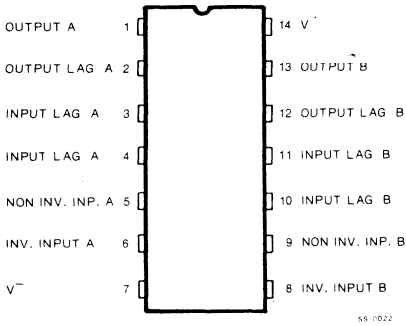
MECHANICAL DATA

Dimensions in mm

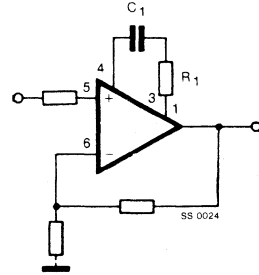


TBA 231A

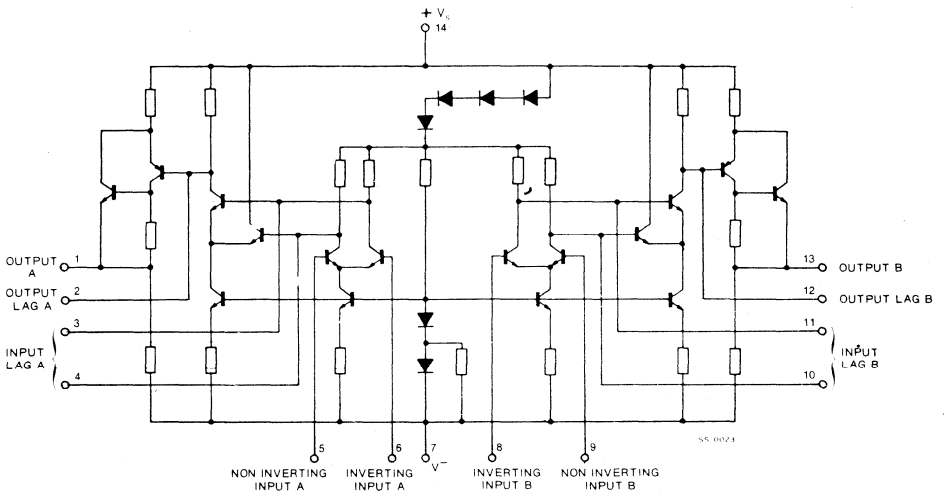
CONNECTION DIAGRAM (top view)



TEST CIRCUIT



SCHEMATIC DIAGRAM



THERMAL DATA

R _{th j-amb}	Thermal resistance junction-ambient	max	180	°C/W
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ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^{\circ}\text{C}$, $R_L = 50\text{ k}\Omega$ to pin 7, unless otherwise specified, $V_s = \pm 15\text{V}$)

Parameter		Test conditions	Min.	Typ.	Max.	Unit
I_d	Quiescent drain current	$V_o = 0$		9	14	mA
V_{OS}	Input offset voltage	$R_g = 200\Omega$		1	6	mV
I_{OS}	Input offset current			50	1000	nA
I_b	Input bias current			250	2000	nA
V_{CM}	Common mode input voltage range		± 10	± 11		V
R_i	Input resistance	$f = 1\text{ kHz}$	37	150		$\text{k}\Omega$
G_v	Voltage gain	$V_o = \pm 5\text{V}$	6500	20 000		—
V_o	Positive output voltage swing		+12	+13		V
V_o	Negative output voltage swing		-14	-15		V
R_o	Output resistance	$f = 1\text{ kHz}$		5		$\text{k}\Omega$
CMR	Common mode rejection	$R_g = 200\Omega$	70	90		dB
SVR	Supply voltage rejection	$R_g = 200\Omega$		50		$\mu\text{V}/\text{V}$
SR	Slew rate	Unity gain $C_1 = 0.1\ \mu\text{F}$ $R_1 = 4.7\Omega$		1		$\text{V}/\mu\text{s}$
CS	Channel separation	$R_g = 10\text{ k}\Omega$ $f = 10\text{ kHz}$		140		dB
NF	Noise figure	$R_g = 10\text{ k}\Omega$ $B = 10\text{ Hz to } 10\text{ kHz}$		1.5		dB

Fig. 1 - Output voltage swing vs. supply voltage

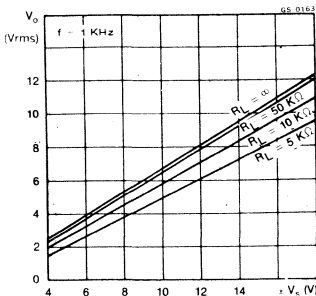


Fig. 2 - Quiescent drain current vs. supply voltage

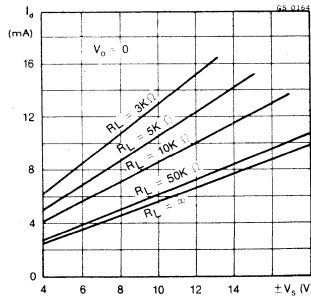
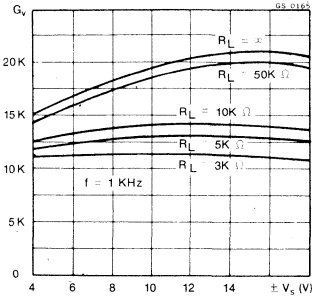


Fig. 3 - Open loop voltage gain vs. supply voltage



TBA 231A

Fig. 4 - Open loop frequency response using recommended compensation networks

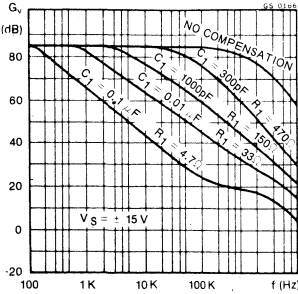


Fig. 5 - Output voltage swing vs. frequency for various compensation networks

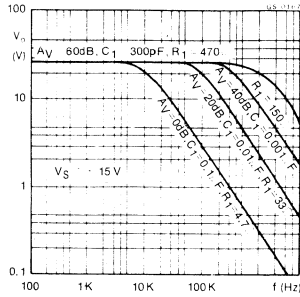


Fig. 6 - Input noise voltage vs. frequency

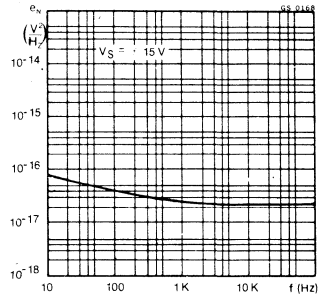


Fig. 7 - Input noise current vs. frequency

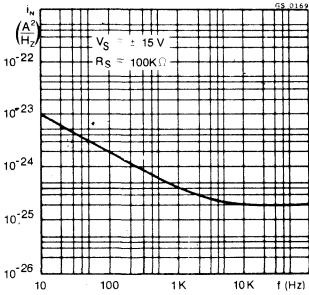


Fig. 8 - Closed loop gain vs. frequency

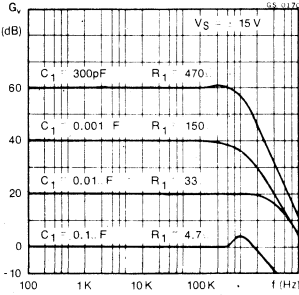
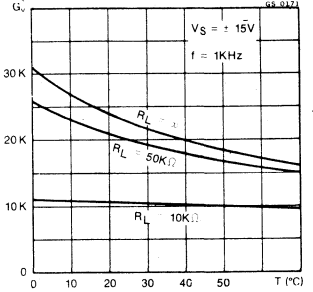
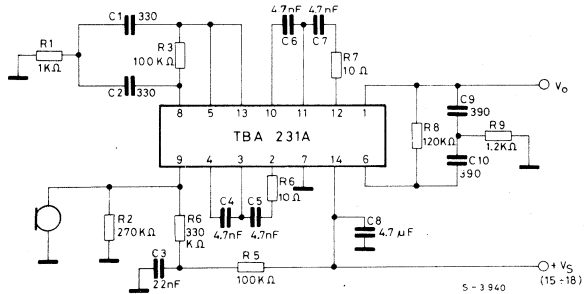


Fig. 9 - Open loop voltage gain vs. temperature



APPLICATION INFORMATION

Fig. 10 - TV remote control receiver



LINEAR INTEGRATED CIRCUIT

NOT FOR NEW DESIGN

TV SIGNAL PROCESSING CIRCUIT

- VIDEO PREAMPLIFIER
- GATED AGC FOR VIDEO IF AMPLIFIER AND TUNER
- NOISE INVERTER CIRCUIT FOR GATING AGC AND SYNC. PULSE SEPARATOR
- HORIZONTAL SYNC. PULSE SEPARATOR
- BLANKING FACILITY

The TBA 311 is a monolithic integrated circuit in a 16-lead dual in-line or quad in-line plastic package. It is intended for use as signal processing circuit for black and white and colour television sets.

The circuit is designed for receivers equipped with tubes or transistors in the deflection and video output stages, and with PNP or NPN transistors in the tuner and NPN in the IF amplifier.

Only signals with the negative modulation can be handled by the circuit. The circuit is protected against short circuit between video output and ground.

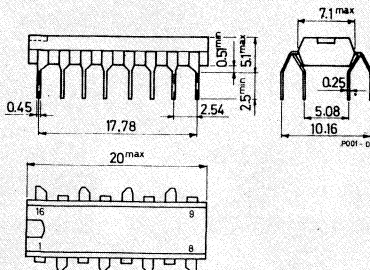
ABSOLUTE MAXIMUM RATINGS

V_s	DC supply voltage	16	V
P_{tot}	Power dissipation	500	mW
T_{stg}	Storage temperature	-55 to 125	°C
T_{op}	Operating temperature	0 to 70	°C

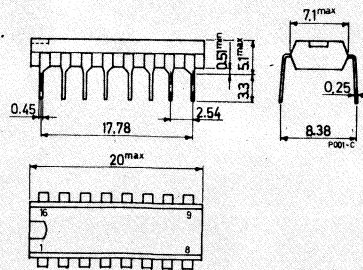
ORDERING NUMBERS: TBA 311 A22 (for 16-lead quad in-line plastic package)
TBA 311 A17 (for 16-lead dual in-line plastic package)

MECHANICAL DATA

Dimensions in mm



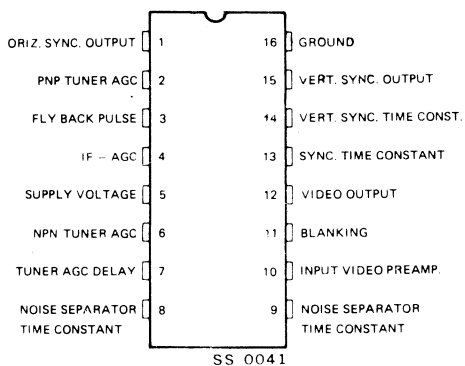
TBA 311 A22



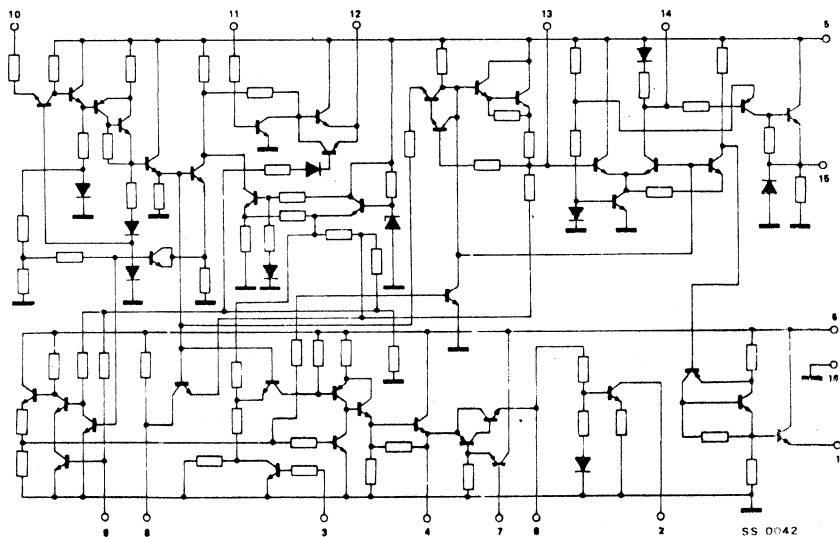
TBA 311 A17

TBA 311

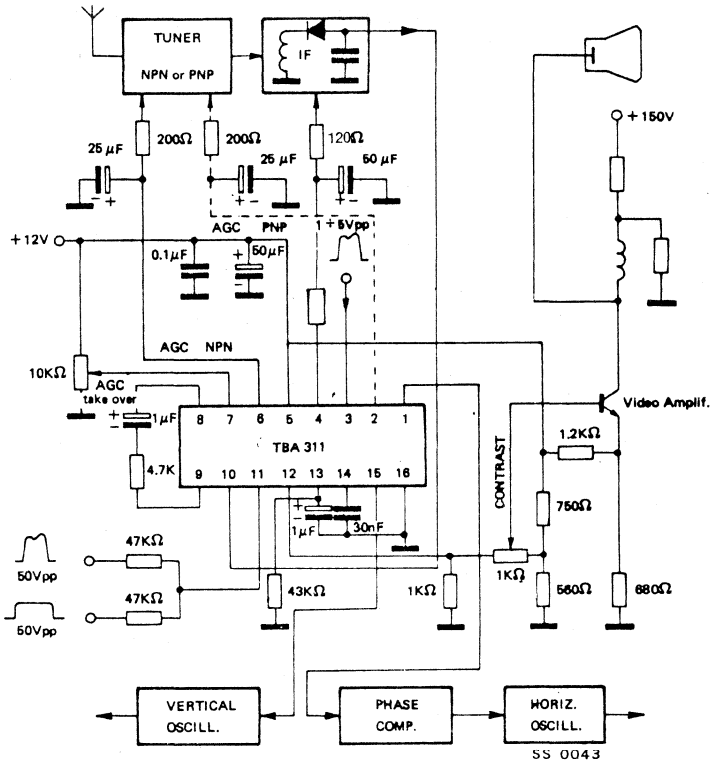
CONNECTION DIAGRAM (top view)



SCHEMATIC DIAGRAM



TEST CIRCUIT



TBA 311

ELECTRICAL CHARACTERISTICS (Refer to the test circuit. $T_{amb} = 25^{\circ}\text{C}$, $V_s = 12\text{V}$ unless otherwise specified)

Parameter	Min.	Typ.	Max.	Unit
I_d Quiescent drain current		14		mA

VIDEO AMPLIFIER

R_i Input resistance (pin 10)		2.7		$\text{k}\Omega$
C_i Input capacitance (pin 10)		0.8		pF
B Bandwidth (-3 dB)	5			MHz
G_v Voltage gain		9.5		dB
V_i Peak to peak video input voltage (pin 10) (1)		2		V
V_o Peak to peak video output voltage (pin 12) (2)		6		V
V Black level at the output (pin 12) (3)		5		V
I_o Available video peak output current (4)		20		mA
$\frac{\Delta V_o}{\Delta T_{amb}}$ Video output voltage temperature drift (5)		1		$\text{mV}/^{\circ}\text{C}$
$\frac{\Delta V}{\Delta T_{amb}}$ Black level temperature drift		0.2		$\text{mV}/^{\circ}\text{C}$
$\frac{\Delta V}{\Delta V_s}$ Black level drift at the output with supply voltage variation		0.5		—

VIDEO BLANKING

V_i Peak to peak input voltage (pin 11)	1		5	V
R_i Input resistance (pin 11)		1		$\text{k}\Omega$

AGC CIRCUIT

V Control voltage IF amplifier (pin 4)		0 to 7.5		V
V Control voltage tuner NPN (pin 6) PNP (pin 2)		0 to 6.5 12 to 6		V V
$\frac{\Delta V_i}{\Delta V}$ Signal expansion for full control of IF amplifier and tuner		10		%
V Peak to peak keying input pulse (pin 3) (6)	1		5	V
R_i Input resistance (pin 3)		2		$\text{k}\Omega$

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Min.	Typ.	Max.	Unit
-----------	------	------	------	------

SYNC. CIRCUITS

V_o	Output voltage of horizontal sync. pulse (pin 1)	8.4	10		V
Z_o	Horizontal output impedance (pin 1)		100		Ω
V_o	Output voltage of vertical sync. pulse (pin 15)	8.4	9.5		V
Z_o	Vertical output impedance (pin 15)		2		$k\Omega$

NOTES:

- 1) Negative going video signal (no pre-bias needed for the detector).
- 2) Video signal with negative going sync. pulse.
- 3) Only valid if the video signal is in accordance with the CCIR standard.
- 4) The total load on pin 12 must be such that under nominal conditions $I_o \leq 20$ mA.
- 5) Because the integrated circuit reaches 95% of its final working temperature in 100 seconds, the temperature variations to be considered are those caused by the slower rise in cabinet temperature and by changes in room temperature.
- 6) The TBA 311 may be operated unkeyed but then point 3 must be connected to the positive supply line via a resistor of suitable value (e.g. 10 $k\Omega$). However, the following consequence should be borne in mind:
 - The decoupling capacitors at the IF and tuner control points must be larger to prevent ripple voltages due to the vertical sync pulses. In consequence the AGC will not follow fast signal fluctuations (aircraft flutter).

TBA 331

LINEAR INTEGRATED CIRCUIT

GENERAL PURPOSE TRANSISTOR ARRAY

The TBA 331 is an array of 5 monolithic NPN transistors in a 14-lead dual in-line plastic package. Two transistors are internally connected to form a differential amplifier.

The transistors of the TBA 331 are well suited to low noise general purpose and to a wide variety of applications in low power systems in the DC through VHF range. They may be used as discrete components in conventional circuits; in addition, they provide the very significant inherent integrated circuit advantages of close electrical and thermal matching.

ABSOLUTE MAXIMUM RATINGS

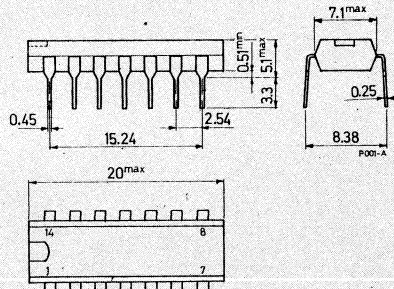
		Each transistor	Total package
V_{CBO}	Collector-base voltage ($I_E = 0$)	20	— V
V_{CEO}	Collector-emitter voltage ($I_B = 0$)	15	— V
V_{CSS}^*	Collector-substrate voltage	20	— V
V_{EBO}	Emitter-base voltage ($I_C = 0$)	5	— V
I_C	Collector current	50	— mA
P_{tot}	Total power dissipation at $T_{amb} \leq 55^\circ\text{C}$	300	750 mW
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$
T_{op}	Operating temperature	0 to 85	$^\circ\text{C}$

* The collector of each transistor of the TBA 331 is isolated from the substrate by an integrated diode. The substrate (pin 13) must be connected to the most negative point in the external circuit to maintain isolation between transistors and to provide for normal transistor action.

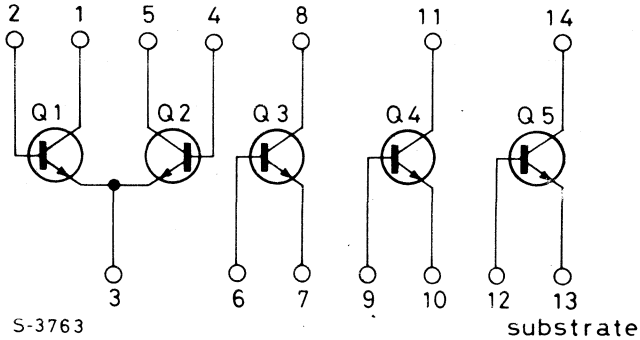
ORDERING NUMBER: TBA 331

MECHANICAL DATA

Dimensions in mm



SCHEMATIC DIAGRAM



THERMAL DATA

		each	Total
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	315° C/W
			126° C/W

ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^{\circ}\text{C}$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig.
I_{CBO} Collector cutoff current ($I_E = 0$)	$V_{CB} = 10\text{ V}$		0.002	40	nA	1
I_{CEO} Collector cutoff current ($I_B = 0$)	$V_{CE} = 10\text{ V}$		see curve	0.5	μA	2
$ I_{B1} - I_{B2} $ Input offset current	$I_C = 1\text{ mA}$ $V_{CE} = 3\text{ V}$		0.3	2	μA	7

TBA 331

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig.
V_{CBO}	Collector-base voltage ($I_E = 0$)					
	$I_C = 10 \mu A$	20	60		V	—
V_{CEO}	Collector-emitter voltage ($I_B = 0$)					
	$I_C = 1 \text{ mA}$	15	24		V	—
V_{CSS}	collector-substrate voltage ($I_{CSS} = 0$)					
	$I_C = 10 \mu A$	20	60		V	—
$V_{CE} \text{ (sat)}$	Collector-emitter saturation voltage					
	$I_B = 1 \text{ mA}$ $I_C = 10 \text{ mA}$		0.23		V	—
V_{EBO}	Emitter-base voltage ($I_C = 0$)					
	$I_E = 10 \mu A$	5	7		V	—
V_{BE}	Base-emitter voltage					
	$I_E = 1 \text{ mA}$ $V_{CE} = 3 \text{ V}$ $I_E = 10 \text{ mA}$ $V_{CE} = 3 \text{ V}$		0.715		V	4
			0.8		V	4
$ V_{BE1} - V_{BE2} $	Input offset voltage					
	$I_C = 1 \text{ mA}$ $V_{CE} = 3 \text{ V}$		0.45	5	mV	4-6
$ V_{BE3} - V_{BE4} $	Input offset voltage					
	$I_C = 1 \text{ mA}$ $V_{CE} = 3 \text{ V}$		0.45	5	mV	4-6
$ V_{BE4} - V_{BE5} $	Input offset voltage					
	$I_C = 1 \text{ mA}$ $V_{CE} = 3 \text{ V}$		0.45	5	mV	4-6
$ V_{BE5} - V_{BE4} $	Input offset voltage					
	$I_C = 1 \text{ mA}$ $V_{CE} = 3 \text{ V}$		0.45	5	mV	4-6
$\frac{\Delta V_{BE}}{\Delta T}$	Base-emitter voltage temperature coefficient					
	$I_C = 1 \text{ mA}$ $V_{CE} = 3 \text{ V}$		-1.9		mV/°C	5
$\frac{ V_{BE1} - V_{BE2} }{\Delta T}$	Input offset voltage temperature coefficient					
	$I_C = 1 \text{ mA}$ $V_{CE} = 3 \text{ V}$		1.1		$\mu V/^\circ C$	6

ELECTRICAL CHARACTERISTICS (continued)

Parameter		Test conditions	Min.	Typ.	Max.	Unit.	Fig.
h _{FE}	DC current gain	I _C = 10 mA V _{CE} = 3 V		100		—	3
		I _C = 1 mA V _{CE} = 3 V	40	100		—	3
		I _C = 10 μA V _{CE} = 3 V		54		—	3
f _T	Transition frequency	I _C = 3 mA V _{CE} = 3 V	300	550		MHz	14
NF	Noise figure	I _C = 100 μA V _{CE} = 3 V f = 1 KHz R _g = 1 kΩ		3.25		dB	8
H _{ie}	Input impedance	I _C = 1 mA V _{CE} = 3 V f = 1 kHz		3.5		kΩ	9
h _{fe}	Forward current transfer ratio	I _C = 1 mA V _{CE} = 3 V f = 1 kHz		110		—	9
h _{re}	Reverse voltage transfer ratio	I _C = 1 mA V _{CE} = 3 V f = 1 kHz		1.8×10 ⁻⁴		—	9
h _{oe}	Output admittance	I _C = 1 mA V _{CE} = 3 V f = 1 kHz		15.6		μS	9
Y _{ie}	Input admittance	I _C = 1 mA V _{CE} = 3 V f = 1 MHz		0.3+j0.04		mS	11
Y _{fe}	Forward transadmittance	I _C = 1 mA V _{CE} = 3 V f = 1 MHz		31-j1.5		mS	10
Y _{re}	Reverse transadmittance	I _C = 1 mA V _{CE} = 3 V f = 1 MHz		see curve		mS	13

TBA 331

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test Conditions	Min.	Typ.	Max.	Unit.	Fig.
Y_{ce}	Output admittance $I_C = 1 \text{ mA}$ $V_{CE} = 3 \text{ V}$ $f = 1 \text{ MHz}$					12
C_{EBO}	Emitter-base capacitance $I_C = 0$ $V_{EB} = 3 \text{ V}$		0.6		pF	—
C_{CBo}	Collector-base capacitance $I_E = 0$ $V_{CB} = 3 \text{ V}$		0.58		pF	—
C_{CSS}	Collector-sustrate capacitance $I_C = 0$ $V_{CSS} = 3 \text{ V}$		2.8		pF	—

Fig. 1 - Collector cutoff current vs ambient temperature

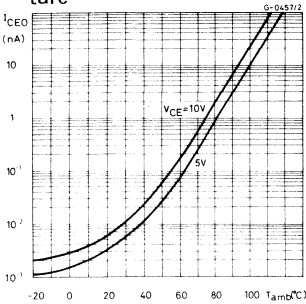


Fig. 2 - DC current gain vs. emitter current.

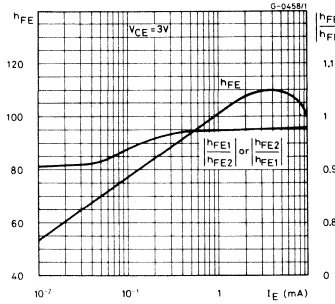


Fig. 3 - Input voltage and input offset voltage vs. emitter current

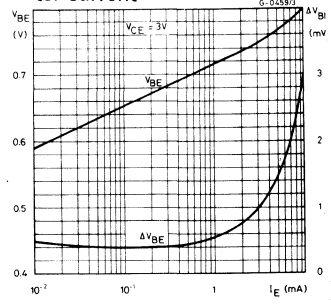


Fig. 4 - Input characteristic for each transistor

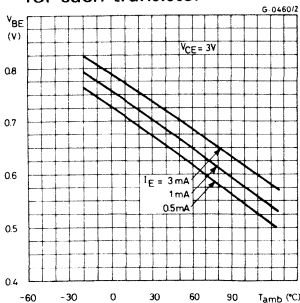


Fig. 5 - Input offset voltage vs. ambient temperature

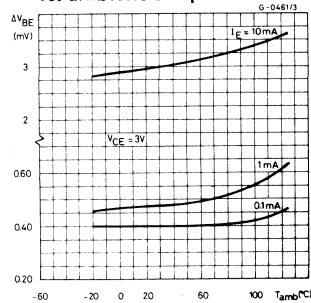


Fig. 6 - Input offset current for matched transistor pair

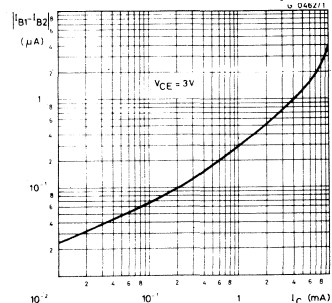


Fig. 7 - Noise figure vs collector current

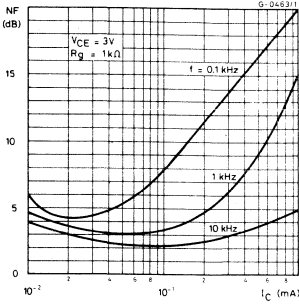


Fig. 8 - Forward admittance

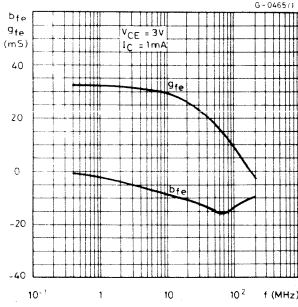


Fig. 9 - Input admittance

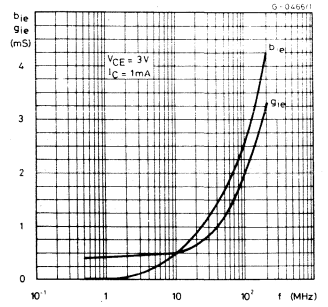


Fig. 10 - Output admittance

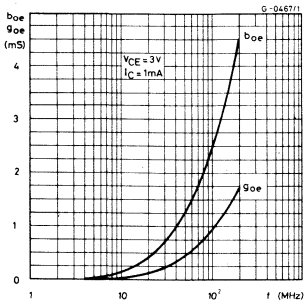


Fig. 11 - Reverse admittance

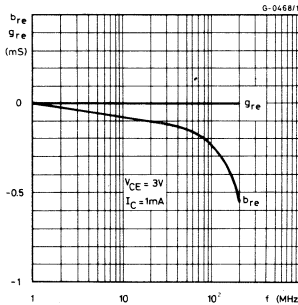
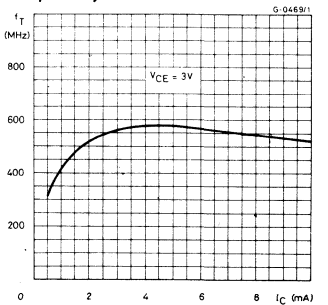


Fig. 12 - Transition frequency



TBA 435

LINEAR INTEGRATED CIRCUIT

NOT FOR NEW DESIGN

8.5V FIXED VOLTAGE REGULATOR

- OUTPUT CURRENT ≥ 100 mA
- LOAD REGULATION $\leq 1\%$
- RIPPLE REJECTION 57 dB TYPICAL
- OVERLOAD AND SHORT CIRCUIT PROTECTION

The TBA 435 is an integrated monolithic 8.5V voltage regulator in TO-39 metal case which can supply more than 100 mA. The device features high temperature stability, internal overload and short circuit protection, low output impedance and excellent transient response. The TBA 435 is intended for use in consumer and industrial applications.

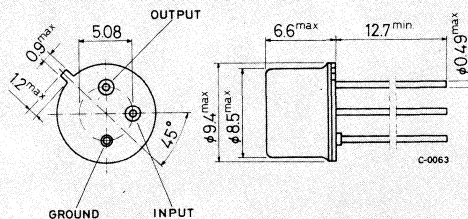
ABSOLUTE MAXIMUM RATINGS

V_i	Input voltage	20	V
P_{tot}	Power dissipation at $T_{amb} = 25^\circ\text{C}$	0.75	W
	at $T_{case} = 25^\circ\text{C}$	4	W
T_{stg}	Storage temperature	-55 to 150	$^\circ\text{C}$
T_j	Junction temperature	175	$^\circ\text{C}$
T_{op}	Operating temperature	0 to 70	$^\circ\text{C}$

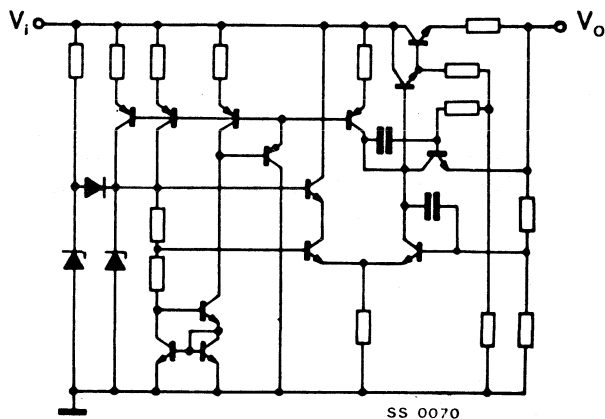
ORDERING NUMBER: TBA 435A X5

MECHANICAL DATA

Dimensions in mm



SCHEMATIC DIAGRAM



THERMAL DATA

$R_{th\ j-case}$	Thermal resistance junction-case	max	37.5	°C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	200	°C/W

ELECTRICAL CHARACTERISTICS ($T_j = 25^\circ\text{C}$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_o Output voltage	$V_i = 11.5\text{V to } 20\text{V}$ $I_o = 5\text{ mA}$ $C_L = 10\ \mu\text{F}$	8.1	8.5	8.9	V
$\frac{\Delta V_o}{V_o}$ Load regulation	$V_i = 11.5\text{V to } 20\text{V}$ $I_o = 5\text{ mA to } 100\text{ mA}$ $C_L = 10\ \mu\text{F}$		0.3	1	%
I_o Regulated output current	$V_i = 15\text{V}; \frac{\Delta V_o}{V_o} \leq 1\%$	100	140		mA
I_o Max. output current	$V_i = 15\text{V}$	130	150	200	mA
R_o Output resistance	$V_i = 15\text{V}$ $I_o = 5\text{ mA to } 100\text{ mA}$		0.1		Ω
$\frac{\Delta V_o}{V_o}$ Line regulation	$V_i = 11.5\text{V to } 20\text{V}$ $I_o = 5\text{ mA}$		0.15	0.6	%
SVR Supply voltage rejection	$V_i = 13.5\text{V}$ $\Delta V_i = 4\text{ V}_{pp}$ $I_o = 5\text{ mA}$ $C_L = 10\ \mu\text{F}$ $f = 100\text{ Hz}$	46	57		dB
e_N Output noise voltage	$V_i = 15\text{V}$ $I_o = 5\text{ mA}$ $C_L = 10\ \mu\text{F}$ $B = 100\text{ Hz to } 100\text{ kHz}$		100		μV

TBA 435

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
I_d Quiescent drain current	$V_i = 20V$ $I_o = 0$	5	9	16	mA
$\frac{\Delta V_o}{\Delta T_{amb}}$ Temperature coefficient	$V_i = 15V$ $I_o = 5 mA$ $C_L = 10 \mu F$ $T_{amb} = 0 \text{ to } 70^\circ C$		0.85		mV/ $^\circ C$
I_{sc} Output short circuit current	$V_i = 20V$ $V_o = 0$		40	60	mA

Fig. 1 - Output voltage vs. output current

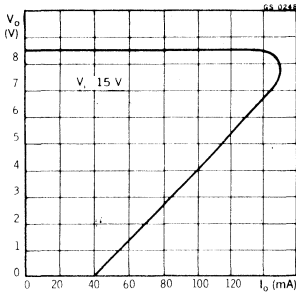


Fig. 4 - Supply ripple rejection vs. regulated output current

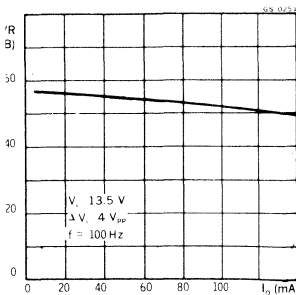


Fig. 2 - Power rating chart

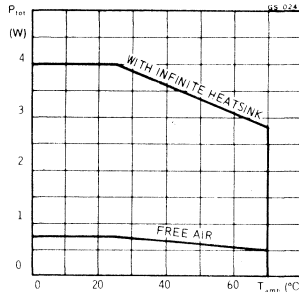


Fig. 5 - Supply ripple rejection vs. frequency

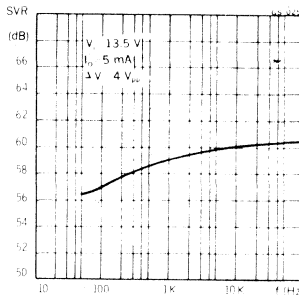


Fig. 3 - Maximum output current vs. junction temperature

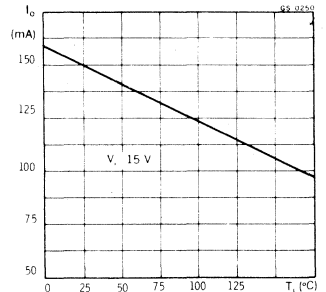


Fig. 6 - Maximum output current vs. input voltage

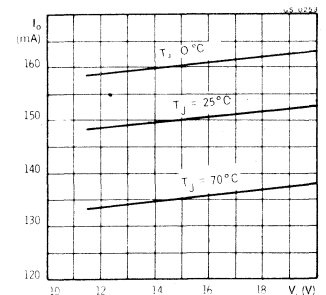


Fig. 7 - Output short circuit current vs. input voltage

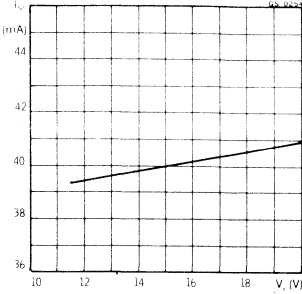


Fig. 8 - Output short circuit current vs. junction temperature

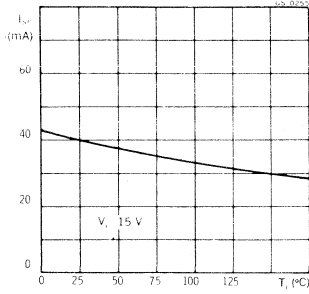


Fig. 9 - Dropout voltage vs. output current

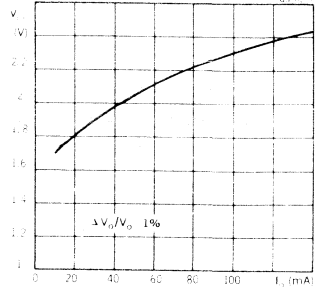


Fig. 10 - Quiescent drain current vs. junction temperature

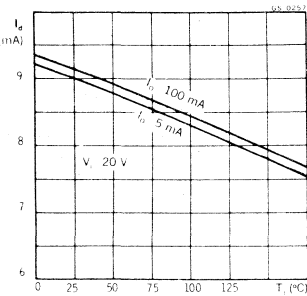


Fig. 11 - Quiescent drain current vs. input voltage

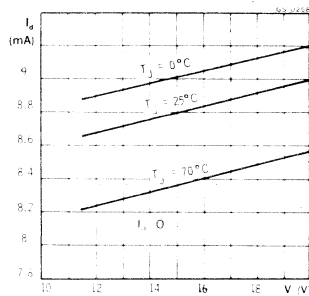
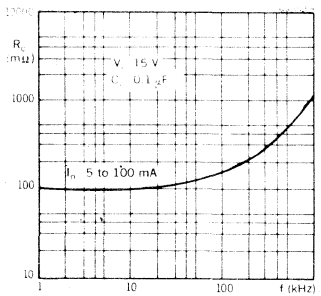
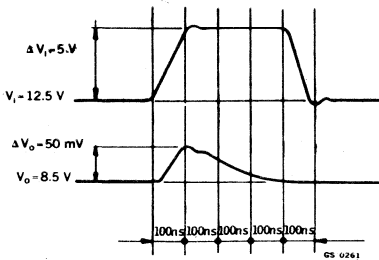


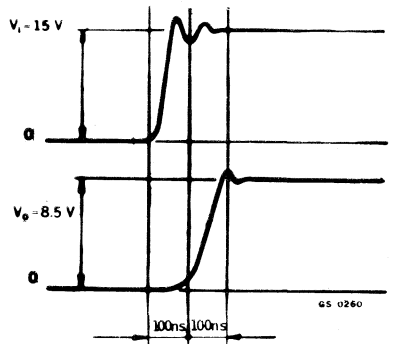
Fig. 12 - Output resistance vs. frequency



Line transient response ($I_o = 5 mA$)



Turn-on time ($I_o = 100 mA$)



TBA 435

TYPICAL APPLICATIONS

Fig. 13 – Positive output voltage regulator

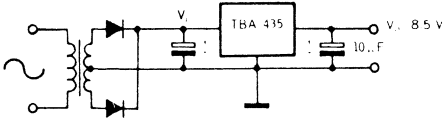


Fig. 14 – Negative output voltage regulator

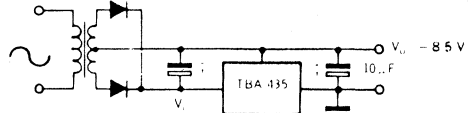
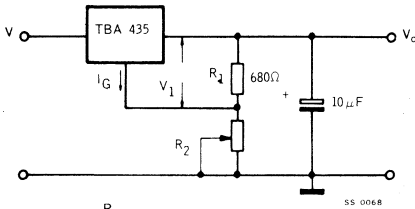


Fig. 15 – Adjustable output voltage regulator



$$V_o = V_1 \left(1 + \frac{R_2}{R_1} \right) + I_G R_2$$

$V_1 = 1.8 \text{ V}$

$V_o = 8.5 \text{ to } 11 \text{ V}$

$I_o > 80 \text{ mA}$

$R_o = 100 \text{ m}\Omega$

R_2 - potentiometer 0 to 150 Ω

Adjustable output voltage vs. output current.

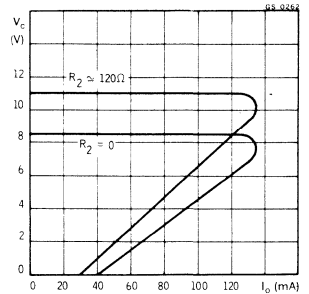
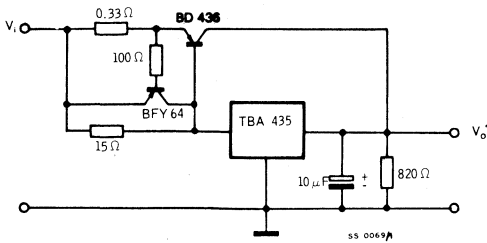


Fig. 16 – PNP current boost circuit



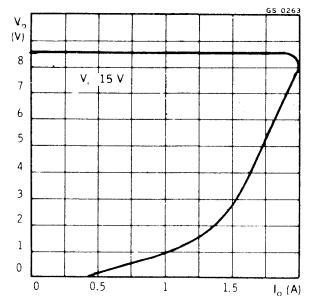
$V_i = 15 \text{ V}$

$V_o = 8.5 \text{ V}$

$I_o = 2 \text{ A}$

$R_o = 20 \text{ m}\Omega$

Output voltage vs. output current.



LINEAR INTEGRATED CIRCUITS

NOT FOR NEW DESIGN

3-TERMINAL POSITIVE VOLTAGE REGULATORS

- OUTPUT VOLTAGE: 5, 12 and 15V
- OUTPUT CURRENT ≥ 100 mA
- LOAD REGULATION $\leq 1\%$
- RIPPLE REJECTION 51 dB TYPICAL
- OVERLOAD AND SHORT CIRCUIT PROTECTION

The TBA 625A/B/C are monolithic integrated voltage regulators in TO-39 metal case which can supply more than 100 mA. The devices feature high temperature stability, internal overload and short circuit protection, low output impedance and excellent transient response. They are intended for use as voltage supply for digital circuits with high noise immunity, linear integrated circuits and for any other industrial applications.

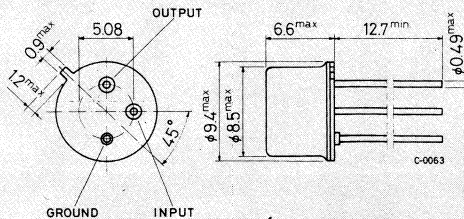
ABSOLUTE MAXIMUM RATINGS

V_i	Input voltage	TBA 625A TBA 625B/C	20 27	V V
P_{tot}	Power dissipation at $T_{amb} = 25^\circ\text{C}$ at $T_{case} = 25^\circ\text{C}$		0.75 4	W W
T_{op}	Storage temperature		-55 to 150	$^\circ\text{C}$
T_j	Junction temperature		175	$^\circ\text{C}$
T_{op}	Operating temperature		0 to 70	$^\circ\text{C}$

ORDERING NUMBERS: TBA 625A X5 ($V_o = 5\text{V}$)
TBA 625B X5 ($V_o = 12\text{V}$)
TBA 625C X5 ($V_o = 15\text{V}$)

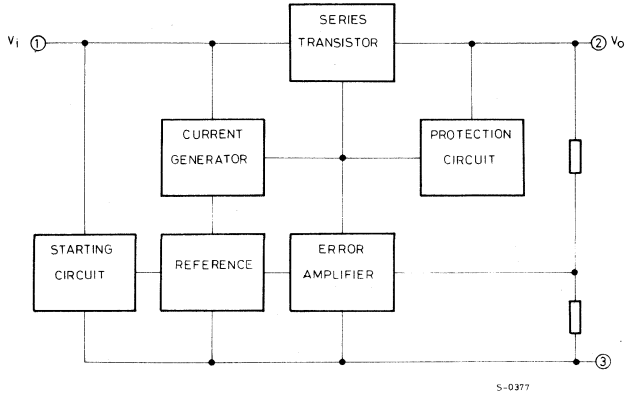
MECHANICAL DATA

Dimensions in mm

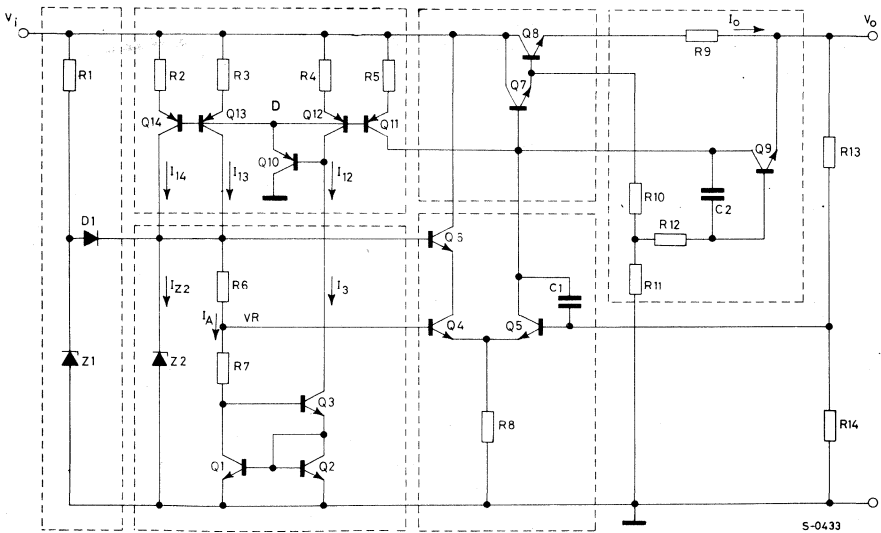


TBA 625A TBA 625B TBA 625C

BLOCK DIAGRAM



SCHEMATIC DIAGRAM



THERMAL DATA

$R_{th\ j-case}$	Thermal resistance junction-case	max	37.5	°C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	200	°C/W

ELECTRICAL CHARACTERISTICS ($C_L = 10\ \mu F$, $T_j = 25^\circ C$, $I_o = 5\ mA$ unless otherwise specified)

Parameter			Test conditions	Min.	Typ.	Max.	Unit
V_o	Output voltage	TBA 625A TBA 625B TBA 625C	$V_i = 8\ to\ 20V$ $V_i = 15\ to\ 27V$ $V_i = 18\ to\ 27V$	4.75 11.4 14.25	5 12 15	5.25 12.6 15.75	V
$\frac{\Delta V_o}{V_o}$	Load regulation		$I_o = 5\ mA\ to\ 100\ mA$		0.3	1	%
I_o	Regulated output current		$\frac{\Delta V_o}{V_o} \leq 1\%$	100	140		mA
I_o	Max. regulated output current			120	150	250	mA
R_o	Output resistance		$I_o = 5\ mA\ to\ 100\ mA$		0.1		Ω
$\frac{\Delta V_o}{V_o}$	Line regulation	TBA 625A TBA 625B TBA 625C	$V_i = 8\ to\ 20V$ $V_i = 15\ to\ 22V$ $V_i = 18\ to\ 27V$		0.2 0.2 0.25	1 0.5 0.5	%
SVR	Supply voltage rejection		$\Delta V_i = 4\ V_{pp}$ $f = 100\ Hz$	46			dB
e_N	Output noise voltage	TBA 625A TBA 625B TBA 625C	$B = 10\ Hz\ to\ 100\ kHz$		70 150 200		μV
I_d	Quiescent drain current	TBA 625A TBA 625B/C		5 6	9 10	16 18	mA
$\frac{\Delta V_o}{\Delta T_{amb}}$	Temperature coefficient	TBA 625A TBA 625B TBA 625C	$T_{amb} = 0\ to\ 70^\circ C$		0.5 0.85 1.5		mV/°C
I_{sc}	Output short circ. current	TBA 625A TBA 625B TBA 625C			45 35 30	65 55 50	mA

TBA 625A TBA 625B TBA 625C

Fig. 1 -- Output voltage vs. output current (TBA 625A)

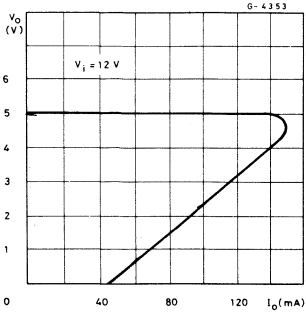


Fig. 2 -- Output voltage vs. output current (TBA 625B)

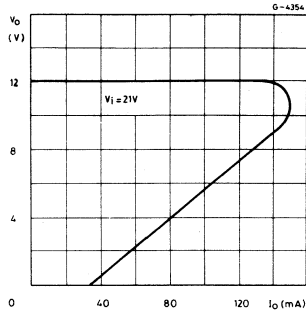


Fig. 3 -- Output voltage vs. output current (TBA 625C)

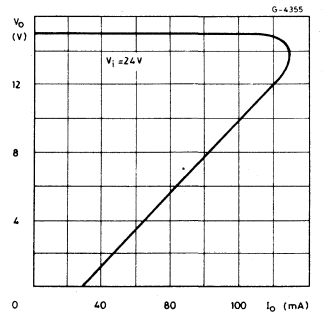


Fig. 4 -- Power rating chart

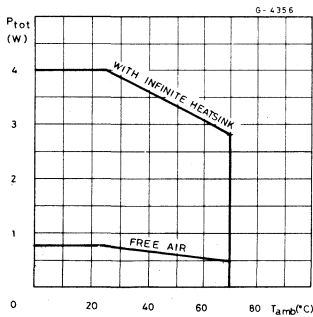


Fig. 5 -- Maximum output current vs. junction temperature

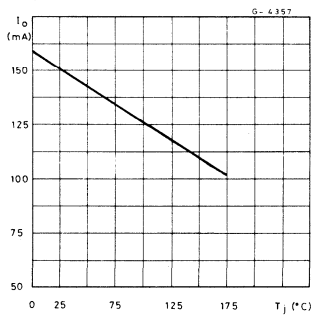


Fig. 6 -- Ripple rejection vs. regulated output current

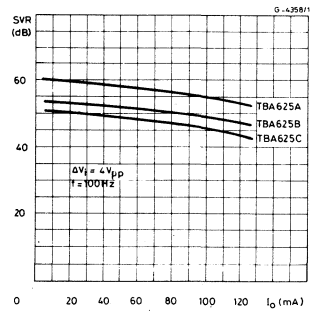


Fig. 7 -- Maximum output current vs. input voltage (TBA 625A)

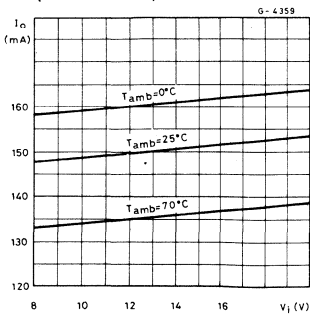


Fig. 8 -- Maximum output current vs. input voltage (TBA 625B)

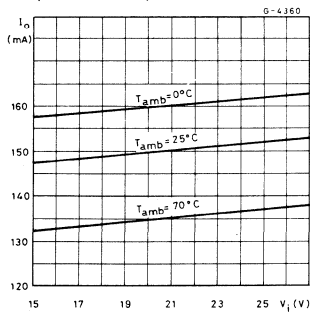


Fig. 9 -- Maximum output current vs. input voltage (TBA 625C)

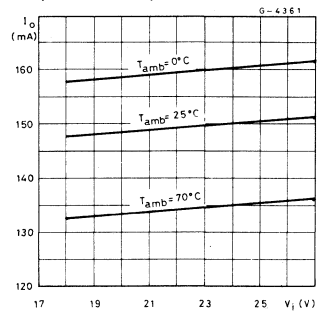


Fig. 10 - Ripple rejection vs. frequency

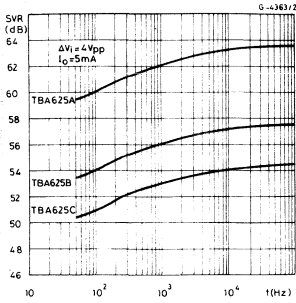


Fig. 11 - Output short circuit current vs. input voltage (TBA 625A)

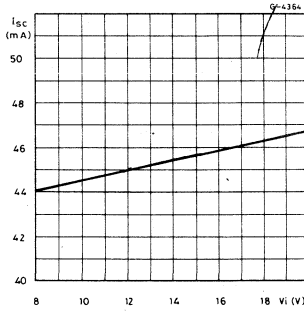


Fig. 12 - Output short circuit current vs. input voltage (TBA 625B/C)

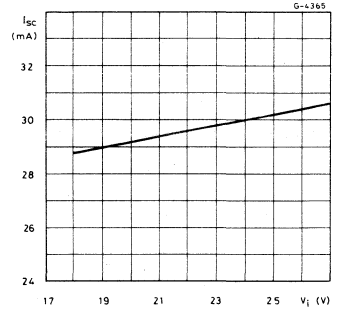


Fig. 13 - Output short circuit current vs. junction temperature

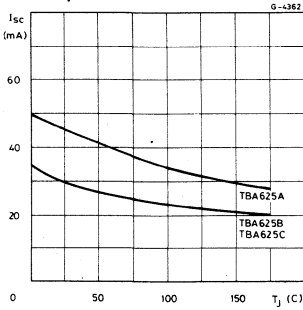


Fig. 14 - Dropout voltage vs. output current

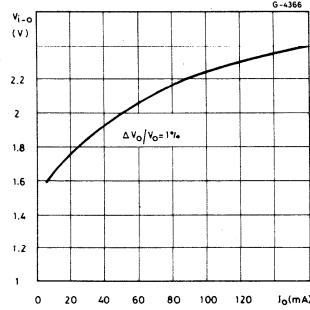


Fig. 15 - Output resistance vs. frequency

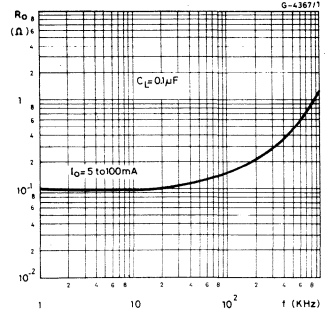


Fig. 16 - Quiescent drain current vs. input voltage (TBA 625A)

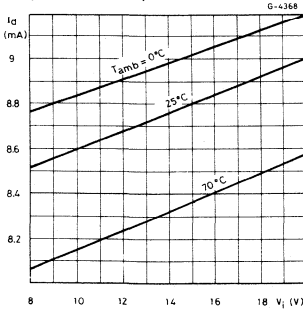


Fig. 17 - Quiescent drain current vs. input voltage (TBA 625B)

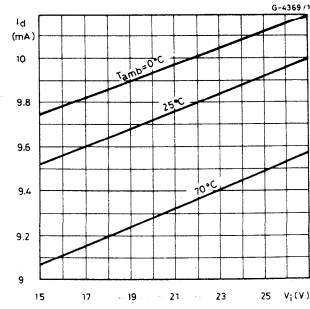
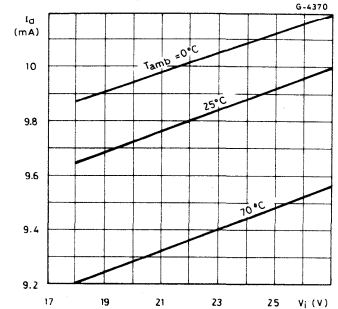


Fig. 18 - Quiescent drain current vs. input voltage (TBA 625C)



TBA 625A TBA 625B TBA 625C

Fig. 19 - Line transient response (TBA 625A)

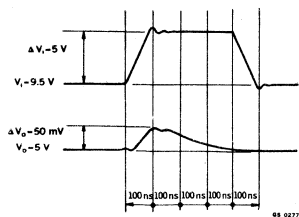


Fig. 20 - Line transient response (TBA 625B)

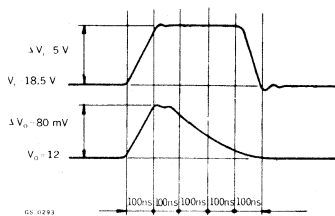


Fig. 21 - Line transient response (TBA 625C)

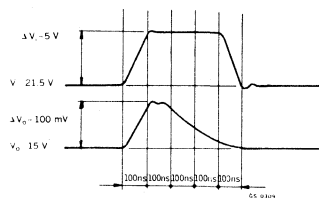


Fig. 22 - Turn-on time ($I_o = 100$ mA) TBA 625A

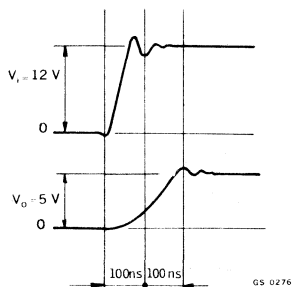


Fig. 23 - Turn-on time ($I_o = 100$ mA) TBA 625B

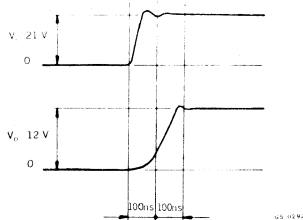
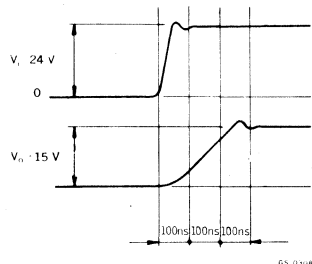
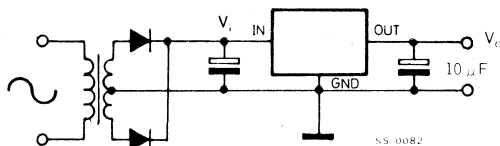


Fig. 24 - Turn-on time ($I_o = 100$ mA) TBA 625C



TYPICAL APPLICATION

Fig. 25 - Positive voltage regulator

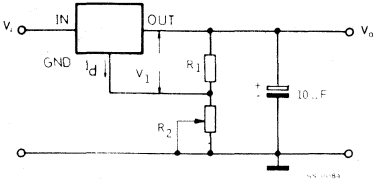


TYPICAL APPLICATION (continued)

Fig. 26 - Adjustable voltage regulator

$$V_o = V_1 (1 + R_2/R_1) + I_d R_2$$

$$R_o \cong 100 \text{ m}\Omega$$



	TBA 625A	TBA 625B	TBA 625C
V_i (V)	16	24	26
V_o (V)	5 ÷ 9	12 ÷ 15	15 ÷ 17
R_1 (Ω)	430	1000	1200
R_2 (Ω)	250	150	150

Fig. 27 - Adjustable output voltage vs. output current (TBA 625A)

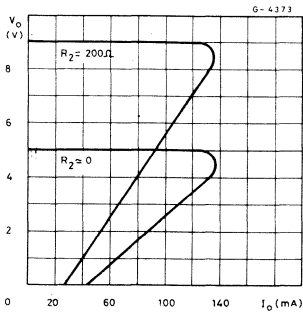


Fig. 28 - Adjustable output voltage vs. output current (TBA 625B)

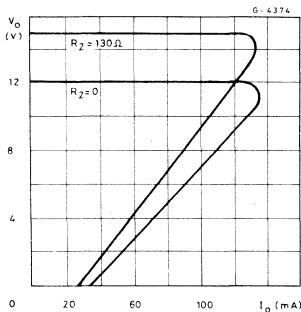


Fig. 29 - Adjustable output voltage vs. output current (TBA 625C)

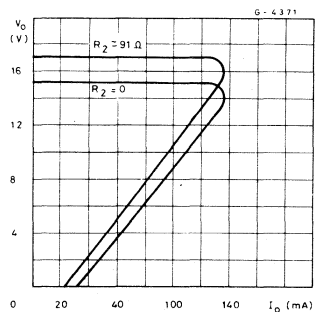
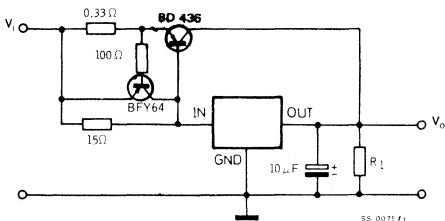


Fig. 30 - 2A PNP current boost circuit ($R_o \cong 20 \text{ m}\Omega$)



	TBA 625A	TBA 625B	TBA 625C
V_i (V)	12	21	24
V_o (V)	5	12	15
R_1 (Ω)	500	1200	1500

TBA 625A
TBA 625B
TBA 625C

Fig. 31 - Output voltage vs. output current (2A max) TBA 625A

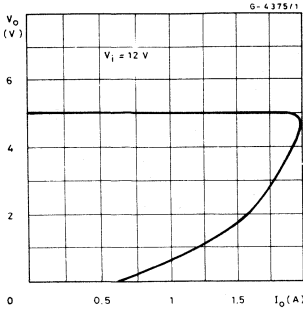


Fig. 32 - Output voltage vs. output current (2A max) TBA 625B

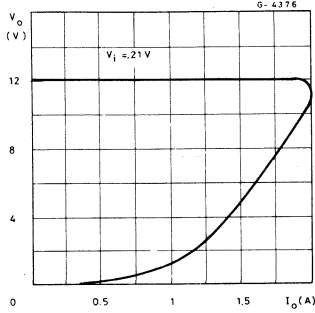
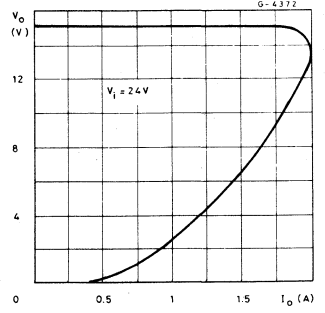


Fig. 33 - Output voltage vs. output current (2A max) TBA 625C



TBA 800

LINEAR INTEGRATED CIRCUIT

5W AUDIO POWER AMPLIFIER

The TBA 800 is a monolithic integrated power amplifier in a 12-lead quad in-line plastic package. The external cooling tabs enable 2.5W output power to be achieved without external heatsink and 5W output power using a small area of the P.C. board copper as a heatsink. It is intended for use as a low frequency Class B amplifier.

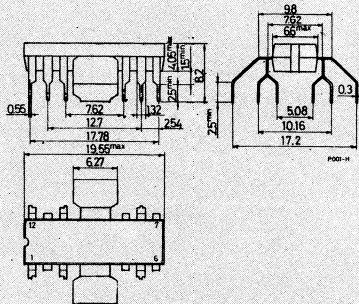
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	30	V
I_o	Peak output current (non repetitive)	2	A
I_o	Peak output current (repetitive)	1.5	A
P_{tot}	Power dissipation at $T_{amb} = 80^\circ\text{C}$ at $T_{tab} = 90^\circ\text{C}$	1	W
T_{stg}, T_j	Storage and junction temperature	5	W
		-40 to 150	$^\circ\text{C}$

ORDERING NUMBER: TBA 800

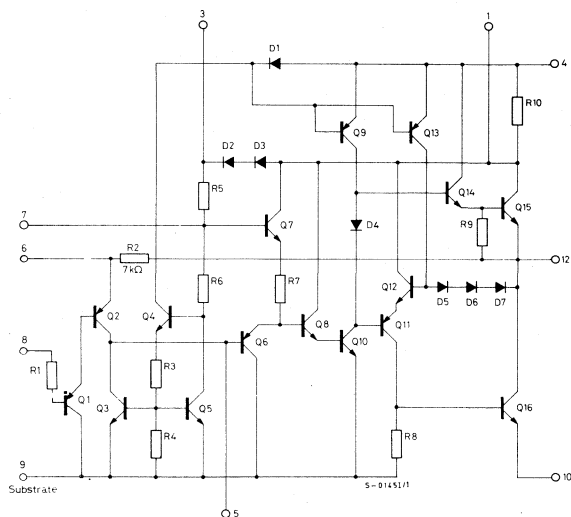
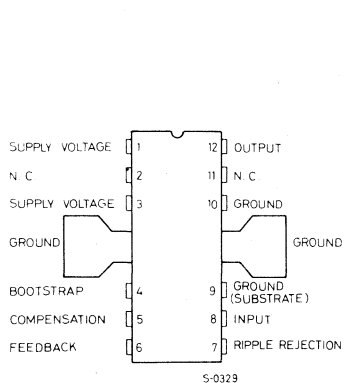
MECHANICAL DATA

Dimensions in mm

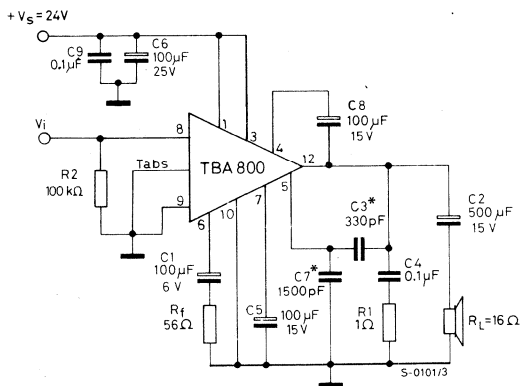


TBA 800

CONNECTION AND SCHEMATIC DIAGRAMS (top view)



TEST CIRCUIT



* C3, C7 see fig. 5.

THERMAL DATA

$R_{th\ j-tab}$	Thermal resistance junction-tab	max	12	°C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	70*	°C/W

* Obtained with tabs soldered to printed circuit with minimized copper area.

ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $T_{amb}=25^{\circ}C$, $V_s=24V$, $R_L=16\Omega$, unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	
V_O	Quiescent output voltage (pin 12)	11	12	13	V	
I_d	Quiescent drain current		9	20	mA	
I_b	Input bias current (pin 8)		1	5	μA	
P_O	Output power	$d = 10\%$ $f = 1\text{ kHz}$	4.4	5	W	
$V_{i(rms)}$	Input saturation voltage		220		mV	
V_i^*	Input sensitivity	$P_O = 5W$ $f = 1\text{ kHz}$		80	mV	
R_i	Input resistance (pin 8)	$f = 1\text{ KHz}$		5	$M\Omega$	
B	Frequency response (-3 dB)	$C3 = 330\text{ pF}$	40 to 20,000			Hz
d	Distortion	$P_O = 50\text{ mW to }2.5W$ $f = 1\text{ kHz}$		0.5	%	
G_v	Voltage gain (open loop)	$f = 1\text{ kHz}$		80	dB	
G_v	Voltage gain (closed loop)	$f = 1\text{ kHz}$	39	42	45	dB
e_N	Input noise voltage	$B = 22\text{ Hz to }22\text{ KHz}$		5	μV	
i_N	Input noise current			0.2	nA	
η	Efficiency	$P_O = 5W$ $f = 1\text{ kHz}$		75	%	
SVR	Supply voltage rejection	$f_{ripple} = 100\text{ Hz}$ $C5 = 25\text{ }\mu F$ $C5 = 100\text{ }\mu F$		35 38	dB dB	
I_d	Drain current	$P_O = 5W$		280	mA	

* See fig. 6.

TBA 800

Fig. 1 - Output power vs. supply voltage

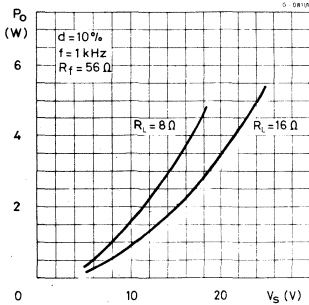


Fig. 2 - Maximum power dissipation vs. supply voltage

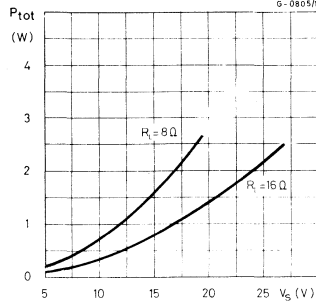


Fig. 3 - Distortion vs. output power

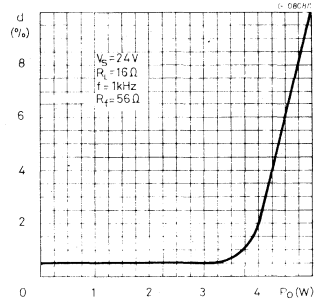


Fig. 4 - Distortion vs. frequency

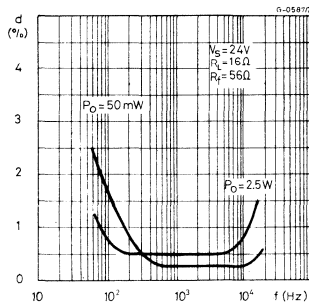


Fig. 5 - Value of C3 vs. Rf for various values of B

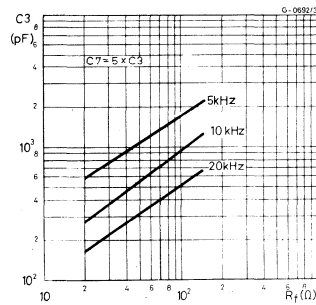


Fig. 6 - Voltage gain (closed loop) and input voltage vs. Rf

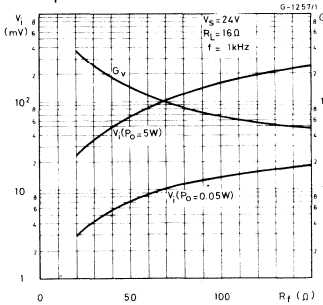


Fig. 7 - Power dissipation and efficiency vs. output power

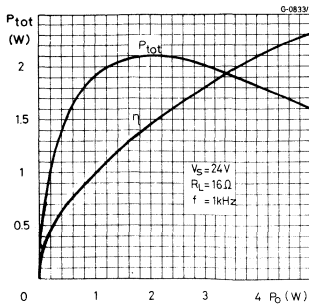


Fig. 8 - Quiescent output voltage (pin 12) vs. supply voltage

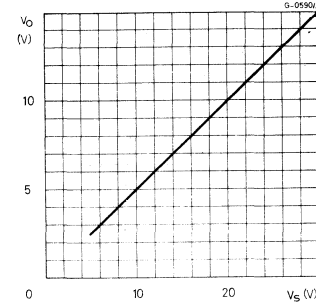
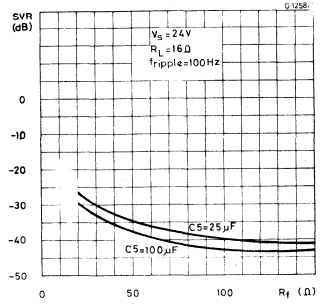
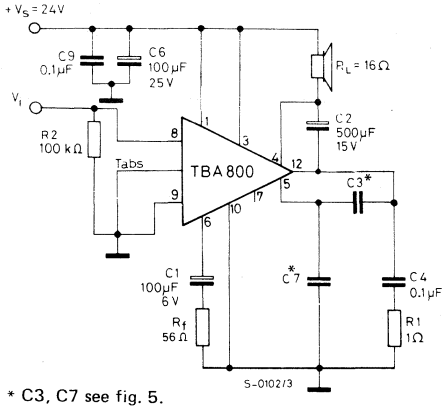


Fig. 9 - Supply voltage rejection vs. Rf



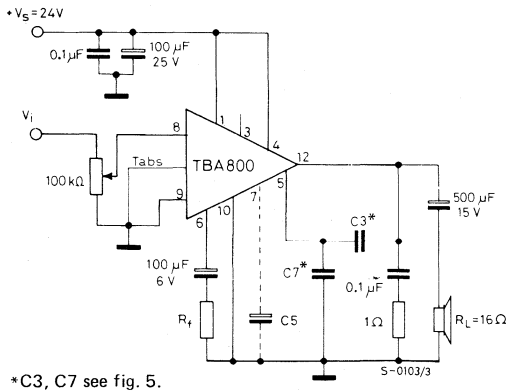
APPLICATION INFORMATION

Fig. 10 - Circuit with the load connected to the supply voltage



Compared with the other circuits, this configuration entails a lower number of external components and can be used at low supply voltages.

Fig. 11 - Circuit with load connected to ground without bootstrap.



This circuit is only for use at high voltages. The pin 3 is left open circuit, this automatically inserts diodes D2-D3 (see schematic diagram) and this enables a symmetrical wave to be obtained at the output. Refer to figs. 12 and 13 for distortion and output power.

TBA 800

Fig. 12 - Distortion vs. output power (fig. 11 circuit)

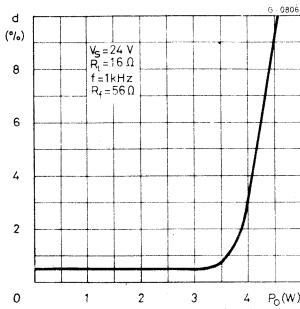


Fig. 13 - Output power vs. supply voltage (fig. 11 circuit)

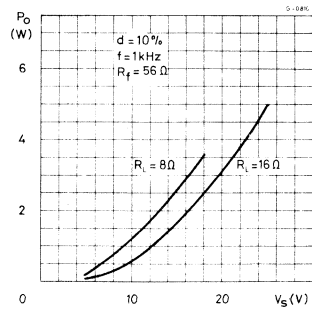
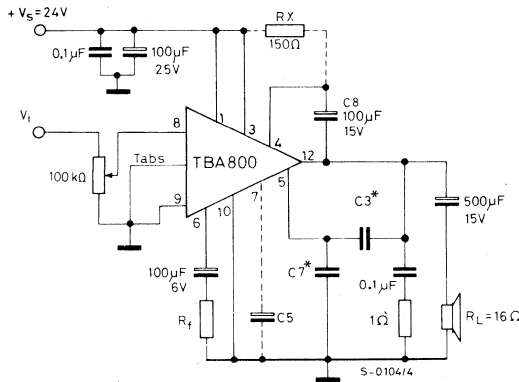


Fig. 14 - Circuit with load connected to ground and with bootstrap.



The bootstrap capacitor C8 enables the same electrical characteristics as those of the test circuit to be achieved. For low supply voltage operation (e.g. 9 to 14V), R_X (150 Ω) is connected between pin 1 and pin 4.

N.B. - For the circuits of figures 11 and 14 an excellent supply voltage ripple rejection is obtained by connecting the capacitor C5 (10 to 100 μ F - 15V) between pin 7 and ground.

MOUNTING INSTRUCTIONS

The tabs on the TBA 800 can be used to conduct away the heat generated in the integrated circuit so that the junction temperature does not exceed the permissible maximum (150 °C).

This may be done by connecting tabs to an external heatsink, or by soldering them to a suitable copper area of the printed circuit board (fig. 15 a).

Fig. 15b shows a simple type of heatsink. Assuming a copper area on the printed circuit board of only 2 cm², the total R_{th} between junction to ambient is approximately 28 °C/W.

External heatsink or printed circuit copper area must be connected to electrical ground.

In the latter case, fig. 16 shows the maximum dissipated power (for $T_{amb} = 55^{\circ}\text{C}$ and $T_{amb} = 70^{\circ}\text{C}$) as a function of the side of two equal square copper areas having a thickness of 35 μ (1.4 mils).

Fig. 15a - Example of a copper area of PC board soldered to the tabs of the TBA 800 which is used as a heatsink.

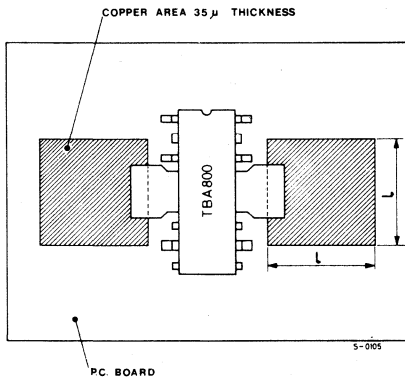


Fig. 15b - Example of TBA 800 with external heatsink.

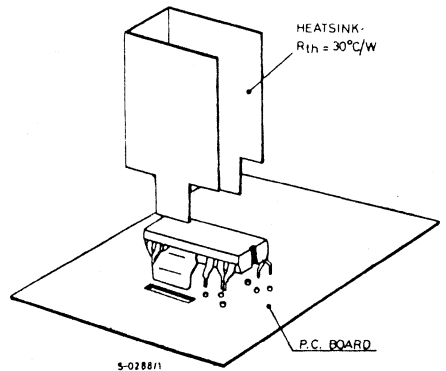


Fig. 16 - Power dissipation vs. "l".

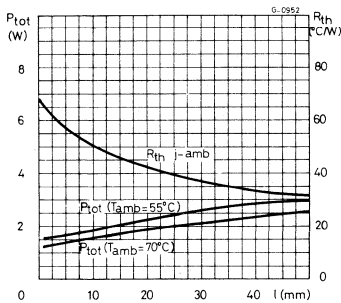
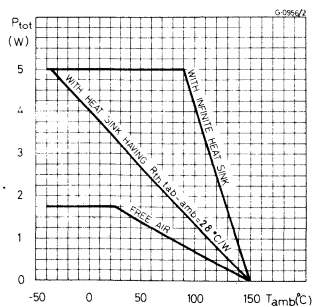


Fig. 17 - Power rating characteristics



TBA 800

Fig. 18 - P.C. board and component layout of the test circuit (1:1 scale)

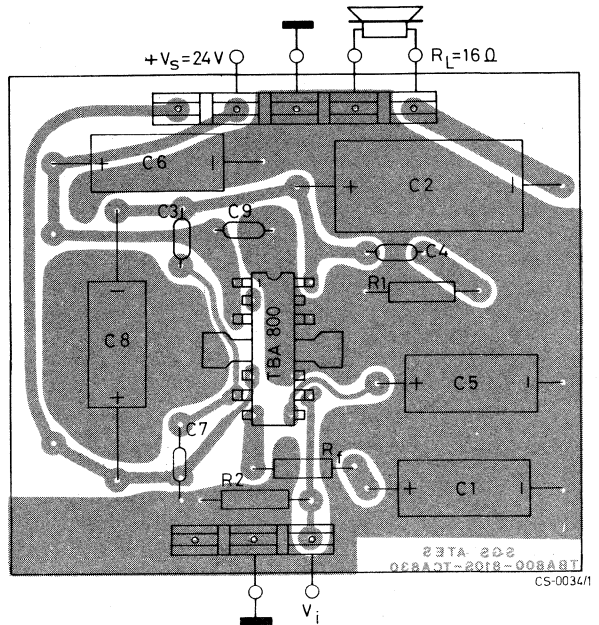
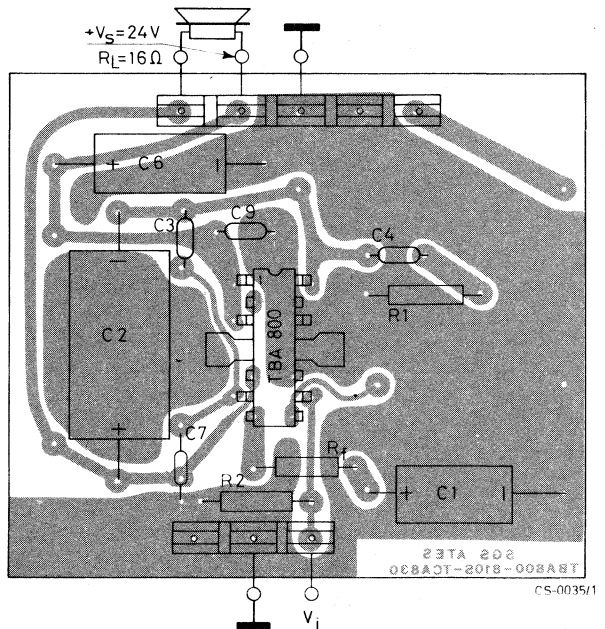


Fig. 19 - P.C. board and component layout of the fig. 10 circuit (1:1 scale)



DESIGN OF HEATSINK COPPER AREA

1) Calculation of maximum power dissipation

$$P_{\text{tot}} = 0.4 \cdot \frac{V_{s \text{ max}}^2}{8 R_L} + V_{s \text{ max}} I_d$$

where:

$V_{s \text{ max}}$ = maximum value of supply voltage (increase 10% if not stabilized)

R_L = load resistance

I_d = quiescent drain current; maximum value at $V_S = 24\text{V}$ is 20 mA (for worst case design).

2) From fig. 16 and knowing $T_{\text{amb max}}$, calculate ℓ .

Examples:

a) V_S (not stabilized) = 24V; $R_L = 16\Omega$; $T_{\text{amb max}} = 55^\circ\text{C}$.

$$P_{\text{tot}} = 0.4 \cdot \frac{(24 + 2.4)^2}{8 \cdot 16} + (24 + 2.4) \cdot 20 \cdot 10^{-3} = 2.6\text{W}$$

From fig. 16 and for $T_{\text{amb max}} = 55^\circ\text{C}$, $\ell \cong 25 \text{ mm}$.

For geometries different from the one of fig. 15a note that copper areas near the tabs have better efficiency as regards power dissipation, Therefore additional safety factors must be added for worst case design.

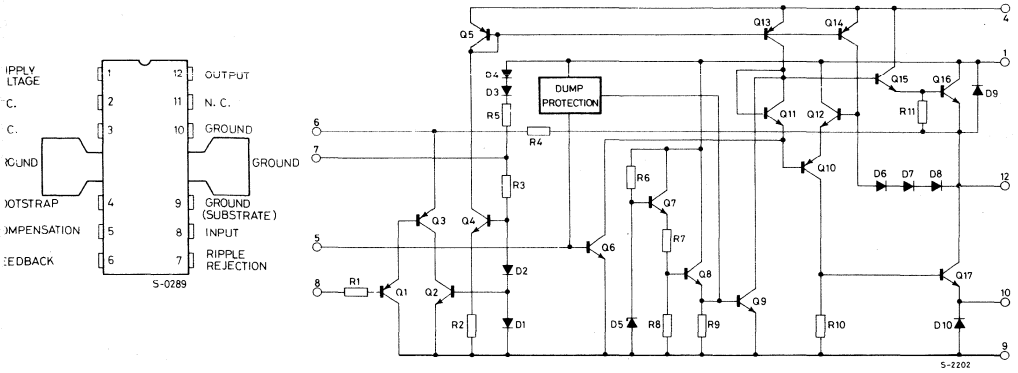
b) V_S (stabilized) = 12V; $R_L = 8\Omega$.

$$P_{\text{tot}} = 0.4 \cdot \frac{12^2}{8 \cdot 8} + 0.02 \cdot 12 = 1\text{W}$$

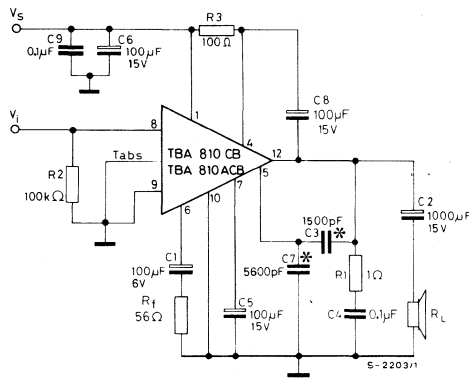
The fig. 16 shows that no heat sink is required if $T_{\text{amb}} \leq 55^\circ\text{C}$.

TBA 810 CB TBA 810 ACB

CONNECTION AND SCHEMATIC DIAGRAMS (top view)



TEST AND APPLICATION CIRCUIT



*C3, C7 SEE FIG. 6

THERMAL DATA

			TBA 810CB	TBA 810ACB
$R_{th \text{ j-tab}}$	Thermal resistance junction-tab	max	12 °C/W	10 °C/W
$R_{th \text{ j-amb}}$	Thermal resistance junction-ambient	max	70* °C/W	80 °C/W

* Obtained with tabs soldered to printed circuit with minimized copper area.

TBA 810CB

TBA 810ACB

ELECTRICAL CHARACTERISTICS (Refer to the test circuit; $V_s = 14.4\text{V}$, $T_{\text{amb}} = 25^\circ\text{C}$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit		
V_s	Supply voltage (pin 1)	4		20	V		
V_o	Quiescent output voltage (pin 12)	6.4	7.2	8	V		
I_d	Quiescent drain current		12	20	mA		
I_b	Input bias current (pin 8)		0.4		μA		
P_o	Output power	d = 10% $R_L = 4\Omega$ $R_L = 2\Omega$	f = 1 kHz 5.5 5.5	6 7	W W		
$V_{i(\text{rms})}$	Input saturation voltage		220		mV		
V_i	Input sensitivity	f = 1 kHz $P_o = 6\text{W}$ $R_f = 56\Omega$ $R_f = 22\Omega$ $P_o = 7\text{W}$ $R_f = 56\Omega$ $R_f = 22\Omega$	$R_L = 4\Omega$ $R_L = 2\Omega$	75 30 55 20	mV mV mV mV		
R_i	Input resistance (pin 8)		5		$\text{M}\Omega$		
B	Frequency response (-3 dB)	$R_L = 4\Omega/2\Omega$ $C_3 = 820\text{ pF}$ $C_3 = 1500\text{ pF}$		40 to 20 000 40 to 10 000	Hz Hz		
d	Distortion	$P_o = 50\text{ mW}$ to 2.5W $R_L = 4\Omega/2\Omega$ f = 1 kHz		0.3	%		
G_v	Voltage gain (open loop)	$R_L = 4\Omega$	f = 1 kHz	80	dB		
G_v	Voltage gain (closed loop)	$R_L = 4\Omega/2\Omega$	f = 1 kHz	34	37	40	dB
e_N	Input noise voltage	$V_s = 16\text{V}$		2	μV		
i_N	Input noise current	B (-3 dB) = 40 to 15 000 Hz		80	pA		
η	Efficiency	$P_o = 6\text{W}$ f = 1 kHz	$R_L = 4\Omega$	75	%		
SVR	Supply voltage rejection	$R_L = 4\Omega$ $i_{\text{ripple}} = 100\text{ Hz}$	$V_{\text{ripple}} = 1\text{ V}_{\text{rms}}$	40	48	dB	

TBA 810CB TBA 810ACB

Fig. 1 - Output power vs. supply voltage

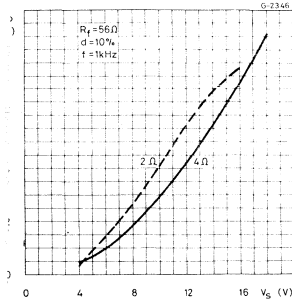


Fig. 2 - Maximum power dissipation vs. supply voltage (sine wave operation)

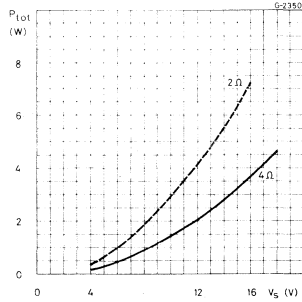


Fig. 3 - Distortion vs. frequency ($R_L = 4 \Omega$)

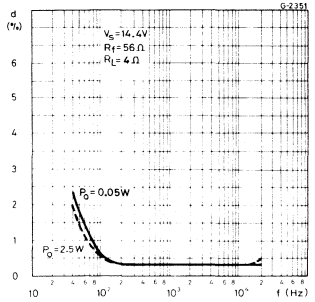


Fig. 4 - Distortion vs. frequency ($R_L = 2 \Omega$)

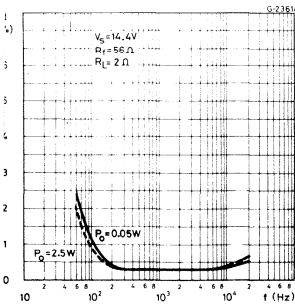


Fig. 5 - Distortion vs. output power

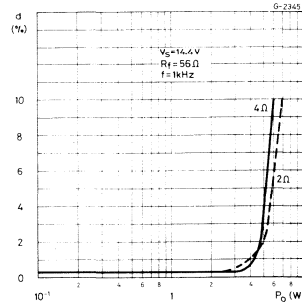


Fig. 6 - Value of C3 vs. feedback resistance for various values of B

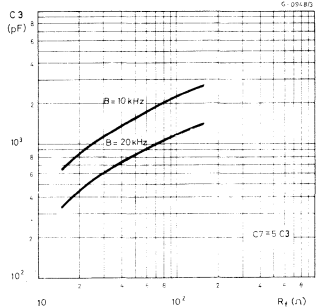


Fig. 7 - Relative voltage gain (closed loop) and input voltage vs. feedback resistance

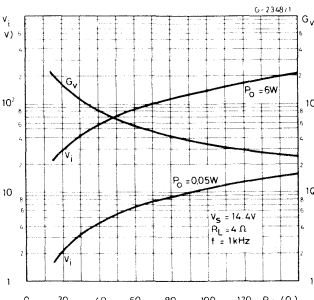


Fig. 8 - Relative voltage gain (closed loop) and input voltage vs. feedback resistance

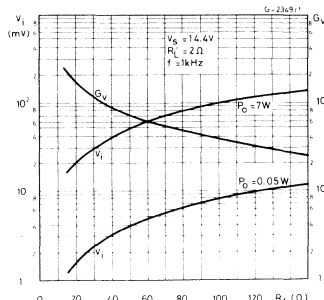
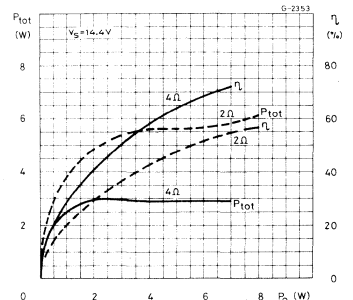


Fig. 9 - Power dissipation and efficiency vs. output power



TBA 810CB TBA 810ACB

Fig. 10 - Quiescent output voltage (pin 12) vs. supply voltage

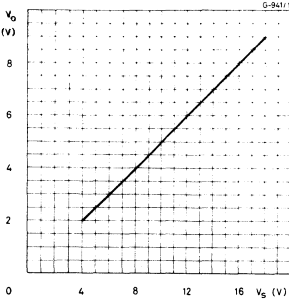


Fig. 11 - Quiescent drain current vs. supply voltage

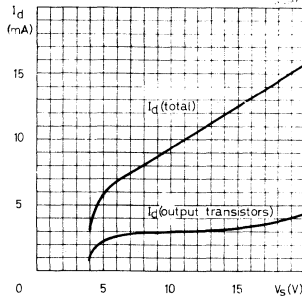
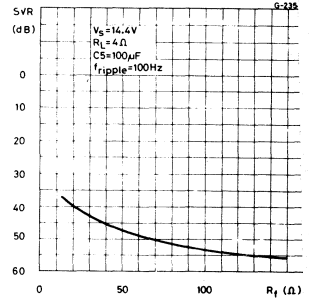


Fig. 12 - Supply voltage rejection vs. feedback resistance



BUILT-IN PROTECTION SYSTEMS

Load dump protection

The load dump case occurs in a car when the engine is running and the battery is disconnected: voltage spikes on the power line are supplied by the alternator since there is no clamping effect due to battery capacitance.

The TBA 810CB was designed to withstand a pulse train on pin 1, of the type shown in Fig. 13. Providing an LC filter is included, as shown in Fig. 14, a much higher pulse train amplitude (up to 100 V_{peak}) is allowed on the supply line with no damage to the device.

Fig. 13

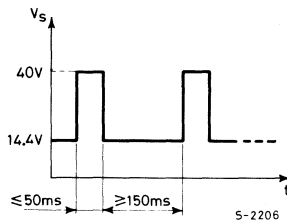
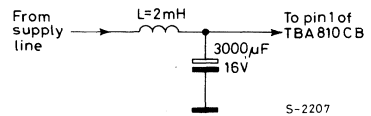


Fig. 14



Short-circuit protection

The TBA 810CB can withstand a permanent short circuit across the load for a supply voltage up to 15V.

Polarity inversion protection

High current (up to 5A) can be handled by the device with no damage for a longer period than the blow-out time of a quick 1A fuse (normally connected in series with the supply).

This feature is added to avoid destruction if, during fitting to the car, a mistake on the connection of the supply is made.

TBA 810 CB TBA 810 ACB

BUILT-IN PROTECTION SYSTEMS (continued)

Open ground protection

When the radio is in the ON condition and the ground is accidentally opened, a standard audio amplifier will be damaged. On the TBA 810CB, protection diodes are included to avoid any damage.

Inductive load protection

A protection diode is provided between pin 12 and pin 1 (see the internal schematic diagram) to allow use of the TBA 810CB with inductive loads.

In particular, the TBA 810CB can drive the coupling transformer for audio modulation in CB transmitters.

DC voltage protection

The maximum operating DC voltage on the TBA 810CB is 20V.

However, the device can withstand a DC voltage up to 28V with no damage. This could occur during winter if two batteries were series connected to crank the engine.

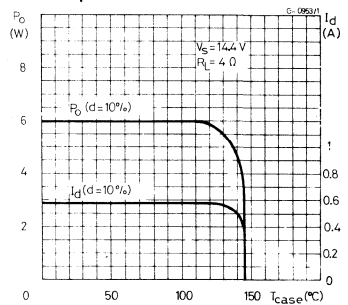
Thermal protection

A thermal limiting circuit is internally provided on TBA 810CB to prevent chip temperature exceeding 150°C. This protection offers the following advantages:

- An overload on the output (even if permanent), or an above-limit ambient temperature can be withstood.
- The heatsink can be designed with smaller safety margins compared with that of a conventional power audio amplifier.

The TBA 810CB will remain undamaged in the event of excessive junction temperature: all that happens is that P_o (and therefore P_{tot}) are reduced (Fig. 15).

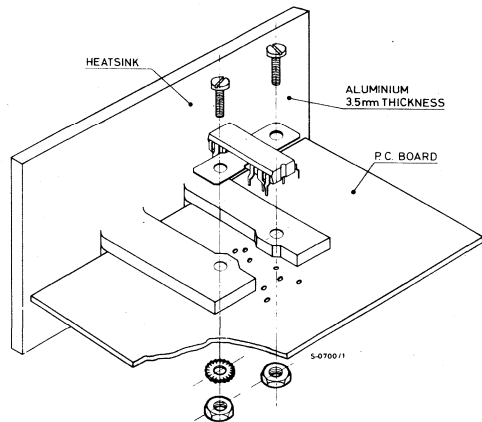
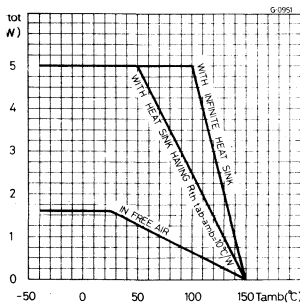
Fig. 15 - Output power and drain current vs. package temperature



MOUNTING INSTRUCTIONS

The thermal power dissipated in the circuit may be removed by connecting the tabs to an external heatsink (Fig. 16) or by soldering them to an area of copper on the printed circuit board (Fig. 17). During soldering, tab temperature must not exceed 260°C and the soldering time must not be longer than 12 seconds.

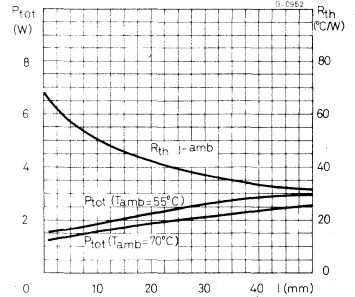
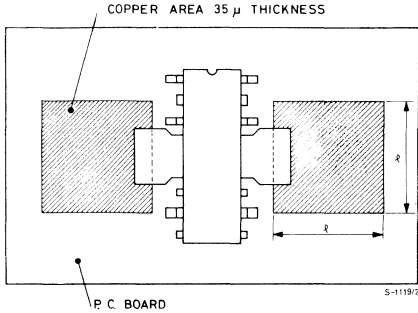
Fig. 16 - TBA 810 ACB mounting example



TBA 810CB TBA 810ACB

MOUNTING INSTRUCTIONS (continued)

Fig. 17 - TBA 810CB mounting example

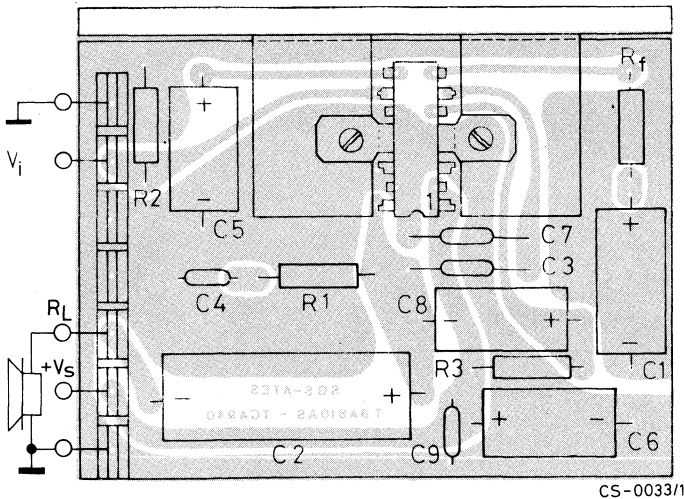


RELIABILITY

The reliability of the TBA 810CB is very high thanks to the Fin-Dip package and assembly process. A CB radio is switched ON and OFF many thousands of times during the lifetime of the car. This causes thermal fatigue of the device and if suitable package and assembly processes were not used, failure of the die or wire bonding would be probable. Thanks to the particular process adopted for the TBA 810CB the device can easily withstand the following stresses:

- thermal fatigue: more than 10^4 cycles with $\Delta T_{\text{case}} = 100^\circ\text{C}$
- thermal cycling: more than 10^3 cycles between -55°C and $+125^\circ\text{C}$
- thermal shocks: more than 10^3 cycles between -55°C and $+125^\circ\text{C}$
- relative humidity of 85% at 85°C is resisted for more than 10^3 hours.

Fig. 18 - P.C. board and component layout for the test and application circuit (1:1 scale)



CS-0033/1

LINEAR INTEGRATED CIRCUITS

7-W AUDIO POWER AMPLIFIER WITH THERMAL SHUT-DOWN, SHORT CIRCUIT PROTECTION

The TBA 810P is an improvement of TBA 810S.

It offers:

- Higher output power ($R_L = 4\Omega$ and 2Ω)
- Lower noise
- Polarity inversion protection
- Fortuitous open ground protection
- Higher supply voltage rejection (40 dB min.)

The TBA 810P is a monolithic integrated circuit in a 12-lead quad in-line plastic package, intended for use as a low frequency class B amplifier.

The TBA 810 P provides 7-W output power at $16V/4\Omega$; 7-W at $14.4V/2\Omega$.

It gives high output current (up to 3A), high efficiency (75% at 6W output), very low harmonic and crossover distortion. The circuit is provided with a thermal limiting circuit and can withstand a short-circuit on the load for supply voltages up to 15V.

The TBA 810AP has the same electrical characteristics as the TBA 810P, but its cooling tabs are flat and pierced so that an external heatsink can easily be attached.

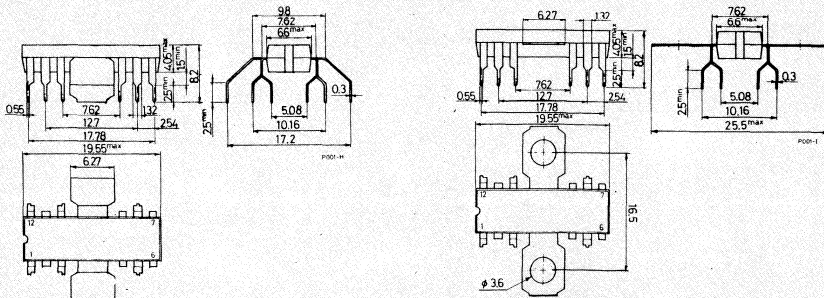
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	20	V
I_o	Output peak current (non repetitive)	4	A
I_o	Output peak current (repetitive)	3	A
P_{tot}	Power dissipation at $T_{amb} \leq 80^\circ\text{C}$ (for TBA 810P) $T_{tab} \leq 100^\circ\text{C}$ (for TBA 810AP)	1	W
		5	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBERS: TBA 810P
TBA 810AP

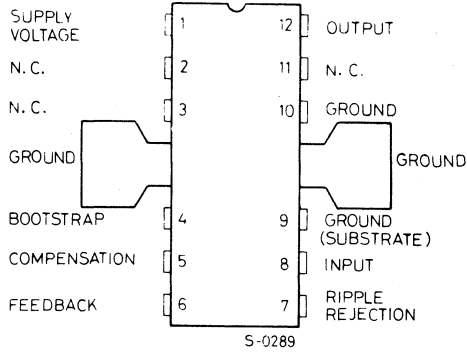
MECHANICAL DATA

Dimensions in mm

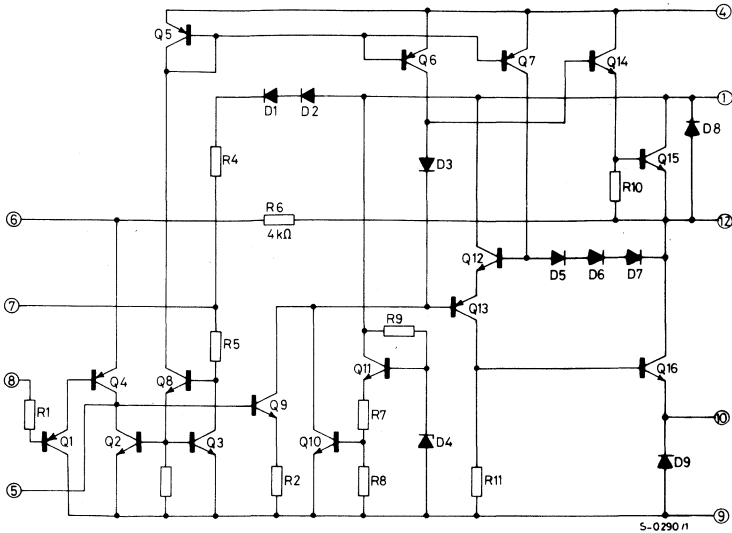


TBA 810P TBA 810AP

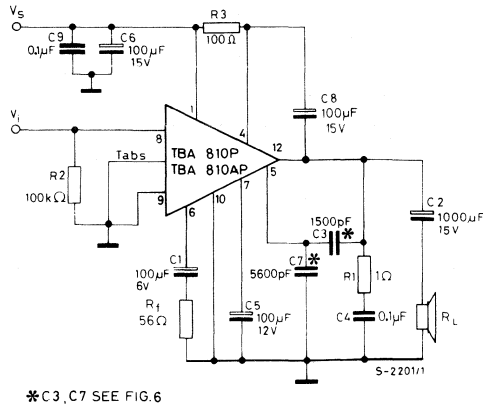
CONNECTION DIAGRAM (top view)



SCHEMATIC DIAGRAM



TEST AND APPLICATION CIRCUIT



THERMAL DATA

			TBA 810P	TBA 810AP
$R_{th j-tab}$	Thermal resistance junction-tab	max	12°C/W	10°C/W
$R_{th j-amb}$	Thermal resistance junction-ambient	max	70°C/W	80°C/W

* Obtained with tabs soldered to printed circuit with minimized copper area

ELECTRICAL CHARACTERISTICS

(Refer to the test circuit; $V_s = 14.4V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s	Supply voltage (pin 1)	4		20	V
V_o	Quiescent output voltage (pin 12)	6.4	7.2	8	V
I_d	Quiescent drain current		12	20	mA
I_b	Input bias current		0.4		μA
P_o	Output power	$d = 10\%$ $R_L = 4\Omega$ $R_L = 2\Omega$	$f = 1 \text{ kHz}$ 5.5 6 7		W W
$V_{i(rms)}$	Input saturation voltage	220			mV

TBA 810P TBA 810AP

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit		
V_i	Input sensitivity	$f = 1 \text{ kHz}$ $P_o = 6 \text{ W}$ $R_f = 56 \Omega$ $R_f = 22 \Omega$ $P_o = 7 \text{ W}$ $R_f = 56 \Omega$ $R_f = 22 \Omega$	$R_L = 4 \Omega$ $R_L = 2 \Omega$	 75 30 55 20	 mV mV mV mV		
R_i	Input resistance (pin 8)		5		M Ω		
B	Frequency response (-3 dB)	$R_L = 4 \Omega / 2 \Omega$ $C_3 = 820 \text{ pF}$ $C_3 = 1500 \text{ pF}$		40 to 20 000 40 to 10 000	Hz Hz		
d	Distortion	$P_o = 50 \text{ mW to } 2.5 \text{ W}$ $R_L = 4 \Omega / 2 \Omega$	$f = 1 \text{ kHz}$	0.3	%		
G_v	Voltage gain (open loop)	$R_L = 4 \Omega$	$f = 1 \text{ kHz}$	80	dB		
G_v	Voltage gain (closed loop)	$R_L = 4 \Omega / 2 \Omega$	$f = 1 \text{ kHz}$	34	37	40	dB
e_N	Input noise voltage	$V_s = 16 \text{ V}$		2	μV		
i_N	Input noise current	B (-3 dB) = 40 to 15 000 Hz		80	pA		
η	Efficiency	$P_o = 6 \text{ W}$ $f = 1 \text{ kHz}$	$R_L = 4 \Omega$	75	%		
SVR	Supply voltage rejection	$R_L = 4 \Omega$ $f_{\text{ripple}} = 100 \text{ Hz}$	$V_{\text{ripple}} = 1 V_{\text{rms}}$	40	48	dB	
I_d	Drain current	$P_o = 6 \text{ W}$	$R_L = 4 \Omega$	600	mA		

Fig. 1 - Output power vs. supply voltage

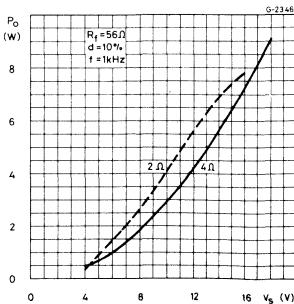


Fig. 2 - Maximum power dissipation vs. supply voltage (sine wave operation)

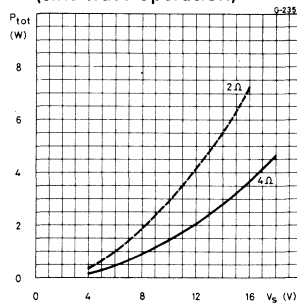


Fig. 3 - Distortion vs. frequency ($R_L = 4 \Omega$)

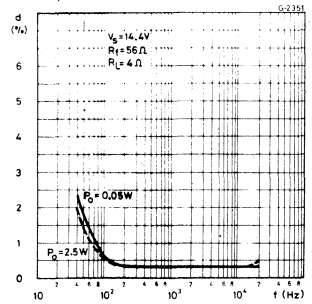


Fig. 4 - Distortion vs. frequency ($R_L = 2\Omega$)

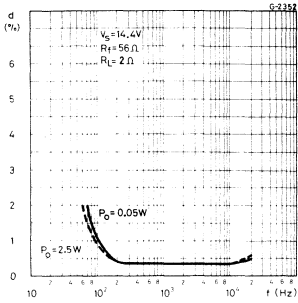


Fig. 5 - Distortion vs. output power

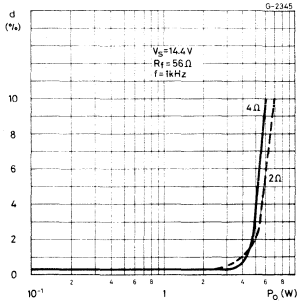


Fig. 6 - Value of C3 vs. feedback resistance for various values of B

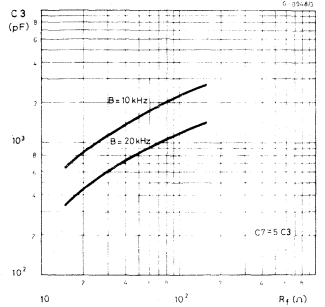


Fig. 7 - Relative voltage gain (closed loop) and input voltage vs. feedback resistance

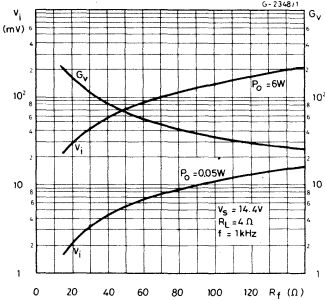


Fig. 8 - Relative voltage gain (closed loop) and input voltage vs. feedback resistance

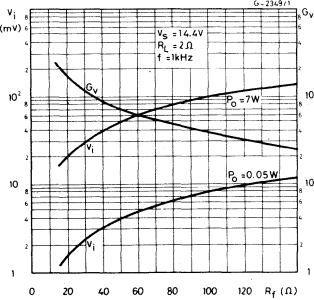


Fig. 9 - Total power dissipation and efficiency vs. output power

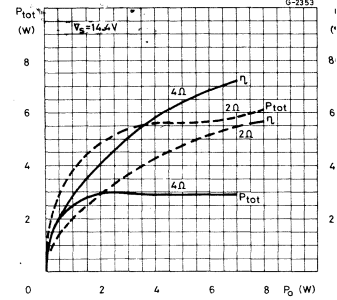


Fig. 10 - Quiescent output voltage (pin 12) vs. supply voltage

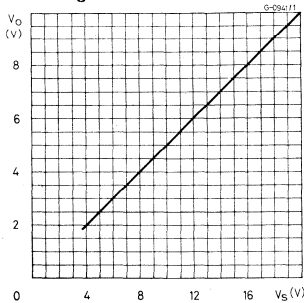


Fig. 11 - Quiescent drain current vs. supply voltage

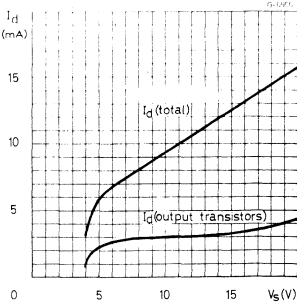
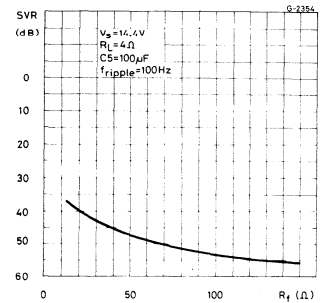


Fig. 12 - Supply voltage rejection vs. feedback resistance



TBA 810P TBA 810AP

MOUNTING INSTRUCTIONS

The thermal power dissipated in the circuit may be removed by connecting the tabs to an external heatsink (TBA 810 AP see figs. 13 and 14), or by soldering them to an area of copper on the printed circuit board (TBA 810P see fig. 15). During soldering, tab temperature must not exceed 260°C and the soldering time must not be longer than 12 seconds.

Fig. 13 - Maximum power dissipation vs. ambient temperature (TBA810AP only)

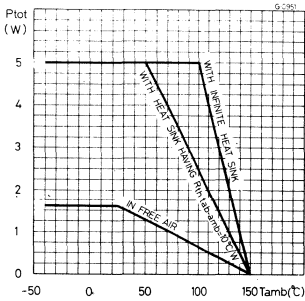


Fig. 14 - Mounting example of the TBA 810 AP

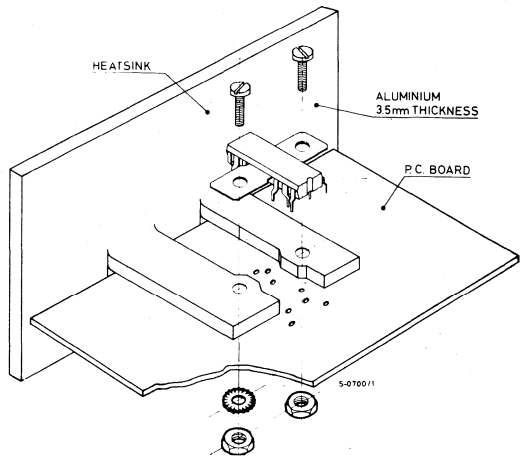
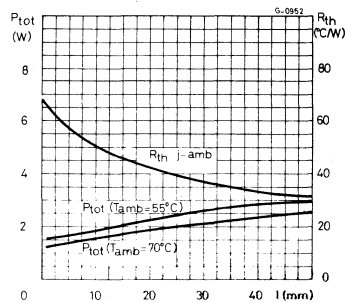
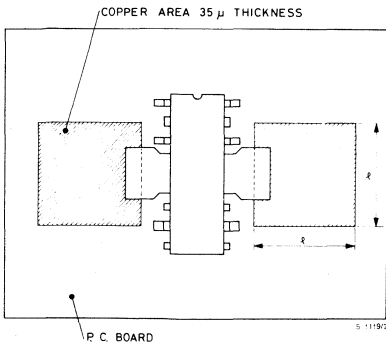


Fig. 15 - Maximum power dissipation vs. copper area of the P.C. board (TBA 810P only)



TBA 810P TBA 810AP

THERMAL SHUTDOWN

The presence of a thermal limiting circuit offers the following advantages:

- 1) An overload on the output (even if it is permanent), or an above-limit ambient temperature can be easily withstood.
- 2) The heatsink can have a smaller factor of safety compared with that of a conventional circuit. There is no device damage in the event of excessive junction temperature: all that happens is that P_o , (and therefore P_{tot}) are reduced.

Fig. 16 - Output power and drain current vs. package temperature

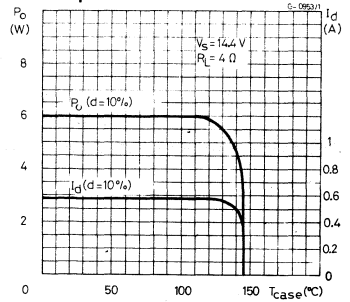
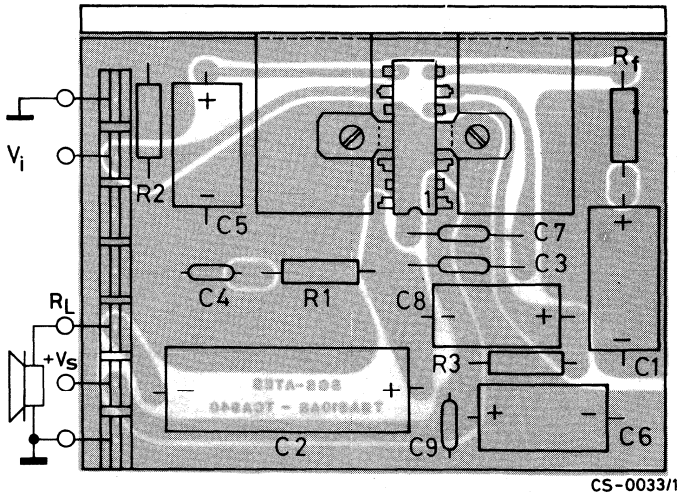


Fig. 17 - P.C. board and component layout for the test and application circuit (1:1 scale)



TBA 810S TBA 810AS

LINEAR INTEGRATED CIRCUITS

7 W AUDIO POWER AMPLIFIER

The TBA 810 S is a monolithic integrated circuit in a 12 lead quad in-line plastic package, intended for use as a low frequency class B amplifier.

The TBA 810 S provides 7 W power output at 16 V/4 Ω , 6 W at 14.4 V/4 Ω , 2.5 W at 9 V/4 Ω , 1 W at 6 V/4 Ω and works with a wide range of supply voltages (4 to 20 V); it gives high output current (up to 2.5 A), high efficiency (75% at 6 W output), very low harmonic and cross-over distortion. In addition, the circuit is provided with a thermal protection circuit.

The TBA 810 AS has the same electrical characteristics as the TBA 810S, but its cooling tabs are flat and pierced so that an external heatsink can easily be attached.

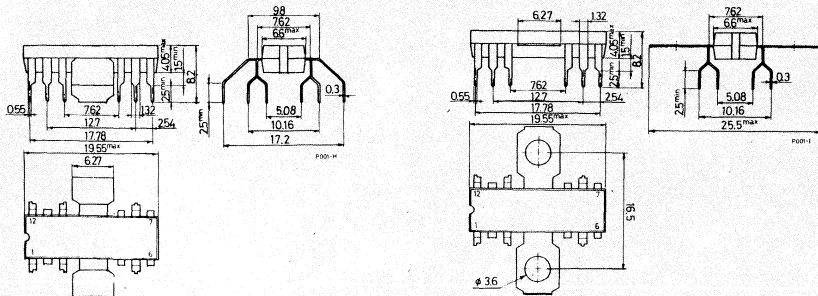
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	20	V
I_o	Output peak current (non-repetitive)	3.5	A
I'_{o}	Output current (repetitive)	2.5	A
P_{tot}	Power dissipation: at $T_{amb} = 70^\circ\text{C}$ (TBA810AS)	1	W
	at $T_{tab} = 100^\circ\text{C}$ (TBA810AS)	5	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBERS: TBA 810 S
TBA 810 AS

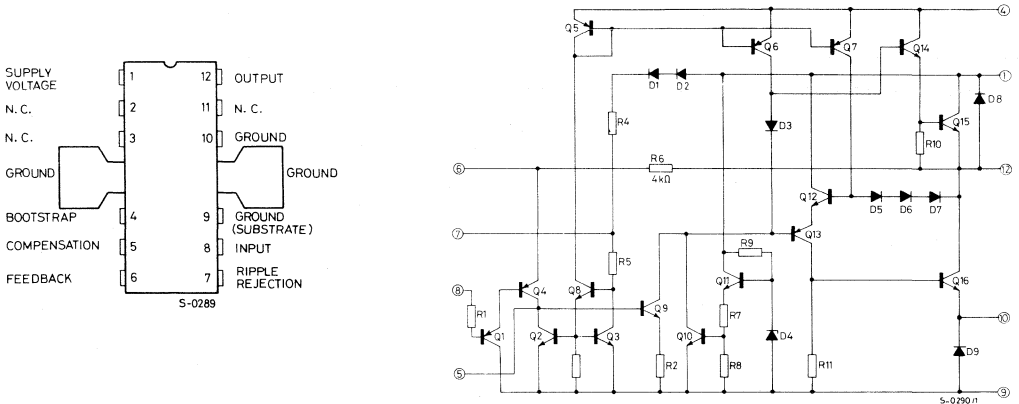
MECHANICAL DATA

Dimensions in mm

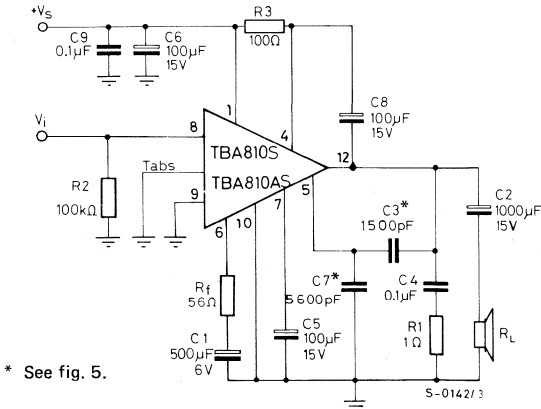


TBA 810S TBA 810AS

CONNECTION AND SCHEMATIC DIAGRAM (top view)



TEST AND APPLICATION CIRCUIT



THERMAL DATA

			TBA810S	TBA810AS
$R_{th \text{ j-tab}}$	Thermal resistance junction-tab	max	12 °C/W	10 °C/W
$R_{th \text{ j-amb}}$	Thermal resistance junction-ambient	max	70* °C/W	80 °C/W

* Obtained with tabs soldered to printed circuit with minimized copper area.

TBA 810S TBA 810AS

ELECTRICAL CHARACTERISTICS (Refer to the test circuit; $T_{amb} = 25^{\circ}\text{C}$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s Supply voltage (pin 1)		4		20	V
V_o Quiescent output voltage (pin 12)	$V_s = 14.4\text{V}$	6.4	7.2	8	V
I_d Quiescent drain current			12	20	mA
I_b Bias current (pin 8)			0.4		μA
P_o Power output		$d = 10\%$ $R_L = 4\Omega$ $f = 1\text{kHz}$ $V_s = 16\text{V}$ $V_s = 14.4\text{V}$ $V_s = 9\text{V}$ $V_s = 6\text{V}$	5.5	7 6 2.5 1	
$V_{i(\text{rms})}$ Input voltage				220	mV
V_i Input sensitivity	$P_o = 6\text{W}$ $V_s = 14.4\text{V}$ $R_L = 4\Omega$ $f = 1\text{kHz}$ $R_f = 56\Omega$ $R_f = 22\Omega$		80 35		mV mV
R_i Input resistance (pin 8)			5		M Ω
B Frequency response (-3 dB)	$V_s = 14.4\text{V}$ $R_L = 4\Omega$ $C_3 = 820\text{pF}$ $C_3 = 1500\text{pF}$		40 to 20,000 40 to 10,000		Hz Hz
d Distorsion	$P_o = 50\text{mW to } 3\text{W}$ $V_s = 14.4\text{V}$ $R_L = 4\Omega$ $f = 1\text{kHz}$		0.3		%
G_v Voltage gain (open loop)	$V_s = 14.4\text{V}$ $R_L = 4\Omega$ $f = 1\text{kHz}$		80		dB
G_v Voltage gain (closed loop)	$V_s = 14.4\text{V}$ $R_L = 4\Omega$ $f = 1\text{kHz}$	34	37	40	dB
e_N Input noise voltage	$V_s = 14.4\text{V}$ $R_g = 0$ B (-3 dB) = 20Hz to 20,000 Hz		2		μV
i_N Input noise current	$V_s = 14.4\text{V}$ B (-3 dB) = 20 Hz to 20,000 Hz		0.1		nA
η Efficiency	$P_o = 5\text{W}$ $V_s = 14.4\text{V}$ $R_L = 4\Omega$ $f = 1\text{kHz}$		70		%
SVR Supply voltage rejection	$V_s = 14.4\text{V}$ $R_L = 4\Omega$ $f_{\text{ripple}} = 100\text{Hz}$		38		dB

Fig. 1 - Power output versus supply voltage

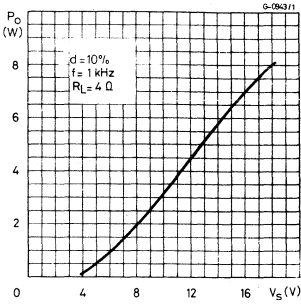


Fig. 2 - Maximum power dissipation versus supply voltage (sine wave operation)

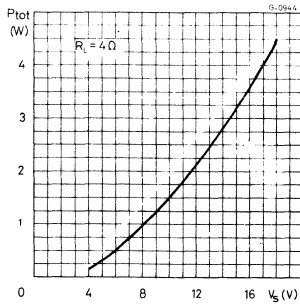


Fig. 3 - Distorsion versus output power

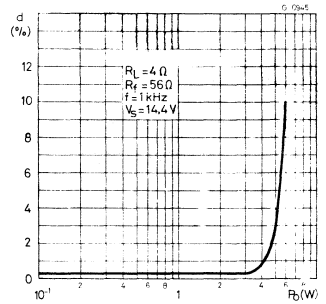


Fig. 4 - Distorsion versus frequency

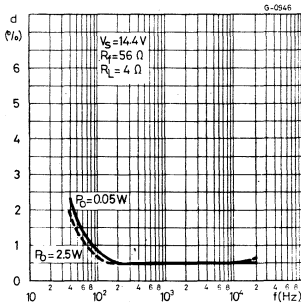


Fig. 5 - Value of C3 versus R_f for various values of B

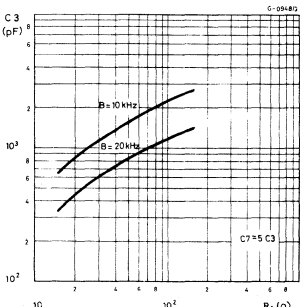


Fig. 6 - Power dissipation and efficiency versus output power

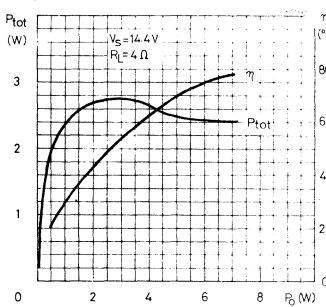


Fig. 7 - Quiescent output voltage (pin 12) versus supply voltage

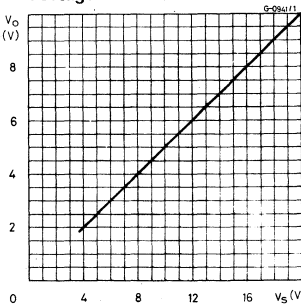


Fig. 8 - Quiescent current versus supply voltage

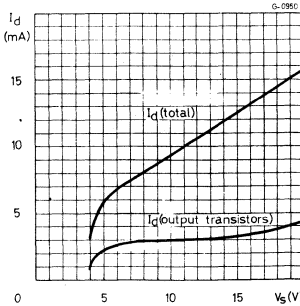
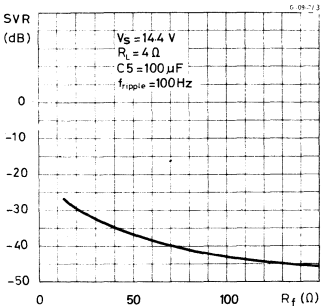


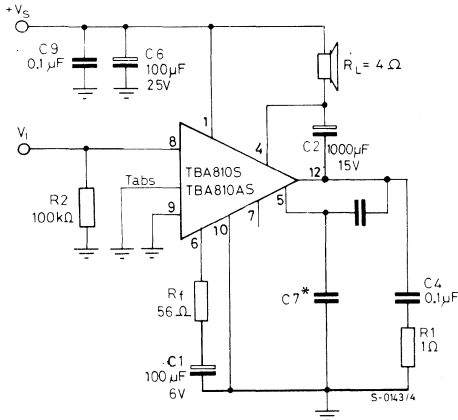
Fig. 9 - Supply voltage rejection



TBA 810S TBA 810AS

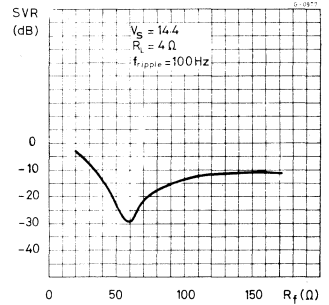
For portable equipment the circuit in Fig. 10 has the advantages of fewer external components and a better behaviour at low supply voltages (down to 4 V).

Fig. 10 – Application circuit with load connected to the supply voltage



* C3, C7 see fig. 5

Fig. 11 – Supply voltage rejection versus R_f (circuit of fig. 10)



MOUNTING INSTRUCTIONS

The thermal power dissipated in the circuit may be removed by connecting the tabs to an external heat sink (TBA 810 AS – fig. 12) or by soldering them to an area of copper on the printed circuit board (TBA 810 S – fig. 13).

Fig. 12 – Maximum power dissipation versus ambient temperature (for TBA 810 AS only)

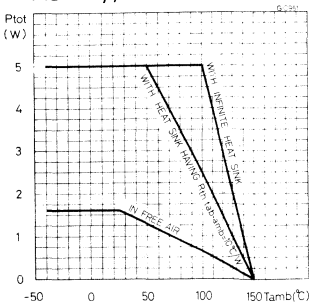
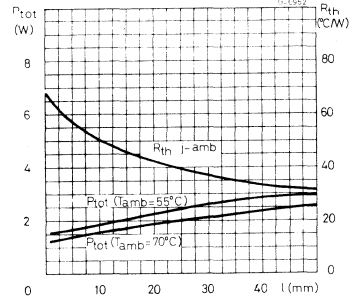
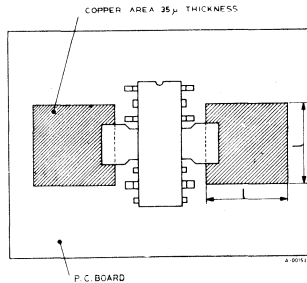


Fig. 13 – Maximum power dissipation versus copper area of the P.C. board (for TBA 810 S only)



During soldering the tabs temperature must not exceed 260 °C and the soldering time must not be longer than 12 seconds.

Fig. 14a and 14b show two ways that can be used for mounting the device.

Fig. 14a shows a method of mounting the TBA 810 S, that is satisfactory both from the point of view of heat dissipation and from mechanical considerations. For TBA 810 AS the desired thermal resistance is obtained by fixing the elements shown in fig. 14b, to a suitably dimensioned plate. This plate can also act as a support for the whole printed circuit board; the mechanical stresses do not damage the integrated circuit. This is firmly fixed to the element, in fig. 14b.

Fig. 14a

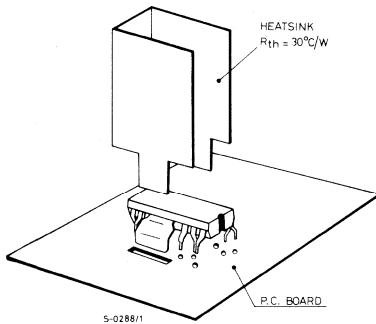
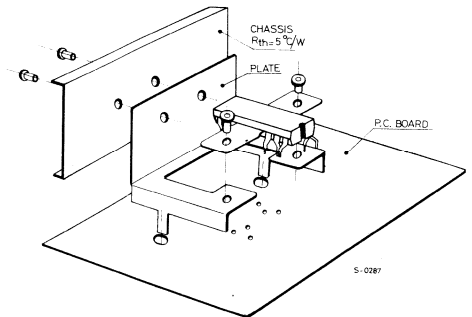


Fig. 14b

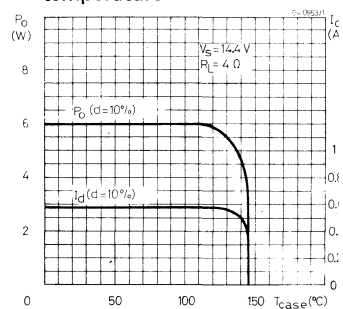


THERMAL SHUT-DOWN

The presence of a thermal limiting circuit offers the following advantages:

- 1) An overload on the output (even if it is permanent), or an above-limit ambient temperature can be easily supported.
- 2) The heat sink can have a smaller factor of safety compared with that of a conventional circuit. There is no device damage in the case of too high a junction temperature: all that happens is that P_O (and therefore P_{tot}) and I_d are reduced (fig. 15).

Fig. 15 - Output power and drain current versus package temperature



TBA 820

LINEAR INTEGRATED CIRCUIT

AUDIO AMPLIFIER

The TBA 820 is a monolithic integrated audio amplifier in a 14-lead quad in-line plastic package. It is intended for use as low frequency class B amplifier with wide range of supply voltage: 3 to 16V.

Main features are: minimum working voltage of 3V, low quiescent current, low number of external components, good ripple rejection, no cross-over distortion, mounting compatibility with TAA 611

Output power:

$P_o = 2W$ at 12V - 8Ω • $P_o = 1.6W$ at 9V - 4Ω • $P_o = 1.2W$ at 9V - 8Ω

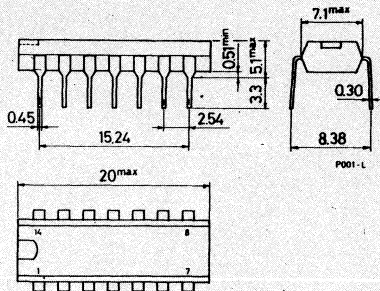
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	16	V
I_o	Output peak current	1.5	A
P_{tot}	Power dissipation at $T_{amb} = 50^\circ C$	1.25	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ C$

ORDERING NUMBER: TBA 820

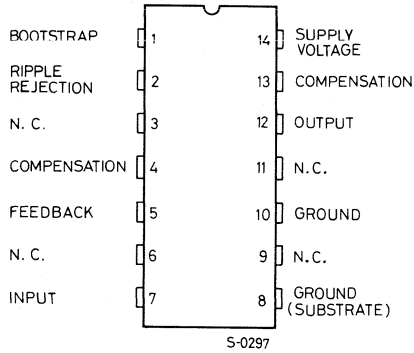
MECHANICAL DATA

Dimensions in mm

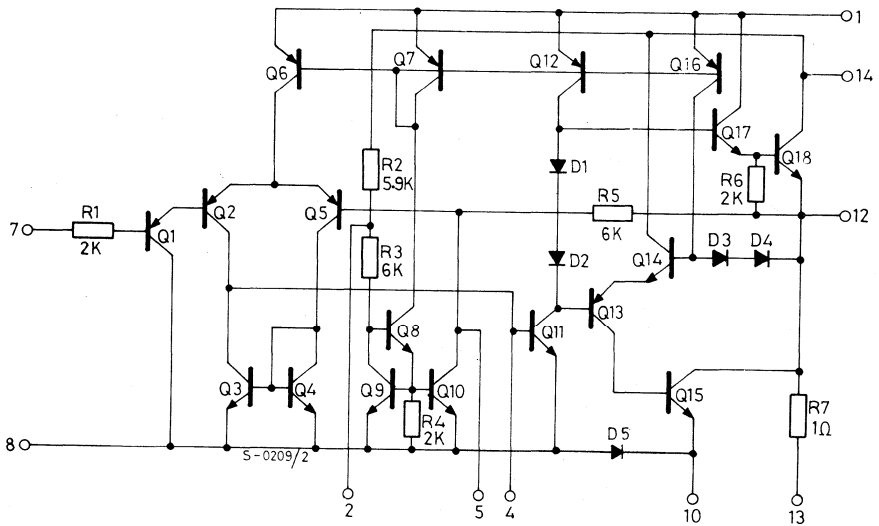


TBA 820

CONNECTION DIAGRAM (top view)



SCHEMATIC DIAGRAM



TBA 820

TEST AND APPLICATION CIRCUITS

Fig. 1 - Circuit diagram with load connected to the supply voltage

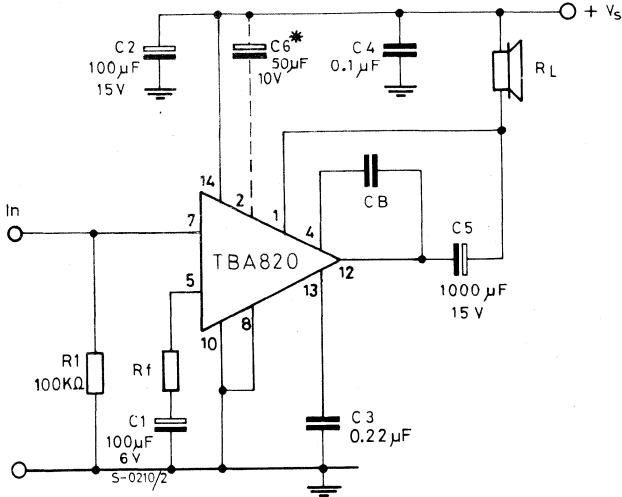
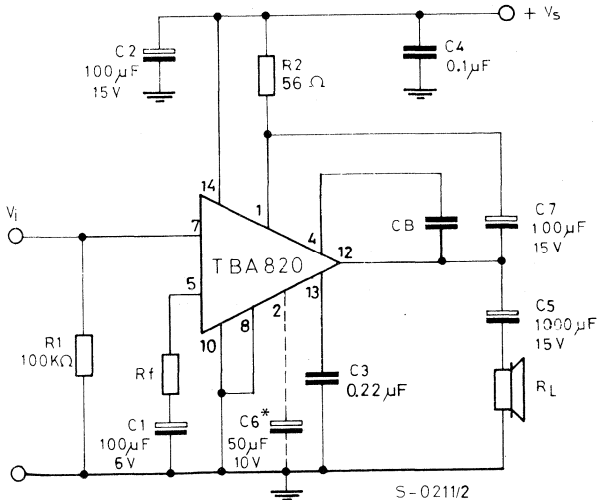


Fig. 2 - Circuit diagram with load connected to ground



* Capacitor C_6 must be used when high ripple rejection is requested

THERMAL DATA

$R_{thj-amb}$	Thermal resistance junction-ambient	80 °C/W
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ELECTRICAL CHARACTERISTICS

($T_{amb} = 25^{\circ}\text{C}$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	
V_s	Supply voltage	3		16	V	
V_o	Quiescent output voltage (pin 12)	$V_s = 9\text{V}$	4	4.5	5	V
I_d	Quiescent drain current	$V_s = 9\text{V}$		4		mA
I_b	Bias current (pin 7)	$V_s = 9\text{V}$		0.1		μA
P_o	Output power (see circuit Fig. 1)	$d = 10\%$ $R_f = 120\ \Omega$ $V_s = 12\text{V}$ $V_s = 9\text{V}$ $V_s = 9\text{V}$ $V_s = 6\text{V}$ $V_s = 3.5\text{V}$	$f = 1\ \text{kHz}$ $R_L = 8\ \Omega$ $R_L = 4\ \Omega$ $R_L = 8\ \Omega$ $R_L = 4\ \Omega$ $R_L = 4\ \Omega$		2 1.6 1.2 0.75 0.22	W W W W W
V_i (rms)	Input sensitivity (see circuit Fig. 1)	$P_o = 1.2\text{W}$ $R_L = 8\ \Omega$ $R_f = 33\ \Omega$ $R_f = 120\ \Omega$	$V_s = 9\text{V}$ $f = 1\ \text{kHz}$		16 60	mV mV
V_i (rms)	Input sensitivity (see circuit Fig. 1)	$P_o = 50\ \text{mW}$ $R_L = 8\ \Omega$ $R_f = 33\ \Omega$ $R_f = 120\ \Omega$	$V_s = 9\text{V}$ $f = 1\ \text{kHz}$		3.5 12	mV mV
R_i	Input resistance			5		$\text{M}\Omega$
B	Frequency response (-3 dB) (see circuit Fig. 1)	$V_s = 9\text{V}$ $R_f = 120\ \Omega$ $C_B = 680\ \text{pF}$ $C_B = 220\ \text{pF}$	$R_L = 8\ \Omega$		25 to 7000 25 to 20000	Hz Hz
d	Distortion (see circuit Fig. 1)	$P_o = 500\ \text{mW}$ $R_L = 8\ \Omega$ $R_f = 33\ \Omega$ $R_f = 120\ \Omega$	$V_s = 9\text{V}$ $f = 1\ \text{kHz}$		0.8 0.4	% %
G_v	Voltage gain (open loop)	$V_s = 9\text{V}$ $f = 1\ \text{kHz}$	$R_L = 8\ \Omega$		75	dB

TBA 820

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
G_V Voltage gain (closed loop)	$V_S = 9V$ $f = 1 \text{ kHz}$ $R_f = 33 \Omega$ $R_L = 8 \Omega$ $R_f = 120 \Omega$		45 34		dB dB
e_N Input noise voltage	$V_S = 9V$ $B = 22 \text{ Hz to } 22 \text{ KHz}$		3		μV
i_N Input noise current			0.4		nA
$\frac{S+N}{N}$ Signal to noise ratio	$V_S = 9V$ $R_f = 120 \Omega$ $P_O = 1.2W$ $R_{L1} = 100 \text{ K}\Omega$ $B = 22 \text{ Hz to } 22 \text{ KHz}$		70		dB
SVR Supply voltage rejection (see circuit Fig. 2)	$V_S = 9V$ $f \text{ (ripple)} = 100 \text{ Hz}$ $C6 = 50 \mu F$ $R_f = 120 \Omega$ $R_L = 8 \Omega$		42		dB

Fig. 3 - Output power vs. supply voltage

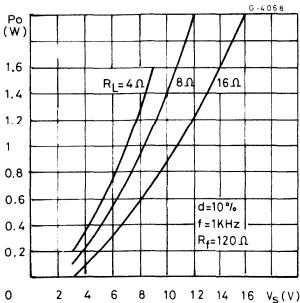


Fig. 4 - Distortion vs. output power

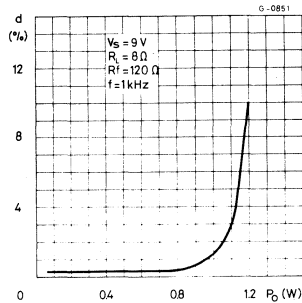


Fig. 5 - Power dissipation and efficiency vs. output power

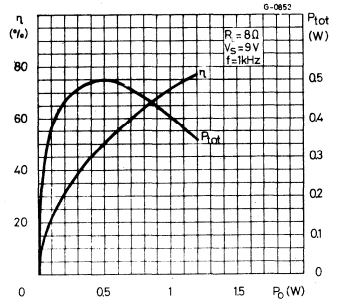


Fig. 6 - Maximum power dissipation (sine wave operation)

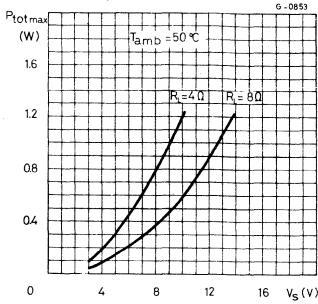


Fig. 7 - Suggested value of C_B versus R_f

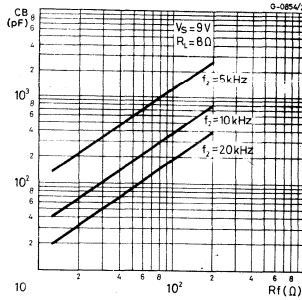


Fig. 8 - Relative frequency response

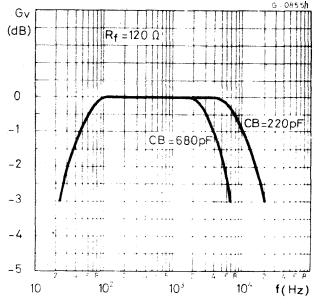


Fig. 9 - Input sensitivity vs. R_f

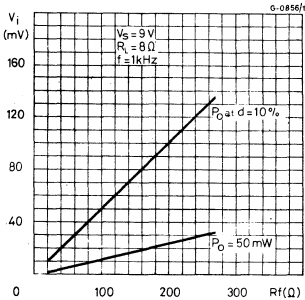


Fig. 10 - Voltage gain (closed loop)

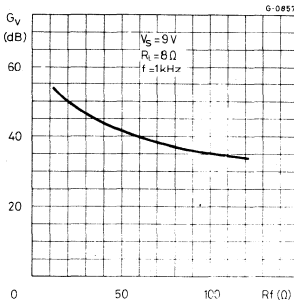


Fig. 11 - Distortion vs. frequency

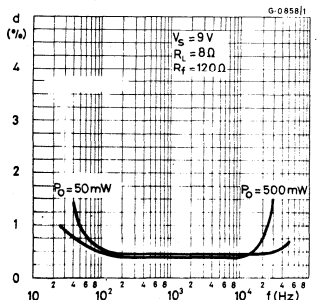


Fig. 12 - Supply voltage rejection (fig. 2 circuit)

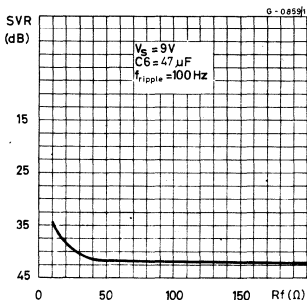


Fig. 13 - Quiescent output voltage at pin 12 vs. supply voltage

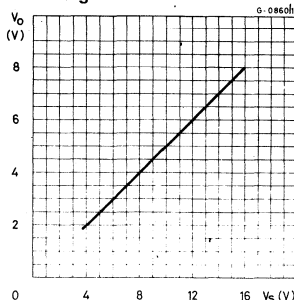
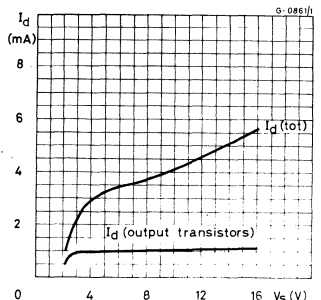


Fig. 14 - Quiescent current vs. supply voltage



TBA 820M

LINEAR INTEGRATED CIRCUIT

MINIDIP AUDIO AMPLIFIER

The TBA 820M is a monolithic integrated audio amplifier in a 8 lead dual in-line plastic package. It is intended for use as low frequency class B power amplifier with wide range of supply voltage: 3 to 16V, in portable radios, cassette recorders and players etc. Main features are: minimum working supply voltage of 3V, low quiescent current, low number of external components, good ripple rejection, no cross-over distortion, low power dissipation.

Output power: $P_o = 2W$ at $12V/8\Omega$, $1.6W$ at $9V/4\Omega$ and $1.2W$ at $9V/8\Omega$.

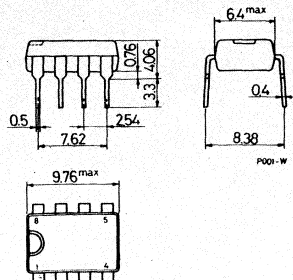
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	16	V
I_o	Output peak current	1.5	A
P_{tot}	Power dissipation at $T_{amb} = 50^\circ C$	1	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ C$

ORDERING NUMBER: TBA 820M

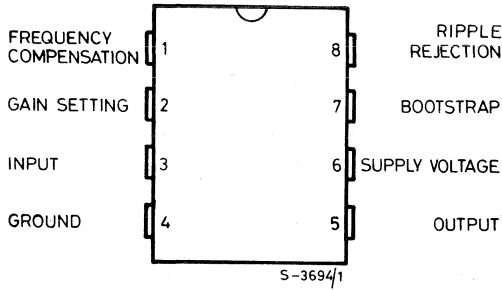
MECHANICAL DATA

Dimensions in mm

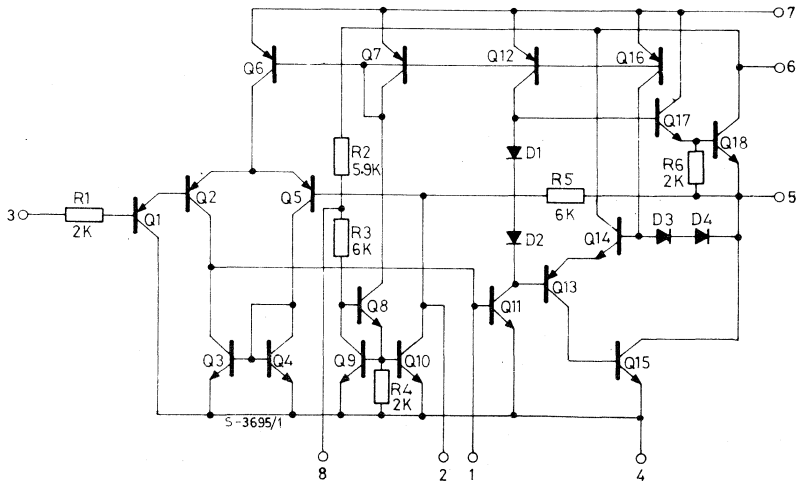


CONNECTION DIAGRAM

(top view)



SCHEMATIC DIAGRAM



TBA 820M

TEST AND APPLICATION CIRCUITS

Fig. 1 - Circuit diagram with load connected to the supply voltage.

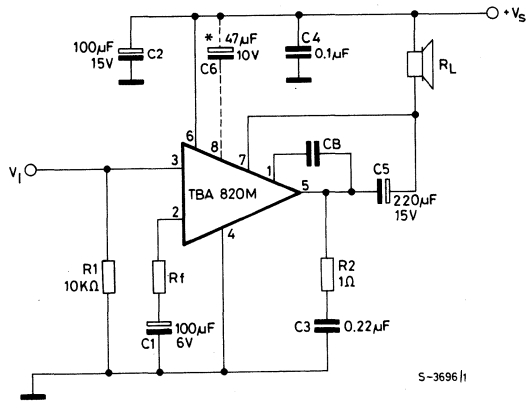
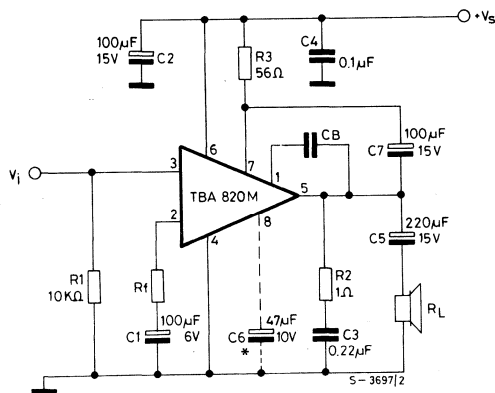


Fig. 2 - Circuit diagram with load connected to ground.



* Capacitor C_6 must be used when high ripple rejection is requested.

THERMAL DATA

$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	100	°C/W
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ELECTRICAL CHARACTERISTICS (Refer to the test circuits $V_s = 9V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	
V_s	Supply voltage	3		16	V	
V_o	Quiescent output voltage (pin 5)	4	4.5	5	V	
I_d	Quiescent drain current		4	12	mA	
I_b	Bias current (pin 3)		0.1		μA	
P_o	Output power	$d = 10\%$ $R_f = 120\Omega$ $V_s = 12V$ $V_s = 9V$ $V_s = 9V$ $V_s = 6V$ $V_s = 3.5V$ $V_s = 3V$	$f = 1\text{ kHz}$ $R_L = 8\Omega$ $R_L = 4\Omega$ $R_L = 8\Omega$ $R_L = 4\Omega$ $R_L = 4\Omega$ $R_L = 4\Omega$	0.9	2 1.6 1.2 0.75 0.25 0.20	W W W W W W
V_i (rms)	Input sensitivity	$P_o = 1.2W$ $R_L = 8\Omega$ $f = 1\text{ kHz}$	$R_f = 33\Omega$		16	mV
			$R_f = 120\Omega$		60	
		$P_o = 50\text{ mW}$ $R_L = 8\Omega$ $f = 1\text{ kHz}$	$R_f = 33\Omega$		3.5	mV
			$R_f = 120\Omega$		12	
R_i	Input resistance (pin 3)	$f = 1\text{ kHz}$		5	M Ω	
B	Frequency response (-3 dB)	$R_L = 8\Omega$ $C_5 = 1000\ \mu F$ $R_f = 120\Omega$	$C_B = 680\text{ pF}$	25 to 7,000		Hz
			$C_B = 220\text{ pF}$	25 to 20,000		
d	Distortion	$P_o = 500\text{ mW}$ $R_L = 8\Omega$ $f = 1\text{ kHz}$	$R_f = 33\Omega$	0.8	%	
			$R_f = 120\Omega$	0.4		
G_v	Voltage gain (open loop)	$f = 1\text{ kHz}$	$R_L = 8\Omega$	75	dB	

TBA 820M

ELECTRICAL CHARACTERISTICS (continued)

Parameter		Test conditions		Min.	Typ.	Max.	Unit
G_V	Voltage gain (closed loop)	$R_L = 8\Omega$ $f = 1 \text{ kHz}$	$R_f = 33\Omega$		45		dB
			$R_f = 120\Omega$		34		
e_N	Input noise voltage (*)				3		μV
i_N	Input noise current (*)				0.4		nA
$\frac{S+N}{N}$	Signal to noise ratio (*)	$P_o = 1.2\text{W}$ $R_L = 8\Omega$ $G_V = 34 \text{ dB}$	$R_1 = 10\text{K}\Omega$		80		dB
			$R_1 = 50 \text{ k}\Omega$		70		
SVR	Supply voltage rejection (test circuit of fig. 2)	$R_L = 8\Omega$ f (ripple) = 100 Hz $C_6 = 47 \mu\text{F}$ $R_f = 120\Omega$			42		dB

(*) B = 22 Hz to 22 KHz

Fig. 3 - Output power vs. supply voltage

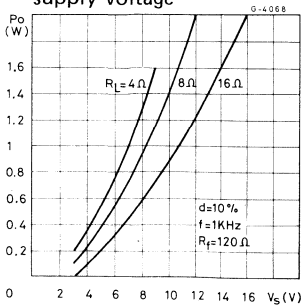


Fig. 4 - Harmonic distortion vs. output power

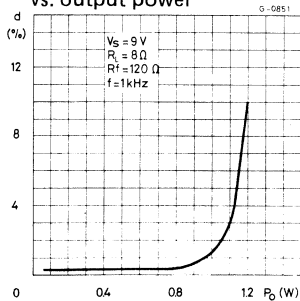


Fig. 5 - Power dissipation and efficiency vs. output power

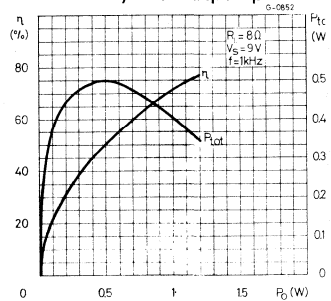


Fig. 6 - Maximum power dissipation (sine wave operation)

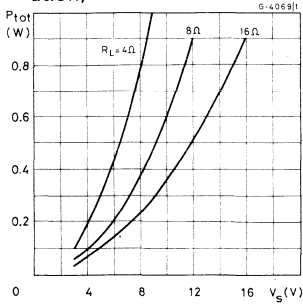


Fig. 7 - Suggested value of C_B vs. R_f

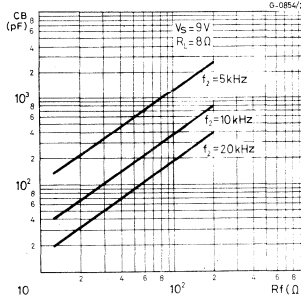


Fig. 8 - Frequency response

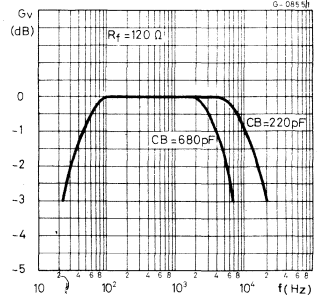


Fig. 9 - input sensitivity vs. R_f

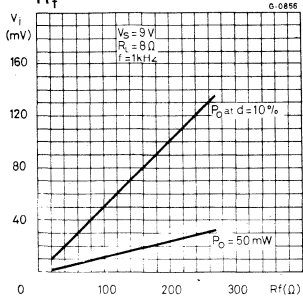


Fig. 10 - Voltage gain (closed loop) vs. R_f

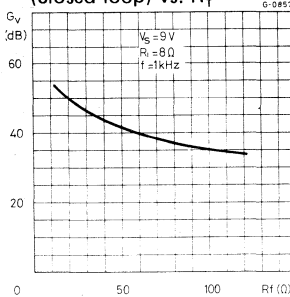


Fig. 11 - Harmonic distortion vs. frequency

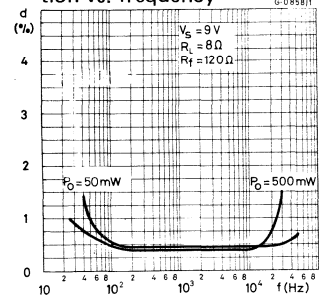


Fig. 12 - Supply voltage rejection (fig. 2 circuit)

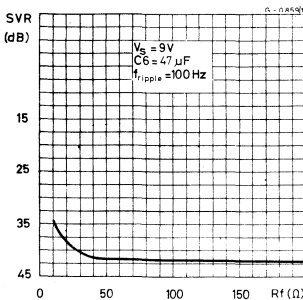


Fig. 13 - Quiescent output voltage at pin 5 vs. supply voltage

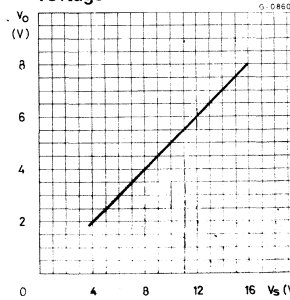
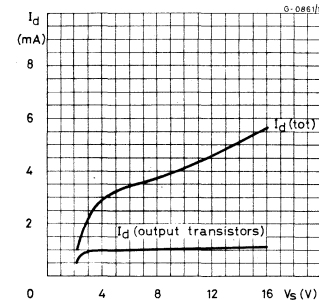


Fig. 14 - Quiescent current vs. supply voltage



TBA 820M

APPLICATION INFORMATION

Fig. 15 - Low cost toy AM radio (0,5 to 1,5 MHz)

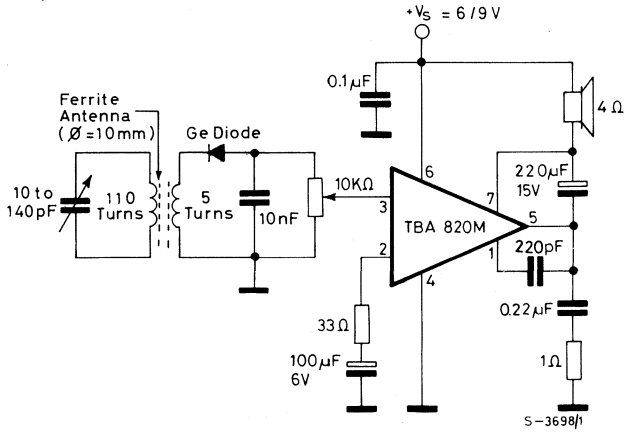
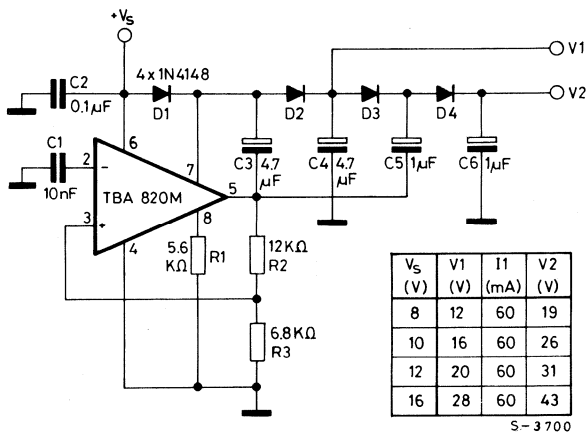
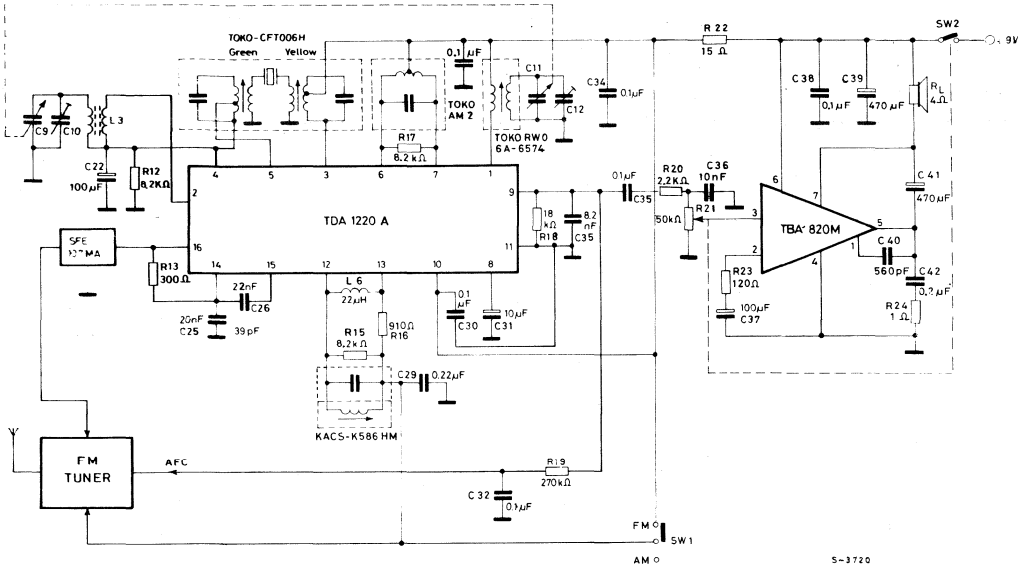


Fig. 16 - 1.5W DC/DC converter ($f = 40$ KHz)



APPLICATION INFORMATION (continued)

Fig. 17 - Low cost AM-FM radio with 1.6W output power ($V_s = 9V$)



S-3720

TCA 511

LINEAR INTEGRATED CIRCUIT

NOT FOR NEW DESIGN

TV HORIZONTAL AND VERTICAL PROCESSOR

The TCA 511 is a monolithic integrated circuit in a 16-lead dual in-line plastic package. It incorporates the following functions: high stability horizontal oscillator, horizontal APC circuit with high noise immunity and large pull-in range, high stability vertical oscillator and sawtooth generator. It is intended for driving TV horizontal and vertical output stages.

ABSOLUTE MAXIMUM RATINGS

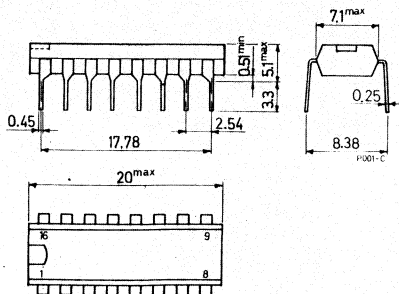
V_s	Vertical section supply voltage (between pins 3 and 13)	15	V
V_s	Horizontal section supply voltage (between pins 4 and 13)	15	V
V_7, V_{12}, V_{15}	Pin 7, 12, 15 voltage (collector to ground)	15	V
V_i	Vertical sync. input voltage (between pins 2 and 13 - see note)	-5	V
V_i	Horizontal sync. input voltage (between pins 6 and 13 - see note)	-5	V
I_8	DC current (from pin 8)	30	mA
I_{12}, I_{14}, I_{15}	Peak current (into pins 12, 14 and 15)	50	mA
P_{tot}	Total power dissipation at $T_{amb} \leq 60^\circ\text{C}$	500	mW
T_{stg}	Storage temperature	-55 to 125	$^\circ\text{C}$
T_{op}	Operating temperature	0 to 70	$^\circ\text{C}$

NOTE: The positive input voltage at pin 2 and pin 6 must not be greater than the voltage at pin 3 and pin 4 respectively.

ORDERING NUMBER: TCA 511

MECHANICAL DATA

Dimensions in mm



ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^{\circ}\text{C}$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig.
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VERTICAL SECTION

I_3	Quiescent current	$V_s = 12\text{V}$ $f = 50\text{ Hz}$		4		mA	2
V_{3^*}	Supply voltage		9			V	
V_1	Peak to peak oscillator sawtooth voltage	$V_s = 12\text{V}$ $f = 50\text{ Hz}$		2.6		V	
V_2	Peak sync. input voltage	$V_s = 12\text{V}$ $f = 50\text{ Hz}$	3			V	3
V_{14}	Low level output voltage	$V_s = 12\text{V}$			1.5	V	
V_{15}	Low level output voltage	$I_{15} = 15\text{ mA}$			0.5	V	
R_2	Parallel input resistance at pin 2	$V_s = 12\text{V}$ $V_2 = 3\text{V}$		50		$\text{k}\Omega$	—
t^{**}	Output pulse width at pin 15	$V_s = 12\text{V}$ $f = 50\text{ Hz}$ $R_{10} = 15\text{ k}\Omega$		0.75		ms	2
Δf	Locking range	$V_s = 12\text{V}$ $f = 50\text{ Hz}$		-17		%	
$\frac{\Delta f}{\Delta T_{amb}}$	Frequency/temperature coefficient	$V_s = 12\text{V}$		-0.015		$\frac{\text{Hz}}{^{\circ}\text{C}}$	

HORIZONTAL SECTION

I_4	Quiescent current	$V_s = 12\text{V}$ $f = 15625\text{ Hz}$ $R_{11-13} = 0$		19		mA	2
V_{4^*}	Supply voltage		9			V	
V_6	Peak sinc. input voltage	$V_s = 12\text{V}$ $f = 15625\text{ Hz}$	3			V	
V_8	Regulated output voltage			7.5		V	2
V_{10}	Peak to peak oscillator sawtooth voltage	$V_s = 12\text{V}$ $f = 15625\text{ Hz}$		3.3		V	
V_{12}	Low level output voltage	$V_s = 12\text{V}$ $I_{12} = 15\text{ mA}$			0.45	V	3
R_6	Parallel input resistance at pin 6	$V_s = 12\text{V}$ $V_6 = 3\text{V}$		50		$\text{k}\Omega$	—

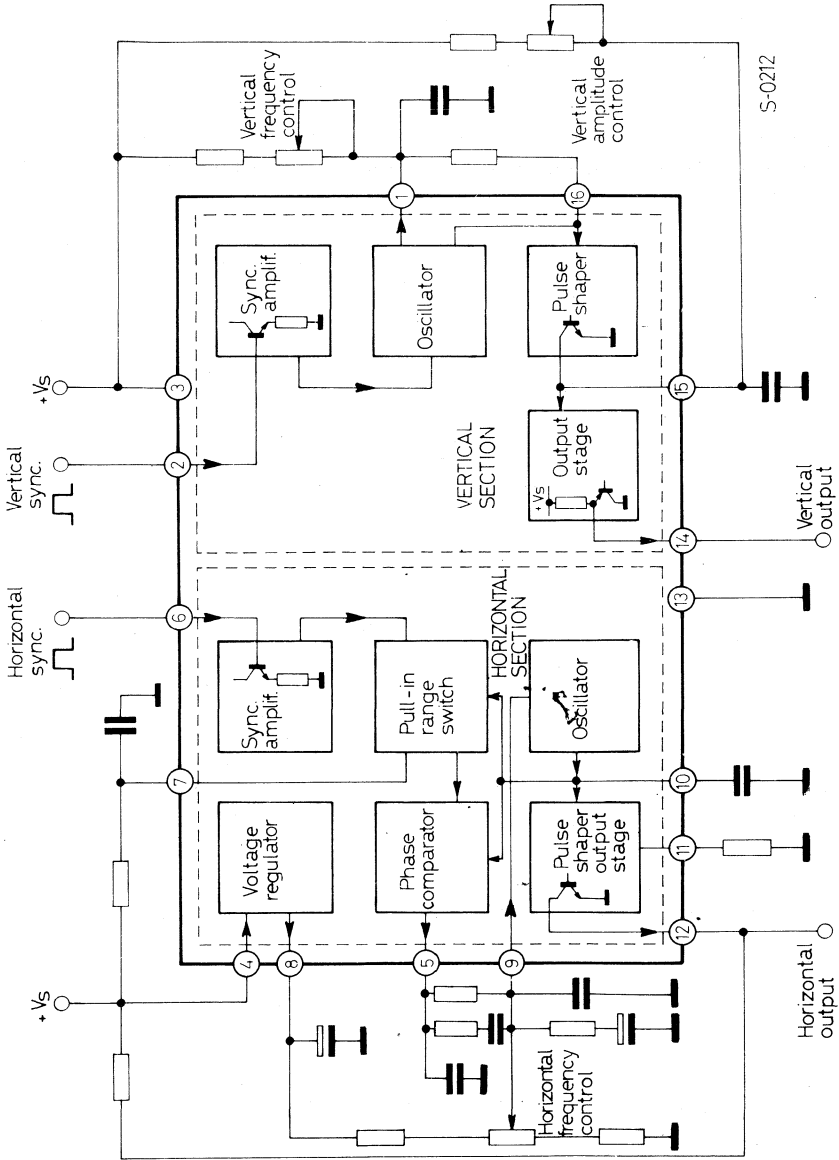
TCA 511

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig.
t ^{***}	Output pulse width at pin 12 V _s = 12V f = 15625 Hz a) R ₁₁₋₁₃ = 0 b) R ₁₁₋₁₃ = ∞		13 35		μs μs	2
t _d	Leading edge of output pulse to leading edge of sync. pulse phasing V _s = 12V f = 15625 Hz		4		μs	
Δf	Pull-in range		±1.3		kHz	
Δf	Hold-in range		±1.4		kHz	
$\frac{\Delta f}{\Delta V_9}$	Oscillator control sensitivity V _s = 12V		10		$\frac{\text{kHz}}{\text{V}}$	
$\frac{\Delta f}{\Delta t_d}$	APC loop gain		2		$\frac{\text{kHz}}{\mu\text{s}}$	
$\frac{\Delta f}{f} / \Delta V_s$	Oscillator frequency drift V _s = 9 to 14V		+0.7		$\frac{\%}{\text{V}}$	
$\frac{\Delta f}{\Delta T_{\text{amb}}}$	Frequency/temperature coefficient V _s = 12V		+ 5		$\frac{\text{Hz}}{^\circ\text{C}}$	

- NOTES:**
- * Minimum supply voltage for correct operation of the device.
 - ** The output pulse width can be adjusted by means of the external resistance connected between pins 1 and 6.
 - *** The output pulse width can be adjusted by means of the external resistance or by a voltage ≤ 5.3V, connected between pin 11 and pin 13.

Fig. 1 - Functional block diagram



TCA 511

Fig. 2 - Test circuit

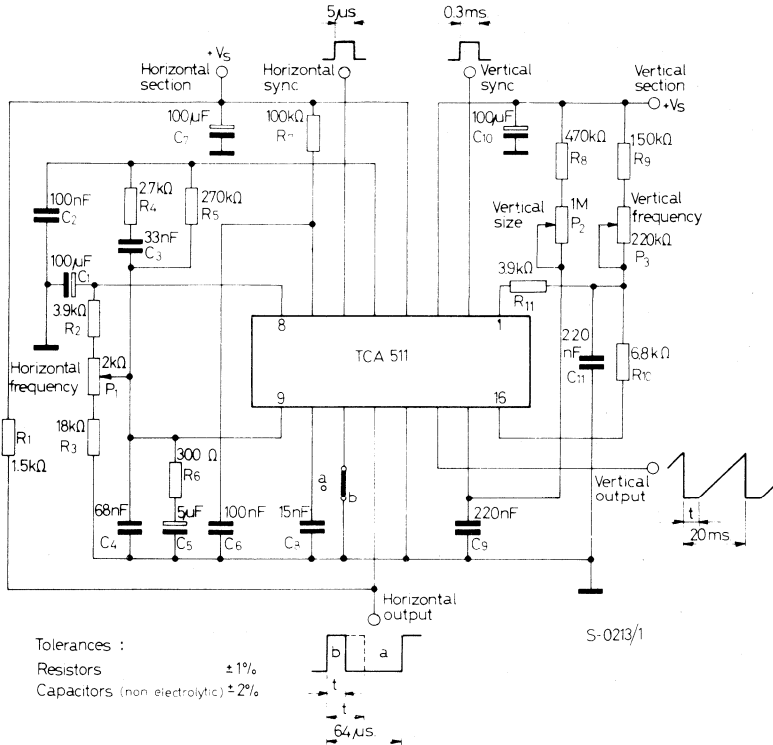


Fig. 3 - V_{12} , V_{14} and V_{15} test circuit

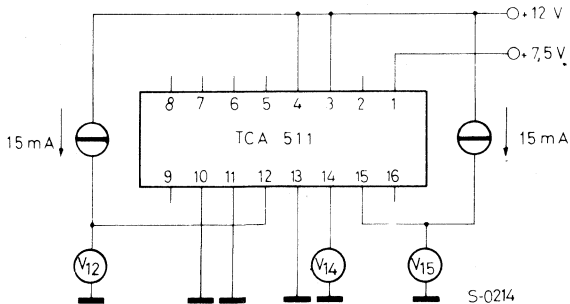
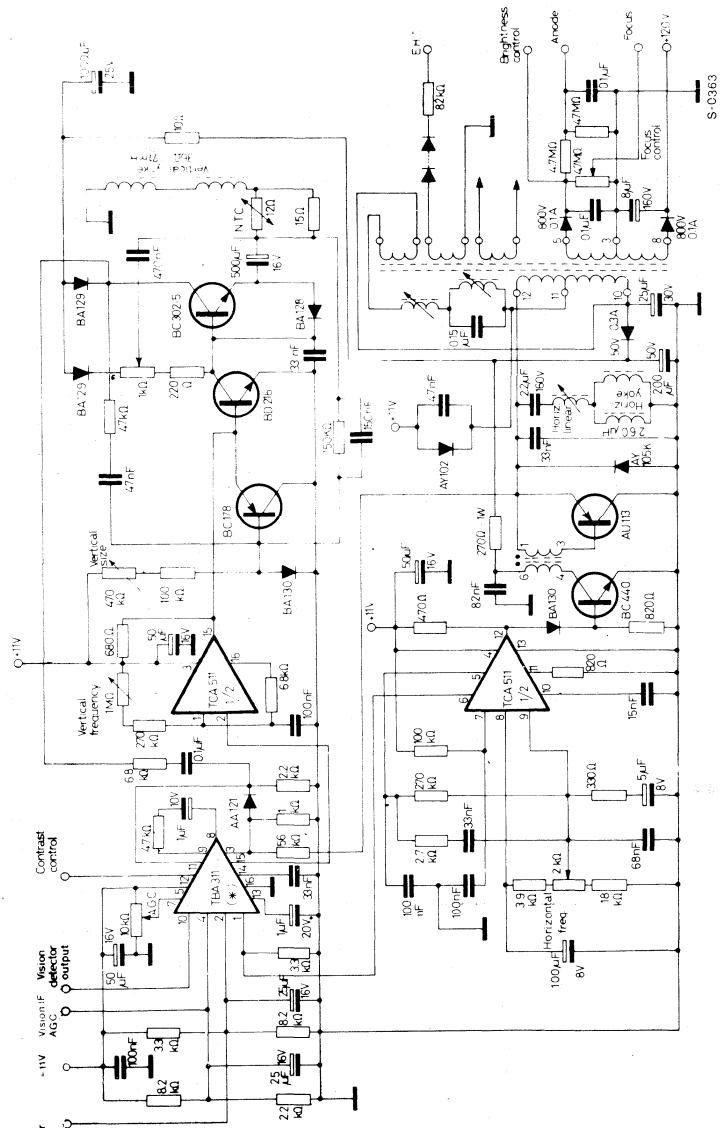


Fig. 4 - Typical application circuit for 12"110° TV set



(*) The jungle circuit TBA 311 performs the following functions: video preamplifier, IF AGC, PNP and NPN tuner AGC, sync. separator, noise gate. It is particularly suitable for driving the TCA 511 sync. inputs.

TCA 511

APPLICATION INFORMATION

Power Supply

The circuit can work with stabilized supply voltage having a value from 9 to 15V.

A dropping resistor and a filter capacitor may be used to obtain the supply from higher voltages, however, the voltage on pin 3 and 4 must never exceed the maximum permitted voltage.

Synchronization

Pins 2 and 6 can be DC driven if the reference level of the synchronization pulses is less than 1V. With reference levels greater than this value, a coupling capacitor must be inserted in series with the input, and pins 2 and 6 must be connected to ground via a resistor.

Vertical Oscillator

The capacitor connected to pin 1 must be selected with regard to the frequency tolerance, to the thermal stability and to the capacitor's ageing.

The width of the output pulse, to be chosen according to the needs of the output stages, is defined by the resistor connected between pin 1 and pin 16.

Vertical Output

The vertical output is taken from pin 14, which is a buffered output of the sawtooth voltage generated at pin 15.

The output current from pin 14 is defined by an internal resistor in the integrated circuit. If a greater current is needed, a resistor may be connected between pin 14 and pin 3.

The oscillator output pulse is available at pin 15 if the capacitor C9 is not connected.

This configuration is used for driving output stages in which the sawtooth is generated by Miller effect.

Horizontal Oscillator

The capacitor connected between pin 10 and ground must be selected with regard to the frequency tolerance, to the thermal stability and to the capacitor's ageing.

In multistandard receivers, the oscillation frequency may be changed by switching the value of the capacitor connected to pin 10.

Phase Comparator

The phase comparator's output consists of current pulses acting on the oscillator control voltage.

The external components C2, C3, C4, C5, R4, R5 and R6 (fig. 2) define the circuit performance with respect to the pull-in range, the hold-in range and the frequency variations that occur on switching-on and switching-off.

Moreover the pull-in range depends on the absolute value of the voltage divider R2, P1 and R3.

A coincidence detector is connected to pin 7; this modifies the pull-in range and the noise immunity, depending on whether the system is synchronised or is searching for synchronization. The time constant applied to pin 7 avoids uncertainty during the switch from one state to the other.

Horizontal Output

The collector of the output transistor is connected to pin 12; its load resistor, externally connected between pin 12 and pin 4, defines the amplitude of the output current pulse.

The width of the output pulse can be varied between 13 and 35 μ s by means of the resistor connected between pin 11 and ground, or else by means of a voltage ≤ 5.3 V applied between pin 11 and ground.

This control acts upon the trailing edge of the pulse, hence the phase advance of the leading edge stays constant with respect to the synchronism.

LINEAR INTEGRATED CIRCUIT

AUDIO POWER AMPLIFIER WITH THERMAL SHUT-DOWN

The TCA 830S is a monolithic integrated circuit in a 12-lead quad in-line plastic package, intended for use as a low frequency class B amplifier. The TCA 830S provides 4.2W output power @ 14V/4Ω, 3.4W @ 12V/4Ω, 2W @ 9V/4Ω, 3.7W @ 16V/8Ω and 2.3W @ 12V/8Ω.

It works with a wide range of supply voltages (4 to 20V), gives high output current (up to 2A) and very low harmonic and cross-over distortion. In addition, the circuit is provided with a thermal limiting circuit which fundamentally changes the criteria normally used in determining the size of the heatsink. The TCA 830S is pin to pin equivalent to the TBA 810S.

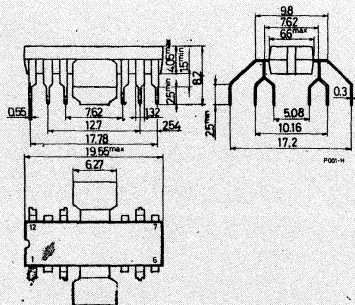
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	20	V
I_o	Output peak current (non-repetitive)	2.5	A
I_o	Output peak current (repetitive)	2	A
P_{tot}	Power dissipation: at $T_{amb} = 80^\circ\text{C}$	1	W
	at $T_{tab} = 90^\circ\text{C}$	5	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBER: TCA 830S

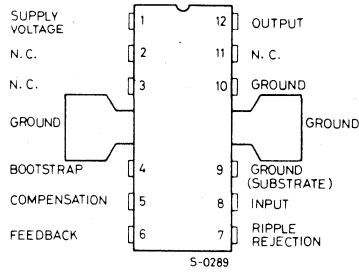
MECHANICAL DATA

Dimensions in mm

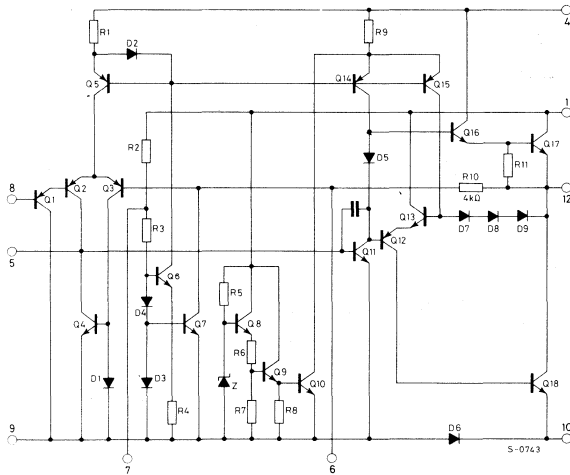


TCA 830S

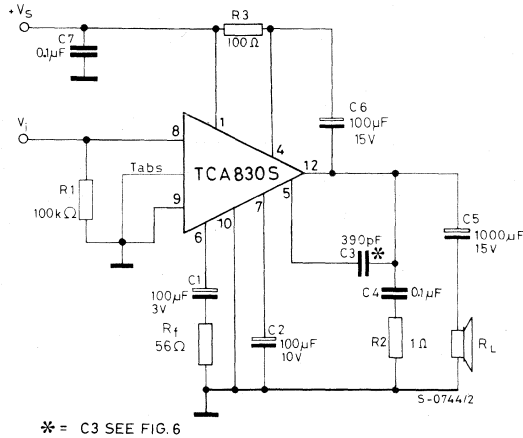
CONNECTION DIAGRAM (top view)



SCHEMATIC DIAGRAM



TEST AND APPLICATION CIRCUIT



THERMAL DATA

$R_{th\ j-tab}$	Thermal resistance junction-tab	max	12	°C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	70*	°C/W

* Obtained with tabs soldered to printed circuit with minimized copper area.

ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $T_{amb} = 25^{\circ}\text{C}$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	
V_S	Supply voltage (pin 1)	4		20	V	
V_O	Quiescent output voltage (pin 12)	$V_S = 12\text{V}$	5.3	6	6.7	V
I_d	Quiescent drain current	$V_S = 9\text{V}$		8.5	16	mA
I_b	Input bias current	$V_S = 12\text{V}$		0.2		μA
P_O	Output power	$d = 10\%$ $V_S = 14\text{V}$ $V_S = 12\text{V}$ $V_S = 9\text{V}$ $V_S = 6\text{V}$ $V_S = 16\text{V}$ $V_S = 12\text{V}$	$f = 1\text{ kHz}$ $R_L = 4\Omega$ $R_L = 4\Omega$ $R_L = 4\Omega$ $R_L = 4\Omega$ $R_L = 8\Omega$ $R_L = 8\Omega$	2.5	4.2 3.4 2 0.8 3.7 2.3	W W W W W W

TCA 830S

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_i (rms) Input saturation voltage		220			mV
V_i Input sensitivity	$P_o = 3.4W$ $R_L = 4\Omega$ $V_s = 12V$ $f = 1\text{ kHz}$		50		mV
B Frequency response (-3 dB)	$V_s = 12V$ $C3 = 390\text{ pF}$ $R_L = 4\Omega$	40 to 10,000			Hz
d Distortion	$P_o = 50\text{ mW to }2W$ $V_s = 12V$ $R_L = 4\Omega$ $f = 1\text{ kHz}$		0.3		%
R_i Input resistance (pin 8)			5		M Ω
G_v Voltage gain (open loop)	$V_s = 12V$ $f = 1\text{ kHz}$ $R_L = 4\Omega$		75		dB
G_v Voltage gain (closed loop)	$V_s = 12V$ $f = 1\text{ kHz}$ $R_L = 4\Omega$	34	37	40	dB
e_N Input noise voltage	$V_s = 12V$ B (-3 dB) = 40 to 10,000 Hz $R_1 = 0$		2		μV
i_N Input noise current	$V_s = 12V$ B (-3 dB) = 40 to 10,000 Hz		0.1		nA
η Efficiency	$P_o = 3.4W$ $R_L = 4\Omega$ $V_s = 12V$ $f = 1\text{ kHz}$		62		%
SVR Supply voltage rejection	$V_s = 12V$ $f_{\text{ripple}} = 100\text{ Hz}$ $C2 = 100\text{ }\mu F$ $C2 = 25\text{ }\mu F$ $R_L = 4\Omega$		45 38		dB dB
I_d Drain current	$P_o = 3.4W$ $R_L = 4\Omega$ $V_s = 12V$		430		mA
T_{sd} *Thermal shut-down case temperature	$P_{tot} = 2.2W$		130		$^{\circ}C$

* See figs. 8 and 13.

Fig. 1 - Output power vs. supply voltage

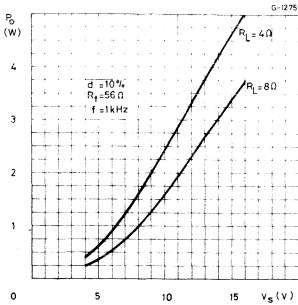


Fig. 2 - Maximum power dissipation vs. supply voltage (sine wave operation)

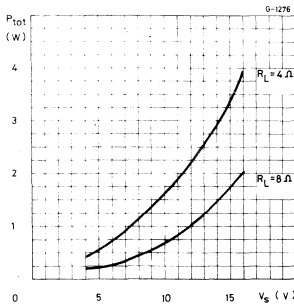


Fig. 3 - Distortion vs. output power

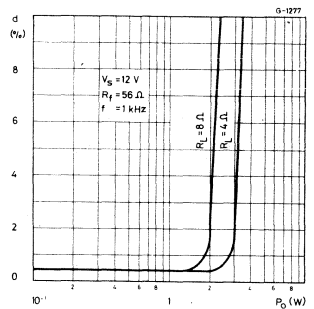


Fig. 4 - Voltage gain (closed loop) and typical input voltage vs. feedback resistance (R_f)

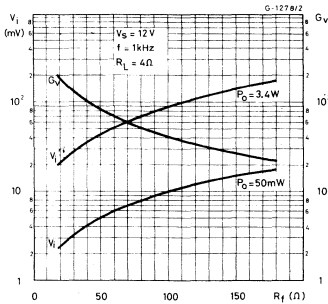


Fig. 5 - Distortion vs. frequency

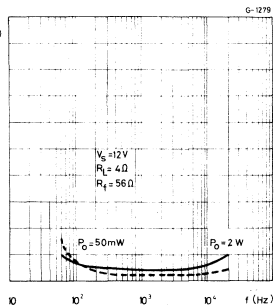


Fig. 6 - C_3 vs. R_f for different bandwidths

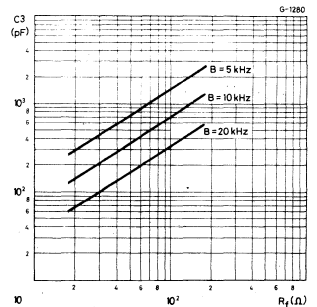


Fig. 7 - Supply voltage rejection

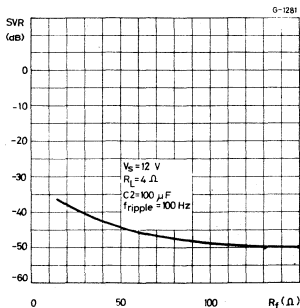


Fig. 8 - Power dissipation and efficiency vs. output power

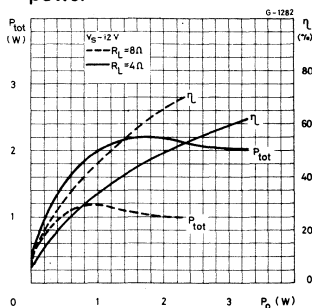
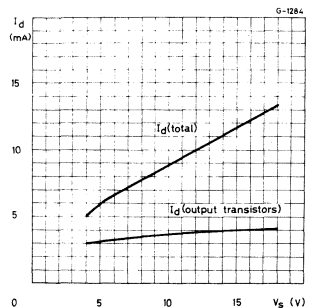


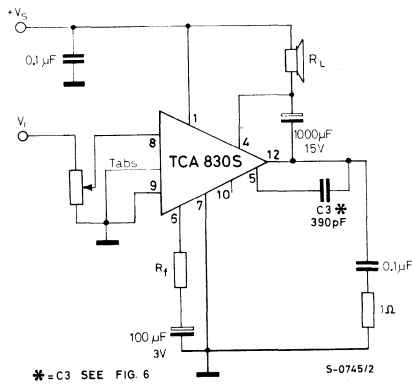
Fig. 9 - Quiescent current vs. supply voltage



TCA 830S

APPLICATION INFORMATION

Fig. 10 - Circuit with load connected to the supply voltage



For line operated equipment the bootstrap can be eliminated using the circuit of fig. 11.

Fig. 11 - Circuit with load connected to ground and without bootstrap, in which V_G spread is reduced (external R_X)

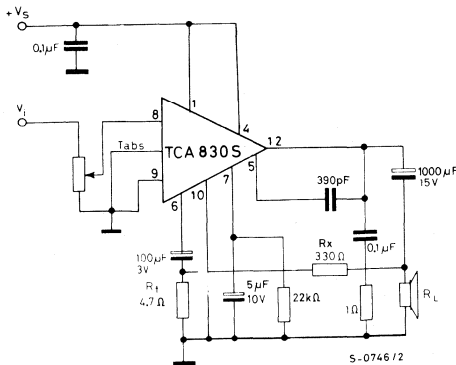
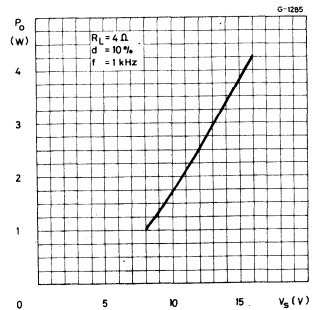


Fig. 12 - Typical output power vs. supply voltage

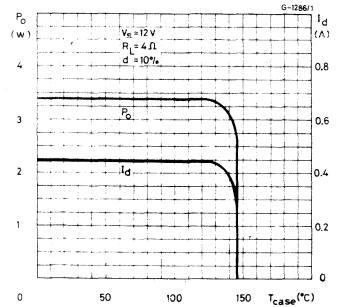


THERMAL SHUT-DOWN

The presence of a thermal limiting circuit offers the following advantages:

- 1) an overload on the output (even if it is permanent) or an above-limit ambient temperature can be easily supported
- 2) the heatsink can have a smaller factor of safety compared with that of a conventional circuit. There is no device damage in the case of too high a junction temperature; all that happens is that P_o (and therefore P_{tot}) and I_d are reduced (fig. 13).

Fig. 13 - Output power and drain current vs. package temperature



MOUNTING INSTRUCTION

The thermal power dissipated in the circuit may be removed by connecting the tabs to an external heatsink or by soldering them to an area of copper on the printed circuit board (fig. 14).

Fig. 15 shows a simple type of heatsink. Assuming an area of copper on the printed circuit board of only 2 cm², the total R_{th} between junction and ambient is approximately 28 $^{\circ}C/W$.

The external heatsink or area of printed circuit copper must be connected to electrical ground.

Fig. 17 gives the maximum power that can be dissipated (for $T_{amb} = 55$ and 70 $^{\circ}C$) as a function of the side of two equal square copper areas having a thickness of 35 μ (1.4 mil). During soldering the tabs temperature must not exceed 260 $^{\circ}C$ and the soldering time must not be longer than 12 seconds.

Fig. 14 - Example of area of P.C. board copper soldered to the tabs of the TCA 830S

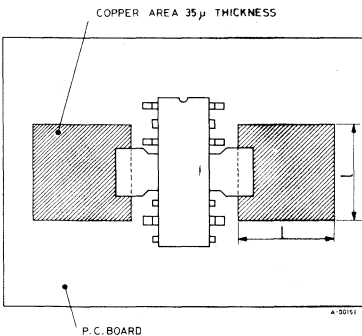
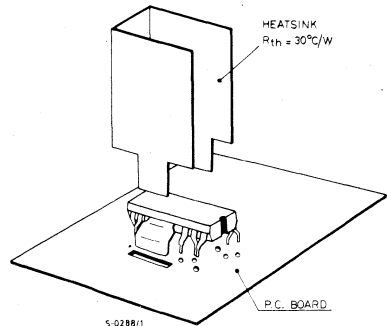


Fig. 15 - Example of TCA830S with external heatsink.



TCA 830S

Fig. 16 - Power that can be dissipation vs. "l"

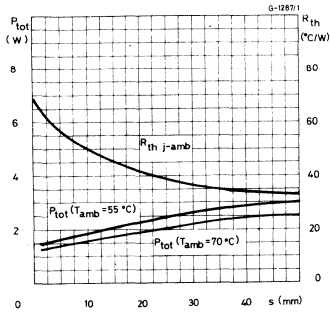


Fig. 17 - Maximum allowable power dissipation vs. ambient temperature

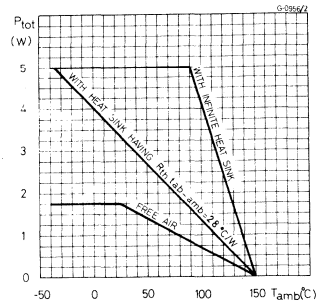
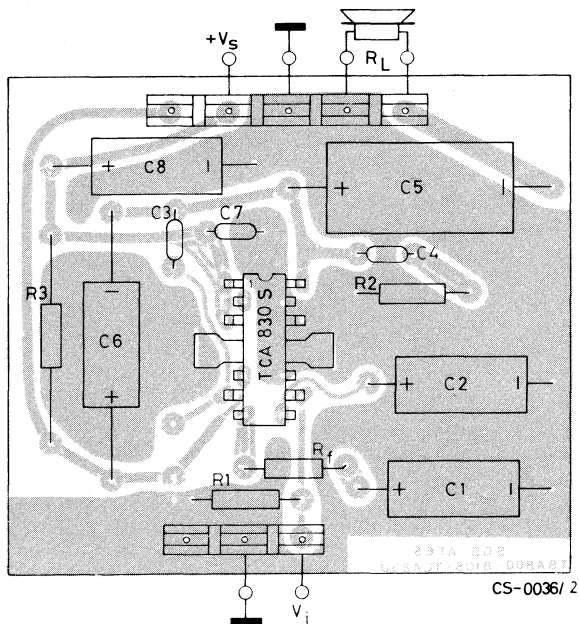


Fig. 18 - P.C. board and component layout of the test and application circuit (1:1 scale).



LINEAR INTEGRATED CIRCUITS

MOTOR SPEED REGULATORS

The TCA 900 and TCA 910 are monolithic integrated circuits in Jedec TO-126 plastic package. They are designed for use as speed regulators for DC motors of record players, cassette recorders and players. The TCA 900 is particularly suitable for battery operated portable equipments, and the TCA 910 for car-battery and mains operations.

ABSOLUTE MAXIMUM RATINGS

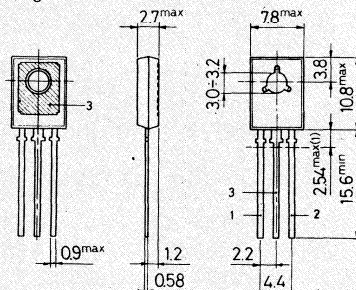
		TCA 900	TCA 910
V_s	Supply voltage	14V	20V
P_{tot}	Total power dissipation at $T_{amb} = 70^\circ\text{C}$ at $T_{case} = 100^\circ\text{C}$		0.8 W 5 W
T_{stg}	Storage temperature		-55 to 150°C
T_j	Junction temperature		150°C

ORDERING NUMBERS: TCA 900
TCA 910

MECHANICAL DATA

Dimensions in mm

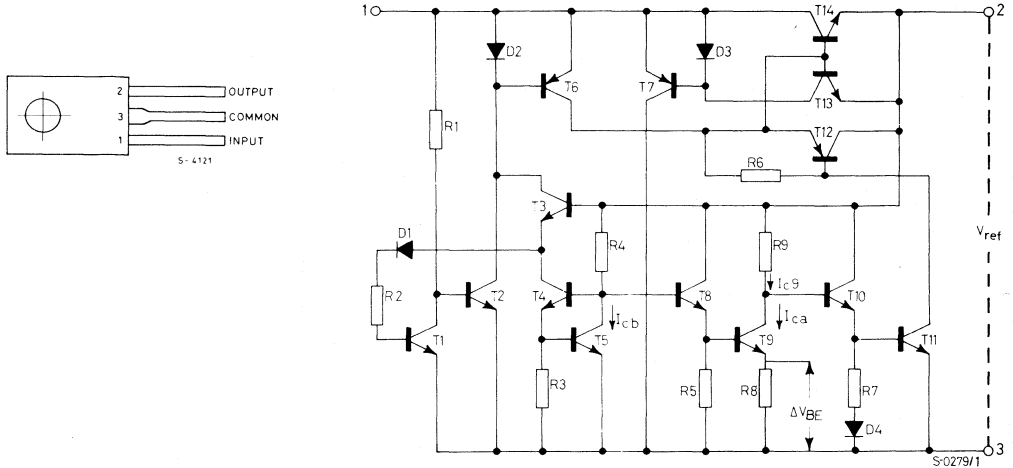
Pin 3 connected to metal part of mounting surface



C-0054/2

TCA 900 TCA 910

CONNECTION AND SCHEMATIC DIAGRAMS



THERMAL DATA

$R_{th \text{ j-case}}$	Thermal resistance junction-case	Typ.	10	°C/W
$R_{th \text{ j-amb}}$	Thermal resistance junction-ambient	Typ.	100	°C/W

ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $T_{amb} = 25^\circ\text{C}$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_{ref}	Reference voltage (between pins 2 and 3) $V_s = 5.5\text{V}$ $I_m = 70\text{ mA}$ $R_T = 0$		2.6		V
I_{d3}	Quiescent current (at pin 3) $V_s = 5.5\text{V}$ $I_m = 0$ $R_T = 0$		2.6		mA
V_m	Output voltage (for TCA 900 only) $V_s = 5.5\text{V}$ $I_m = 70\text{ mA}$ $R_T = 91\Omega$		3.6	3.9	V
V_m	Output voltage (for TCA 910 only) $V_s = 9\text{V}$ $I_m = 70\text{ mA}$ $R_T = 270\Omega$		5.6	6.3	V

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_{1-2} Dropout voltage	$\Delta V_m/V_m = -1\%$ $I_m = 70 \text{ mA}$ $R_T = 91\Omega$		1.2		V
I_2 Limiting output current (at pin 2)	$V_s = 5.5\text{V}$ $V_{2-3} = 0$		400		mA
$k = \Delta I_2/\Delta I_3$	$V_s = 5.5\text{V}$ $I_2 = 70 \text{ mA}$ $\Delta I_2 = \pm 10 \text{ mA}$ $R_T = 0$		8.5		—
$\frac{\Delta V_m}{V_m} / \Delta V_s$ Line regulation (for TCA 900 only)	$V_s = 5.5\text{V to } 12\text{V}$ $I_m = 70 \text{ mA}$ $R_T = 91\Omega$		0.1		%/V
$\frac{\Delta V_m}{V_m} / \Delta V_s$ Line regulation (for TCA 910 only)	$V_s = 10\text{V to } 16\text{V}$ $I_m = 70 \text{ mA}$ $R_T = 270\Omega$		0.1		%/V
$\frac{\Delta V_m}{V_m} / \Delta I_m$ Load regulation	$V_s = 5.5\text{V}$ $I_m = 40 \text{ to } 100 \text{ mA}$ $R_T = 0$		0.005		%/mA
$\frac{\Delta V_{ref}}{V_{ref}} / \Delta T_{amb}$ Temperature coefficient	$V_{1-3} = 5.5\text{V}$ $I_2 = 70 \text{ mA}$ $T_{amb} = -20 \text{ to } 70^\circ\text{C}$		0.01		%/°C

Fig. 1 - Test circuit.

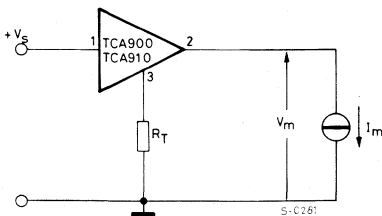
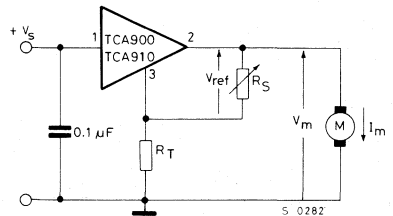


Fig. 2 - Typical application circuit.



TCA 900 TCA 910

Fig. 3 - Normalized k vs. I_2 .

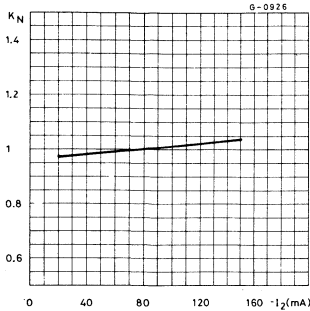


Fig. 4 - Dropout voltage vs. output current

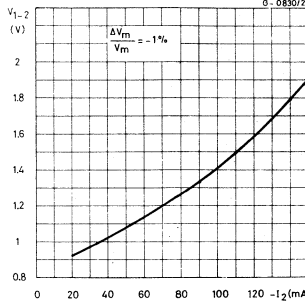
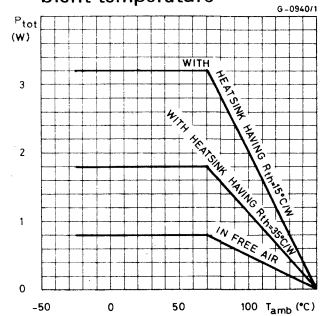


Fig. 5 - Maximum allowable power dissipation vs. ambient temperature



APPLICATION INFORMATION

The regulator supplies the motor in such a way as to keep its speed constant, independent of supply voltage, applied torque and ambient temperature variations.

The basic equation for the motor is:

$$V_m = E_0 + R_m I_m = a_1 n + a_2 c$$

Where: V_m = supply voltage applied to the motor
 E_0 = back electromotive force
 n = motor speed (r.p.m.)
 R_m = internal resistance (of the motor)
 I_m = current absorbed (by the motor)
 a_1 and a_2 = constants
 c = drive torque

A voltage supply with the following characteristics

$E = E_0$ E = electromotive force

$R_o = -R_m$ R_o = output resistance

gives performance required.

This means that a variation in current absorbed by the motor, due to a variation in torque applied, causes a proportional variation in regulator output voltage. In fig. 6 is shown the minimum allowable E_0 vs. R_T . The TCA 900 and TCA 910 give a reference constant voltage V_{ref} (between pins 2 and 3) independent of variations of V_s , I_2 and ambient temperature.

They also give: $I_3 = I_{d3} + I_2/k$

Where: I_3 = total current at pin 3
 I_{d3} = quiescent current at pin 3 ($I_2 = 0$)
 I_2 = current at pin 2
 k = constant

The output voltage V_m , applied to the motor has the following value:

$$V_m = \underbrace{V_{ref} + R_T \left[\frac{V_{ref}}{R_s} \left(1 + \frac{1}{k} \right) + I_{d3} \right]}_{\text{Term 1}} + \underbrace{\frac{I_m}{k} R_T}_{\text{Term 2}}$$

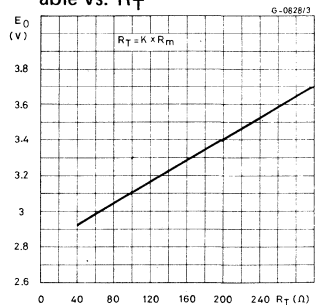
Term 1 equals E_0 and fixes the motor speed by means of the variable resistor R_s ;

Term 2 $\frac{I_m}{k} R_T$. R_T equals the term $R_m \cdot I_m$ and, therefore, compensates variations of torque applied. Complete compensation is achieved when:

$$R_T = k R_m$$

$I_f R_{T \max} > k R_{m \min}$ instability may occur.

Fig. 6 - Minimum E_0 allowable vs. R_T



LINEAR INTEGRATED CIRCUIT

10W AUDIO POWER AMPLIFIER

The TCA 940N is a monolithic integrated circuit in a 12-lead quad in-line plastic package, intended for use as a low frequency class B amplifier. The TCA 940N provides 10W output power @ 20V/4Ω, 7W @ 16V/4Ω and 6.5W @ 20V/8Ω. It gives high output current (up to 3A), very low harmonic and cross-over distortion. Besides the thermal shut-down, the device contains a current limiting circuit which restricts the operation within the safe operating area of the power transistors. The TCA 940N is pin to pin equivalent to the TBA 810 AS.

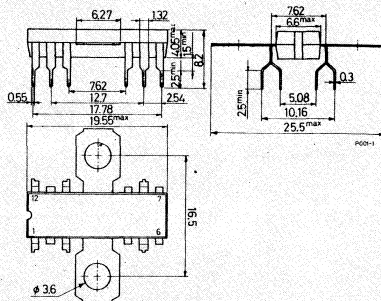
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	28	V
I_o	Output peak current (non-repetitive)	3.5	A
I_o	Output peak current (repetitive)	3	A
P_{tot}	Power dissipation: at $T_{amb} = 50^\circ\text{C}$	1.25	W
	at $T_{tab} = 70^\circ\text{C}$	8	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBER: TCA 940N

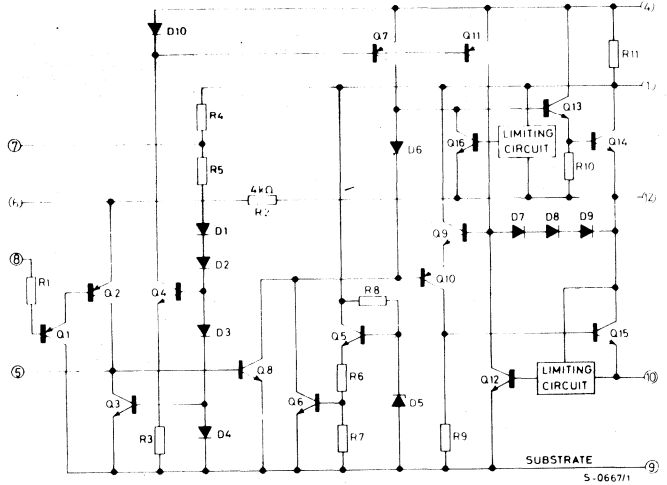
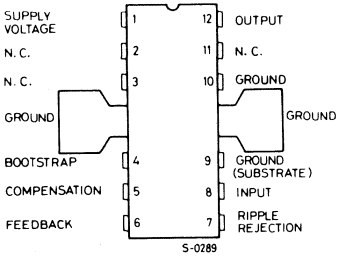
MECHANICAL DATA

Dimensions in mm

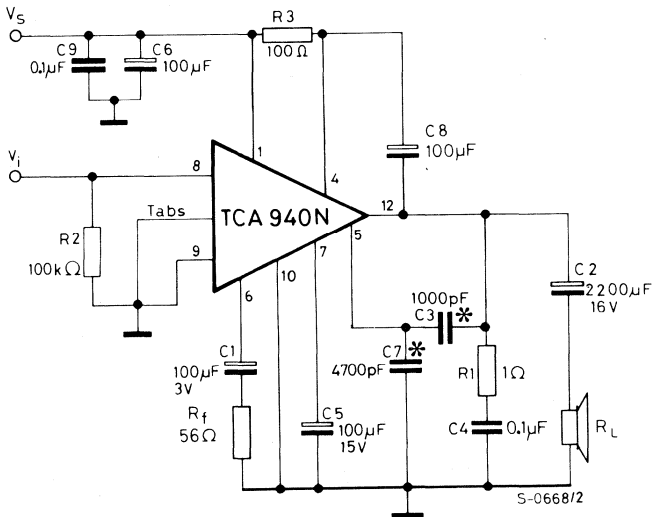


TCA 940N

CONNECTION AND SCHEMATIC DIAGRAMS (top view)



TEST AND APPLICATION CIRCUIT



*= C3, C7 SEE FIG. 7

THERMAL DATA

$R_{th\ j-tab}$	Thermal resistance junction-tab	max	10	°C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	80	°C/W

ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $T_{amb} = 25^{\circ}C$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit		
V_s	Supply voltage (pin 1)	6		28	V		
V_o	Quiescent output voltage (pin 12)	$V_s = 18V$	8.2	9	9.8	V	
I_d	Quiescent drain current	$V_s = 12V$ $V_s = 24V$		13 20		mA mA	
I_b	Input bias current (pin 8)	$V_s = 18V$		0.5		μA	
P_o	Output power	$d = 10\%$ $V_s = 20V$ $V_s = 18V$ $V_s = 16V$ $V_s = 20V$ $V_s = 18V$	$f = 1\ kHz$ $R_L = 4\ \Omega$ $R_L = 4\ \Omega$ $R_L = 4\ \Omega$ $R_L = 8\ \Omega$ $R_L = 8\ \Omega$	7	10 9 7 6.5 5	W W W W W	
$V_{i(rms)}$	Voltage for input saturation		250			mV	
V_i	Input sensitivity	$P_o = 9W$ $R_L = 4\ \Omega$	$V_s = 18V$ $f = 1\ kHz$		90	mV	
B	Frequency response (-3 dB)	$V_s = 18V$ $C_3 = 1000\ \mu F$	$R_L = 4\ \Omega$	40 to 20,000			
d	Distortion	$P_o = 50\ mW\ to\ 5W$ $V_s = 18V$ $f = 1\ kHz$	$R_L = 4\ \Omega$		0.3	%	
R_i	Input resistance (pin 8)			5		M Ω	
G_v	Voltage gain (open loop)	$V_s = 18V$ $f = 1\ kHz$	$R_L = 4\ \Omega$		75	dB	
G_v	Voltage gain (closed loop)	$V_s = 18V$ $f = 1\ kHz$	$R_L = 4\ \Omega$	34	37	40	dB
e_N	Input noise voltage	$V_s = 18V$	$R_g = 0$		3	μV	
i_N	Input noise current	$V_s = 18V$			0.15	nA	

TCA 940N

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
η Efficiency	$P_O = 9W$ $R_L = 4\Omega$ $f = 1\text{ kHz}$ $V_S = 18V$		65		%
SVR Supply voltage rejection	$V_S = 24V$ $f_{\text{ripple}} = 100\text{ Hz}$ $R_L = 4\Omega$		45		dB
I_d Drain current	$P_O = 9W$ $R_L = 4\Omega$ $V_S = 18V$		770		mA
T_{sd} Thermal shut-down (*) Case temperature	$P_{\text{tot}} = 4.8W$		110		$^{\circ}C$

(*) See fig. 15.

Fig. 1 - Output power vs. supply voltage.

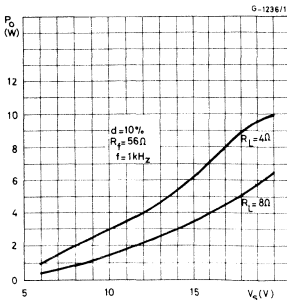


Fig. 2 - Maximum power dissipation vs. supply voltage (sine wave operation)

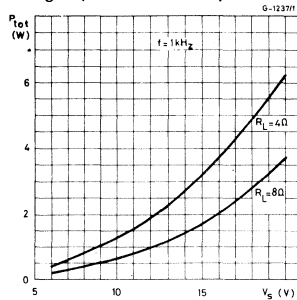


Fig. 3 - Distortion vs. output power.

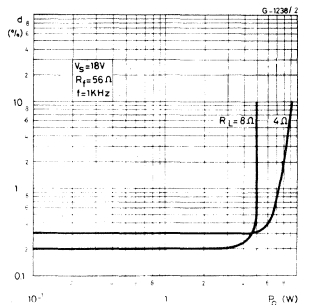


Fig. 4 - Voltage gain and input sensitivity vs. feedback resistance (R_f)

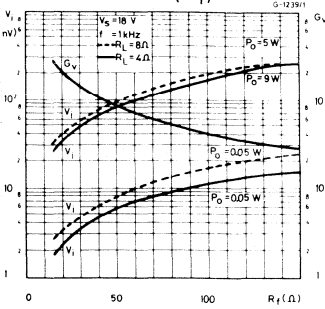


Fig. 5 - Distortion vs. frequency ($R_L = 4\ \Omega$)

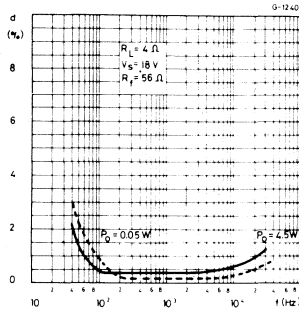


Fig. 6 - Distortion vs. frequency ($R_L = 8\ \Omega$)

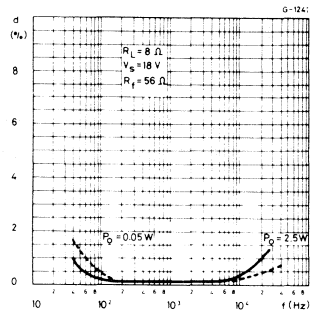


Fig. 7 - Value of C3 vs. R_f for different bandwidths

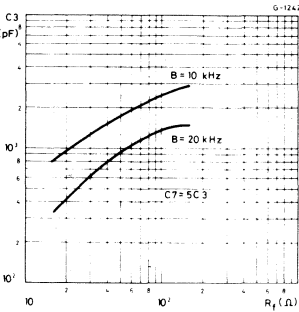


Fig. 8 - Supply voltage rejection vs. feedback resistance (R_f)

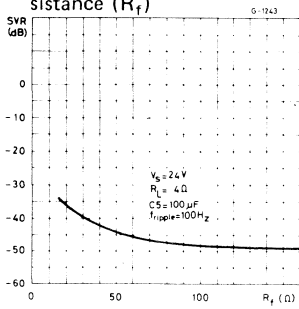


Fig. 9 - Power dissipation and efficiency vs. output power ($R_L = 4\ \Omega$)

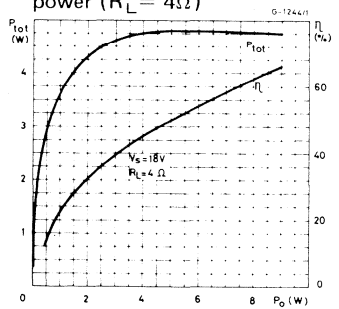


Fig. 10 - Power dissipation and efficiency vs. output power ($R_L = 8\ \Omega$)

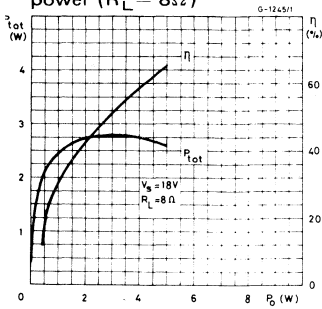


Fig. 11 - Quiescent output voltage (pin 12) vs. supply voltage

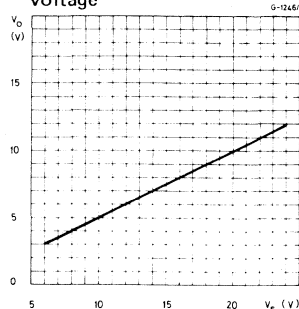
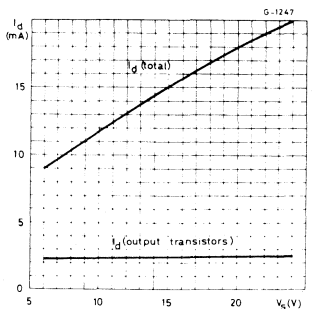


Fig. 12 - Quiescent current vs. supply voltage



TCA 940N

SHORT CIRCUIT PROTECTION

The most important innovation in the TCA 940N is an original circuit which limits the current of the output transistors. Fig. 13 shows that the maximum output current is a function of the collector-emitter voltage; hence the circuit works within the safe operating area of the output power transistors. This can therefore be considered as being power limiting rather than simple current limiting. The TCA 940N is thus protected against temporary overloads or short circuit by the above circuit. Should the short circuit exist for a longer time, the thermal shut-down comes into action and keeps the junction temperature within safe limits.

Fig. 13 - Maximum output current vs. voltage (V_{CE}) across each output transistor

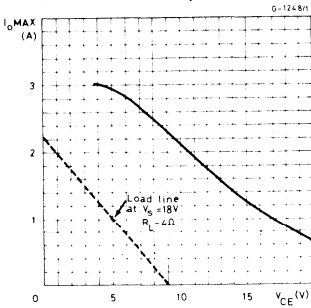
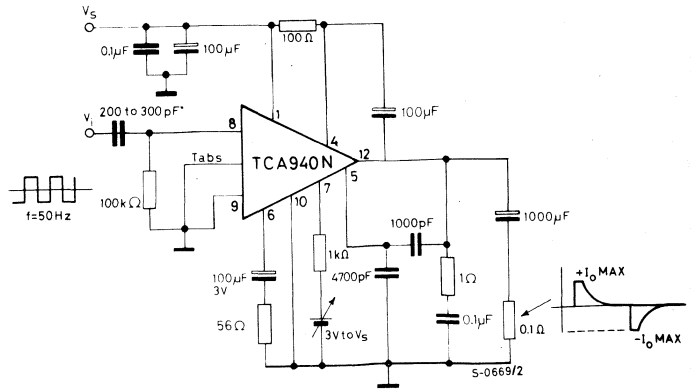


Fig. 14 - Test circuit for the limiting characteristics

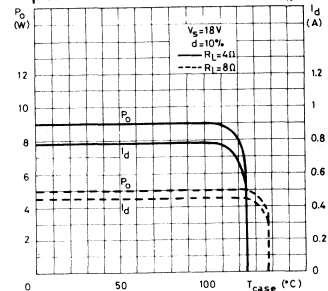


THERMAL SHUT-DOWN

The presence of a thermal limiting circuit offers the following advantages:

- 1) an overload on the output (even if it is permanent), or an above-limit ambient temperature can be easily supported.
- 2) the heatsink can have a smaller factor of safety compared with that of a conventional circuit. There is no device damage in the case of too high a junction temperature: all that happens is that P_o (and therefore P_{tot}) and I_d are reduced (fig. 15).

Fig. 15 - Output power and drain current vs. case temperature



MOUNTING INSTRUCTION

The power dissipated in the circuit may be removed by connecting the tabs to an external heatsink according to fig. 16. The desired thermal resistance may be obtained by fixing the TCA 940N to a suitably dimensioned plate as shown in fig. 17. This plate can also act as a support for the whole printed circuit board; the mechanical stresses do not damage the integrated circuit. During soldering the tabs temperature must not exceed 260°C and the soldering time must not be longer than 12 seconds.

Fig. 16 - Maximum allowable power dissipation vs. ambient temperature

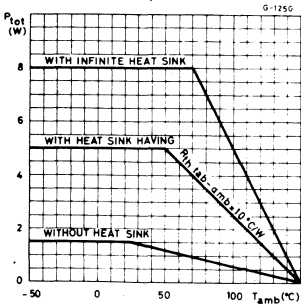


Fig. 17 - Mounting example

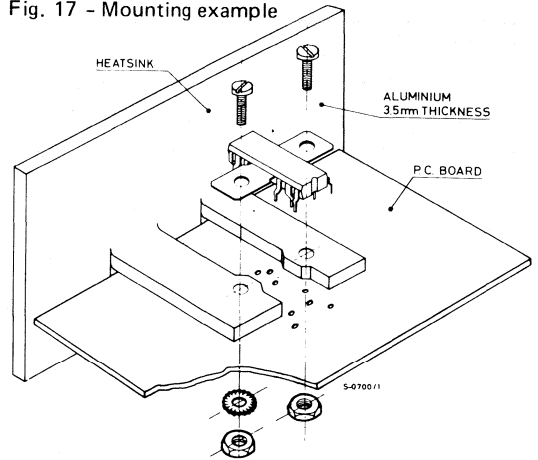
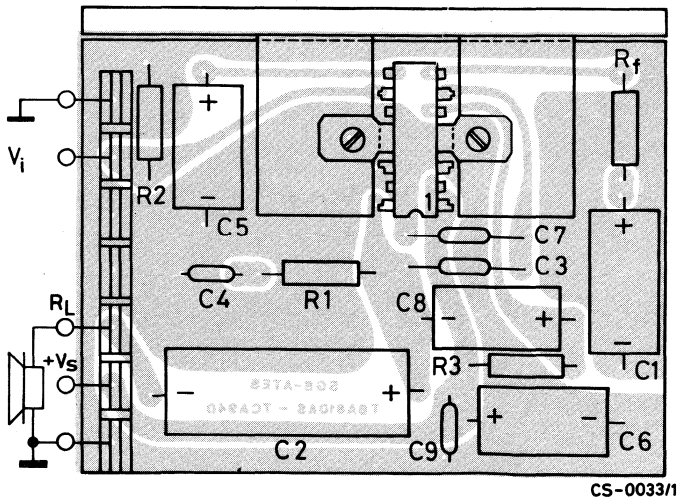


Fig. 18 - P.C. board and components layout of the test and application circuit (1:1 Scale).



TCA 3089

LINEAR INTEGRATED CIRCUIT

FM-IF RADIO SYSTEM

- HIGH LIMITING SENSITIVITY
- HIGH AMR
- HIGH RECOVERED AUDIO
- GOOD CAPTURE RATIO
- LOW DISTORTION
- MUTING CAPABILITY

The TCA 3089 is a monolithic integrated circuit in a 16-lead dual in-line plastic package. It provides a complete subsystem for amplification of FM signals.

The functions incorporated are:

- FM amplification and detection
- Interchannel controlled muting
- AFC and delayed AGC for FM tuner
- Switching of stereo decoder
- Driver of a field strength meter

The TCA 3089 can be used for FM-IF amplifier application in Hi-Fi, car-radios and communication receivers.

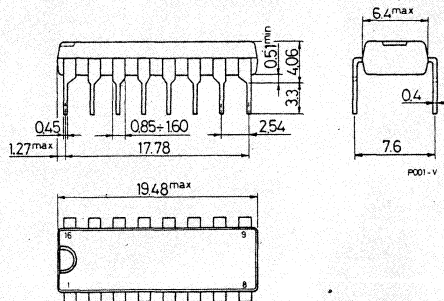
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	16	V
I_o	Output current (from pin 15)	2	mA
P_{tot}	Total power dissipation at $T_{amb} \leq 70^\circ\text{C}$	800	mW
T_{stg}	Storage temperature	-55 to 150	$^\circ\text{C}$
T_{op}	Operating temperature	-25 to 70	$^\circ\text{C}$

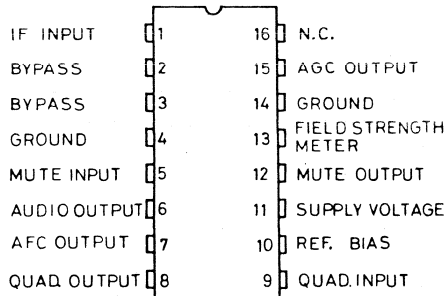
ORDERING NUMBER: TCA 3089

MECHANICAL DATA

Dimensions in mm

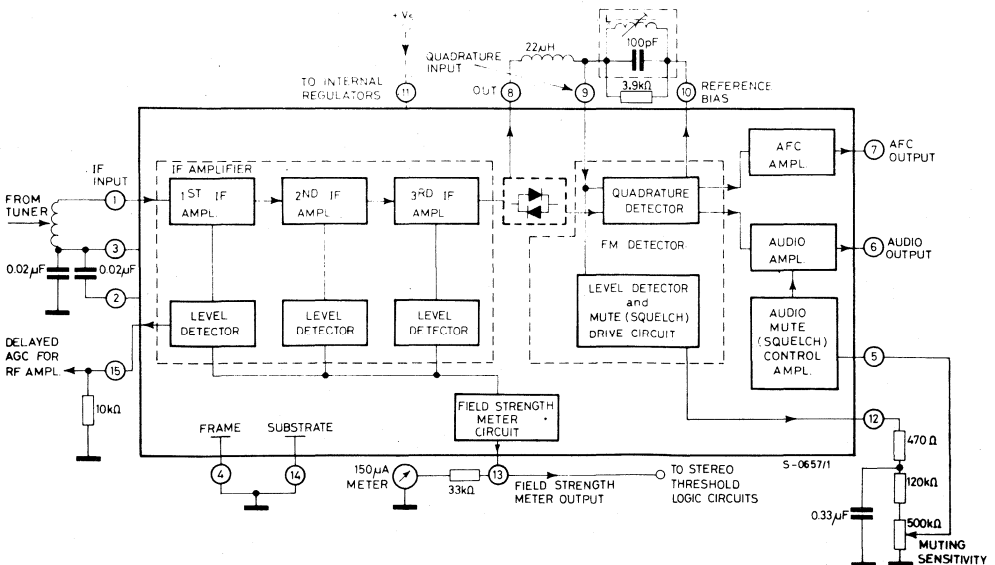


CONNECTION DIAGRAM (top view)



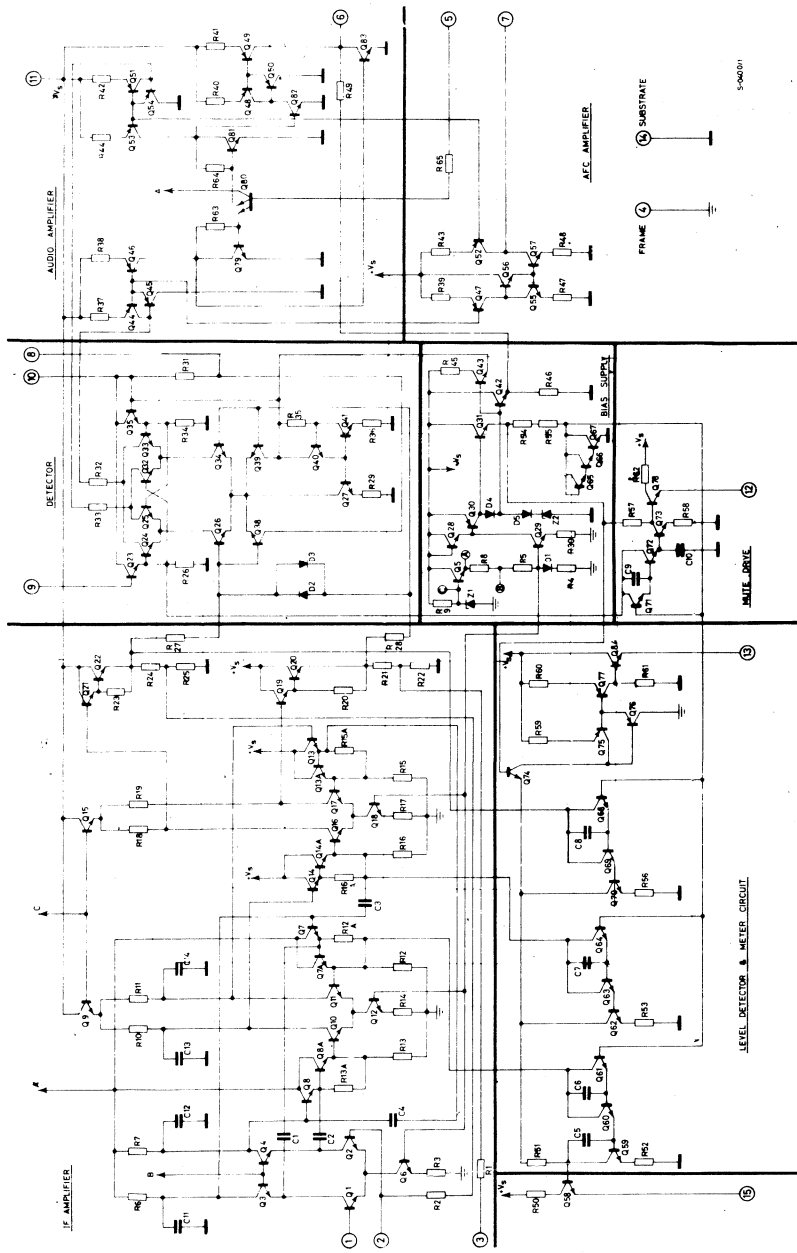
S-0398/1

BLOCK DIAGRAM



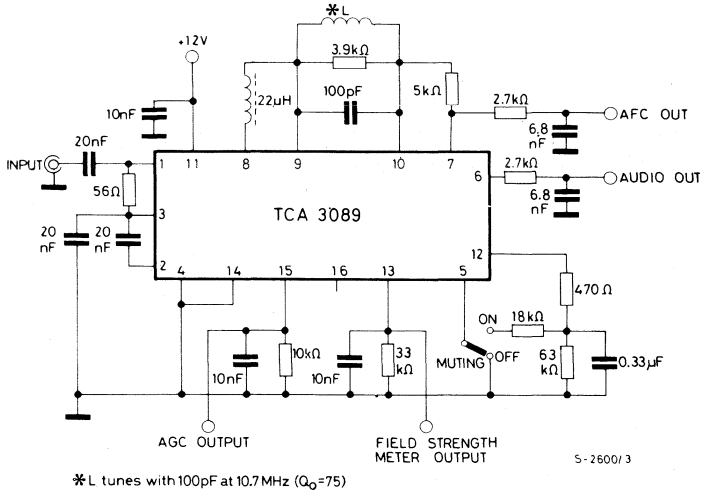
TCA 3089

SCHEMATIC DIAGRAM



TCA 3089

TEST CIRCUIT



THERMAL DATA

$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	100	°C/W
-----------------	-------------------------------------	-----	-----	------

ELECTRICAL CHARACTERISTICS (Refer to the test circuit; $V_s = 12V$, $f_o = 10.7\text{ MHz}$, $V_5 = 0V$, $T_{amb} = 25^\circ\text{C}$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
-----------	-----------------	------	------	------	------

DC CHARACTERISTICS

I_s	Supply current	16	23	30	mA
V_i	Voltage at the IF amplifier input	1.2	1.9	2.4	V
V_2, V_3	Voltage at the input bypassing	1.2	1.9	2.4	V
V_6	Voltage at the audio output	5	5.6	6	V
V_{10}	Reference bias voltage	5	5.6	6	V

TCA 3089

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	
AC CHARACTERISTICS						
$V_{i(\text{threshold})}$	Input limiting voltage (-3 dB) at pin 1	$f_m = 1 \text{ kHz}$ $\Delta f = \pm 75 \text{ kHz}$		12	25	μV
V_o	Recovered audio voltage (pin 6)	$V_i \geq 100 \mu\text{V}$ $f_m = 1 \text{ kHz}$ $\Delta f = \pm 75 \text{ kHz}$	300	400	500	mV
V_7	Recovered audio voltage (pin 7)		200	350	500	mV
d	Distortion	$V_i \geq 1 \text{ mV}$ $f_m = 1 \text{ kHz}$ $\Delta f = \pm 75 \text{ kHz}$		0.5	1	%
$\frac{S+N}{N}$	Signal to noise ratio		60	67		dB
AMR	Amplitude modulation rejection	$V_i = 100 \text{ mV}$ $f_m = 1 \text{ kHz}$ $\Delta f = \pm 75 \text{ kHz}$ $m = 0.3$	45	55		dB
V_i	Input voltage for delayed AGC action (pin 1)			10		mV
V_{15}	AGC output	$V_i = 100 \text{ mV}$			0.5	V
$\frac{\Delta I_7}{\delta f}$	AFC control slope (note 1)	$V_i = 10 \text{ mV}$		1.2		$\frac{\mu\text{A}}{\text{kHz}}$
V_{13}	Field strength meter output sensitivity	$V_i = 0.5 \text{ mV}$		1.5		V
	No signal mute (note 2)	muting: ON	55			dB

Note: 1) $\Delta I_7 = \frac{\Delta V_{7,10}}{R_{7,10}}$

2) No signal mute = $20 \log \frac{V_o @ V_i \geq 100 \mu\text{V}}{V_o @ V_i = 0}$

Fig. 1 - Relative recovered audio and noise output vs. input voltage

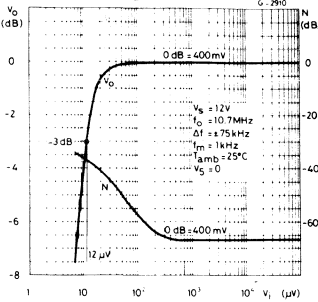


Fig. 2 - Capture ratio vs. input voltage

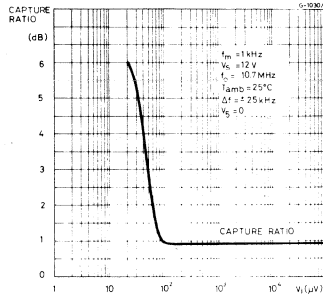


Fig. 3 - AGC (V_{15}) and field strength meter output (V_{13}) vs. input voltage

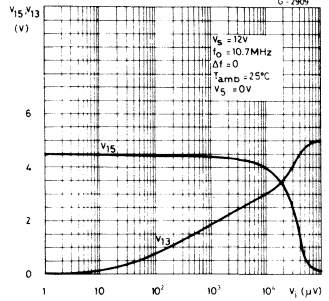


Fig. 4 - AFC output current vs. change in tuning frequency

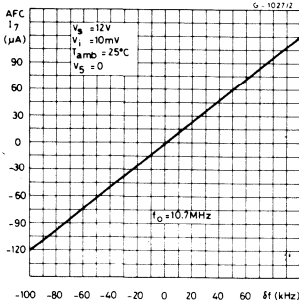


Fig. 5 - Amplitude modulation rejection vs. input voltage

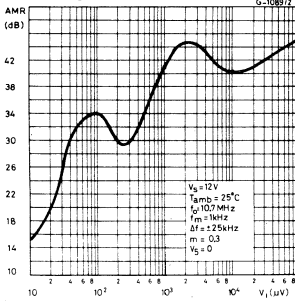
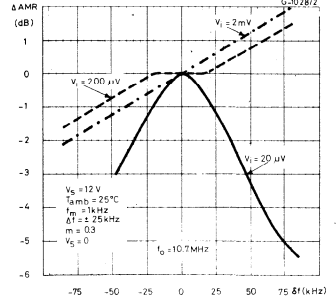
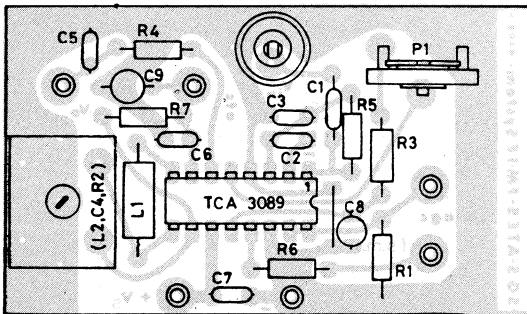


Fig. 6 - AMR vs. change in tuning frequency



APPLICATION INFORMATION

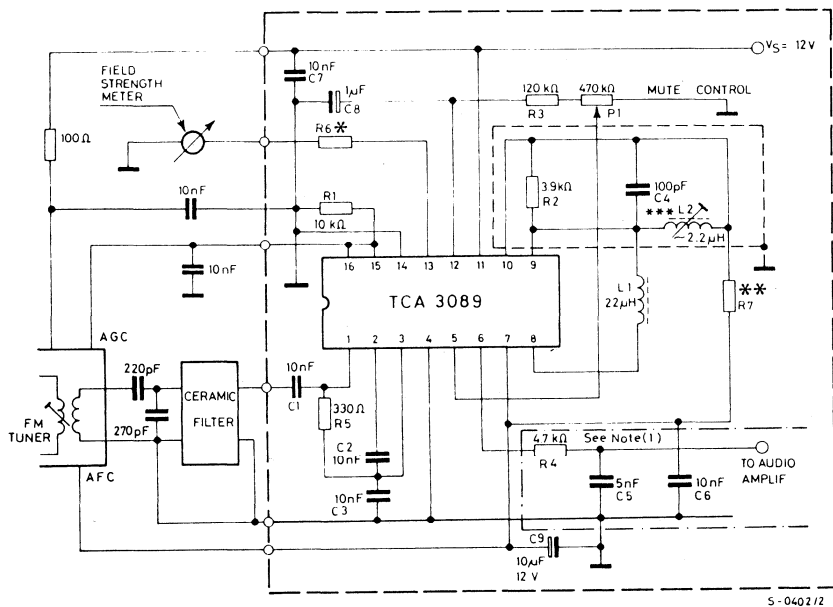
Fig. 7 - P.C. board and component layout of the circuit of fig. 8 (1:1 scale)



CS-0087

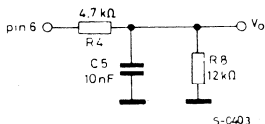
TCA 3089

Fig. 8 - Typical application circuit



5-0402/2

Notes (1): When V_s is less than 12V, a resistor $R_8 = 12\text{ k}\Omega$ must be connected between audio output and ground, and the integrator capacitor C_5 must be changed to 10 nF, as follows:



5-C403

- * Dependent on field strength meter sensitivity.
- ** Dependent on the tuner's AFC circuit.
- *** L2 tunes with 100 pF at 10.7 MHz ($Q_o = 75$)

LINEAR INTEGRATED CIRCUIT

FM-IF HIGH QUALITY RADIO SYSTEM

- EXCEPTIONAL LIMITING SENSITIVITY
- VERY LOW DISTORTION (0.1% - DOUBLE TUNED DETECTOR COIL)
- IMPROVED S/N RATIO
- EXTERNALLY PROGRAMMABLE AUDIO LEVEL
- ON CHANNEL STEP FOR SEARCH CONTROL
- PROGRAMMABLE AGC VOLTAGE AND AFC FOR TUNER
- INTERCHANNEL MUTING (SQUELCH)
- DEVIATION MUTING
- DIRECT DRIVE OF TUNING METER
- DIRECT DRIVE OF FIELD STRENGTH METER

The TCA 3189 is a monolithic integrated circuit in a 16-lead dual in-line plastic package, which provides a **complete subsystem** for amplification of 10.7 MHz FM signal in Hi-Fi, car-radios and communications receivers.

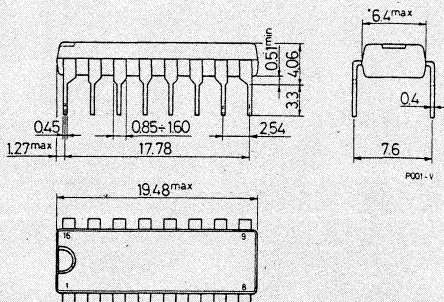
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	16	V
I_o	Output current (from pin 15)	2	mA
P_{tot}	Total power dissipation at $T_{amb} \leq 70^\circ\text{C}$	800	mW
T_{stg}	Storage temperature	-55 to 150	$^\circ\text{C}$
T_{op}	Operating temperature	-25 to 85	$^\circ\text{C}$

ORDERING NUMBER: TCA 3189

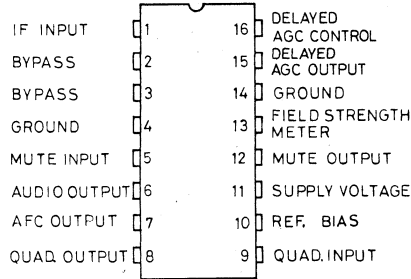
MECHANICAL DATA

Dimensions in mm



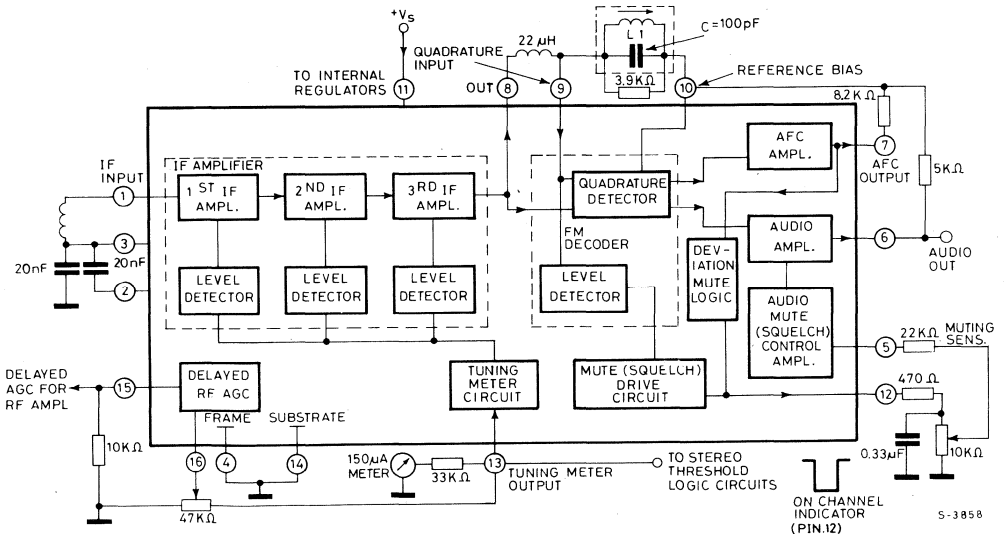
TCA 3189

CONNECTION DIAGRAM (top view)



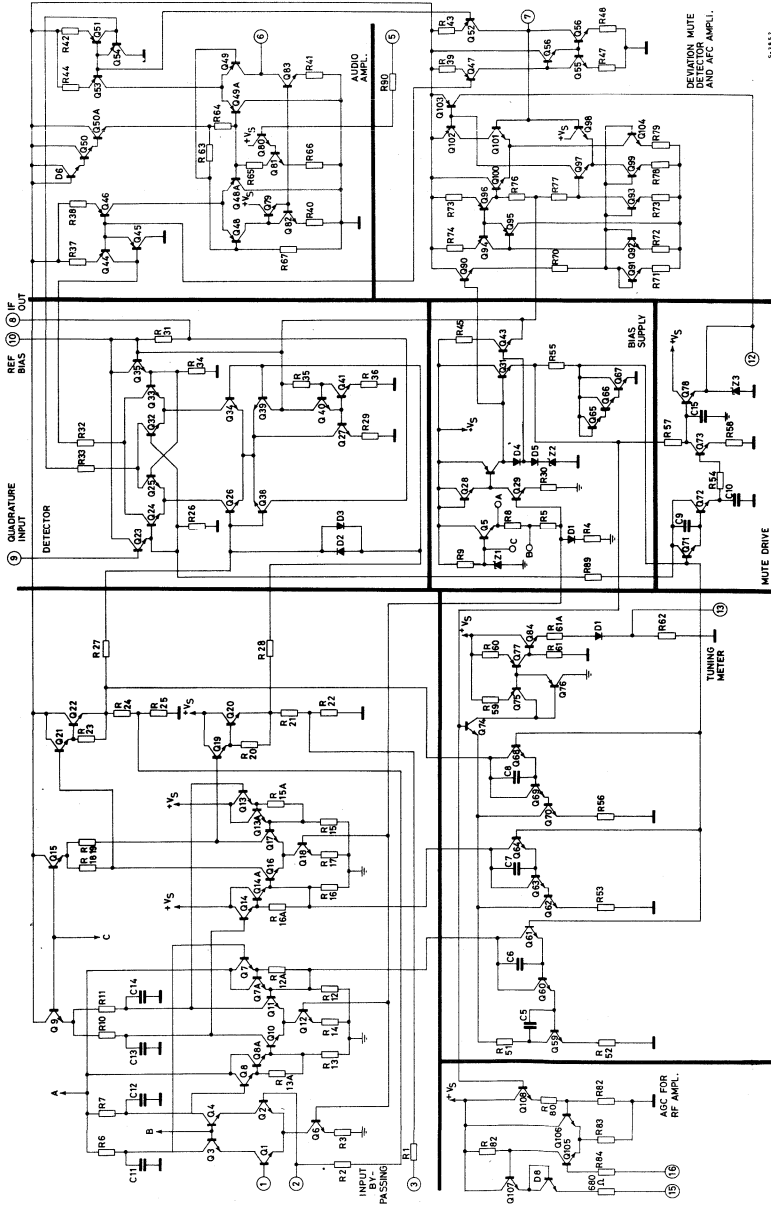
S-3286

BLOCK DIAGRAM



5-3858

SCHEMATIC DIAGRAM



5-1812

TCA 3189

THERMAL DATA

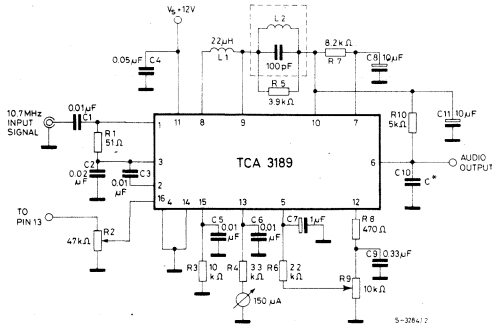
$R_{th\ j-amb}$ Thermal resistance junction-ambient	max. 100 °C/W
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ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $V_s = 12V$, $T_{amb} = 25^\circ C$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s Supply voltage range	No signal input, non muted	9		16	V
I_s Supply current		20	31	44	mA
V_1 Voltage at the IF amplifier input		1.2	1.9	2.4	V
V_2, V_3 Voltage at the input bypass		1.2	1.9	2.4	V
V_{15} Voltage at the pin 15 (RF AGC)		7.5	9.5	11	V
V_{10} Reference bias voltage		5	5.6	6	V
V_i Input limiting voltage (-3 dB) at pin 1	$f_o = 10.7\text{ MHz}$ $f_m = 1\text{ KHz}$ $\Delta f = \pm 75\text{ KHz}$		12	25	μV
V_o Recovered audio voltage (pin 6)	$V_i \geq 50\ \mu V$ $f_o = 10.7\text{ MHz}$ $f_m = 1\text{ KHz}$ $\Delta f = \pm 75\text{ KHz}$	325	500	650	mV
d Distortion (single tuned)	$V_i \geq 1\text{ mV}$ $f_o = 10.7\text{ MHz}$ $f_m = 1\text{ KHz}$ $\Delta f = \pm 75\text{ KHz}$		0.5	1	%
d Distortion (double tuned)			0.1		%
$\frac{S+N}{N}$ Signal to noise ratio		65	72		dB
AMR Amplitude modulation rejection	$V_i = 100\text{ mV}$ $f_o = 10.7\text{ MHz}$ $f_m = 1\text{ KHz}$ $\Delta f = \pm 75\text{ KHz}$ AM mod. 30%	45	55		dB
V_{16} RF AGC threshold			1.25		V
$\frac{\Delta I_7}{\Delta f}$ AFC control slope			1.9		$\frac{\mu A}{KHz}$
V_{12} On channel step (deviation mute)	$V_i = 100\text{ mV}$ $f_o = 10.7\text{ MHz}$	$f_{DEV.} < \pm 40\text{ KHz}$		0	V
		$f_{DEV.} > \pm 40\text{ KHz}$		5.6	V

TEST CIRCUITS

Single tuned detector coil



Double tuned detector coil

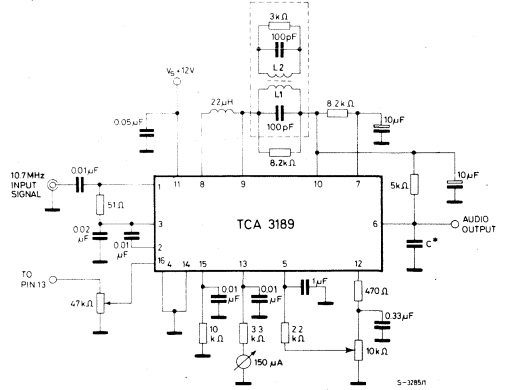
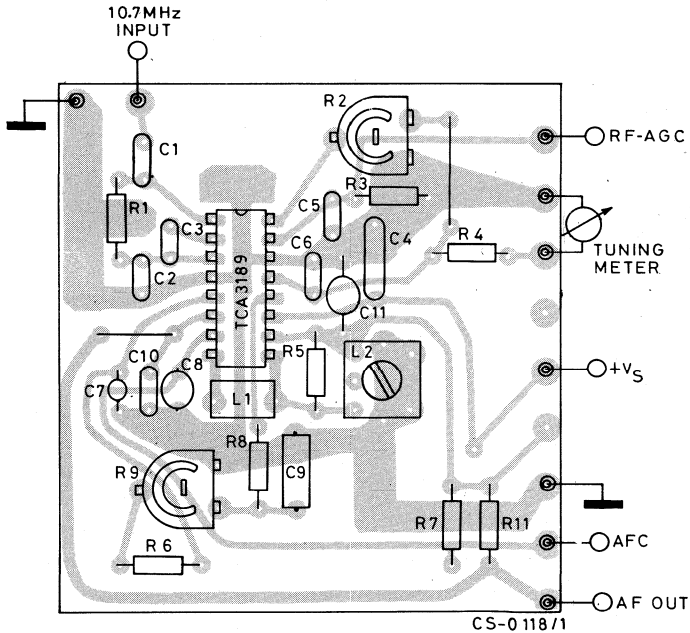


Fig. 1 - P.C. board and component layout of the single tuned circuit (1:1 scale)



TCA 3189

Fig. 2 - Limiting and noise characteristics

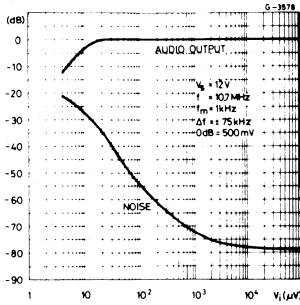


Fig. 3 - Deviation mute threshold vs. $R7-10$

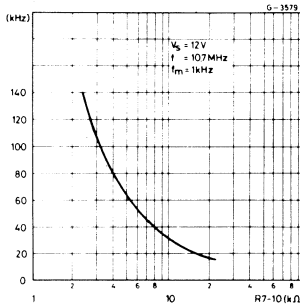


Fig. 4 - Recovered audio level and muting action vs. input level

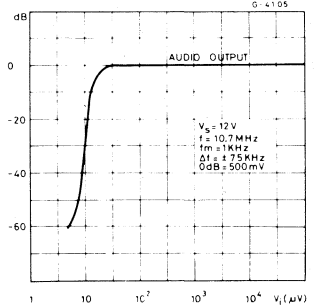


Fig. 5 - AFC characteristics

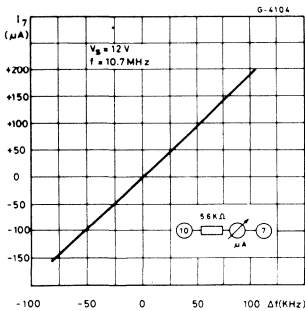


Fig. 6 - AGC voltage for FM tuner vs. input level

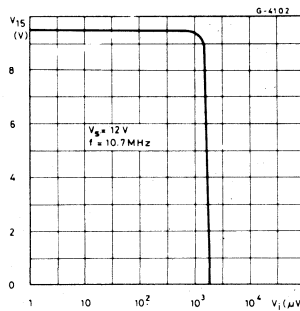
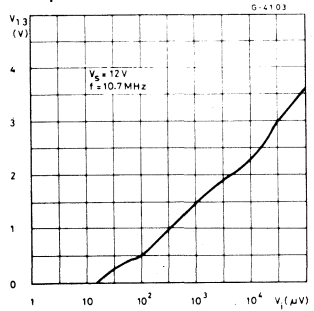


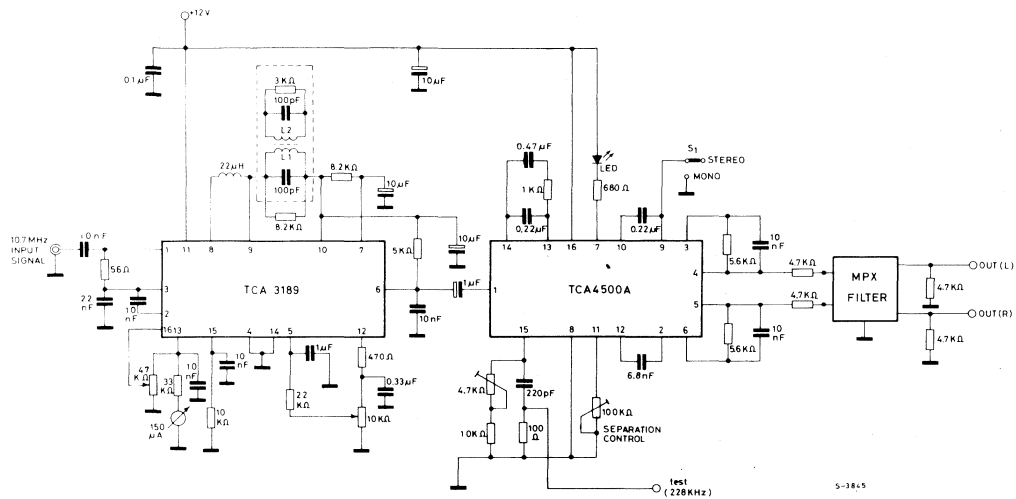
Fig. 7 - Field strength and tuning meter output vs. input level



FEATURES	TCA 3189	TCA 3089	TDA 1200
Low Limiting Sensitivity (25 μV max.)	Yes	Yes	No
Low Distortion (< 1%)	Yes	Yes	No
Single-coil Tuning Capability	Yes	Yes	Yes
Programmable Audio Level	Yes	No	No
S/N Mute	Yes	Yes	Yes
Deviation Mute	Yes	No	No
AFC and delayed AGC	Yes	Yes	Yes
Programmable AGC Threshold and Voltage	Yes	No	No
Typical S + N/N > 70 dB	Yes	No	No
Typical S + N/N > 60 dB	Yes	Yes	No
Meter Drive Voltage Depressed at Very-Low Signal Levels	Yes	No	No
On-Channel Step Control Voltage	Yes	No	No

TCA 3189

Fig. 9 - Hi-Fi FM-tuner and stereo decoder



LINEAR INTEGRATED CIRCUIT

TV VISION IF SYSTEM

The TDA 440S is a monolithic integrated circuit in a 16-lead dual in-line plastic package. The functions incorporated are:

- Gain controlled vision IF amplifier
- Synchronous detector
- AGC detector with gating facility
- AGC amplifier for PNP tuner drive with variable delay
- Video preamplifier with positive and negative outputs.

It is intended for use in black and white and colour TV receivers.

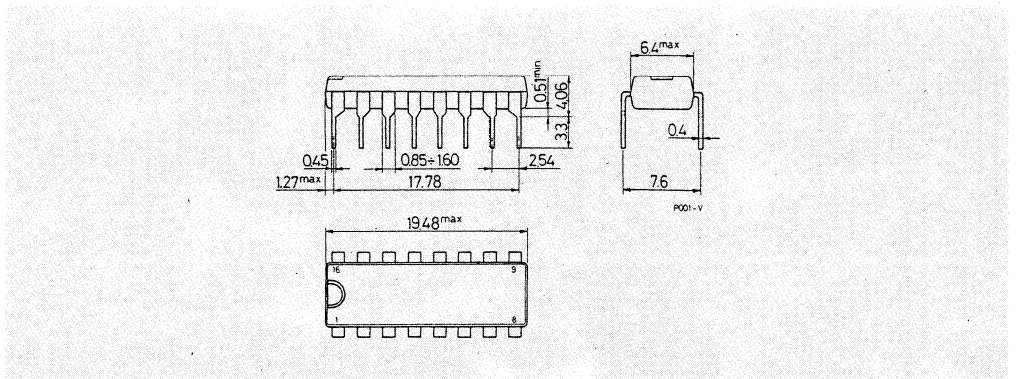
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage (pin 13)	15	V
V_5	Voltage at pin 5	15	V
V_{10}	Voltage at pin 10	-1	V
V_{11}	Voltage at pin 11 (with load connected to V_s)		3
I_{11}, I_{12}	Output current	8	V
P_{tot}	Total power dissipation at $T_{amb} \leq 70^\circ\text{C}$	5	mA
T_{stg}	Storage temperature	800	mW
T_{op}	Operating temperature	-55 to 150	$^\circ\text{C}$
		0 to 70	$^\circ\text{C}$

ORDERING NUMBER: TDA 440S

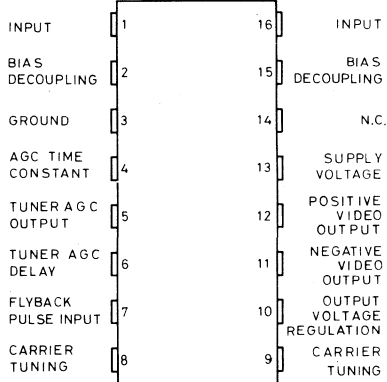
MECHANICAL DATA

Dimensions in mm



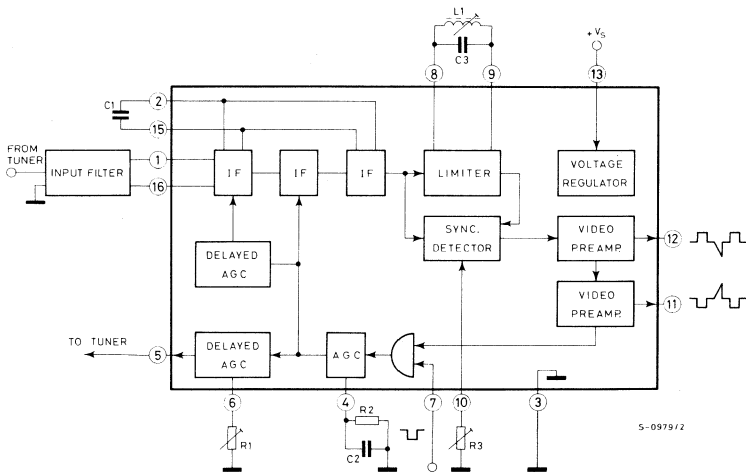
TDA 440S

CONNECTION DIAGRAM (top view)



5-0978/1

BLOCK DIAGRAM



5-0979/2

THERMAL DATA

$R_{thj-amb}$	Thermal resistance junction-ambient	max	100	°C/W
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ELECTRICAL CHARACTERISTICS (Refer to fig. 1 test circuit, $T_{amb} = 25^{\circ}\text{C}$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig.
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DC CHARACTERISTICS

V_s	Supply voltage range (pin 13)		10	12	15	V	
I_s	Supply current (pin 13)	$V_s = 12\text{V}$		50		mA	1a
$-I_{11}^{(1)}$	Output current	$V_s = 15\text{V}$ $V_{11} = 8\text{V}$		1.6		mA	1b
$V_{11}^{(2)}$	Output voltage	$V_s = 12\text{V}$ $R_5 = \infty$			4.5	V	1a
				7			
$V_{12}^{(2)}$	Output voltage	$V_s = 12\text{V}$ $V_{11} = 5.5\text{V}$		5.6		V	1a
$\frac{\Delta V_{11}}{\Delta V_s}$	Output voltage drift	$V_s = 11$ to 14V		3.5		%	1b

AC CHARACTERISTICS (Refer to fig. 2 test circuit, $V_s = 12\text{V}$, $T_{amb} = 25^{\circ}\text{C}$)

$I_5^{(3)}$	Tuner AGC current	$V_7 = 0$ $f_0 = 38.9\text{ MHz}$ $R_4 = 2.5\text{ K}\Omega$	6	9.5		mA	3c
V_7	AGC gating pulse input peak voltage	$f = 15.6\text{ kHz}$	-1.5		-5	V	-
$V_i^{(4)}$	Input sensitivity	$V_7 = 0$ $f_0 = 38.9\text{ MHz}$ $V_{11} = 3.3\text{V peak to peak}$	100	150	220	μV	3c
ΔV_i	AGC range	$V_7 = 0$ $f_0 = 38.9\text{ MHz}$ $V_{11} = 3.3\text{V peak to peak}$ $\Delta V_o = 1\text{ dB}$	50	60		dB	
V_o	Peak to peak output voltage at pin 11	$V_7 = 0$ $f_0 = 38.9\text{ MHz}$ $V_{11} = 5.5\text{V}$ $V_i = \text{see note (5)}$	3.3	3.5	3.7	V	

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ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig.
ΔV_o	Video output variation over the AGC range (0 to 5.5 MHz) $V_7 = 0$ $\Delta V_i = 50$ dB $V_{11} = 3.3$ V peak to peak $f_0 = 38.9$ MHz $f_m = 0$ to 5.5 MHz		1	2	dB	3b
V_{11}, V_{12}	Sound IF at video outputs (5.5 MHz) $V_7 = 0$ $V_i =$ see note (5) f_0 (vision) = 38.9 MHz f_0 (sound) = 33.4 MHz	30			mV	3d
	Differential error of the output voltage (B & W) $V_7 = 0$ $f_0 = 38.9$ MHz $V_{11} = 3.3$ V peak to peak			15	%	—
V_{11}, V_{12}	Video carrier and video carrier 2 nd harmonic leakage at video outputs $V_7 = 0$ $V_i =$ see note (5) $f_0 = 38.9$ MHz		15		mV	3c
V_{11}, V_{12}			5		mV	
B		Frequency response (-3 dB)	8	10		MHz
d_{im}	Intermodulation products at video outputs $V_7 = 0$ $V_i =$ see note (5) f_0 (vision) = 38.9 MHz f_0 (sound) = 33.4 MHz f_0 (chroma) = 34.5 MHz		-50	-40	dB	3a
R_i	Input resistance (between pins 1 and 16) $V_7 = 0$ $V_i =$ see note (5)		1.4		k Ω	—
C_i	Input capacitance (between pins 1 and 16) $f_0 = 38.9$ MHz		2		pF	—

NOTES:

- (1) Current flowing out from pin 11 with the load connected to $V = 8$ V.
- (2) V_{11} and V_{12} are adjustable simultaneously by means of the resistance, or by a variable voltage ≤ 0.6 V, connected between pin 10 and ground.
- (3) Measured with an input voltage 10 dB higher than the V_i at which the tuner AGC current starts.
- (4) RMS values of the unmodulated video carrier (modulation down).
- (5) The input voltage V_i can have any value within the AGC range.

Fig. 1a - Test circuit for measurement of I_S , V_{11} , V_{12}

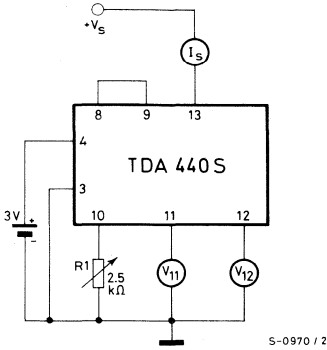


Fig. 1b - Test circuit for measurement of I_{11} and $\Delta V_{11}/\Delta V_S$

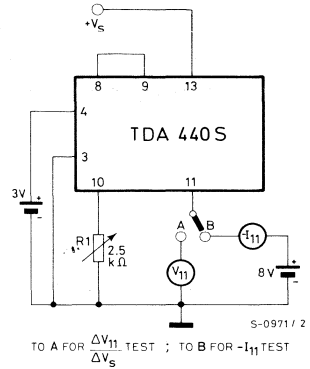
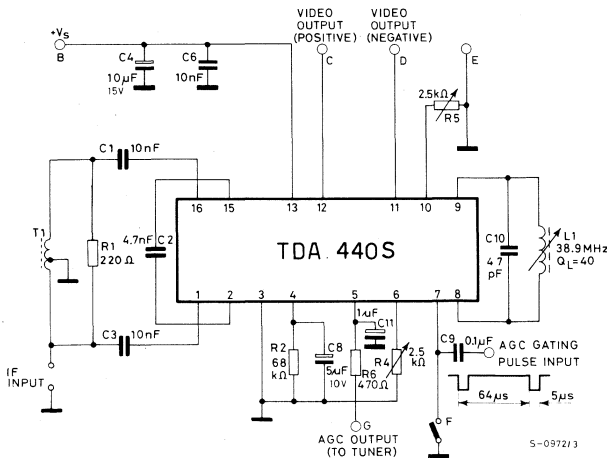


Fig. 2 - AC test circuit



Note: $T_1 = 50/200\Omega$ Balun transformer.
 V_i = Input voltage between pins 1 and 16.

TDA 440S

Fig. 3a - Set-up for measurement of d_{im}

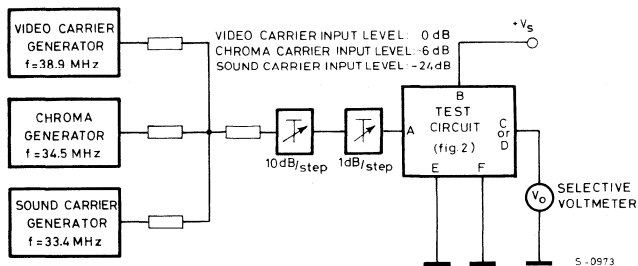


Fig. 3b - Set-up for measurement of ΔV_o

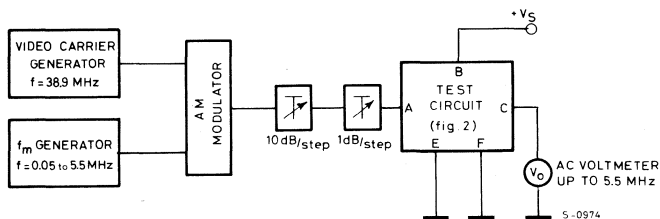


Fig. 3c - Set-up for measurement of I_s , V_i , ΔV_i , V_o , V_{11} and V_{12}

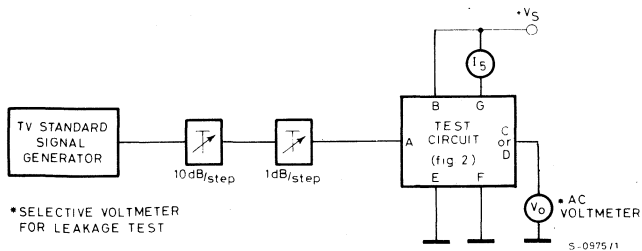


Fig. 3d - Set-up for measurement of B, V_{11} and V_{12}

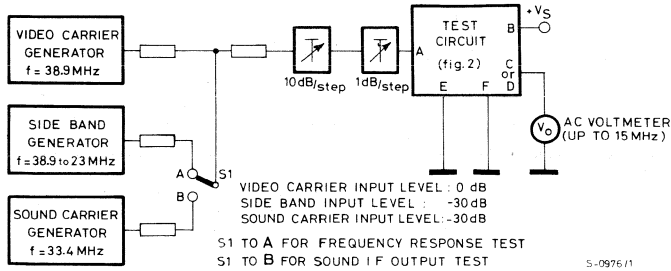


Fig. 4 - AGC voltage vs. input voltage variation

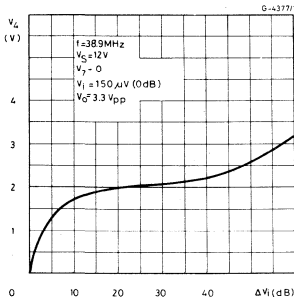


Fig. 5 - Tuner AGC output current vs. IF gain variation

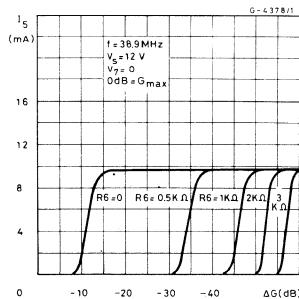
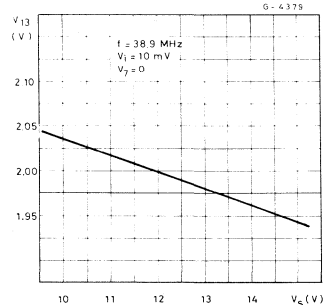


Fig. 6 - Output black level vs. supply voltage



APPLICATION INFORMATION

The TDA 440S enables very compact IF amplifiers to be designed and provides the performance demanded by high quality receivers.

The input tuning-trapping circuitry and the detector network can be aligned independently with respect to each other.

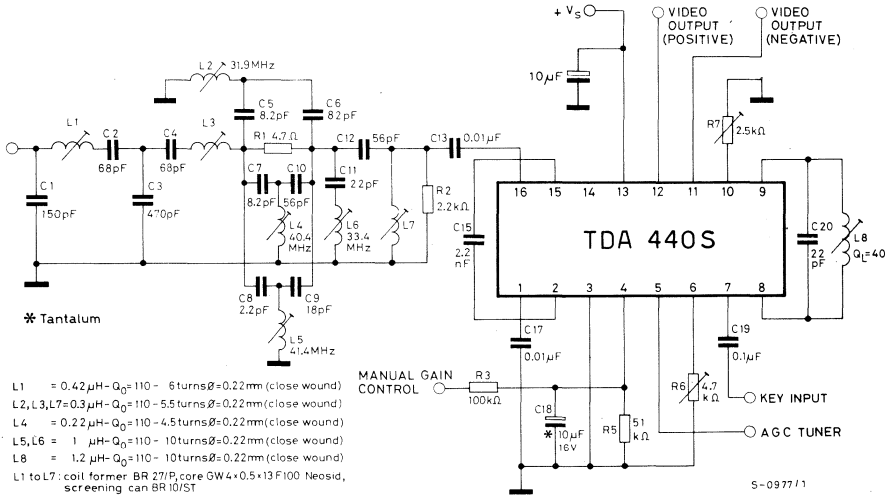
The value of Q for the parallel tuned circuit between pin 8 and 9 is not critical, although the higher it is, the better is the chroma-sound beat rejection, but the tuning is more critical. Values of Q from 30 to 50 give good rejection with non-critical tuning.

The LC circuit between pins 8 and 9 is tuned to the vision carrier thus appreciably attenuating the sidebands. Hence a small amount of signal can be removed whose amplitude is almost constant over the whole working range of the AGC and it can be used to drive an AFC circuit.

The black level at the output is very stable against variations of V_S and of temperature: this enables the contrast control to be kept simple. The AGC is of the gated type and can take the top of the synchronism or the black level (back porch) as its reference: when the latter is used, the output black level is particularly stable.

TDA 440S

Fig. 8 - Typical application circuit.



Typical performance of the Fig. 8 circuit

Frequency response (f_0 vision = 38.9 MHz, f_0 sound = 33.4 MHz) standard CCIR

Sound carrier attenuation	28	dB
31.9 MHz trap attenuation	≥ 60	dB
40.4 MHz trap attenuation	≥ 56	dB
41.4 MHz trap attenuation	≥ 44	dB
AGC range	55	dB
Overall gain including IF filter and trap circuits (note 1)	86	dB
Intermodulation products over the whole AGC range (note 2)	- 55	dB

- NOTES: (1) The gain is measured at video output 3.3V peak to peak and is defined as peak to peak output voltage to RMS input voltage (modulation down).
 (2) Measured at 1.07 MHz, vision carrier level = 0 dB, chroma carrier level = -6 dB, sound carrier level = -6 dB.

Fig. 9 - Overall frequency response of the fig. 8 circuit

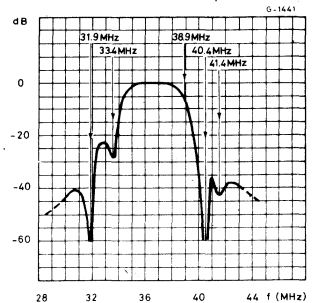
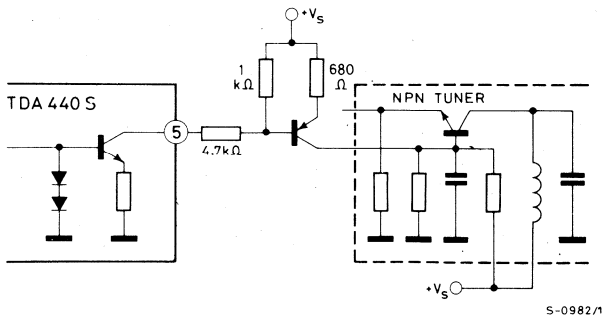
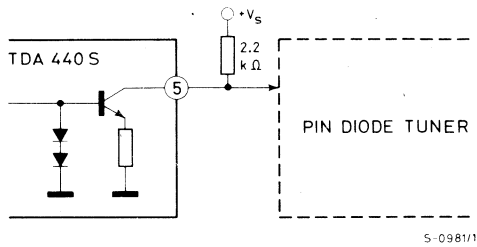
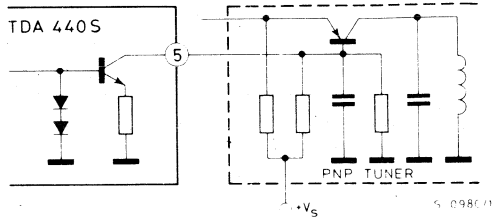


Fig. 10 - Circuit options for tuner AGC driving



TDA 1054M

LINEAR INTEGRATED CIRCUIT

PREAMPLIFIER WITH ALC FOR CASSETTE RECORDERS

- EXCELLENT VERSATILITY in USE (V_s from 4 to 20V)
- HIGH OPEN LOOP GAIN
- LOW DISTORTION
- LOW NOISE
- LARGE AUTOMATIC LEVEL CONTROL RANGE
- GOOD SUPPLY RIPPLE REJECTION
- STEREO MATCHING BETTER THAN 3 dB

The TDA 1054M is a monolithic integrated circuit in a 16-lead dual in-line plastic package. The functions incorporated are:

- Low noise preamplifier
- Automatic level control system (ALC)
- High gain equalization amplifier
- Supply voltage rejection facility (SVRF).

It is intended as preamplifier in cassette tape recorders and players, dictaphones, compressor and expander in industrial equipments, Hi-Fi preamplifiers and in wire diffusion receivers; for stereo applications the ALC matching is better than 3 dB.

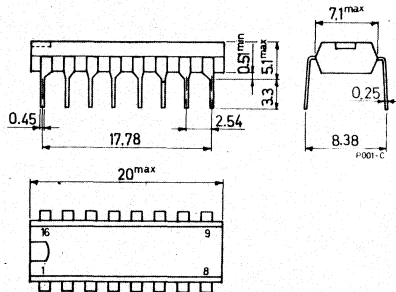
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	20	V
P_{tot}	Total power dissipation at $T_{amb} \leq 50^\circ\text{C}$	500	mW
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBERS: TDA 1054M mono applications
2 TDA 1054M stereo applications

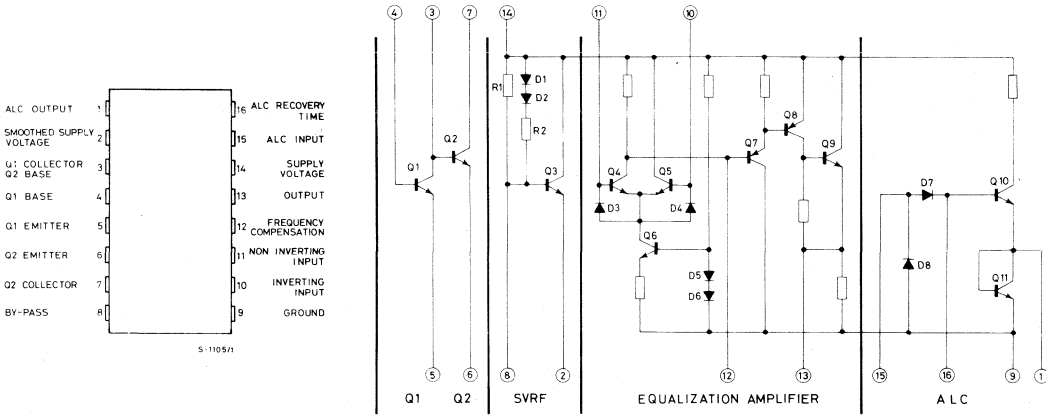
MECHANICAL DATA

Dimensions in mm

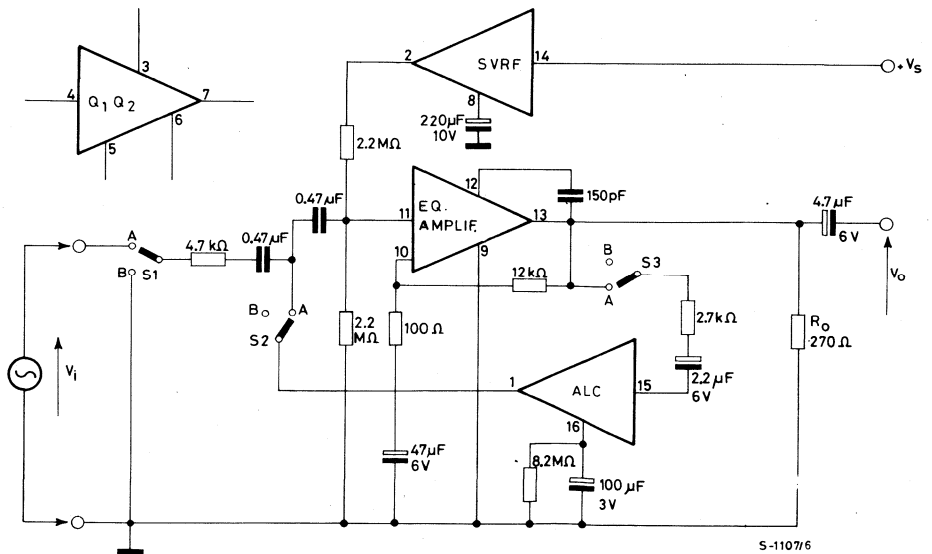


CONNECTION AND SCHEMATIC DIAGRAMS

(top view)



TEST CIRCUIT



TDA 1054M

THERMAL DATA

$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	200	$^{\circ}\text{C/W}$
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ELECTRICAL CHARACTERISTICS

(Refer to the test circuit, $T_{amb} = 25^{\circ}\text{C}$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	
V_s	Supply voltage	4		20	V	
I_d	Quiescent drain current	$V_s = 9\text{V}$ $S1 = S2 = S3 = B$	$R_L = \infty$ 6		mA	
h_{FE}	DC current gain	$I_C = 0.1\text{ mA}$	$V_{CE} = 5\text{V}$	300	500	—
e_N	Input noise voltage (Q1)	$I_C = 0.1\text{ mA}$ $f = 1\text{ kHz}$	$V_{CE} = 5\text{V}$	2	$\frac{nV}{\sqrt{Hz}}$	
i_N	Input noise current (Q1)			0.5	$\frac{pA}{\sqrt{Hz}}$	
NF	Noise figure (Q1)	$I_C = 0.1\text{ mA}$ $R_g = 4.7\text{ k}\Omega$ $B (-3\text{ dB}) = 20\text{ to }10,000\text{ Hz}$	$V_{CE} = 5\text{V}$	0.5	4	dB
G_V	Open loop voltage gain (for equalization amplifier)	$V_s = 9\text{V}$	$f = 1\text{ kHz}$	60		dB
V_o	Output voltage with A.L.C.	$V_s = 9\text{V}$ $f = 1\text{ kHz}$	$V_i = 100\text{mV}$ $S1 = S2 = S3 = A$	1.1		V
R1	(for SVRF system)	see schematic diagram		7.5		k Ω
R2	(for SVRF system)			120		Ω
e_N	Input noise voltage (for equalization amplifier pin 11)	$V_s = 9\text{V}$ $G_V = 40\text{ dB}$ $B (-3\text{ dB}) = 22\text{ Hz to }22\text{ KHz}$	$R_g = 4.7\text{ k}\Omega$ $S1 = B$	1.3		μV
V_{DR}	Drop-out (between pins 14 and 2)	$V_s = 9\text{V}$	$I_d = 6\text{ mA}$	0.8		V

Fig. 1 - Equivalent input spot voltage and noise current vs. bias current (input transistor Q_1)

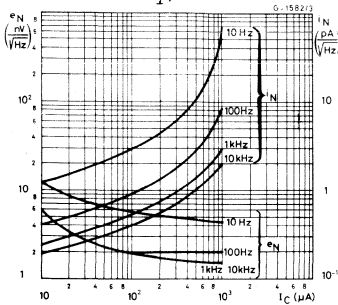


Fig. 2 - Equivalent input noise current vs. frequency (input transistor Q_1)

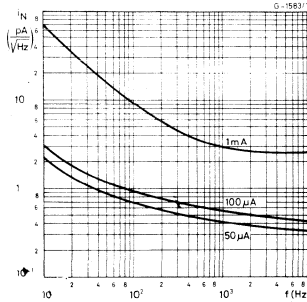


Fig. 3 - Equivalent input noise voltage vs. frequency (input transistor Q_1)

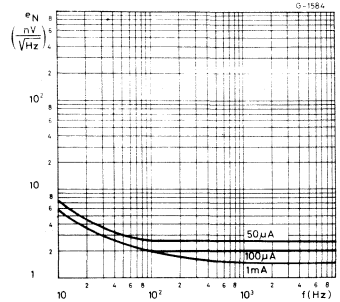


Fig. 4 - Noise figure vs. bias current (input transistor Q_1)

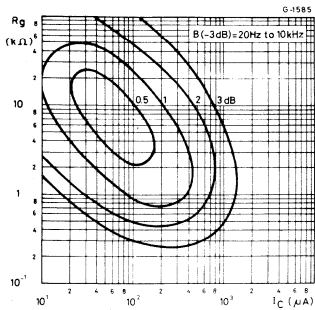


Fig. 5 - Optimum source resistance and minimum NF vs. bias current (input transistor Q_1)

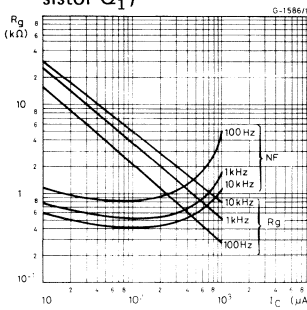


Fig. 6 - Current gain vs. collector current (input transistor Q_1)

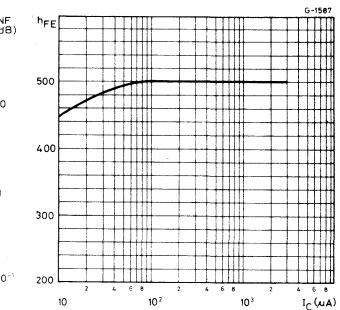


Fig. 7 - Open loop gain vs. frequency (equalization amplifier)

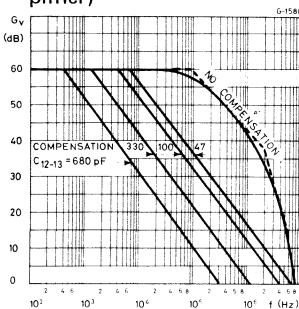
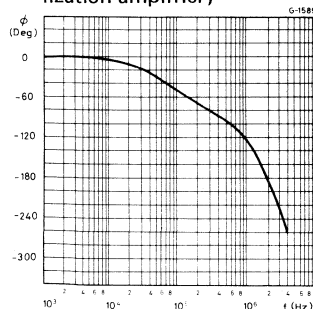


Fig. 8 - Open loop phase response vs. frequency (equalization amplifier)



TDA 1054M

APPLICATION INFORMATION

Fig. 9 - Application circuit for battery/mains cassette player and recorder

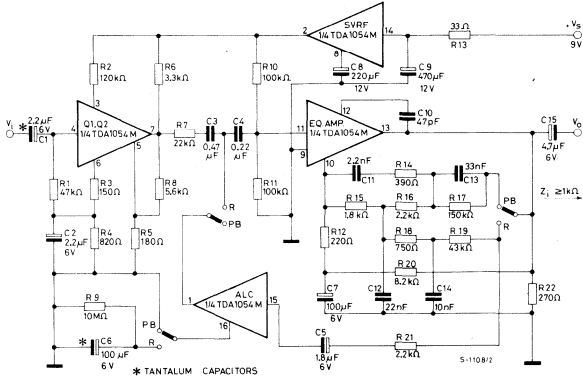
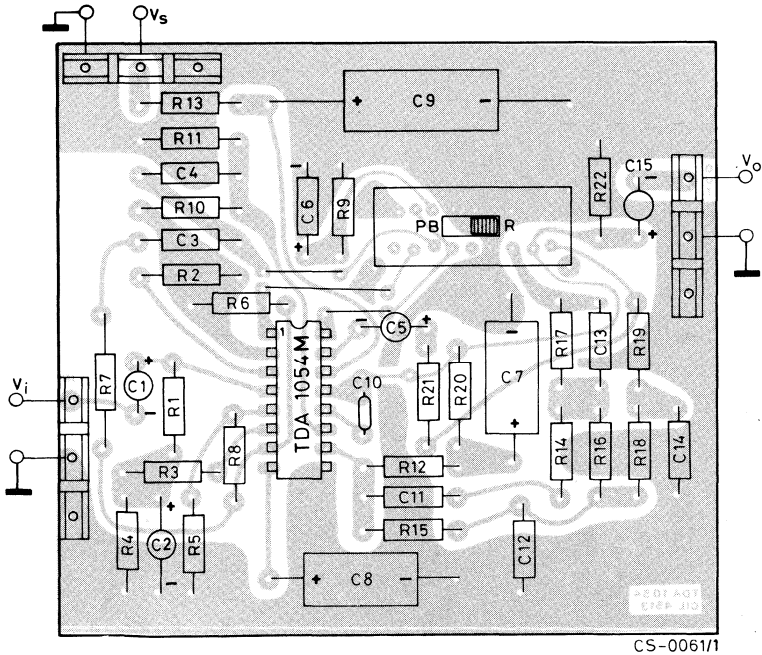


Fig. 10 - P.C. board and component layout for the circuit fig. 9 (1:1 scale)



Typical performance of circuit in fig. 9

($T_{amb} = 25^{\circ}\text{C}$, $V_s = 9\text{V}$)

Parameter		Test conditions	Min.	Typ.	Max.	Unit
PLAYBACK						
G_v	Voltage gain (open loop)	$f = 20$ to $20,000$ Hz		110		dB
G_v	Voltage gain (closed loop)	$f = 1$ kHz		57		dB
$ Z_i $	Input impedance	$f = 100$ Hz $f = 1$ kHz $f = 10$ kHz		10 41 43		k Ω k Ω k Ω
$ Z_o $	Output impedance	$f = 1$ kHz		12	35	Ω
B	Frequency response		see fig. 12			
d	Distortion	$V_o = 1\text{V}$ $f = 1$ kHz		0.1		%
	Output background noise	$Z_g = 300 \Omega + 120$ mH (DIN 45405)		1.3		mV
***	Output weighted background noise			1.3		mV
$\frac{S+N}{N}$	Signal to noise ratio	$V_o = 1.3\text{V}$ $Z_g = 300 \Omega + 120$ mH		60		dB
SVR	Supply voltage ripple rejection at the output	$f_{ripple} = 100$ Hz		30		dB
t_{on}^{**}	Switch-on time	$V_o = 1\text{V}$		500		ms
RECORDING						
G_v	Voltage gain (open loop)	$f = 20$ to $20,000$ Hz		110		dB
G_v	Voltage gain (closed loop)	$f = 1$ kHz		70		dB
B	Frequency response		see fig. 14			
d*	Distortion without ALC	$V_o = 1.1\text{V}$ $f = 1$ kHz		0.3		%
d	Distortion with ALC	$V_o = 1.1\text{V}$ $f = 10$ kHz		0.4		%
ALC	Automatic level control range (for 3 dB of output voltage variation)	$V_i \leq 40$ mV $f = 10$ kHz		54		dB
V_o	Output voltage before clipping without ALC	$f = 1$ kHz		2.3		V
V_o	Output voltage with ALC	$V_i = 30$ mV $f = 10$ kHz		1.1		V

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Typical performance of circuit in fig. 9 (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
t_l^{**}	Limiting time (see fig. 11)	$\Delta V_i = +40 \text{ dB}$ $f = 1 \text{ kHz}$	75		ms
t_{set}^{**}	Level setting time (see fig. 11)		300		ms
t_{rec}^{**}	Recovery time (see fig. 11)	$\Delta V_i = -40 \text{ dB}$ $f = 1 \text{ kHz}$	150		s
t_{on}^{**}	Switch-on time	$V_o = 1.1 \text{ V}$	500		ms
$\frac{S+N}{N}^{****}$	Signal to noise ratio with ALC	$V_o = 1.1 \text{ V}$ $R_g = 470 \Omega$	64		dB

* Measured with selective voltmeter

** This value depends on external network

*** When the DIN 45511 norm for frequency response is not mandatory the equalization peak at 10 kHz can be avoided – so halving the output noise

**** Weighted noise measurement (DIN 45405)

Fig. 11 - Limiting, level setting, recovery time

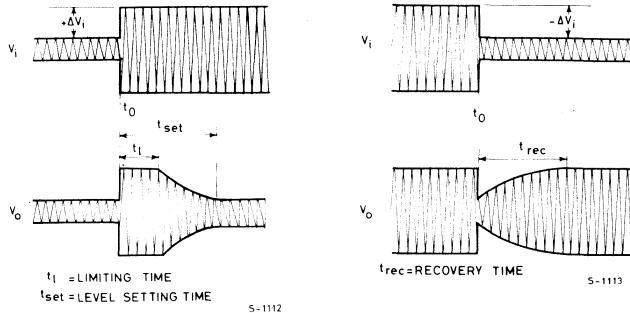


Fig. 12 - Relative frequency response for the circuit in fig. 9 (playback)

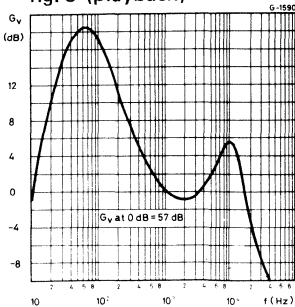


Fig. 13 - Distortion vs. frequency for the circuit in fig. 9 (playback)

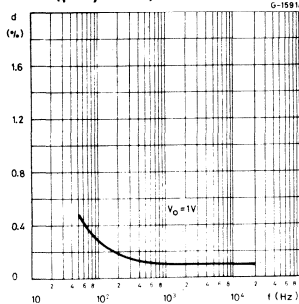


Fig. 14 - Relative frequency response for the circuit in fig. 9 (recording)

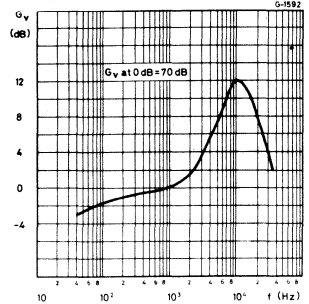


Fig. 15 - Output voltage variation and distortion with ALC vs. input voltage for the circuit in fig. 9 (recording)

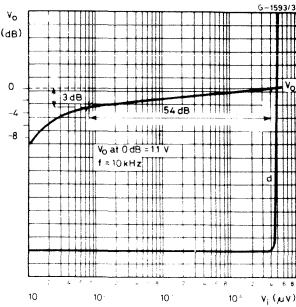


Fig. 16 - Distortion vs. frequency with ALC for the circuit in fig. 9 (recording)

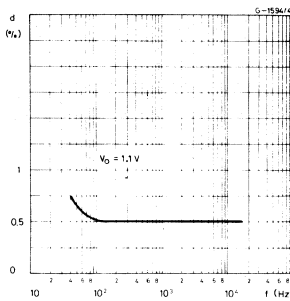


Fig. 17 - Limiting and level setting time vs. input signal variation

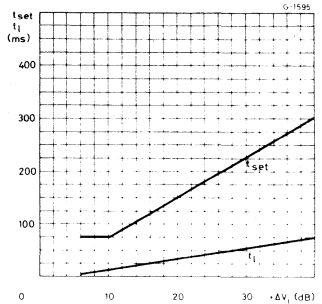
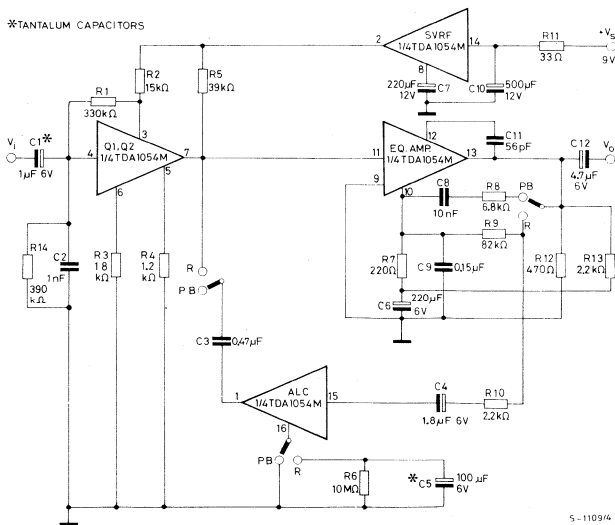
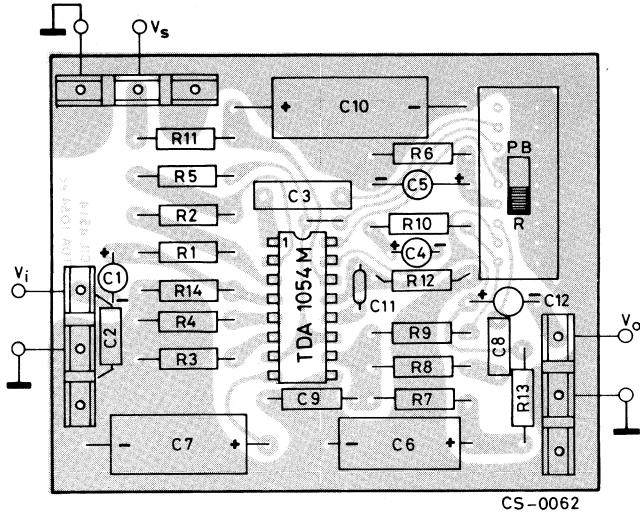


Fig. 18 - Low cost application circuit



TDA 1054M

Fig. 19 – P.C. board and component layout for the circuit in fig. 18 (1:1 scale)



Typical performance of circuit in fig. 18

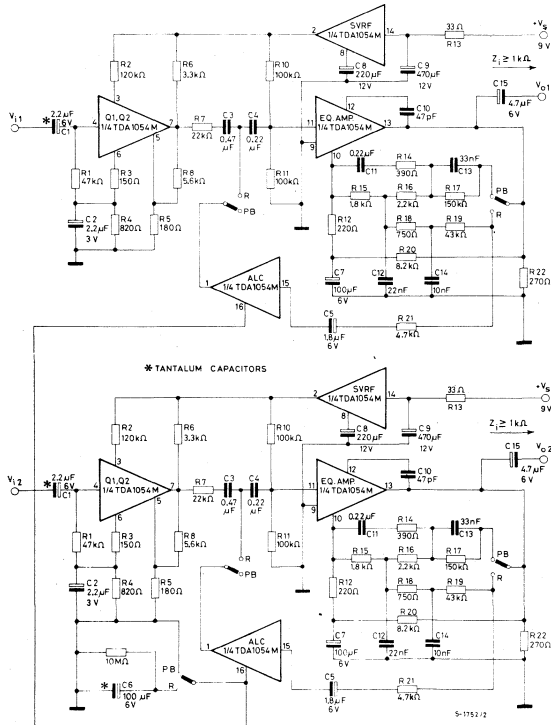
($T_{amb} = 25^{\circ}\text{C}$, $V_s = 9\text{V}$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
PLAYBACK					
V_s	Supply voltage	5		12	V
I_d	Quiescent drain current		18		mA
G_V	Voltage gain (closed loop)		54		dB
B	Frequency response	$f = 100\text{ Hz}$ $f = 1\text{ kHz}$ $f = 6\text{ kHz}$ $f = 10\text{ kHz}$ $f = 60\text{ kHz}$	12 0 5 11 10		dB dB dB dB dB
d	Distortion	$V_o = 1\text{ V}$	0.6		%
e_N	Output weighted background noise	$Z_g = 300\ \Omega + 120\text{ mH}$ (DIN 45405)	1.3		mV

Typical performance of circuit in fig. 18 (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
RECORDING					
G_v	Voltage gain (closed loop)	$f = 1 \text{ kHz}$		70	dB
B	Frequency response	$f = 140 \text{ Hz}$ $f = 1 \text{ kHz}$ $f = 10 \text{ kHz}$		-3 0 4	dB dB dB
d	Distortion	$V_o = 1.1\text{V}$ $f = 10 \text{ kHz}$		0.7	%
ALC	Range for 3 dB of output voltage variation	$V_i \leq 40 \text{ mV}$ $f = 10 \text{ kHz}$		54	dB

Fig. 20 - Typical stereo application circuit for battery/mains cassette player and recorder



TDA 1054M

Fig. 21 - Low cost stereo application circuit

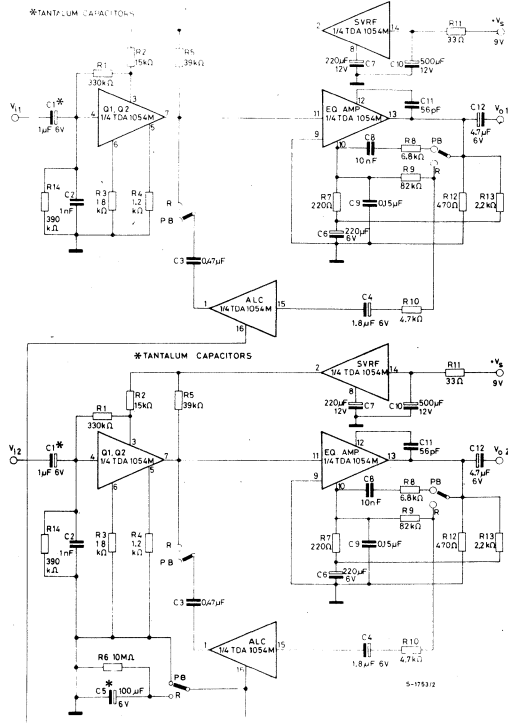


Fig. 22 - Complete cassette player and recorder

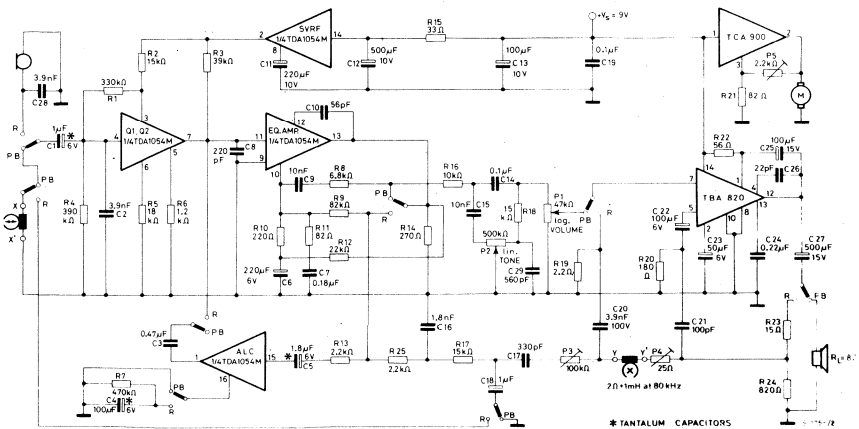


Fig. 23 - P.C. board and component layout for the circuit in fig. 22 (1:1 scale)

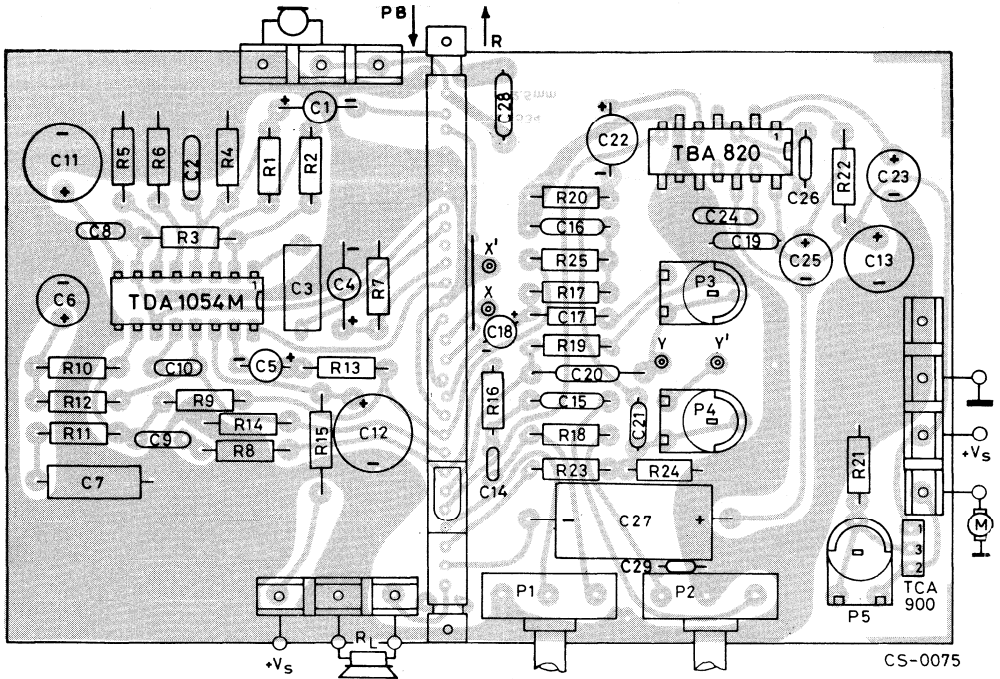
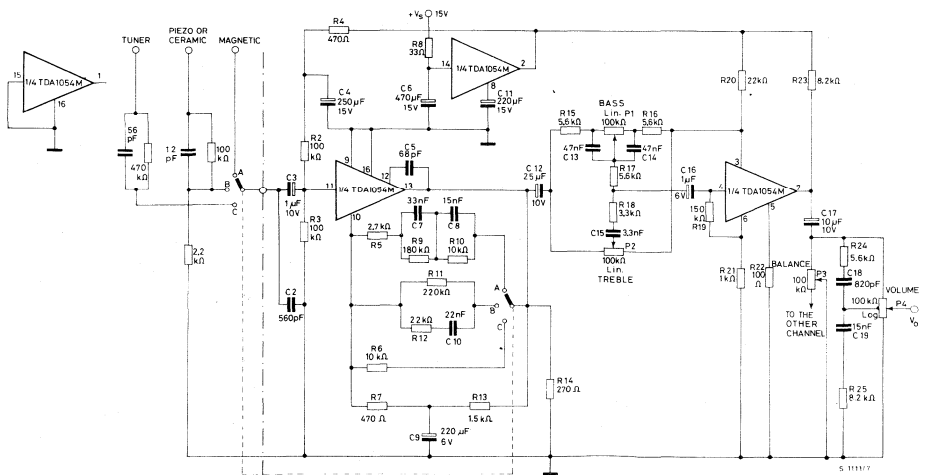
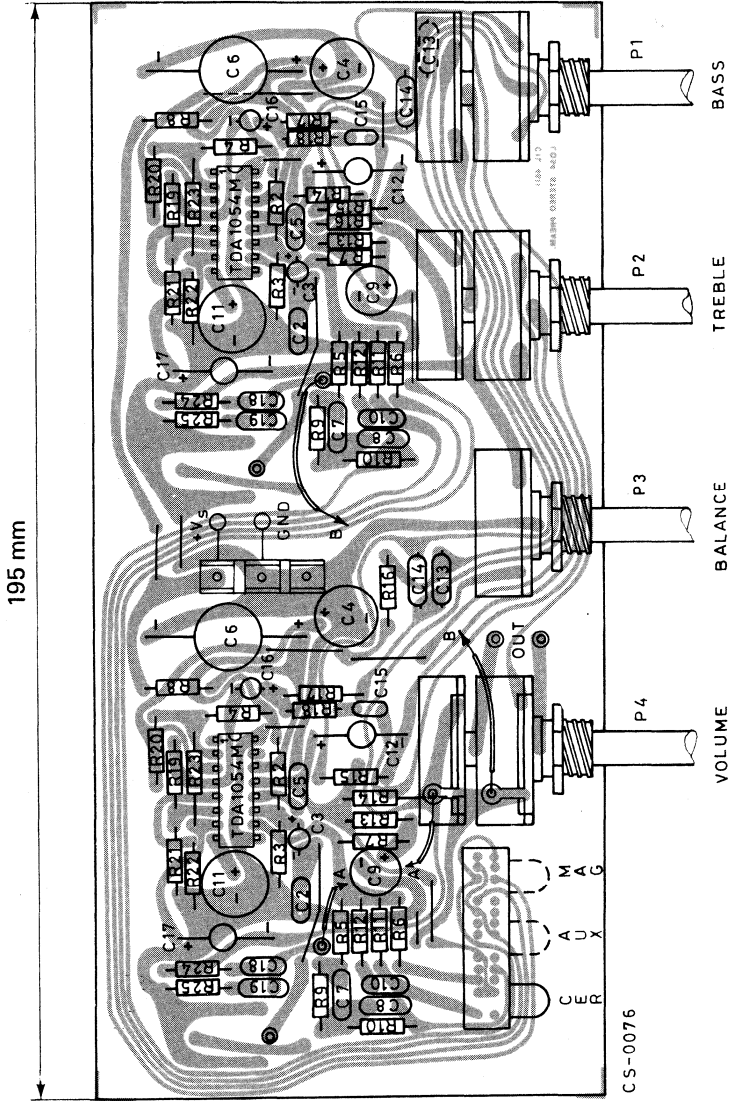


Fig. 24 - Hi-Fi preamplifier for magnetic and ceramic pick-ups



TDA 1054M

Fig. 25 - P.C. board and component layout for the circuit in fig. 24 (1:1 scale)



Typical performance of circuit in fig. 24

($T_{amb} = 25^{\circ}\text{C}$, $V_s = 15\text{V}$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s Supply voltage		12	15	18	V
V_i Input sensitivity for magnetic pick-ups	$V_o = 300\text{ mV}$ $f = 1\text{ kHz}$		2.5		mV
V_i Input sensitivity for ceramic pick-ups			100		mV
V_o Output voltage before clipping	$f = 1\text{ kHz}$		2.5		V
RIAA equalization for magnetic pick-ups	$B = 40\text{ to }18,000\text{ Hz}$		± 1		dB
$\frac{S+N}{N}$ Signal to noise ratio for magnetic pick-ups	$R_g = 4.7\text{ k}\Omega$ $B (-3\text{ dB}) = 20\text{ to }20,000\text{ Hz}$		66		dB
$ Z_i $ Input impedance for magnetic pick-ups	$f = 1\text{ kHz}$		47		$\text{k}\Omega$
$ Z_i $ Input impedance for ceramic pick-ups		100			$\text{k}\Omega$

Fig. 26 - Distortion vs. frequency for the circuit in fig. 24

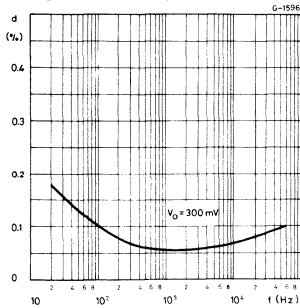
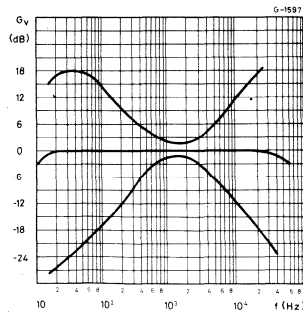
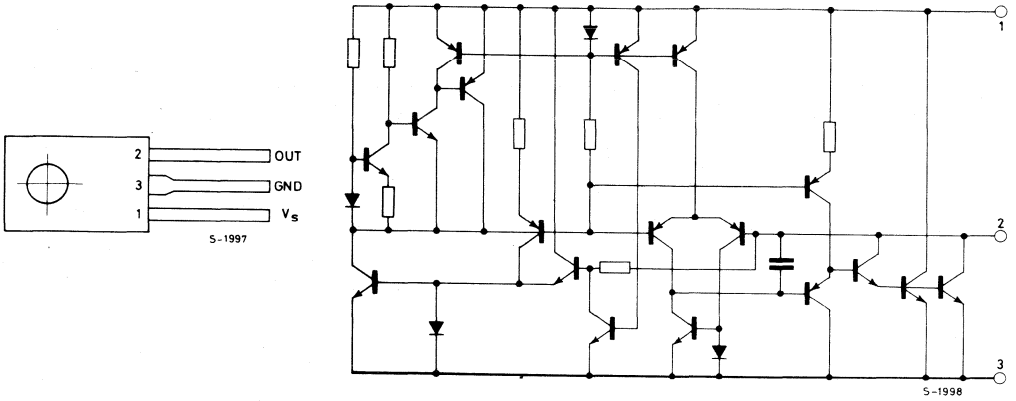


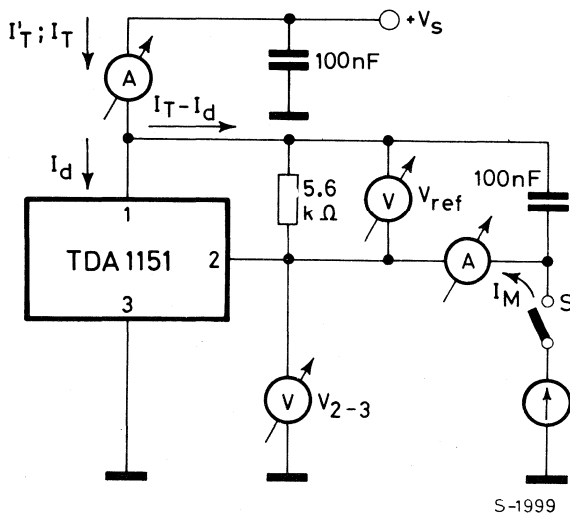
Fig. 27 - Frequency response for the circuit in fig. 24



CONNECTION AND SCHEMATIC DIAGRAMS



TEST CIRCUIT



TDA 1151

THERMAL DATA

$R_{th\ j-case}$	Thermal resistance junction-case	max	10	°C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	100	°C/W

ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $T_{amb} = 25^{\circ}C$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	
V_{ref}	Reference voltage (between pins 1 and 2)	$V_s = 6V$ $I_M = 0.1A$	1.1	1.2	1.3	V
I_d	Quiescent drain current	$V_s = 6V$ $I_M = 100\ \mu A$		1.7		mA
I_{MS}	Starting current	$V_s = 5V$ $\Delta V_{ref}/V_{ref} = -50\%$	0.8			A
V_{1-3}	Minimum supply voltage	$I_M = 0.1A$ $\Delta V_{ref}/V_{ref} = -5\%$			2.5	V
$K = I_M/I_T$	Reflection coefficient	$V_s = 6V$ $I_M = 0.1A$	18	20	22	—
$\frac{\Delta K}{K}/\Delta V_s$		$V_s = 6V$ to $18V$ $I_M = 0.1A$		0.45		%/V
$\frac{\Delta K}{K}/\Delta I_M$		$V_s = 6V$ $I_M = 25$ to $400\ mA$		0.005		%/mA
$\frac{\Delta K}{K}/\Delta T$		$V_s = 6V$ $I_M = 0.1A$ $T_{amb} = -20$ to $70^{\circ}C$		0.02		%/°C
$\frac{\Delta V_{ref}}{V_{ref}}/\Delta V_s$	Line regulation	$V_s = 6V$ to $18V$ $I_M = 0.1A$		0.02		%/V
$\frac{\Delta V_{ref}}{V_{ref}}/\Delta I_M$	Load regulation	$V_s = 6V$ $I_M = 25$ to $400\ mA$		0.009		%/mA
$\frac{\Delta V_{ref}}{V_{ref}}/\Delta T$	Temperature coefficient	$V_s = 6V$ $I_M = 0.1A$ $T_{amb} = -20$ to $70^{\circ}C$		0.02		%/°C

Fig. 1 - Quiescent drain current vs. power supply

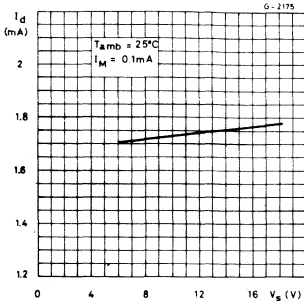


Fig. 2 - Quiescent drain current vs. ambient temperature

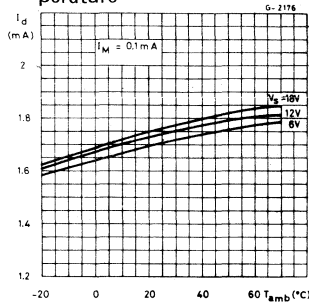


Fig. 3 - Reference voltage vs. supply voltage

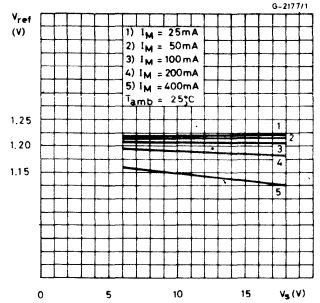


Fig. 4 - Reference voltage vs. motor current

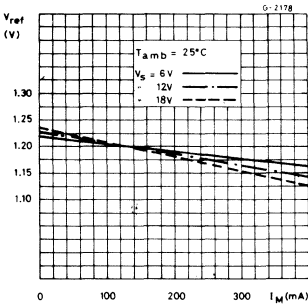


Fig. 5 - Reference voltage vs. ambient temperature

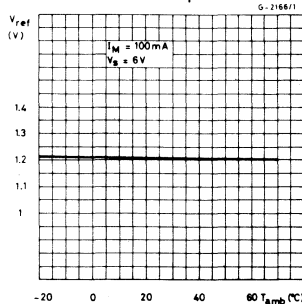


Fig. 6 - Reflection coefficient vs. supply voltage

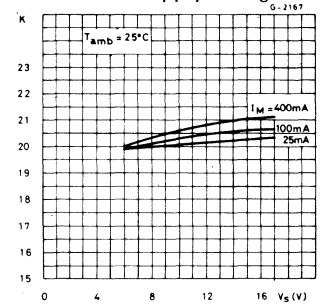


Fig. 7 - Reflection coefficient vs. motor current

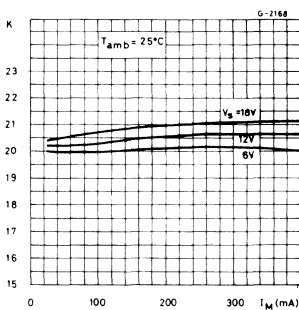


Fig. 8 - Reflection coefficient vs. ambient temperature

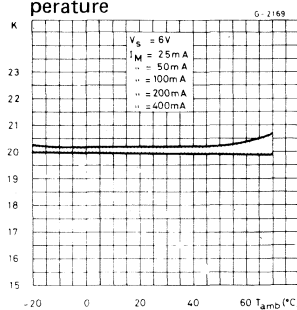
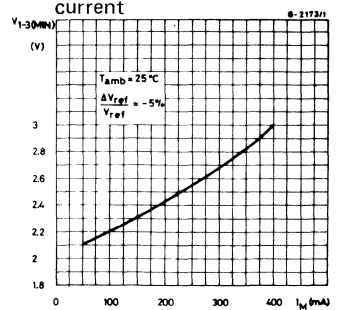
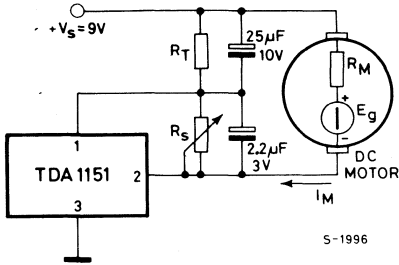


Fig. 9 - Typical minimum supply voltage vs. motor current



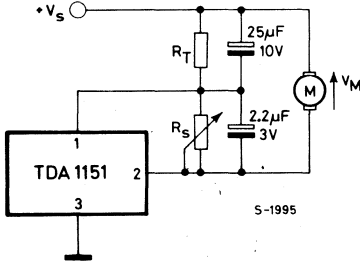
TDA 1151

APPLICATION INFORMATION



I_M = Motor current at rated speed
 R_M = Motor resistance
 E_g = Back electromotive force
 $R_{S \min} = \frac{V_{ref} \cdot R_T}{E_g - (V_{ref} - I_d \cdot R_T)}$
 $R_T = K \cdot R_M$
 $R_T = K_{typ} \cdot R_{M \text{ typ}}$
 If $R_{T \max} > K R_{M \min}$ instability may occur

Application circuit



$V_s = +9V$
 $R_M = 14.2\Omega$
 $R_T = 280\Omega$
 $R_S = 1 \text{ k}\Omega$
 $E_g = 2.9V$
 $I_M = 150 \text{ mA}$
 $V_M = R_M \cdot I_M + E_g = 5.03V$

Note: A ceramic capacitor of 10 nF between pins, 1 and 2 improves stability in some applications.

Fig. 10 – Speed variation vs. supply voltage

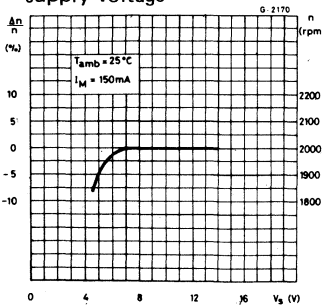


Fig. 11 – Speed variation vs. motor current

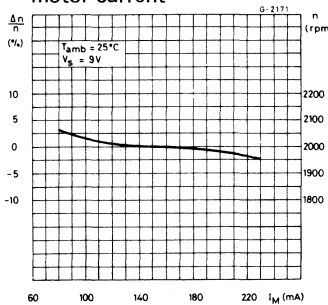
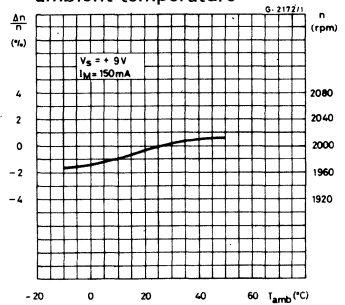
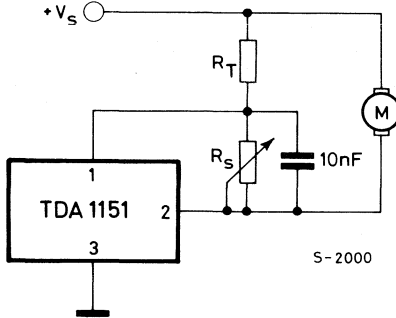


Fig. 12 – Speed variation vs. ambient temperature



APPLICATION INFORMATION (continued)

Low cost application circuit



$$\begin{aligned} V_S &= +12V \\ R_M &= 14.7\Omega \\ R_T &= 290\Omega \\ R_S &= 1\text{ k}\Omega \\ E_g &= 2.65V \\ I_M &= 110\text{ mA} \end{aligned}$$

Fig. 13 - Speed variation vs. supply voltage

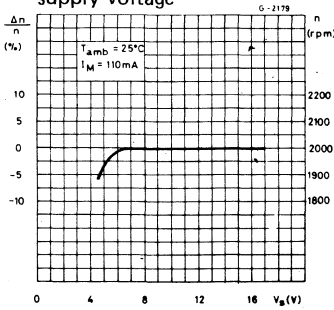


Fig. 14 - Speed variation vs. motor current

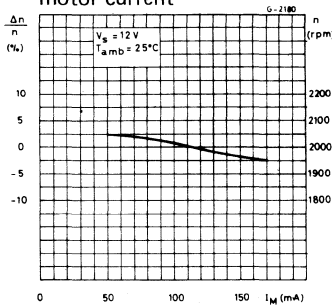
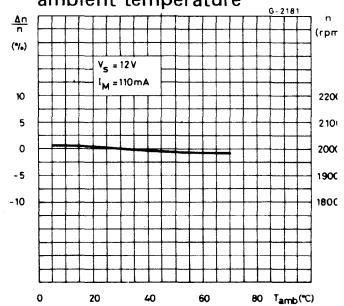


Fig. 15 - Speed variation vs. ambient temperature



TDA 1170

LINEAR INTEGRATED CIRCUIT

TV VERTICAL DEFLECTION SYSTEM

The TDA 1170 is a monolithic integrated circuit in a 12-lead quad in-line plastic package. It is designed mainly for use in large and small screen black and white TV receivers.

The functions incorporated are:

- oscillator
- voltage ramp generator
- high power gain amplifier
- flyback generator

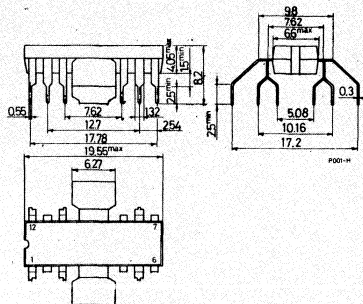
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage (pin 2)	27	V
V_4-V_5	Flyback peak voltage	58	V
V_8	Sync. input voltage	± 12	V
V_{10}	Power amplifier input voltage	$\left. \begin{array}{l} 10 \\ -0.5 \end{array} \right\}$	V
I_o	Output peak current (non-repetitive) @ $t = 2 \text{ ms}$	2	A
I_o	Output peak current @ $f = 50 \text{ Hz}, t \leq 10 \mu\text{s}$	2.5	A
I_o	Output peak current @ $f = 50 \text{ Hz}, t > 10 \mu\text{s}$	1.5	A
P_{tot}	Power dissipation: at $T_{tab} = 90^\circ\text{C}$	5	W
	at $T_{amb} = 80^\circ\text{C}$ (free air)	1	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBER: TDA 1170

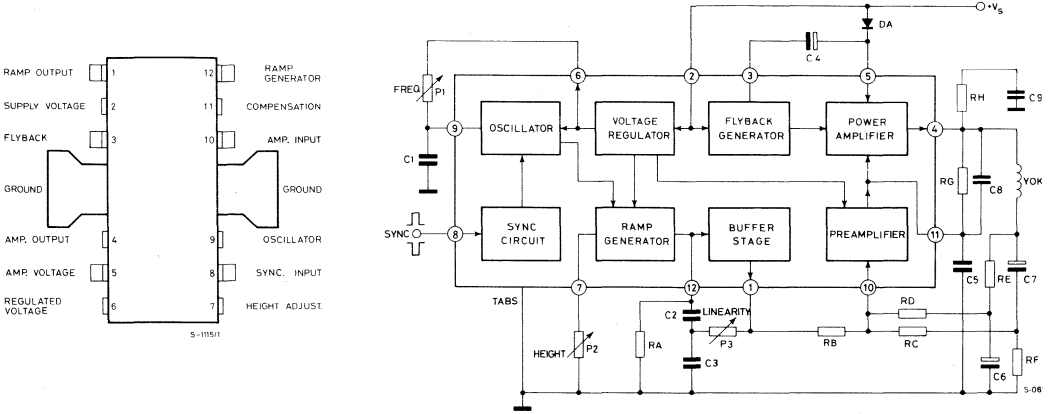
MECHANICAL DATA

Dimensions in mm

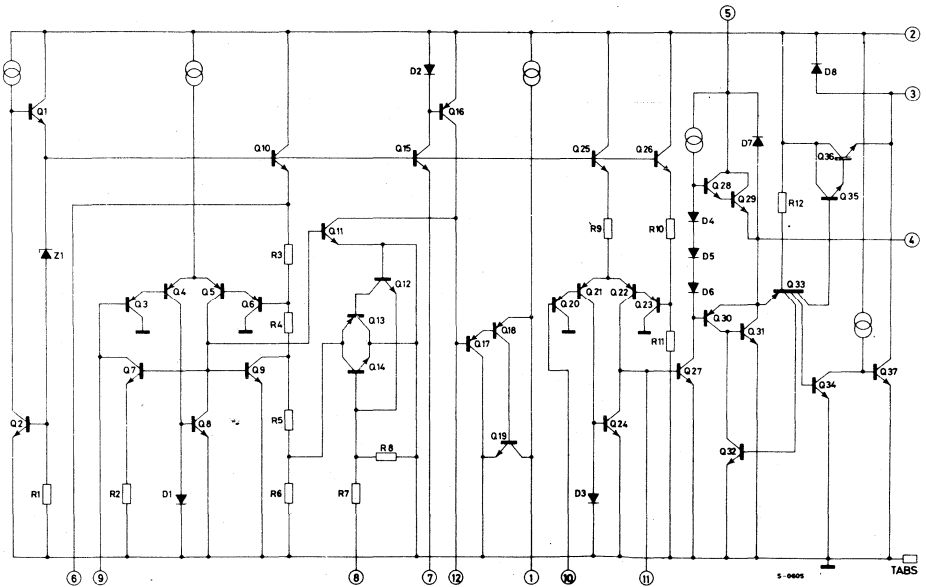


TDA 1170

CONNECTION AND BLOCK DIAGRAM (top view)



SCHEMATIC DIAGRAM



TDA 1170

THERMAL DATA

$R_{th\ j-tab}$	Thermal resistance junction-tab	max	12	°C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	70*	°C/W

* Obtained with tabs soldered to printed circuit with minimized area.

ELECTRICAL CHARACTERISTICS (Refer to the test circuits, $V_s = 25V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig.
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DC CHARACTERISTICS

$-I_9$	Oscillator bias current	$V_9 = 1V$		0.2	1	μA	1a
$-I_{10}$	Amplifier input bias current	$V_{10} = 1V$		0.15	1	μA	1b
$-I_{12}$	Ramp generator bias current			0.05	0.5	μA	1a
V_s	Supply voltage		10			V	—
V_4	Quiescent output voltage	$R_2 = 10\ k\Omega$ $V_s = 25V$ $R_1 = 30\ k\Omega$ $V_s = 10V$ $R_1 = 10\ k\Omega$	8 4	8.8 4.4	9.6 4.8	V V	1a
V_6, V_7	Regulated voltage		6	6.5	7	V	1b
$\frac{\Delta V_6}{\Delta V_s}, \frac{\Delta V_7}{\Delta V_s}$	Line regulation	$V_s = 10\ to\ 27V$		1.5		mV/V	

AC CHARACTERISTICS (f = 50 Hz)

I_s	Supply current	$I_Y = 1A$		140		mA	2
I_Y	Peak to peak yoke current (pin 4)				1.6	A	
V_4	Flyback voltage	$I_Y = 1A$		51		V	
V_8	Peak sync. input voltage (positive or negative)		1			V	

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig.
V_9 Peak to peak oscillator sawtooth voltage			2.4		V	2
R_8 Sync. input resistance	$V_8 = 1V$		3.5		$k\Omega$	
t_{fly} Flyback time	$I_Y = 1A$		0.6	0.8	ms	
δf Pull-in range (below 50 Hz)			7		Hz	
$\frac{\delta f}{\Delta V_s}$ Oscillator frequency drift with supply voltage	$V_s = 10$ to $27V$		0.01		$\frac{Hz}{V}$	
$\frac{\delta f}{\Delta T_{tab}}$ Oscillator frequency drift with tab temperature	$T_{tab} = 40$ to $120^\circ C$		0.015		$\frac{Hz}{^\circ C}$	

Fig. 1a - DC test circuit for measurement of $-I_9$, $-I_{12}$ and V_4

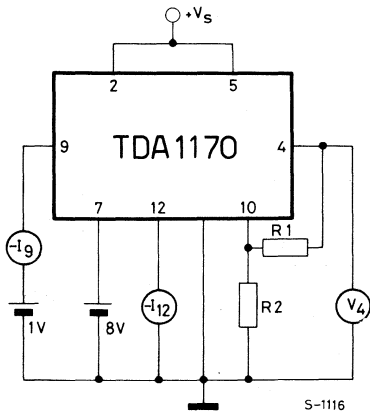
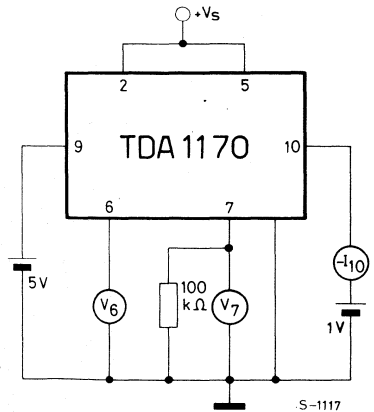


Fig. 1b - DC test circuit for measurement of $-I_{10}$, V_6 , V_7 , $\Delta V_6/\Delta V_s$ and $\Delta V_7/\Delta V_s$



TDA 1170

Fig. 2 - AC test circuit

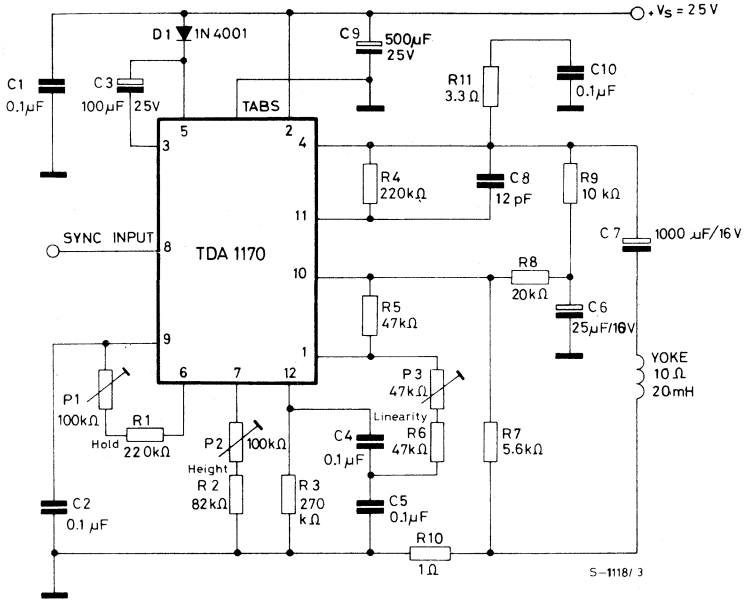


Fig. 3 - Relative quiescent voltage variation vs. supply voltage

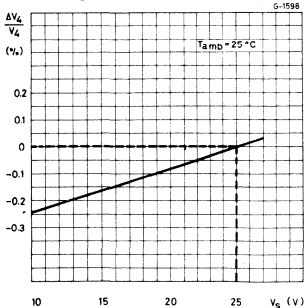


Fig. 4 - Relative quiescent voltage variation vs. tab temperature

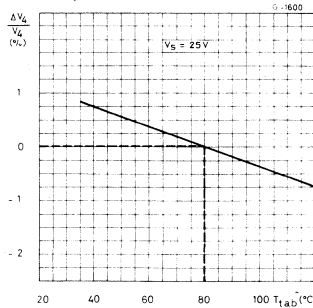


Fig. 5 - Regulated voltage vs. supply voltage

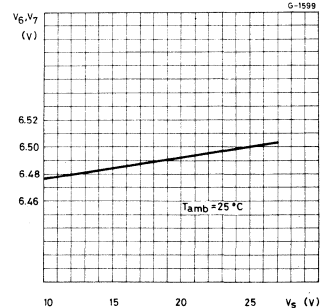


Fig. 6 - Regulated voltage vs. tab temperature

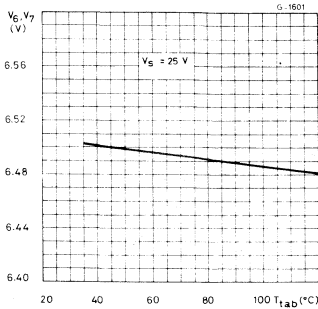


Fig. 7 - Frequency variation of unsynchronized oscillator vs. supply voltage

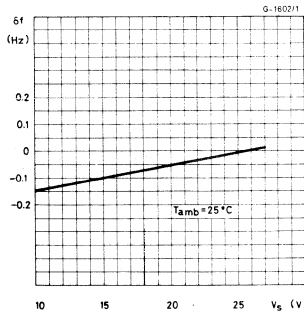
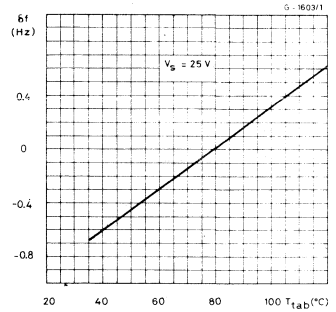


Fig. 8 - Frequency variation of unsynchronized oscillator vs. tab temperature



APPLICATION INFORMATION

The thermistor in series to the yoke is not required because the current feedback enables the yoke current to be independent of yoke resistance variations due to thermal effects. The oscillator is directly synchronized by the sync. pulses (positive or negative), therefore its free frequency must be lower than the sync. frequency. The flyback generator applies a voltage, about twice the supply voltage, to the yoke. This produces short flyback time together with a high useful power to dissipated power ratio.

The flyback time is:

$$t_{fly} \cong \frac{2}{3} \frac{L_Y I_Y}{V_s}$$

where: L_Y = Yoke inductance
 V_s = Supply voltage
 I_Y = Peak to peak yoke current

The supply current is:

$$I_s \cong \frac{I_Y}{8} + 0.02 \text{ (A)}$$

It does not depend on the value of V_s but only on yoke characteristics. The minimum value of V_s necessary for the required output current permits the maximum efficiency.

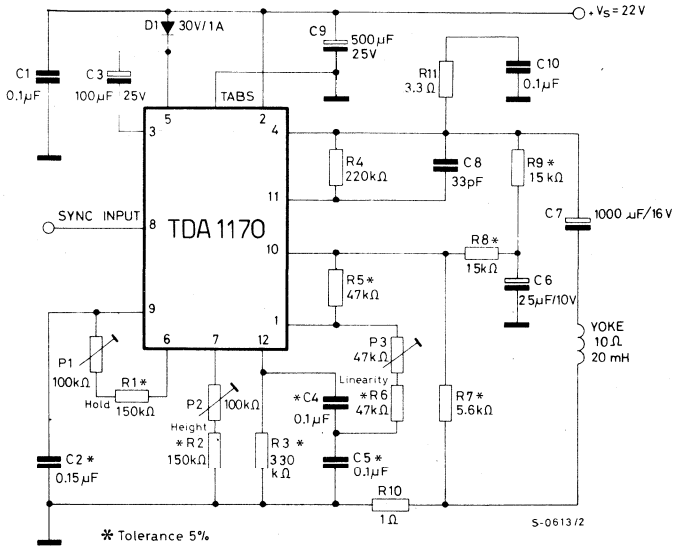
The quiescent output voltage (pin 4) is fixed by the voltage feedback network R7, R8 and R9 (refer to fig. 2) according to:

$$V_4 = V_{10} \frac{R7 + R8 + R9}{R7}$$

Pin 10 is the inverting input of the amplifier and its voltage is $V_{10} \cong 2V$.

TDA 1170

Fig. 9 – Typical application circuit for B & W 24" 110° TV sets

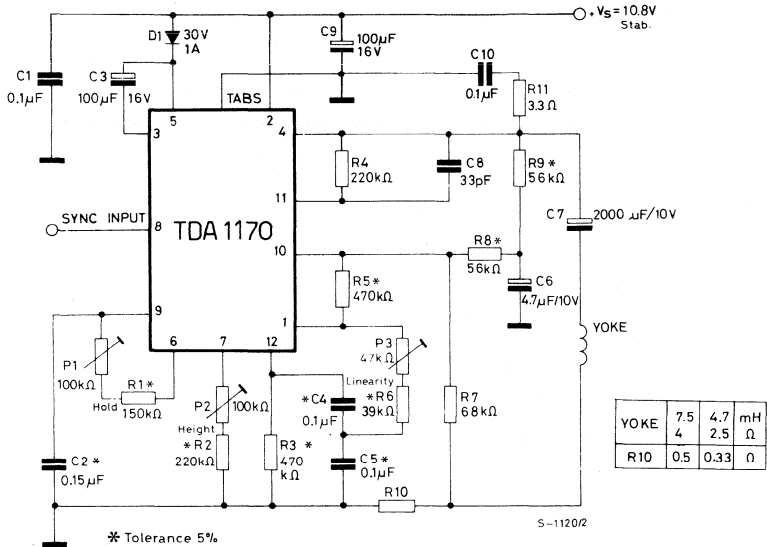


Typical performance ($V_s = 22V$; $I_V = 1A$; $R_V = 10\Omega$; $L_V = 20\text{ mH}$)

I_s	Supply current	140	mA
t_{fly}	Flyback time	0.75	ms
$I_{V.}$	Maximum scanning current (peak to peak)	1.2	A
V_s	Operating supply voltage	20 to 24	V
P_{tot}	TDA 1170 power dissipation	2.2	W

For safe working up to $T_{amb} = 50^\circ\text{C}$ a heatsink of $R_{th} = 40^\circ\text{C/W}$ is required and each tab of TDA 1170 must be soldered to 1 cm² copper area of the printed circuit board.

Fig. 10 - Typical application circuit for B & W small screen TV sets



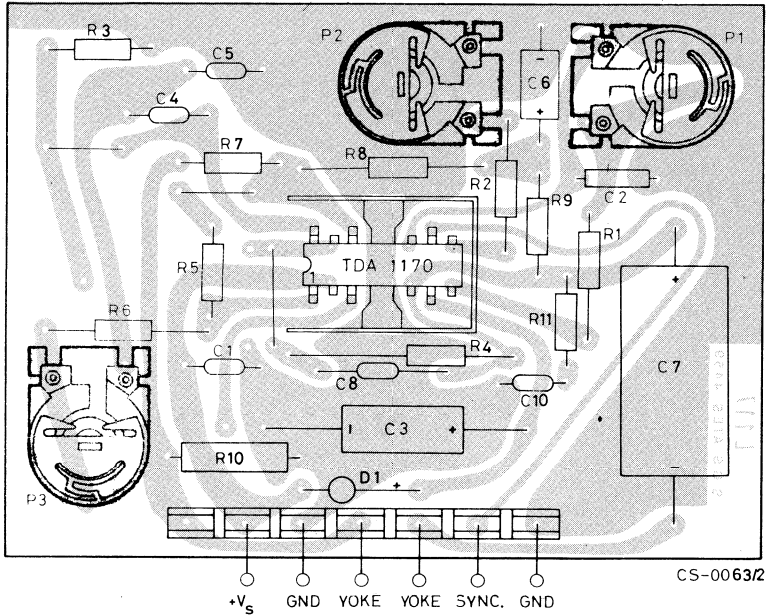
Typical performance ($V_s = 10.8V$; $I_Y = 1A$; $R_Y = 4\Omega$; $L_Y = 7.5 mH$)

I_s	Supply current	150	mA
t_{fly}	Flyback time	0.7	ms
I_Y	Maximum scanning current (peak to peak)	1.15	A
V_s	Operating supply voltage	10.8	V
P_{tot}	TDA 1170 power dissipation	1.3	W

For safe working up to $T_{amb} = 50^\circ C$ a heatsink of $R_{th} = 30^\circ C/W$ is required and each tab of the TDA 1170 must be soldered to 1 cm² copper area of the printed circuit board.

TDA 1170

Fig. 11 - P.C. board and component layout for the circuit of fig. 9 and fig. 10 (1:1 scale)



C9 is not mounted on the P.C. board.

MOUNTING INSTRUCTIONS

The junction to ambient thermal resistance of the TDA 1170 can be reduced by soldering the tabs to a suitable copper area of the printed circuit board (fig. 12) or to an external heatsink (fig. 13).

The diagram of fig. 16 shows the maximum dissippable power P_{tot} and the $R_{th j-amb}$ as a function of the side "s" of two equal square copper areas having a thickness of 35μ (1.4 mil).

During soldering the tab temperature must not exceed $260^\circ C$ and the soldering time must not be longer than 12 seconds.

The external heatsink or printed circuit copper area must be connected to electrical ground.

Fig. 12 - Example of P.C. board copper area used as heatsink

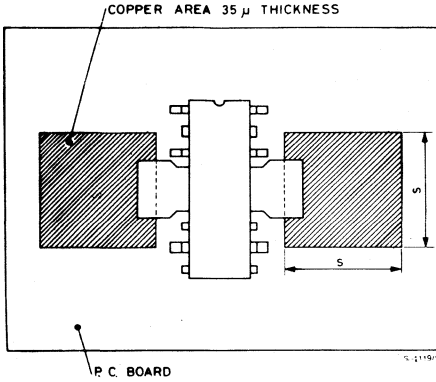


Fig. 13 - Example of TDA 1170 with external heatsink

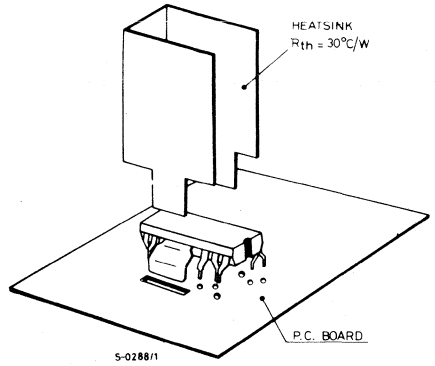


Fig. 14 - Maximum power dissipation and junction-ambient thermal resistance vs. "S"

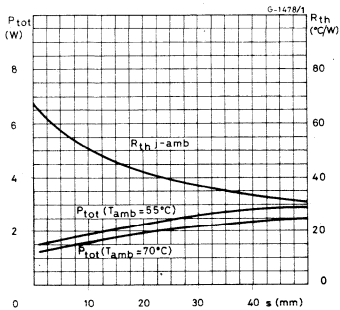
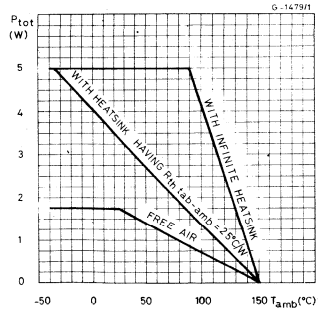


Fig. 15 - Maximum allowable power dissipation vs. ambient temperature



TDA 1170S TDA 1170SH

LINEAR INTEGRATED CIRCUITS

TV VERTICAL DEFLECTION SYSTEM

The TDA 1170S is a monolithic integrated circuit in a 12-lead quad in-line plastic package. It is intended for use in black and white and colour TV receivers.

The functions incorporated are:

- synchronization circuit
- oscillator and ramp generator
- high power gain amplifier
- flyback generator
- voltage regulator

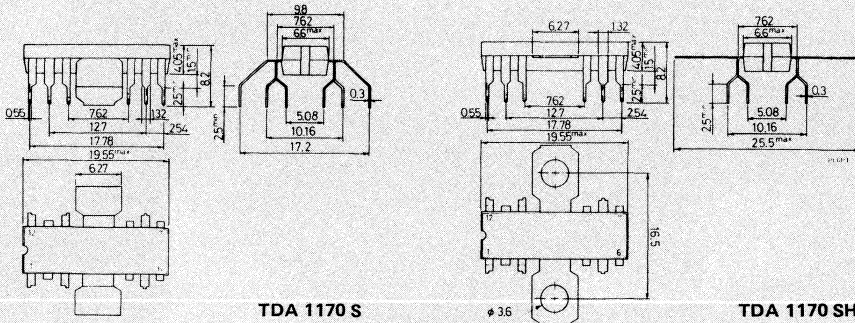
ABSOLUTE MAXIMUM RATINGS

V_5	Supply voltage at pin 2	35	V
V_4, V_5	Flyback peak voltage	60	V
V_{10}	Power amplifier input voltage	+ 10 - 0.5	V V
I_o	Output peak current (non repetitive) at $t = 2$ msec	2	A
I_o	Output peak current at $f = 50$ Hz $t \leq 10$ μ sec	2.5	A
I_o	Output peak current at $f = 50$ Hz $t > 10$ μ sec	1.5	A
I_3	Pin 3 DC current at $V_4 < V_2$	100	mA
I_3	Pin 3 peak to peak flyback current for $f = 50$ Hz, $t_{fly} \leq 1.5$ msec	1.8	A
I_8	Pin 8 current	± 20	mA
P_{tot}	Power dissipation: at $T_{tab} = 90^\circ\text{C}$ (TDA1170S) at $T_{amb} = 80^\circ\text{C}$ (TDA1170S)	5 1	W W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

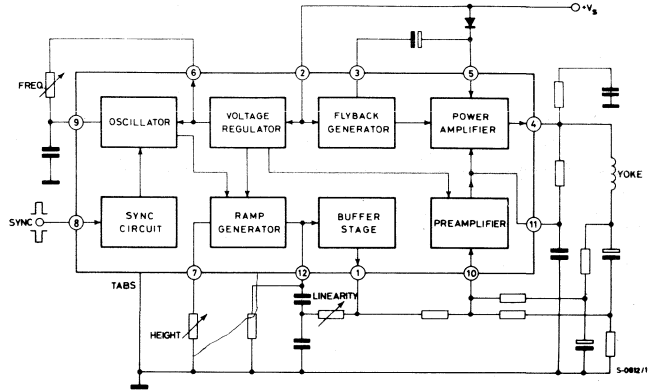
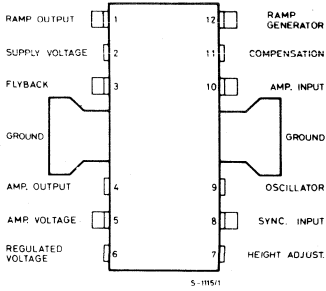
ORDERING NUMBERS: TDA 1170 S
TDA 1170 SH

MECHANICAL DATA

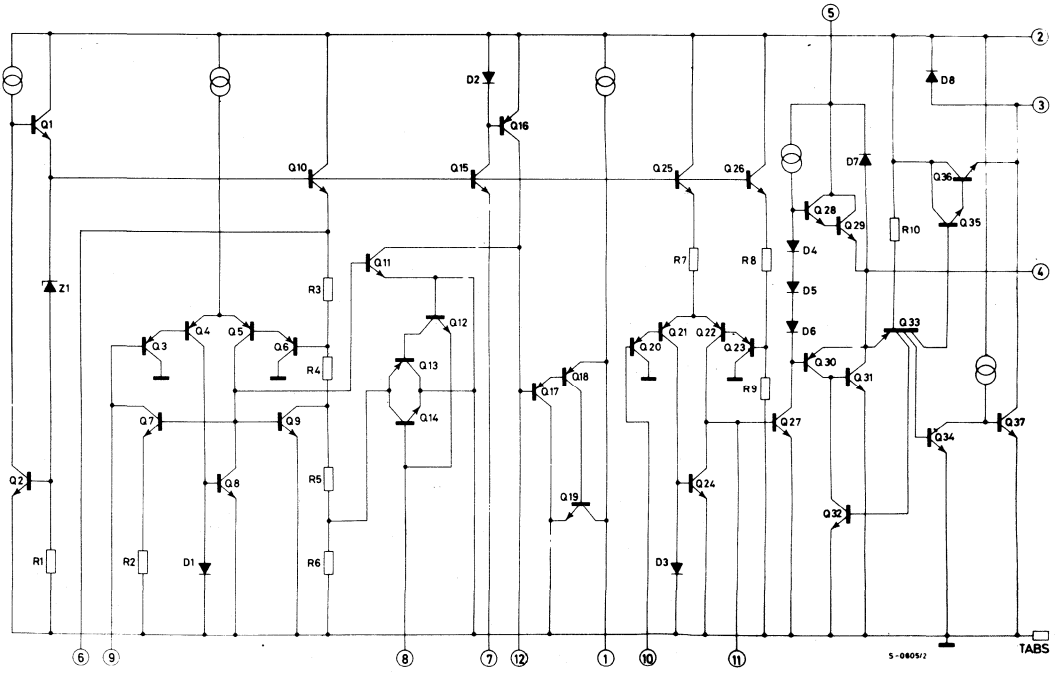
Dimensions in mm



CONNECTION AND BLOCK DIAGRAMS



SCHEMATIC DIAGRAM



TDA 1170S TDA 1170SH

THERMAL DATA

THERMAL DATA		TDA 1170S	TDA 1170SH
$R_{th\ j-tab}$	Thermal resistance junction-tab	max 12°C/W	max 10°C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max 70°C/W(°)	max 80°C/W

(°) Obtained with tabs soldered to printed circuit with minimized copper area.

ELECTRICAL CHARACTERISTICS (Refer to the test circuits, $V_s = 35V$, $T_{amb} = 25^\circ C$, unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig.
-----------	-----------------	------	------	------	------	------

DC CHARACTERISTICS

I_2	Pin 2 quiescent current	$I_3 = 0$		7	14	mA	1b
I_5	Pin 5 quiescent current	$I_4 = 0$		8	15	mA	1b
$-I_9$	Oscillator bias current	$V_9 = 1V$		0.1	1	μA	1a
$-I_{10}$	Amplifier input bias current	$V_{10} = 1V$		0.1	1	μA	1b
$-I_{12}$	Ramp generator bias current	$V_{12} = 0$		0.02	0.3	μA	1a
$-I_{12}$	Ramp generator current	$I_7 = 20\ \mu A$ $V_{12} = 0$	19	20	24	μA	1b
$\frac{\Delta I_{12}}{I_{12}}$	Ramp generator non-linearity	$\Delta V_{12} = 0$ to 12V $I_7 = 20\ \mu A$		0.2	1	%	1b
V_s	Supply voltage range		10		36	V	—
V_1	Pin 1 saturation voltage to ground	$I_1 = 1\ mA$		1	1.4	V	—
V_3	Pin 3 saturation voltage to ground	$I_3 = 10\ mA$		1.7	2.6	V	1a
V_4	Quiescent output voltage	$V_s = 10V$ $R_1 = 10\ K\Omega$ $R_2 = 10\ K\Omega$	4.17	4.4	4.63	V	1a
		$V_s = 35V$ $R_1 = 30\ K\Omega$ $R_2 = 10\ K\Omega$	8.35	8.8	9.25	V	1a
V_{4L}	Output saturation voltage to ground	$-I_4 = 0.1A$		0.9	1.2	V	1c
		$-I_4 = 0.8A$		1.9	2.3	V	1c
V_{4H}	Output saturation voltage to supply	$I_4 = 0.1A$		1.4	2.1	V	1d
		$I_4 = 0.8A$		2.8	3.2	V	1d
V_6	Regulated voltage at pin 6		6.1	6.5	6.9	V	1b
V_7	Regulated voltage at pin 7	$I_7 = 20\ \mu A$	6.2	6.6	7	V	1b
$\frac{\Delta V_6}{\Delta V_s}; \frac{\Delta V_7}{\Delta V_s}$	Regulated voltage drift with supply voltage	$\Delta V_s = 10$ to 35V		1		mV/V	1b
V_{10}	Amplifier input reference voltage		2.07	2.2	2.3	V	—
R_8	Pin 8 input resistance	$V_8 \leq 0.4V$	1			M Ω	1a

TDA 1170S TDA 1170SH

Fig. 1 - DC test circuits

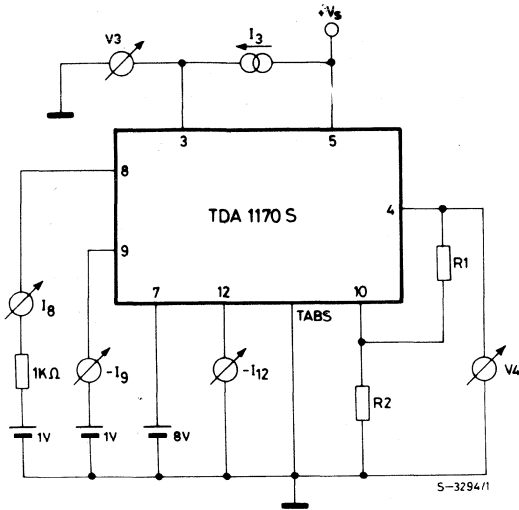


Fig. 1a

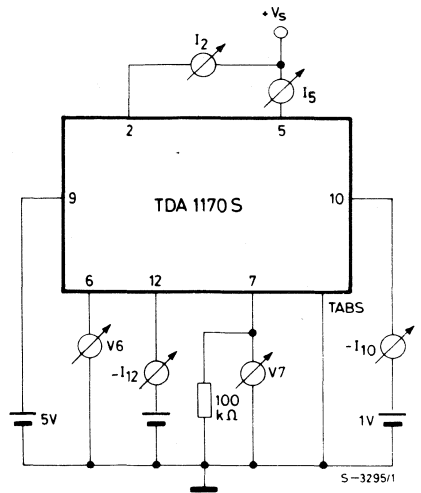


Fig. 1b

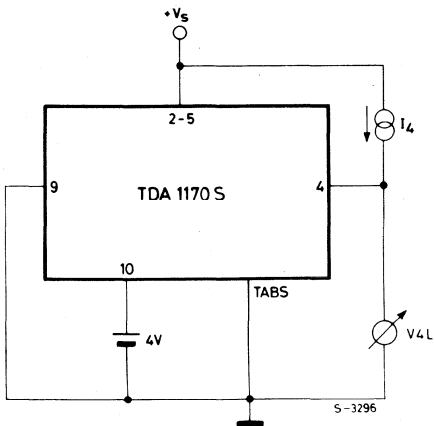


Fig. 1c

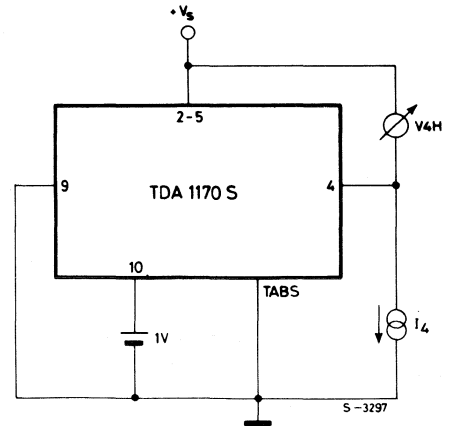


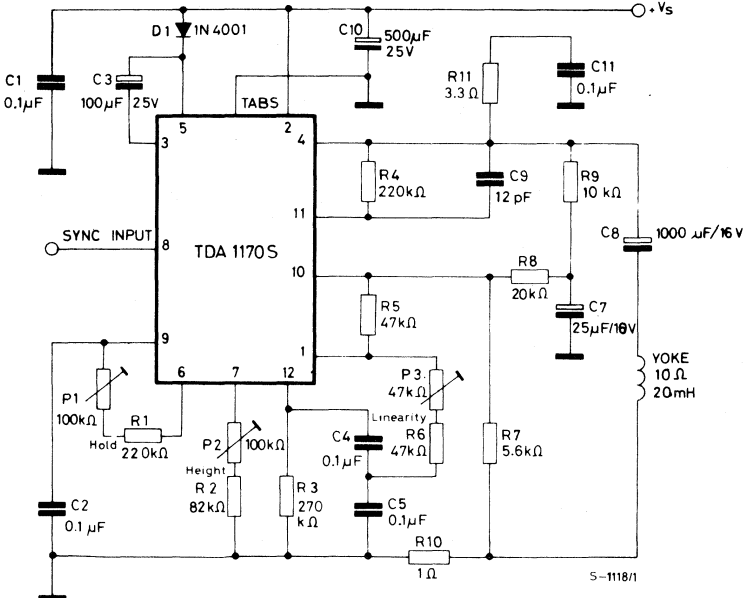
Fig. 1d

TDA 1170S TDA 1170SH

AC CHARACTERISTICS (Refer to the test circuit, $V_S = 25\text{V}$; $f = 50\text{ Hz}$; $T_{\text{amb}} = 25^\circ\text{C}$, unless otherwise specified)

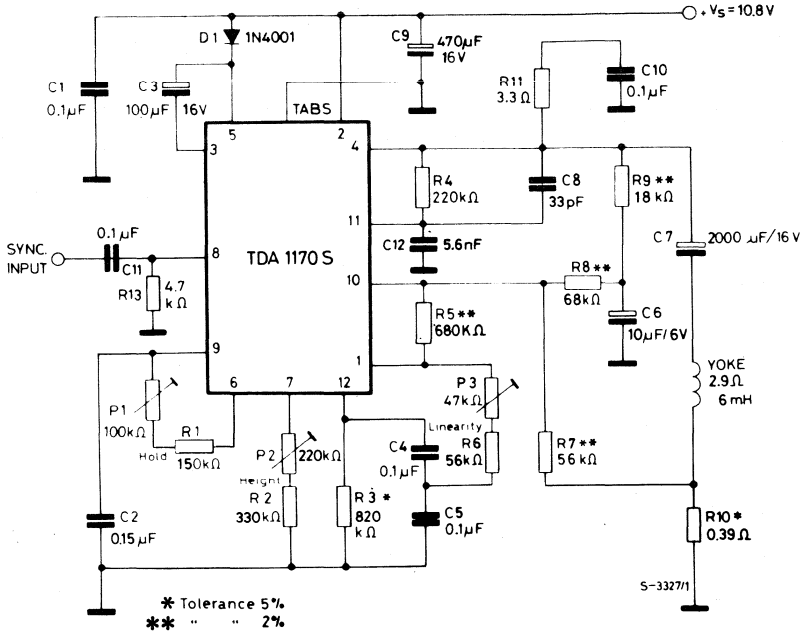
Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig.
I_s	Supply current		140		mA	2
I_8	Sync. input current (positive or negative)	500			μA	2
V_4	Flyback voltage		51		V	2
V_9	Peak to peak oscillator sawtooth voltage		2.4		V	2
t_{fly}	Flyback time	$I_y = 1\text{ App}$	0.7		ms	2
f_o	Free running frequency	$(P_1 + R_1) = 300\text{ K}\Omega$ $C_2 = 100\text{ nF}$	44		Hz	2
		$(P_1 + R_1) = 260\text{ K}\Omega$ $C_2 = 100\text{ nF}$	52		Hz	2
Δf	Synchronization range	$I_8 = 0.5\text{ mA}$	14		Hz	2
$\frac{\Delta f}{\Delta V_S}$	Frequency drift with supply voltage	$V_S = 10\text{ to }35\text{ V}$	0.005		Hz/V	2
$\left \frac{\Delta f}{\Delta T_{\text{tab}}} \right $	Frequency drift with tab temperature	$T_{\text{tab}} = 40\text{ to }120^\circ\text{C}$	0.01		Hz/ $^\circ\text{C}$	2

Fig. 2 - AC test circuit



TDA 1170S TDA 1170SH

Fig. 3 - Typical application circuit for small screen B/W TV set ($R_y = 2.9\Omega$, $L_y = 6\text{ mH}$; $I_y = 1.1\text{ App}$)



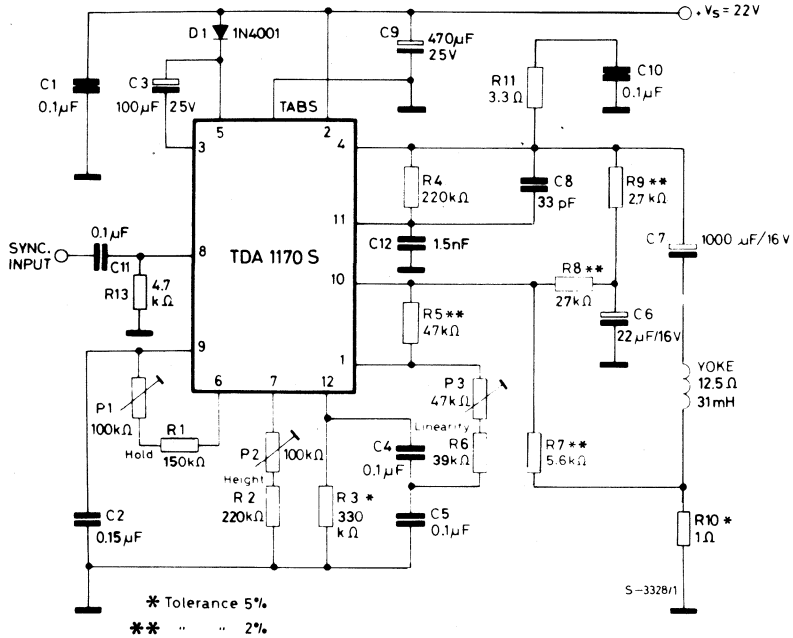
Typical performance

V_s	Operating supply voltage	10.8	V
I_s	Supply current	155	mA
t_{fly}	Flyback time	0.5	ms
P_{tot}	TDA 1170S power dissipation	1.35	W
I_y	Maximum scanning current (peak to peak)	1.30	A

For safe working up to $T_{amb} = 60^\circ\text{C}$ a heatsink of $R_{th} = 30^\circ\text{C/W}$ is required.

TDA 1170S TDA 1170SH

Fig. 4 - Typical application circuit for small screen 90° PIL TVC set ($R_y = 12.5\Omega$; $L_y = 31\text{ mH}$; $I_y = 0.8\text{ App}$)



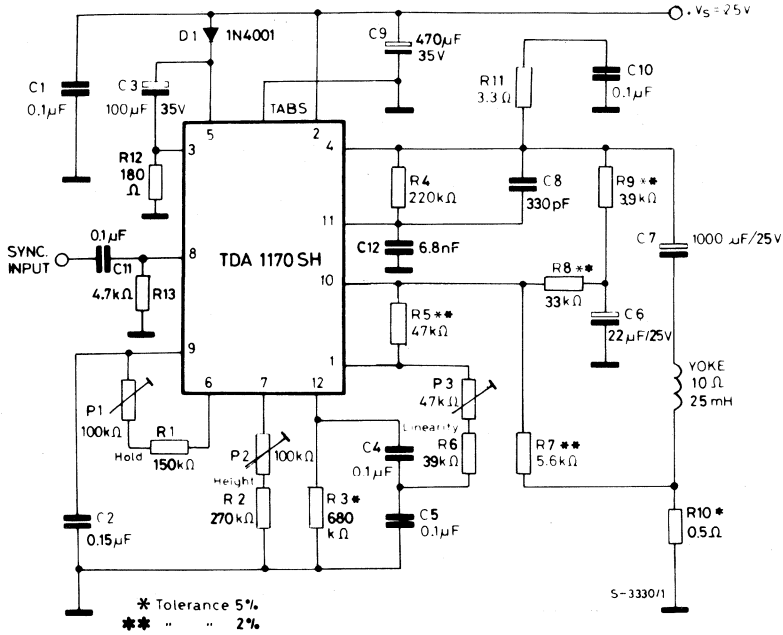
Typical performance

V_s	Operating supply voltage	22	V
I_s	Supply current	120	mA
t_{fly}	Flyback time	0.8	ms
P_{tot}	TDA 1170S power dissipation	1.95	W
I_y	Maximum scanning current (peak to peak)	1.0	A

For safe working up to $T_{amb} = 60^\circ\text{C}$ a heatsink of $R_{th} = 18^\circ\text{C/W}$ is required.

TDA 1170S TDA 1170SH

Fig. 6 - Typical application circuit for large screen 110° PIL TVC set ($R_y = 10\Omega$; $L_y = 25\text{ mH}$; $I_y = 1.25\text{ A}$)

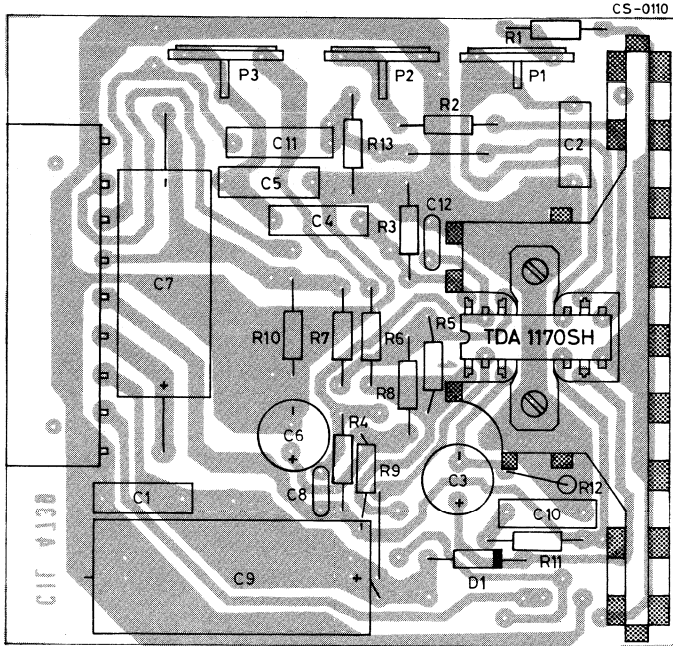


Typical performance

V_s	Operating supply voltage	25	V
I_s	Supply current	175	mA
t_{fly}	Flyback time	1	ms
P_{tot}	TDA 1170SH power dissipation	3.25	W
I_y	Maximum scanning current (peak to peak)	1.4	A

For safe working up to $T_{amb} = 60^\circ\text{C}$ a heatsink of $R_{th} = 8.5^\circ\text{C/W}$ is required.

Fig. 7 - P.C. board and component layout of the circuit of fig. 6 (1 : 1 scale)



Note: For the heatsink (1170 S and 1170 SH) see mounting instructions

MOUNTING INSTRUCTIONS

During soldering the tab temperature must not exceed 260°C and the soldering time must not be longer than 12 seconds.

The external heatsink or printed circuit copper area must be connected to electrical ground.

TDA 1170S

The junction to ambient thermal resistance of the TDA 1170S can be reduced by soldering the tabs to a suitable copper area of the printed circuit board (fig. 8) or to an external heatsink (fig. 9).

The diagram of fig. 10 shows the maximum dissipable power P_{tot} and the $R_{th\ j-amb}$ as a function of the side "s" of two equal square copper areas having a thickness of 35 μ (1.4 mil).

TDA 1170S TDA 1170SH

MOUNTING INSTRUCTIONS (continued)

Fig. 8 - Example of P.C. board copper area used as heatsink.

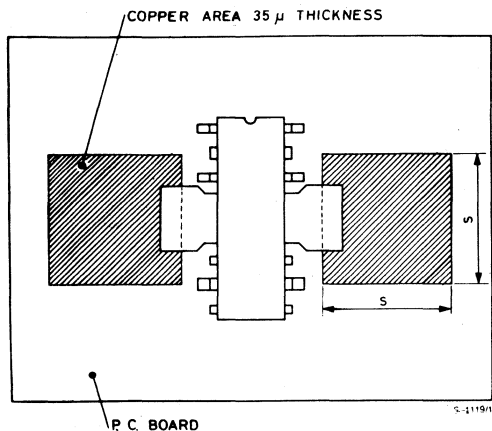


Fig. 9 - Example of TDA 1170 S with external heatsink.

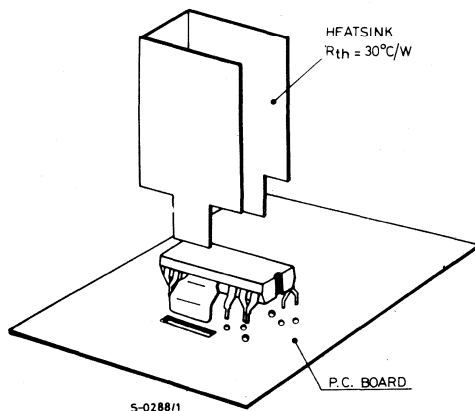


Fig. 10 - Maximum Power dissipation and junction-ambient thermal resistance vs. "S"

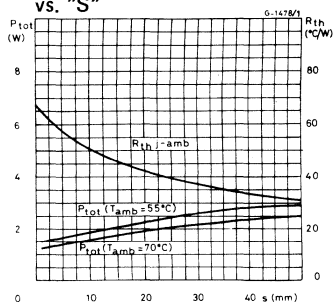


Fig. 11 - Maxim. allowable power dissipation vs. ambient temp. (TDA1170S)

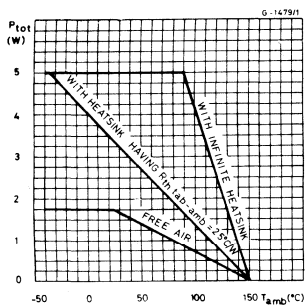
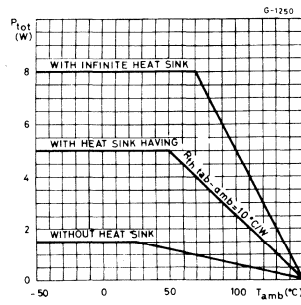


Fig. 12 - Maxim. allowable power dissipation vs. ambient temp. (TDA1170SH)

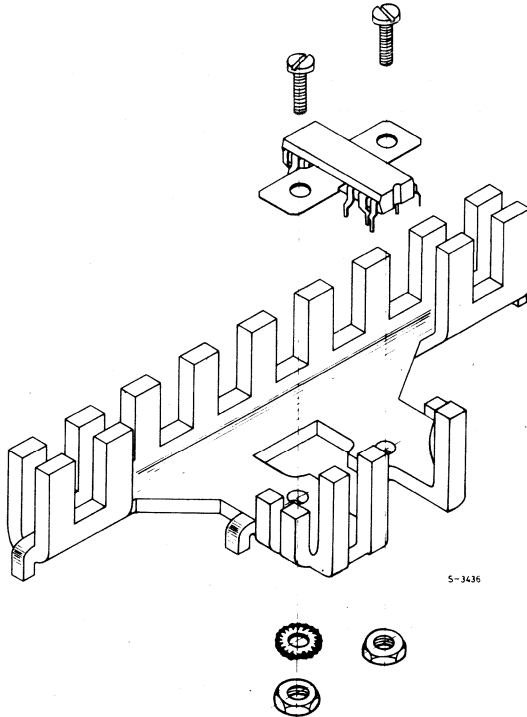


TDA 1170SH

The power dissipated in the circuit may be removed by connecting the tabs to an external heatsink according to fig. 12. The desired thermal resistance may be obtained by fixing the TDA1170SH to a suitable dimensioned plate as shown in fig. 13.

MOUNTING INSTRUCTIONS (continued)

Fig. 13 - Mounting example.



TDA 1180F

LINEAR INTEGRATED CIRCUIT

TV HORIZONTAL PROCESSOR

The TDA 1180F is a horizontal processor circuit for b.w. and colour television receiver. It is a monolithic integrated circuit encapsulated in 16-lead dual in-line plastic package. The TDA 1180F is a modified version of the TDA 1180P particularly suited for France standard and Bi-standard application. It combines the following functions:

- Noise gated horizontal sync separator.
- Noise gated vertical sync separator.
- Horizontal oscillator with frequency range limiter.
- Phase comparator between sync pulses and oscillator pulses (PLL).
- Phase comparator between flyback pulses and oscillator pulses (PLL).
- Loop gain and time constant switching (VCR).
- Composite blanking and key pulse generator.
- Protection circuits.
- Output stages with high current capability.

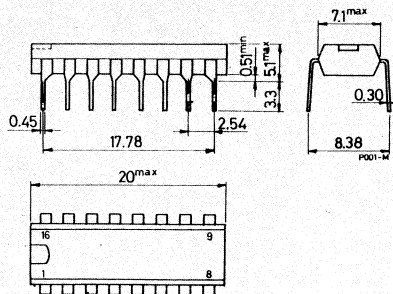
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage (pin 1)	15	V
V_2	Voltage at pin 2	18	V
V_4	Voltage at pin 4	V_s	
V_8	Voltage at pin 8	{ V_s -6	V
V_9	Voltage at pin 9	{ +6 -6	V
V_{11}	Voltage at pin 11	V_s	
I_2	Pin 2 peak current	1	A
I_3	Pin 3 peak current	0.5	A
I_6	Pin 6 current	30	mA
I_7	Pin 7 current	20	mA
I_{10}	Pin 10 current	30	mA
P_{tot}	Total power dissipation at $T_{amb} \leq 70^\circ\text{C}$	1	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

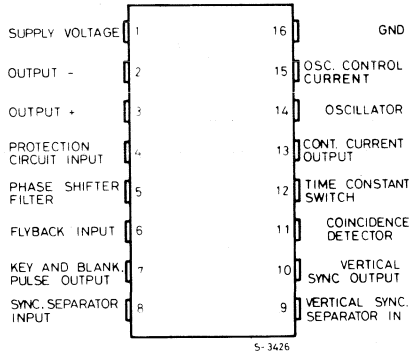
ORDERING NUMBER: TDA 1180F

MECHANICAL DATA

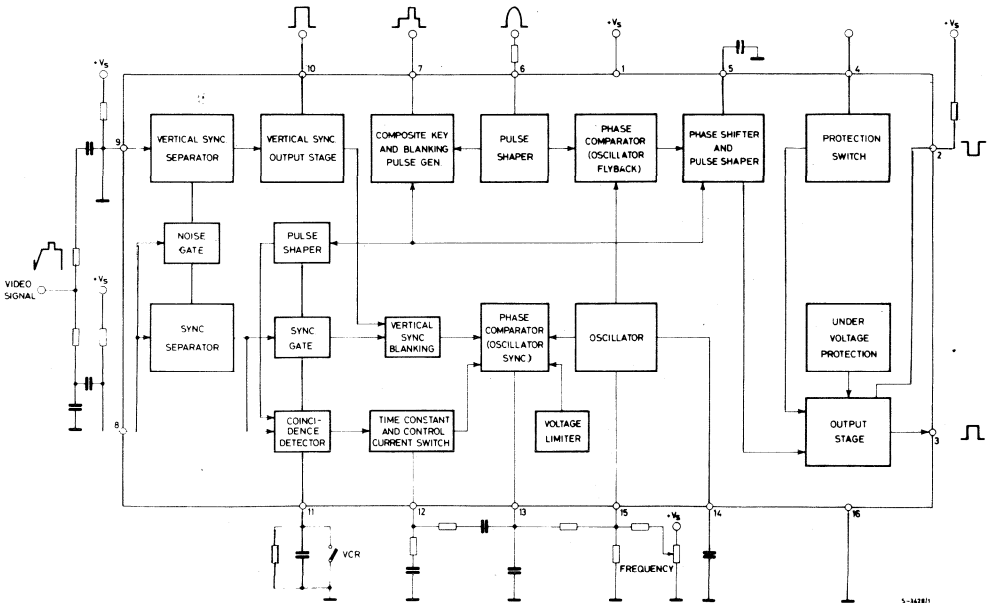
Dimensions in mm



CONNECTION DIAGRAM

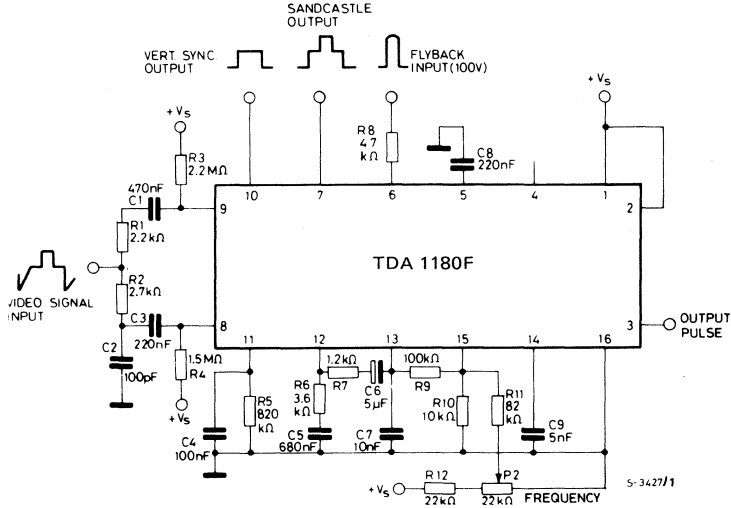


BLOCK DIAGRAM



TDA 1180F

TEST CIRCUIT



THERMAL DATA

$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	80	$^{\circ}C/W$
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ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $V_s = 12V$, $T_{amb} = 25^{\circ}C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s Supply voltage range		10	12	13.2	V
I_s Supply current	$I_3 = 0$		40	52	mA
V_s Supply voltage at which the output pulses (at pin 2 and 3) are switched off				4	V

HORIZONTAL SYNC. SEPARATOR AND NOISE GATE

V_i	Peak to peak input signal		1	3	6	V
V_8	Input switching voltage	$I_8 = 80\ \mu A$		1.5		V
I_8	Input switching current	$V_8 = 1.4V$		10		μA
I_8	Input blocking current for noise suppression _v			0.9		mA
V_8	Input switching voltage for noise suppression			2.1		V
I_8	Leakage current	$V_8 = -5V$			1	μA

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
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VERTICAL SYNC. SEPARATOR

V_I	Peak to peak input signal		1	3	6	V
V_9	Input switching voltage	$I_9 = 80 \mu\text{A}$		1.5		V
I_9	Input switching current	$V_9 = 1.4\text{V}$		5		μA
I_9	Leakage current	$V_9 = -5\text{V}$			1	μA
V_{10}	Vertical sync. pulse output voltage	No load at pin 10	11			V
R_{10}	Output resistance			10		$\text{K}\Omega$
t_{LV}	Delay between leading edge of input and output signals		9.5	12	17	μs
t_{TV}	Delay between trailing edge of input and output signals			50		μs
t_V	Vertical sync pulse duration			190		μs

PROTECTION CIRCUIT

V_4	Input voltage for switching off the output pulses	Output pulses OFF			0.5	V
		Output pulses ON	1			
R_4	Input resistance			200		$\text{K}\Omega$
I_4	Input current		5			μA

FLYBACK PULSE

V_6	Input threshold voltage of blanking generator			1.5		V
V_6	Input threshold voltage of phase comparator			7.6		V
I_6	Input switching current	$V_6 \geq 1.7\text{V}$		0.23		mA

OUTPUT PULSE

V_3	Peak to peak output voltage	$I_3 = 150 \text{ mApp}$		10		V
I_3	Output current	$V_3 = 5\text{V}$		500		mA
R_3	Output resistance	at leading edge of output pulse		3		Ω
		at trailing edge of output pulse		20		
t_p	Output pulse duration		26	28	32	μs

COMPOSITE BLANKING AND KEY PULSE

V_{7K}	Key pulse output peak voltage		9	11		V
V_{7B}	Blanking pulse output voltage		4.2	4.5	4.8	V
R_7	Output resistance			100		Ω
t_{SK}	Phase relation between trailing edge of key pulse and middle of sync input pulse			2.7		μs
t_K	Key pulse duration		3.5	3.8		μs
t_{fb}	Delay between flyback pulse and blanking pulse	$V_6 = 1.7\text{V}$			0.2	μs

TDA 1180F

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
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INTERNAL GATING PULSE

t_g	Gating pulse duration		7.5		μs
t	Phase relation between middle of sync pulse and trailing and leading edge of gating pulse		3.75		μs

COINCIDENCE DETECTOR

V_{11}	Output voltage	with coincidence	6.8		V
		without coincidence		4	
I_{11}	Peak output current		0.5		mA

VCR SWITCH

V_{11}	Input voltage		0 to 4 or 8.5 to 12		V
$-I_{11}$	Output current		35		μA
I_{11}	Output current		0.4		mA

TIME CONSTANT SWITCH

V_{12}	Output voltage		3		V
R_{12}	Output resistance	$4.5V < V_{11} < 8V$	100		Ω
		$V_{11} > 8.5V$ or $V_{11} < 4V$	40		K Ω

OSCILLATOR

V_{14}	Low level threshold voltage		5.4		V
V_{14}	High level threshold voltage		8.2		V
I_{14}	Charge current		0.6		mA
I_{14}	Discharge current		0.3		mA
V_{15}	Current source supply voltage		3		V
I_{15}	Current source supply current		0.3		mA
f_o	Free running frequency		15625		Hz
$\frac{\Delta f_o}{f_o}$	Adjustment range		± 10		%
$\frac{\Delta f_o}{\Delta I_{15}}$	Frequency control sensitivity		52		$\frac{Hz}{\mu A}$
Δf_o	Frequency change when V_s drops to 4V			± 10	%

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
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OSCILLATOR-FLYBACK PULSE PHASE COMPARATOR

V_5	Control voltage range		9.4 to 8.2		V
I_5	Peak control current			± 0.5	mA
I_5	Input current (blocked phase detector)			5	μ A
t_d	Permissible delay between output pulse leading edge and flyback pulse leading edge		$t_p - t_f$		μ s
$\frac{\Delta t}{\Delta t_d}$	Static control error			0.2	%

SYNC PULSE-OSCILLATOR PHASE COMPARATOR

V_{13}	Control voltage range		4.6 to 1.4		V
I_{13}	Control peak current		± 2		mA
$\frac{\Delta f}{\Delta t}$	Phase lock loop gain		2		$\frac{\text{KHz}}{\mu\text{s}}$
f	Catching and holding range		± 700		Hz

OVERALL PHASE RELATIONSHIP

t_o	Phase relation between middle of flyback pulse and middle of sync pulse		2.6		μ s
$\frac{\Delta V_5}{\Delta t_o}$	Adjustment sensitivity		65		$\frac{\text{mV}}{\mu\text{s}}$
$\frac{\Delta I_5}{\Delta t_o}$	Adjustment sensitivity		10		$\frac{\mu\text{A}}{\mu\text{s}}$

TDA 1180P

LINEAR INTEGRATED CIRCUIT

TV HORIZONTAL PROCESSOR

The TDA 1180P is a horizontal processor circuit for b.w. and colour television receiver. It is a monolithic integrated circuit encapsulated in 16-lead dual in-line plastic package. The TDA 1180P combines the following functions:

- Noise gated horizontal sync separator.
- Noise gated vertical sync separator.
- Horizontal oscillator with frequency range limiter.
- Phase comparator between sync pulses and oscillator pulses (PLL).
- Phase comparator between flyback pulses and oscillator pulses (PLL).
- Loop gain and time constant switching (VCR).
- Composite blanking and key pulse generator.
- Protection circuits.
- Output stages with high current capability.

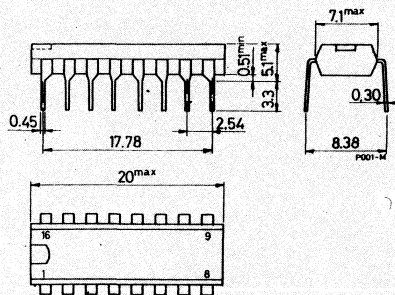
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage (pin 1)	15	V
V_2	Voltage at pin 2	18	V
V_4	Voltage at pin 4	V_s	
V_8	Voltage at pin 8	{ V_s -6	V
V_9	Voltage at pin 9	{ +6 -6	V
V_{11}	Voltage at pin 11	V_s	
I_2	Pin 2 peak current	1	A
I_3	Pin 3 peak current	0.5	A
I_6	Pin 6 current	30	mA
I_7	Pin 7 current	20	mA
I_{10}	Pin 10 current	30	mA
P_{tot}	Total power dissipation at $T_{amb} \leq 70^\circ\text{C}$	1	W
T_{stg}, T_J	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBER: TDA 1180P

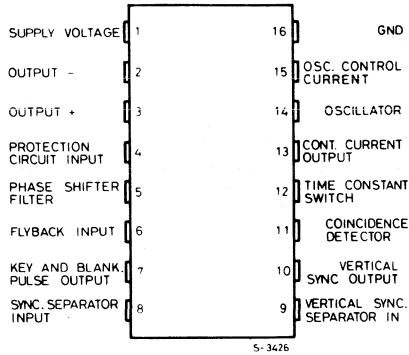
MECHANICAL DATA

Dimensions in mm

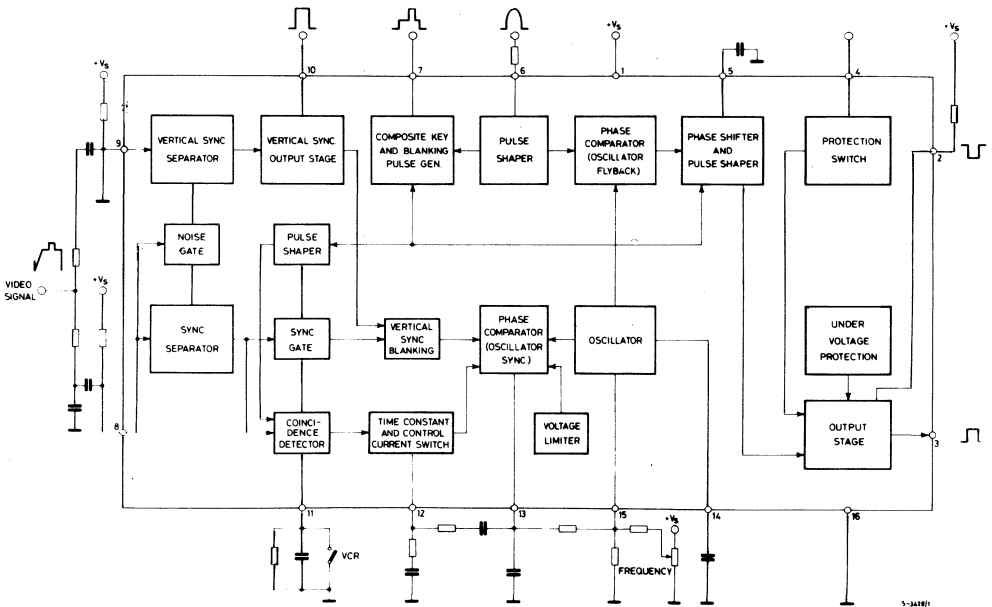


CONNECTION DIAGRAM

(top view)

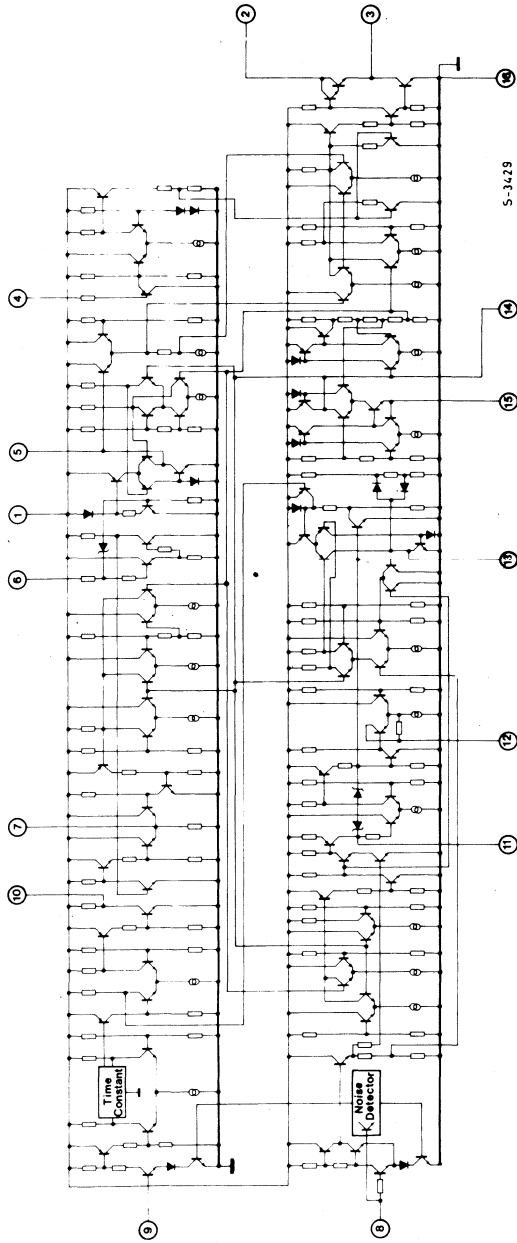


BLOCK DIAGRAM

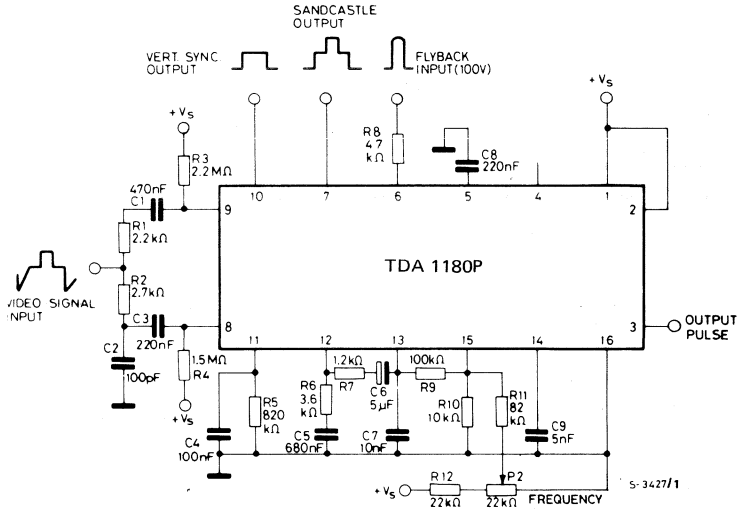


TDA 1180P

SCHEMATIC DIAGRAM



TEST CIRCUIT



THERMAL DATA

$R_{th j-amb}$	Thermal resistance junction-ambient	max	80	$^{\circ}C/W$
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ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $V_s = 12V$, $T_{amb} = 25^{\circ}C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s	Supply voltage	10	12	13.2	V
I_s	Supply current	$I_3 = 0$	40	52	mA
V_s	Supply voltage at which the output pulses (at pin 2 and 3) are switched off			4	V

HORIZONTAL SYNC. SEPARATOR AND NOISE GATE

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_i	Peak to peak input signal	1	3	6	V
V_B	Input switching voltage	$I_B = 80 \mu A$	1.5		V
I_B	Input switching current	$V_B = 1.4V$	10		μA
I_B	Input blocking current for noise suppression		0.9		mA
V_B	Input switching voltage for noise suppression		2.1		V
I_B	Leakage current	$V_B = -5V$		1	μA

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ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
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VERTICAL SYNC. SEPARATOR

V_i	Peak to peak input signal		1	3	6	V
V_9	Input switching voltage	$I_9 = 80 \mu\text{A}$		1.5		V
I_9	Input switching current	$V_9 = 1.4\text{V}$		5		μA
I_9	Leakage current	$V_9 = -5\text{V}$			1	μA
V_{10}	Vertical sync. pulse output voltage	No load at pin 10	11			V
R_{10}	Output resistance			10		$\text{K}\Omega$
t_{LV}	Delay between leading edge of input and output signals			17		μs
t_{TV}	Delay between trailing edge of input and output signals			50		μs
t_V	Vertical sync pulse duration			190		μs

PROTECTION CIRCUIT

V_4	Input voltage for switching off the output pulses	Output pulses OFF			0.5	V
		Output pulses ON	1			
R_4	Input resistance			200		$\text{K}\Omega$
I_4	Input current		5			μA

FLYBACK PULSE

V_6	Input threshold voltage of blanking generator			1.5		V
V_6	Input threshold voltage of phase comparator			7.6		V
I_6	Input switching current	$V_6 \geq 1.7\text{V}$		0.23		mA

OUTPUT PULSE

V_3	Peak to peak output voltage	$I_3 = 150 \text{ mApp}$		10		V
I_3	Output current	$V_3 = 5\text{V}$		500		mA
R_3	Output resistance	at leading edge of output pulse		3		Ω
		at trailing edge of output pulse		20		
t_p	Output pulse duration		20	22	26	μs

COMPOSITE BLANKING AND KEY PULSE

V_{7K}	Key pulse output peak voltage		9	11		V
V_{7B}	Blanking pulse output voltage		4.2	4.5	4.8	V
R_7	Output resistance			100		Ω
t_{SK}	Phase relation between trailing edge of key pulse and middle of sync input pulse			2.7		μs
t_K	Key pulse duration		3.5	3.8		μs
t_{fb}	Delay between flyback pulse and blanking pulse	$V_6 = 1.7 \text{ V}$			0.2	μs

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
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INTERNAL GATING PULSE

t_g	Gating pulse duration		7.5		μs
t	Phase relation between middle of sync pulse and trailing and leading edge of gating pulse		3.75		μs

COINCIDENCE DETECTOR

V_{11}	Output voltage	with coincidence		6.8		V
		without coincidence			4	
I_{11}	Peak output current		0.5		mA	

VCR SWITCH

V_{11}	Input voltage		0 to 4 or 8.5 to 12		V
$-I_{11}$	Output current		35		μA
I_{11}	Output current		0.4		mA

TIME CONSTANT SWITCH

V_{12}	Output voltage		3		V
R_{12}	Output resistance	$4.5\text{V} < V_{11} < 8\text{V}$	100		Ω
		$V_{11} > 8.5\text{V}$ or $V_{11} < 4\text{V}$	40		$\text{K}\Omega$

OSCILLATOR

V_{14}	Low level threshold voltage		5.4		V
V_{14}	High level threshold voltage		8.2		V
I_{14}	Charge current		0.6		mA
I_{14}	Discharge current		0.3		mA
V_{15}	Current source supply voltage		3		V
I_{15}	Current source supply current		0.3		mA
f_o	Free running frequency		15625		Hz
$\frac{\Delta f_o}{f_o}$	Adjustment range		± 10		%
$\frac{\Delta f_o}{\Delta I_{15}}$	Frequency control sensitivity		52		$\frac{\text{Hz}}{\mu\text{A}}$
Δf_o	Frequency change when V_s drops to 4V			± 10	%

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ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
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OSCILLATOR-FLYBACK PULSE PHASE COMPARATOR

V_5	Control voltage range		9.4 to 8.2		V
I_5	Peak control current			± 0.5	mA
I_5	Input current (blocked phase detector)			5	μ A
t_d	Permissible delay between output pulse leading edge and flyback pulse leading edge		$t_p - t_f$		μ s
$\frac{\Delta t}{\Delta t_d}$	Static control error			0.2	%

SYNC PULSE-OSCILLATOR PHASE COMPARATOR

V_{13}	Control voltage range		4.6 to 1.4		V
I_{13}	Control peak current		± 2		mA
$\frac{\Delta f}{\Delta t}$	Phase lock loop gain		2		$\frac{\text{KHz}}{\mu\text{s}}$
f	Catching and holding range		± 700		Hz

OVERALL PHASE RELATIONSHIP

t_o	Phase relation between middle of flyback pulse and middle of sync pulse		2.6		μ s
$\frac{\Delta V_5}{\Delta t_o}$	Adjustment sensitivity		65		$\frac{\text{mV}}{\mu\text{s}}$
$\frac{\Delta I_5}{\Delta t_o}$	Adjustment sensitivity		10		$\frac{\mu\text{A}}{\mu\text{s}}$

Fig. 1 - Vertical sync. output pulse

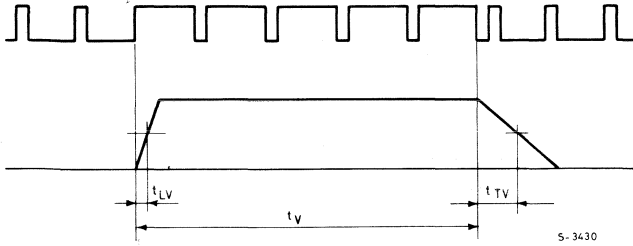
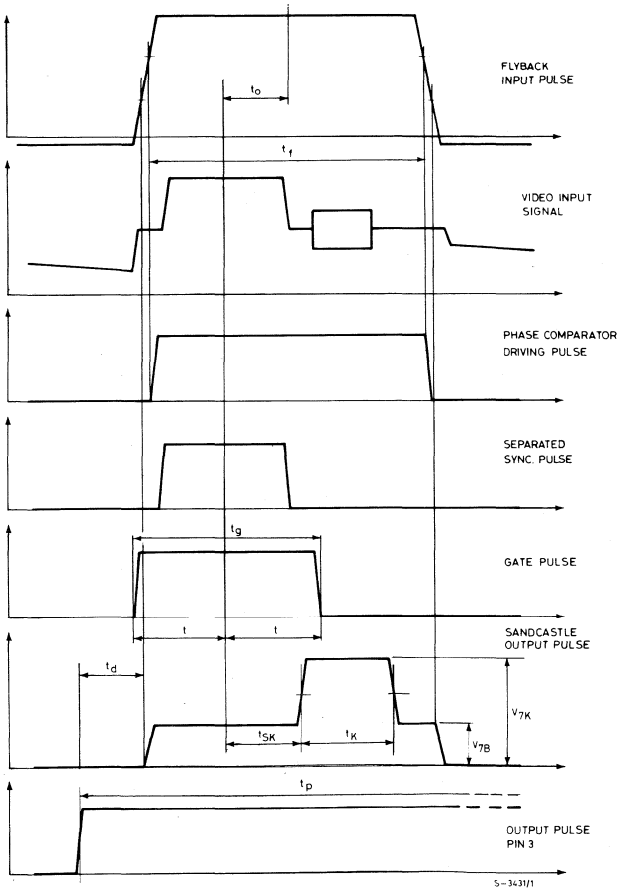


Fig. 2 - Relationship of main waveform phases



TDA 1180P

Fig. 3 - Free running frequency vs. supply voltage

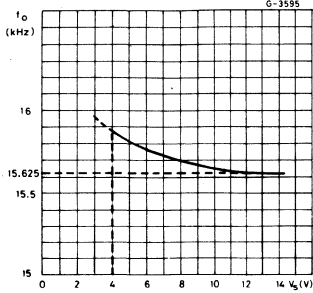


Fig. 4 - Overall phase relation vs. supply voltage

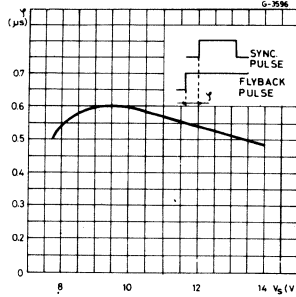
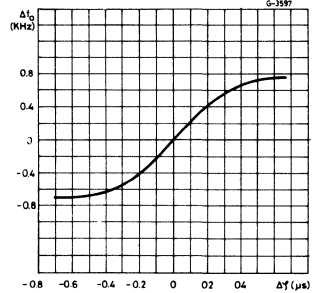


Fig. 5 - Loop gain



APPLICATION INFORMATION

Pin 1 - Positive supply

The operating supply voltage of the device ranges from 10V to 13.2V.

Pin 2 and 3 - Output

The outputs of TDA 1180P are suitable for driving transistor output stages, they deliver positive pulse at pin 3 and negative pulse at pin 2.

The negative pulse is used for direct driving of the output stage, while positive pulse is useful when a driver stage is required.

The rise and fall times of the output pulses are about 150 ns so that interference due to radiation are avoided.

Furthermore the output stages are internally protected against short circuit.

Pin 4 - Protection circuit input

By connecting pin 4 of the IC to earth the output pulses at pin 2 and 3 are shut off; this function has been introduced to protect the final stages from overloads.

The same pulses are also shut off when the supply voltage falls below 4V.

Pin 5 - Phase shifter filter

To compensate for the delay introduced by the line final stages, the flyback pulses to pin 6 and the oscillator waveform are compared in the oscillator-flyback pulse phase comparator.

The result of the comparison is a control current which, after it has been filtered by the external capacitor connected to pin 5, is sent to a phase shifter which adequately regulates the phase of the output pulses.

The maximum phase shift allowed is:

$$t_d = t_p - t_f$$

where t_f is the flyback pulse duration.

Pin 5 has high input and output resistance (current generator).

APPLICATION INFORMATION (continued)

Pin 6 – Flyback input

The flyback pulse drives the high impedance input through a resistor in order to limit the input current to suitable maximum values.

The flyback input pulses are processed by a double threshold circuit; this generates the blanking pulses by sensing low level flyback voltage and the pulses to drive the phase comparator by sensing high level flyback voltage, therefore phase jitter caused by ringing normally associated with the flyback pulse, is avoided.

Pin 7 – Key and blanking pulse output

The key pulse for taking out the burst from the chrominance signal is generated from the oscillator ramp and has therefore a fixed phase position with respect to the sync.

The key pulse is then added internally to the blanking pulse obtained by correctly forming the flyback pulse present at pin 6.

The sum of the two signals (sandcastle pulse) is available on low impedance at output pin 7.

Pin 8 and 9 – Sync separators inputs

The video signal is applied by means of two distinct biasing networks to pins 8 and 9 of the IC and therefore to the respective vertical and horizontal sync separators.

The latter take the sync pulses out of the video signal and make them available to the rest of the circuit for further processing.

An amplitude detector also connected to pin 8, blocks operation of the sync separators when interference or noise peaks exceed a certain preset value.

Pin 10 – Vertical sync output

The vertical sync pulse, obtained by internal integration of the synchronizing signal, is available at this pin.

The output impedance is typically $10K\Omega$ and the lowest amplitude without load is 11V.

Pin 11 – Coincidence detector

From the oscillator waveform a gate pulse $7\ \mu s$ wide is taken whose phase position is centered on the horizontal synchronism.

The gate pulse not only controls a logic block which permits the sync to reach the oscillator-sync phase comparator only for as long as its duration, but also allows the latching and de-latching conditions of the oscillator to be established.

This function is obtained by a coincidence detector which compares the phase of the gate pulses with that of the sync.

When the two signals are not accurately aligned in time it means that the oscillator is not synchronized. In this case the detector acts on the logic block to eliminate its filtering effect and on the time constant switching block to establish a high impedance on pin 12 (small time constant of low-pass filter).

This latter block also acts on the oscillator-sync phase detector to increase its sensitivity and with it the loop gain of the synchronizing system.

In this conditions the phase lock has low noise immunity (wide equivalent noise bandwidth) and rapid pull-in time which allows fairly short synchronization times.

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APPLICATION INFORMATION (continued)

Once locking has taken place the coincidence detector enables the logic block, causes a low impedance on pin 12 and reduces the sensitivity of the phase comparator.

In these conditions the phase lock has high noise immunity (narrow equivalent noise bandwidth) due to the complete elimination of interference which occurs during the scanning period and the greater inertia with which the oscillator can change its frequency.

To optimize the behaviour of the IC if a video recorder is used, the state of the detector can be forced by connecting pin 11 to earth or to $+V_s$. The characteristics of the phase lock thus correspond to the lack of synchronization.

Pin 12 — Time constant switch, (see pin 11)

Pin 13 — Control current output

The oscillator is synchronized by comparing the phase of its waveform with that of the sync pulses in the oscillator-sync phase comparator and sending its output current I_{13} (proportional to the phase difference between the two signals) to pin 15 of the oscillator after it has been filtered properly with an external low-pass circuit.

The time constant of the filter can be switched between two values according to the impedance presented by pin 12.

The voltage limiter at the output of the phase comparator limits the voltage excursion on pin 13 and therefore the frequency range in which the oscillator remains held-in.

The output resistance of pin 13 is :

$$\begin{aligned} \text{low when } V_{13} > 4.3\text{V or } V_{13} < 1.6\text{V} \\ \text{high when } 1.6\text{V} < V_{13} < 4.3\text{V} \end{aligned}$$

To prevent the vertical sync from reaching the oscillator-sync phase comparator along with the horizontal sync, a signal which inhibits the phase detector during the vertical interval is taken from the vertical output stage; inhibition remains even if the video signal is not present.

The free running frequency of the oscillator is determined by the values of the capacitor and of the resistor connected to pins 14 and 15 respectively.

To generate the line frequency output pulses, two thresholds are fixed along the fall ramp of the triangular waveform of the oscillator.

Pin 14 — Oscillator (see pin 13)

Pin 15 — Oscillator control current input (see pin 13)

Pin 16 — Ground

Fig. 6 – Application circuit for large screen b.w. and colour TV

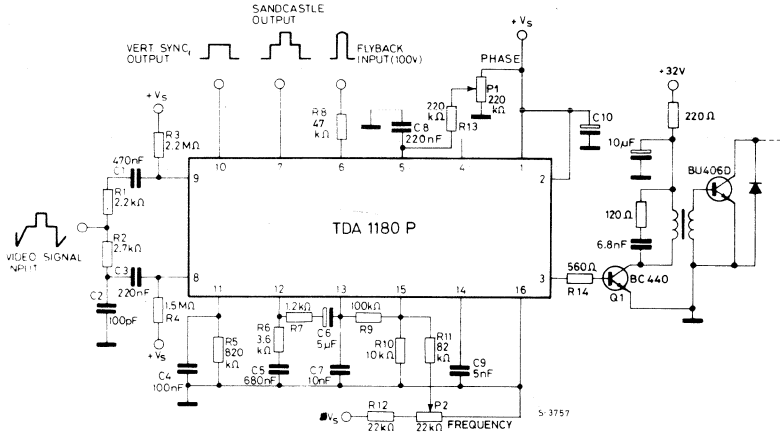
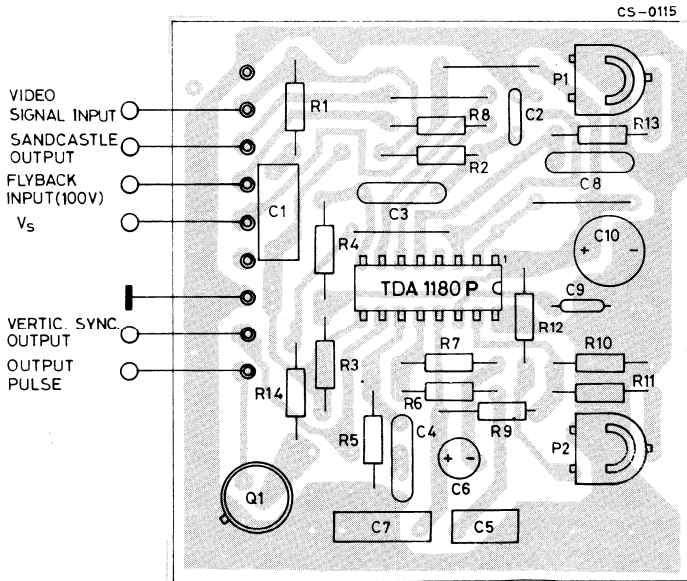


Fig. 7 – P.C. board and component layout for the circuit in fig. 6 (1:1 scale)



TDA 1180P

Fig. 8 - Application circuit for small screen b.w. TV.

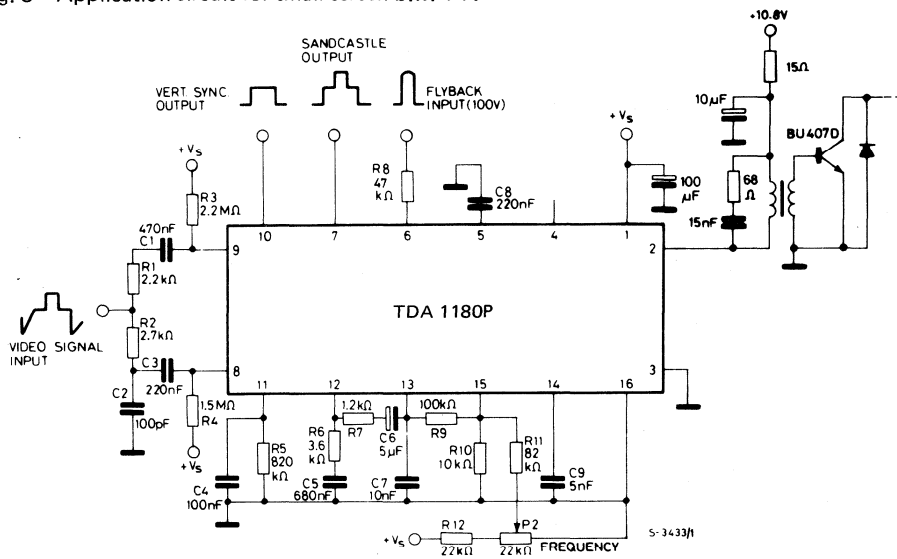
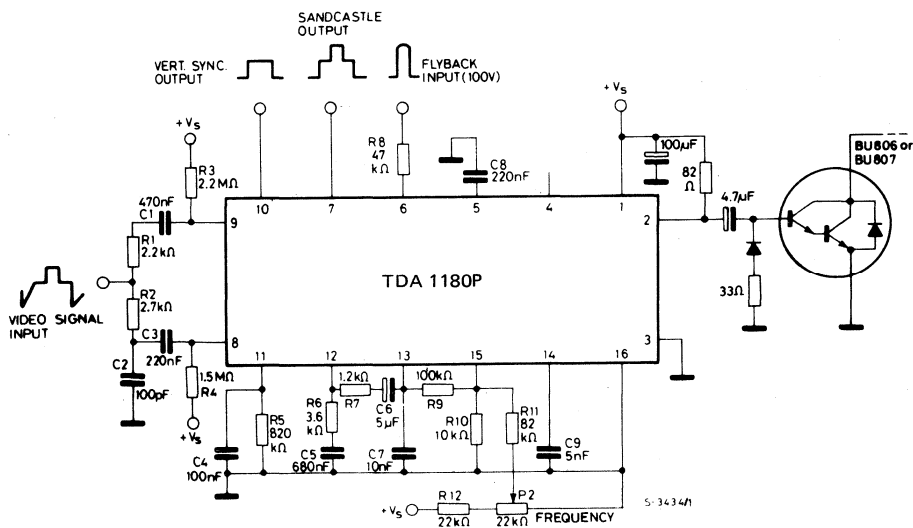
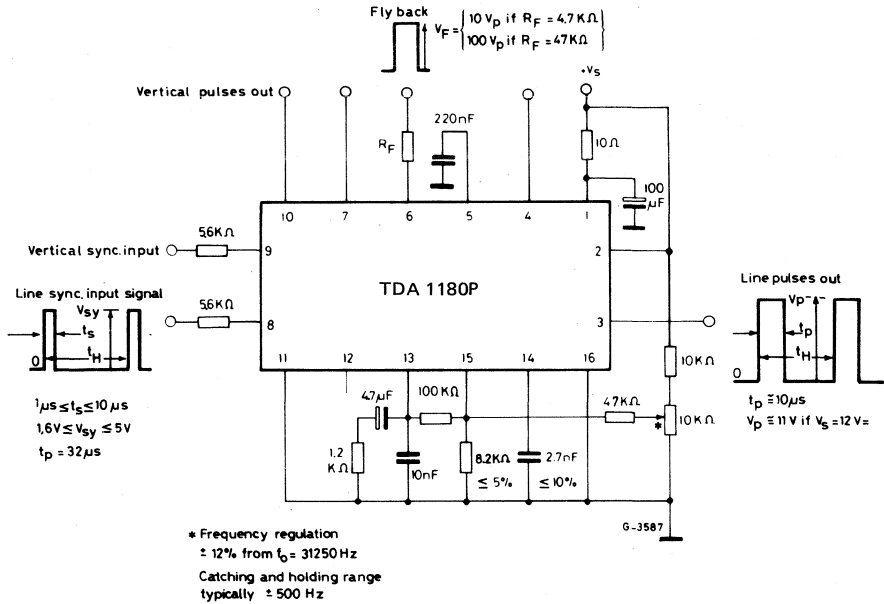


Fig. 9 - Application circuit for Darlington output stage



TDA 1180P

Fig. 10 - Application circuit for high definition TV Monitors; $f_M = 31250$ Hz; sync input signal TTL compatible.



COMPLETE TV SOUND CHANNEL

The TDA 1190 is a monolithic integrated circuit in a 12-lead quad in-line plastic package. It performs all the functions needed for the TV sound channel:

- IF limiter-amplifier
- Active low-pass filter
- FM detector
- DC volume control
- AF preamplifier
- AF output stage

The TDA 1190 can give an output power of 4.2W (d = 10%) into a 16Ω load at $V_s = 24V$, or 1.5W (d = 10%) into an 8Ω load at $V_s = 12V$. This performance, together with the FM-IF section characteristics of high sensitivity, high AM rejection and low distortion, enables the device to be used in almost every type of television receivers. The device has no irradiation problems, hence no external screening is needed.

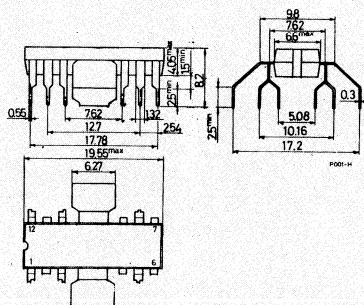
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage (pin 10)	28	V
V_i	Input signal voltage (pin 1)	1	V
I_o	Output peak current (non-repetitive)	2	A
I_o	Output peak current (repetitive)	1.5	A
P_{tot}	Power dissipation: at $T_{tab} = 90^\circ C$	5	W
	at $T_{amb} = 80^\circ C$ (free air)	1	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ C$

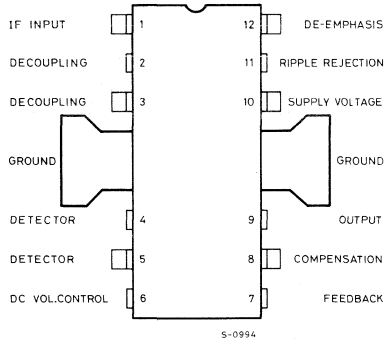
ORDERING NUMBER: TDA 1190

MECHANICAL DATA

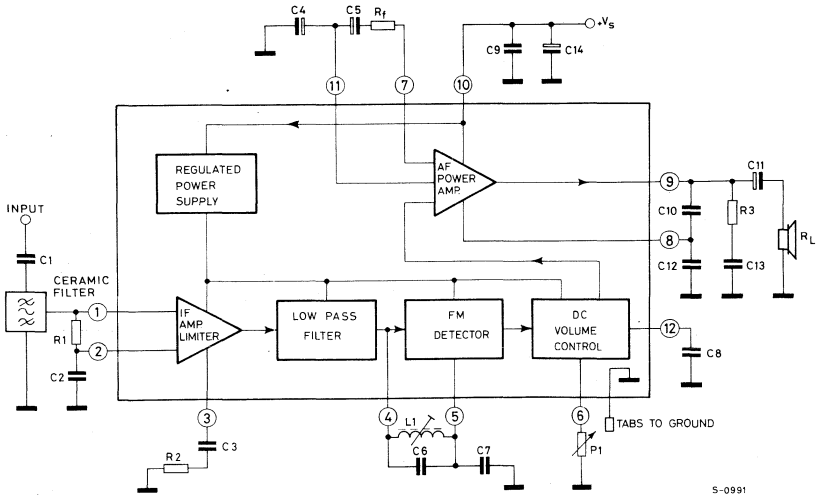
Dimensions in mm



CONNECTION DIAGRAM (top view).

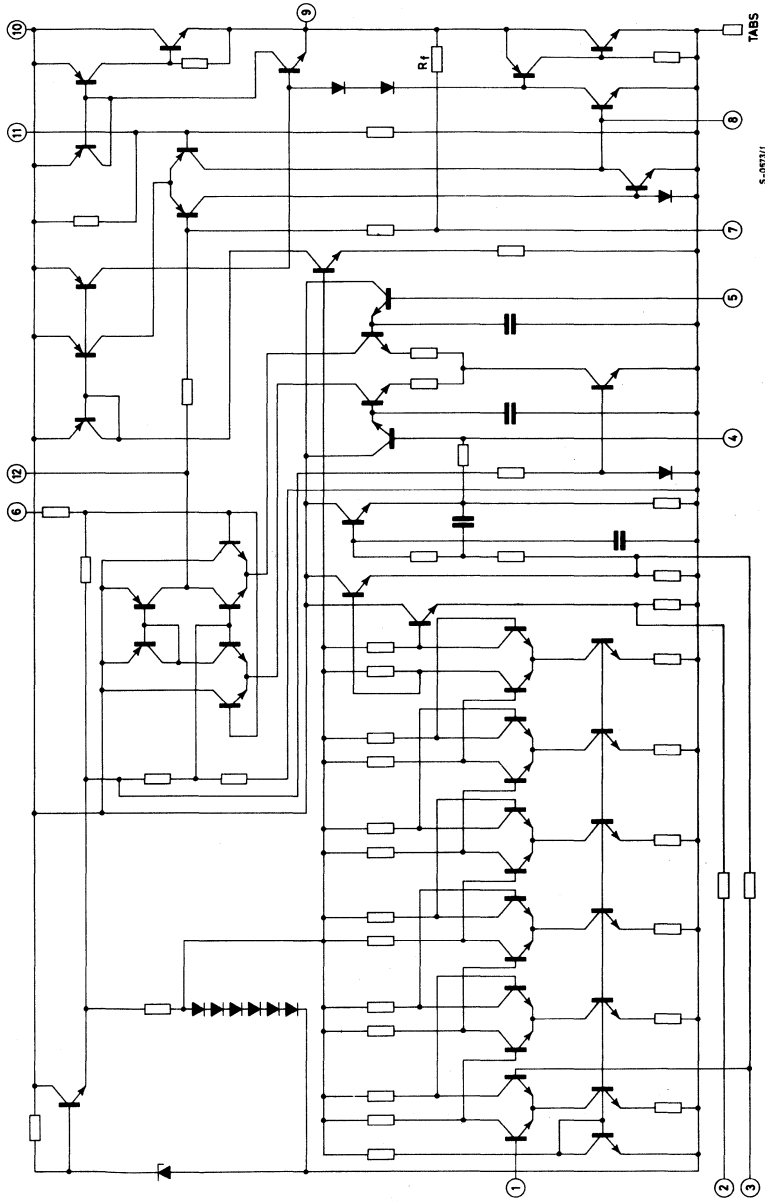


BLOCK DIAGRAM

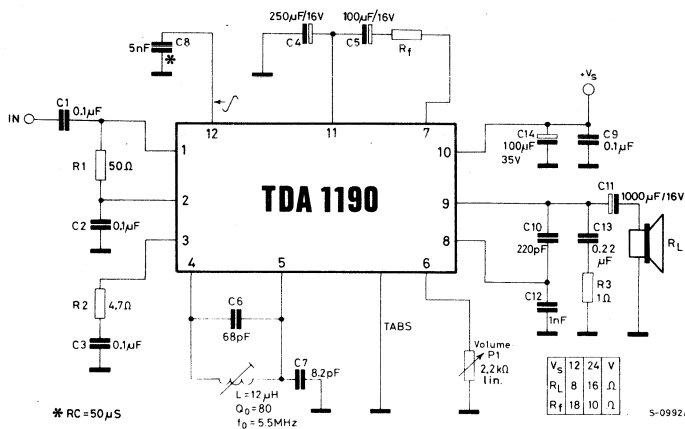


TDA 1190

SCHEMATIC DIAGRAM



TEST CIRCUIT



THERMAL DATA

R _{th j-tab}	Thermal resistance junction-tab	max	12 °C/W
R _{th j-amb}	Thermal resistance junction-ambient	max	70* °C/W

* Obtained with tabs soldered to printed circuit with minimized copper area

ELECTRICAL CHARACTERISTICS

(Refer to the test circuit, V_s = 24V, T_{amb} = 25°C unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V _s	Supply voltage (pin 10)	9		28	V
V _o	Quiescent output voltage (pin 9)	V _s = 24V 11 V _s = 12V 5.5	12 6	13 6.5	V V
I _d	Quiescent drain current	P1 = 2.2 kΩ V _s = 24V V _s = 12V	22 19	35 31	mA mA
P _o	Output power	d = 10% f ₀ = 5.5 MHz f _m = 1 kHz Δf = ± 25 kHz V _s = 24V V _s = 12V	R _L = 16 Ω 4.2 R _L = 8 Ω 1.5		W W

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ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
P_o	Output power $d = 2\%$ $f_o = 5.5 \text{ MHz}$ $f_m = 1 \text{ kHz}$ $\Delta f = \pm 25 \text{ kHz}$ $V_s = 24\text{V}$ $R_L = 16 \Omega$ $V_s = 12\text{V}$ $R_L = 8 \Omega$		3.4 1.35		W W
V_i	Input limiting voltage (-3 dB) at pin 1 $f_o = 5.5 \text{ MHz}$ $f_m = 1 \text{ kHz}$ $\Delta f = \pm 7.5 \text{ kHz}$ $P_1 = 0$		30		μV
d	Distortion $P_o = 50 \text{ mW}$ $f_o = 5.5 \text{ MHz}$ $f_m = 1 \text{ kHz}$ $\Delta f = \pm 7.5 \text{ kHz}$ $V_s = 24\text{V}$ $R_L = 16 \Omega$ $V_s = 12\text{V}$ $R_L = 8 \Omega$		0.55 0.65		% %
B	Frequency response of audio amplifier (-3 dB) $R_L = 16 \Omega$ $C_{10} = 220 \text{ pF}$ $C_{12} = 1000 \text{ pF}$ $P_1 = 2.2 \text{ k}\Omega$ $R_f = 18 \Omega$ $R_f = 10 \Omega$		50 to 12,000 50 to 9,100		Hz Hz
V_o	Recovered audio voltage (pin 12) $V_i \geq 1 \text{ mV}$ $f_o = 5.5 \text{ MHz}$ $f_m = 1 \text{ kHz}$ $\Delta f = \pm 7.5 \text{ kHz}$ $P_1 = 0$		60		mV
AMR	Amplitude modulation rejection $V_i \geq 1 \text{ mV}$ $f_o = 5.5 \text{ MHz}$ $f_m = 1 \text{ kHz}$ $\Delta f = \pm 50 \text{ kHz}$ $m = 0.3$		55		dB
$\frac{S+N}{N}$	Signal to noise ratio $V_i \geq 10 \text{ mV}$ $f_o = 5.5 \text{ MHz}$ $V_o = 4\text{V}$ $f_m = 1 \text{ kHz}$ $\Delta f = \pm 50 \text{ MHz}$		70		dB
R_f	Internal feedback resistance (pins 7 and 9)	3.5	5	6.5	$\text{k}\Omega$
R_i	Input resistance (pin 1) $V_i = 1 \text{ mV}$ $f_o = 5.5 \text{ MHz}$		30		$\text{K}\Omega$
C_i	Input capacitance (pin 1)		5		pF
SVR	Supply voltage rejection $R_L = 16 \Omega$ $f_{\text{ripple}} = 100 \text{ Hz}$ $P_1 = 2.2 \text{ k}\Omega$		46		dB
A	DC volume control attenuation $P_1 = 2.2 \text{ k}\Omega$		90		dB

Fig. 1 - Relative audio output voltage and output noise vs. input signal.

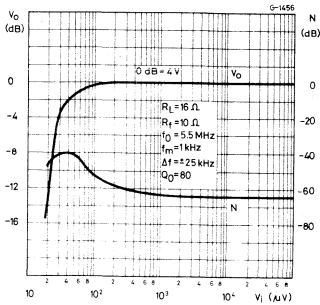


Fig. 2 - Output voltage attenuation vs. DC volume control resistance.

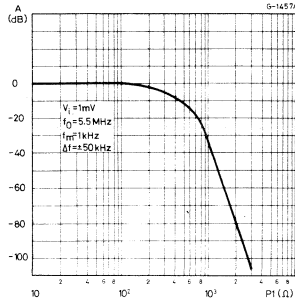


Fig. 3 - Amplitude modulation rejection vs. input signal.

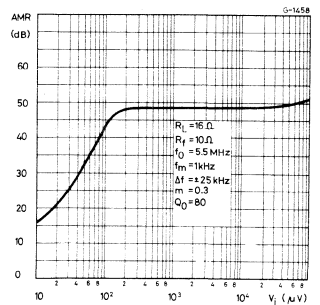


Fig. 4 - ΔAMR vs. tuning frequency change.

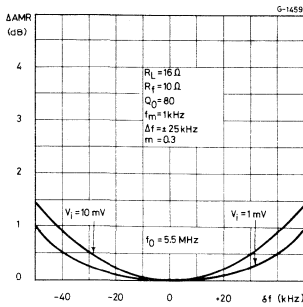


Fig. 5 - Recovered audio voltage vs. unloaded Q factor of the detector coil.

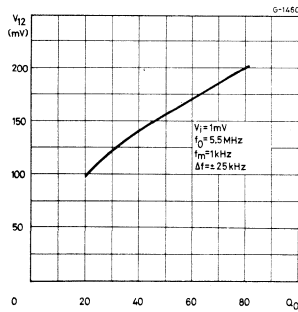


Fig. 6 - Distortion vs. output power.

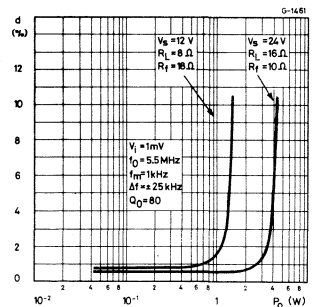


Fig. 7 - Distortion vs. frequency deviation.

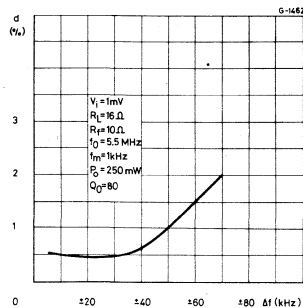


Fig. 8 - Distortion vs. tuning frequency change.

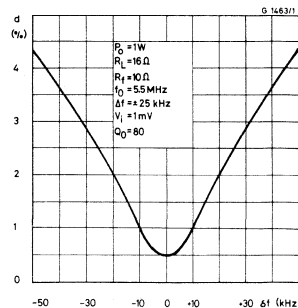
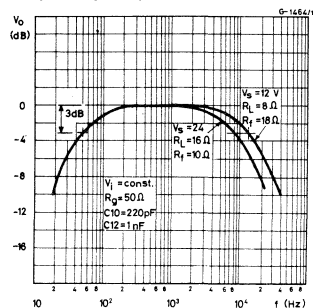


Fig. 9 - Audio amplifier frequency response.



TDA 1190

Fig. 10 - Supply voltage ripple rejection vs. ripple frequency

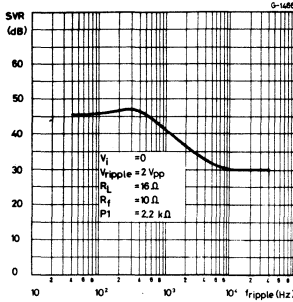


Fig. 11 - Supply voltage ripple rejection vs. volume control attenuation

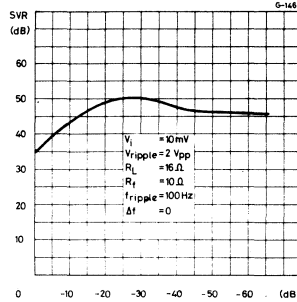


Fig. 12 - Output power vs. supply voltage

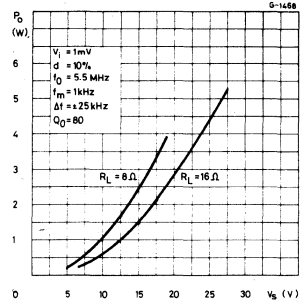


Fig. 13 - Maximum power dissipation vs. supply voltage (sine wave operation)

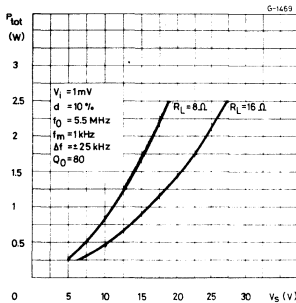


Fig. 14 - Power dissipation and efficiency vs. output power

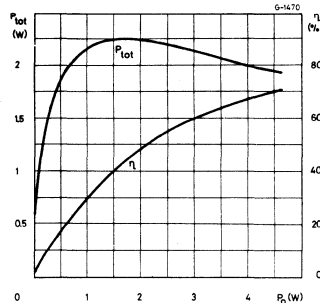
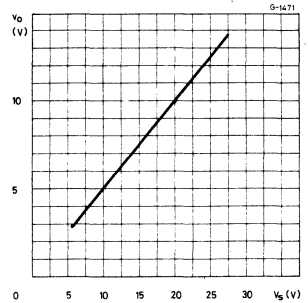


Fig. 15 - Quiescent output voltage (pin 9) vs. supply voltage



APPLICATION INFORMATION

The electrical characteristics of the TDA 1190 remain almost constant over the frequency range of 4.5 to 6 MHz, therefore it can be used in all television standards (FM mod.). The TDA 1190 has a high input impedance, so it can function with a ceramic filter or with a tuned circuit that provide the necessary input selectivity.

The value of the resistor connected to pin 7, determines the AC gain of the audio frequency amplifier. This enables the desired gain to be selected in relation to the frequency deviation at which the output stage of the AF amplifier must enter into clipping.

The capacitor connected between pins 9 and 8 determines the upper cut-off frequency of the audio band.

The capacitor connected between pin 12 and ground, together with the internal resistor of 10 k Ω , forms the de-emphasis network. The Boucherot cell eliminates the high frequency oscillations caused by the inductive load and the wires connecting the loudspeaker.

APPLICATION INFORMATION (continued)

Fig. 16 - Typical application circuit

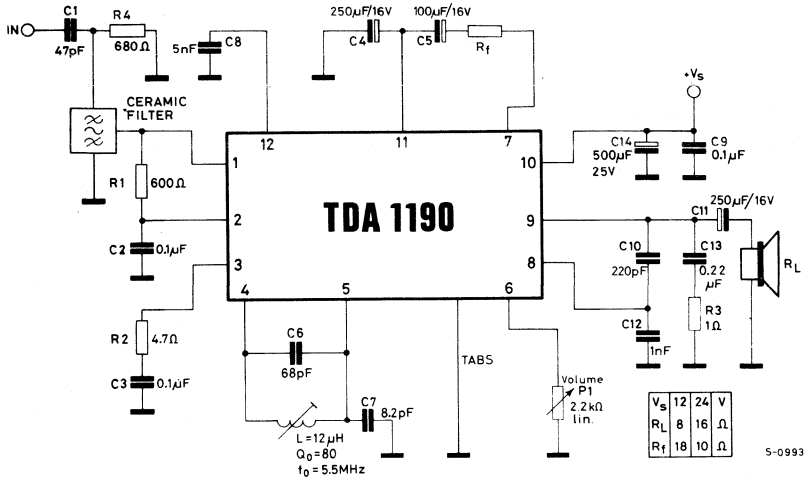
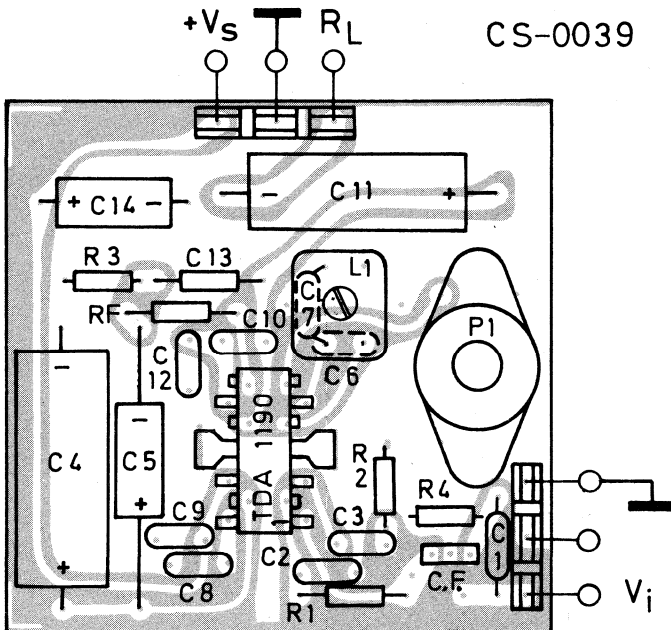


Fig. 17 - P.C. board and component layout of the circuit shown in fig. 16 (1:1 scale)



TDA 1190

MOUNTING INSTRUCTION

The $R_{th\ j-amb}$ of the TDA 1190 can be reduced by soldering the tabs to a suitable copper area of the printed circuit board (Fig. 18) or to an external heatsink (Fig. 19).

The diagram of figure 20 shows the maximum dissippable power P_{tot} and the $R_{th\ j-amb}$ as a function of the side "l" of two equal square copper areas having a thickness of $35\ \mu$ (1.4 mils).

During soldering the tab temperature must not exceed $260\ ^\circ\text{C}$ and the soldering time must not be longer than 12 seconds.

The external heatsink or printed circuit copper area must be connected to electrical ground.

Fig. 18 - Exempler of P.C. board copper area which is used as heatsink

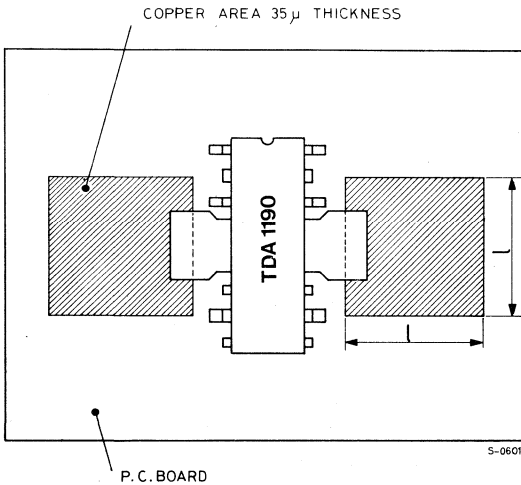


Fig. 19 - External heatsink mounting example

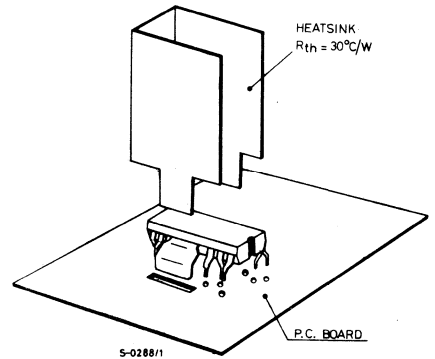


Fig. 20 - Maximum dissippable power and junction to ambient thermal resistance vs. side "l"

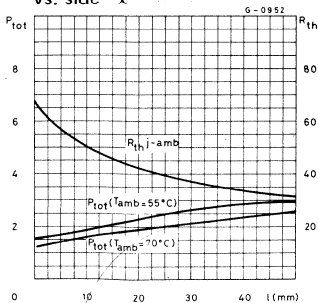
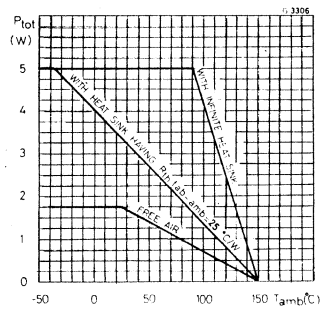


Fig. 21 - Maximum allowable power dissipation vs. ambient temperature



LINEAR INTEGRATED CIRCUIT

COMPLETE TV SOUND CHANNEL

The TDA 1190Z is a monolithic integrated circuit in a 12-lead quad in-line plastic package. It performs all the functions needed for the TV sound channel:

- IF limiter-amplifier
- Active low-pass filter
- FM detector
- DC volume control
- AF preamplifier
- AF output stage

The TDA 1190Z can give an output power of 4.2W ($d = 10\%$) into a 16Ω load at $V_s = 24V$, or 1.5W ($d = 10\%$) into an 8Ω load at $V_s = 12V$. This performance, together with the FM-IF section characteristics of high sensitivity, high AM rejection and low distortion, enables the device to be used in almost every type of television receivers.

The device has no irradiation problems, hence no external screening is needed.

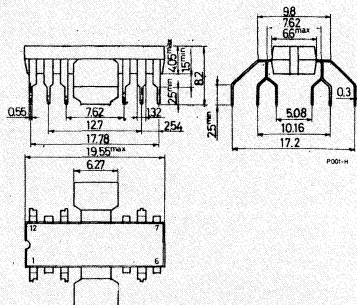
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage (pin 10)	28	V
V_i	Input signal voltage (pin 1)	1	V
I_o	Output peak current (non-repetitive)	2	A
I_o	Output peak current (repetitive)	1.5	A
P_{tot}	Power dissipation: at $T_{tab} = 90^\circ C$	5	W
	at $T_{amb} = 80^\circ$ (free air)	1	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ C$

ORDERING NUMBER: TDA 1190Z

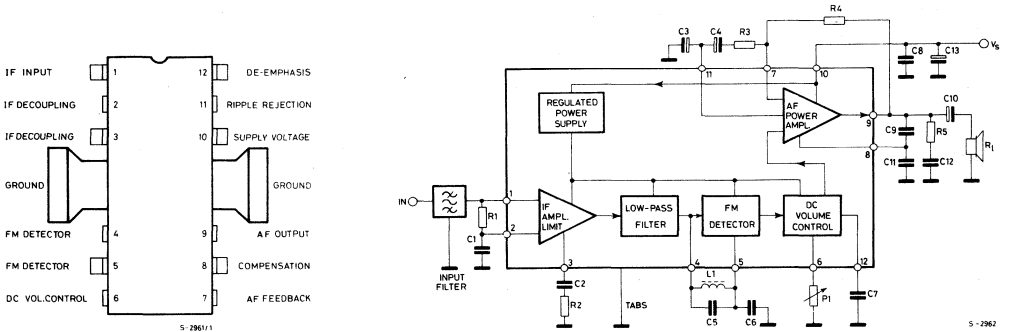
MECHANICAL DATA

Dimensions in mm

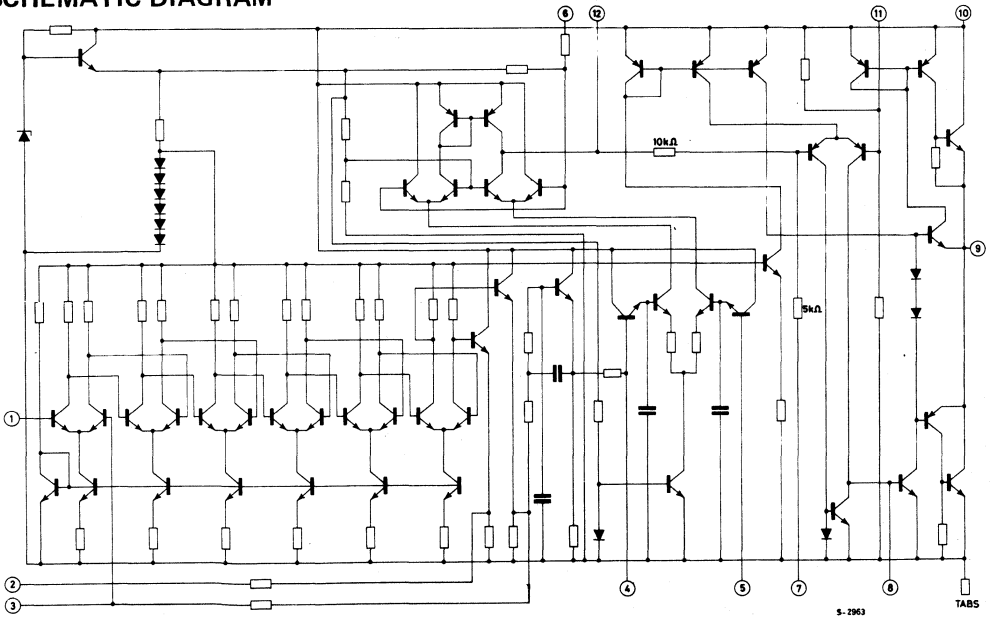


TDA 1190Z

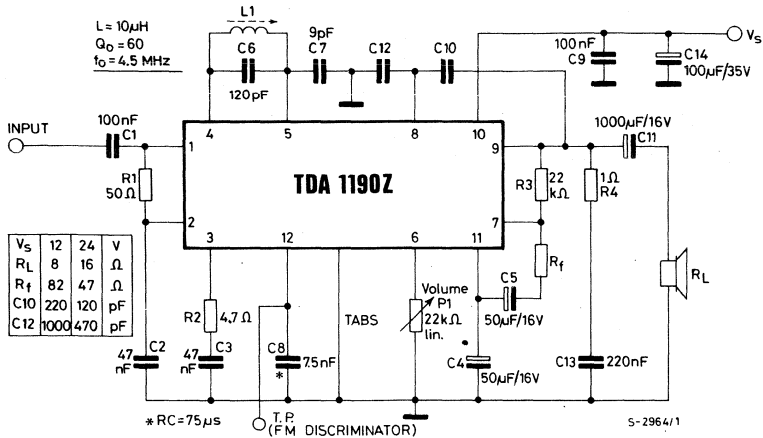
CONNECTION AND BLOCK DIAGRAM (top view)



SCHEMATIC DIAGRAM



TEST CIRCUIT



THERMAL DATA

$R_{th\ j-tab}$	Thermal resistance junction-tab	max.	12	°C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max.	70*	°C/W

* Obtained with tabs soldered to printed circuit with minimized copper area.

ELECTRICAL CHARACTERISTICS

(Refer to the test circuit, $V_s = 24V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s	Supply voltage (pin 10)	9		28	V
V_o	Quiescent output voltage (pin 9)	$V_s = 24V$ 11 $V_s = 12V$ 5.1	12 6	13 6.9	V V
I_d	Quiescent drain current	$P_1 = 22\ K\Omega$ $V_s = 24V$ 11 $V_s = 12V$	22 19	45 40	mA mA
P_o	Output power	$d = 10\%$ $f_o = 4.5\ MHz$ $V_s = 24V$ $V_s = 12V$	$f_m = 400\ Hz$ $\Delta f = \pm 25\ kHz$ $R_L = 16\ \Omega$ 4.2 $R_L = 8\ \Omega$ 1.5		W W

TDA 1190Z

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
P_o Output power	$d = 2\%$ $f_o = 4.5 \text{ MHz}$ $V_s = 24\text{V}$ $V_s = 12\text{V}$ $f_m = 400 \text{ Hz}$ $\Delta f = \pm 25 \text{ kHz}$ $R_L = 16\Omega$ $R_L = 8\Omega$		3.5 1.4		W W
V_i Input limiting voltage (-3 dB) at pin 1	$f_o = 4.5 \text{ MHz}$ $f_m = 400 \text{ Hz}$ $P_1 = 0$ $\Delta f = \pm 7.5 \text{ kHz}$		40	100	μV
d Distortion	$P_o = 50 \text{ mW}$ $f_o = 4.5 \text{ MHz}$ $V_s = 24\text{V}$ $V_s = 12\text{V}$ $f_m = 400 \text{ Hz}$ $\Delta f = \pm 7.5 \text{ kHz}$ $R_L = 16\Omega$ $R_L = 8\Omega$		0.75 1		% %
B Frequency response of audio amplifier (-3 dB)	$R_L = 16\Omega$ $C_{12} = 470 \text{ pF}$ $R_f = 82\Omega$ $R_f = 47\Omega$ $C_{10} = 120 \text{ pF}$ $P_1 = 22 \text{ k}\Omega$		70 to 12 000 70 to 7 000		Hz Hz
V_o Recovered audio voltage (PIN. 12)	$V_i \geq 1 \text{ mV}$ $f_m = 400 \text{ Hz}$ $P_1 = 0$ $f_o = 4.5 \text{ MHz}$ $\Delta f = \pm 7.5 \text{ kHz}$		120		mV
AMR Amplitude modulation rejection	$V_i \geq 1 \text{ mV}$ $f_m = 400 \text{ Hz}$ $m = 0.3$ $f_o = 4.5 \text{ MHz}$ $\Delta f = \pm 25 \text{ kHz}$		55		dB
$\frac{S+N}{N}$ Signal to noise ratio	$V_i \geq 1 \text{ mV}$ $f_o = 4.5 \text{ MHz}$ $\Delta f = \pm 25 \text{ kHz}$ $V_o = 4 \text{ V}$ $f_m = 400 \text{ Hz}$	50	65		dB
R_f External feedback resistance (between pins 7 and 9)				25	k Ω
R_i Input resistance (pin 1)	$V_i = 1 \text{ mV}$		30		k Ω
C_i Input capacitance (pin 1)	$f_o = 4.5 \text{ MHz}$		5		pF
SVR Supply voltage rejection	$R_L = 16\Omega$ $f_{\text{ripple}} = 120 \text{ Hz}$ $P_1 = 22 \text{ k}\Omega$		46		dB
A DC volume control attenuation	$P_1 = 12 \text{ k}\Omega$		90		dB

Fig. 1 - Relative audio output voltage and output noise vs. input signal

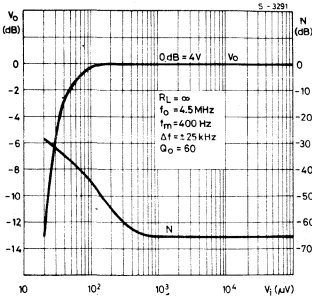


Fig. 2 - Output voltage attenuation vs. DC volume control resistance

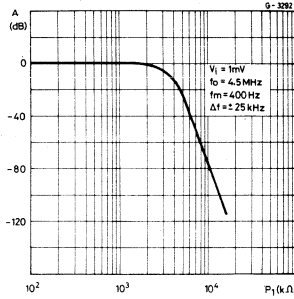


Fig. 3 - Amplitude modulation rejection vs. input signal

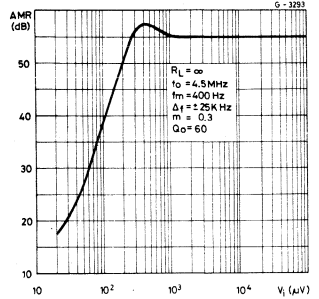


Fig. 4 - ΔAMR vs. tuning frequency change

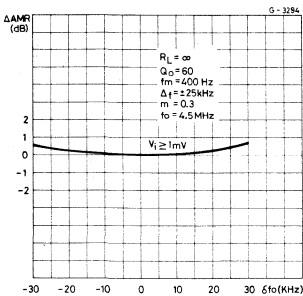


Fig. 5 - Recovered audio voltage vs. unloaded Q factor of the detector coil

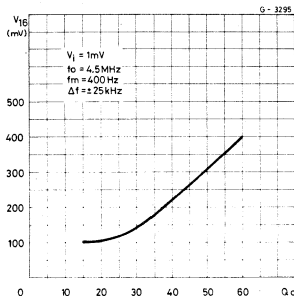


Fig. 6 - Distortion vs. output power

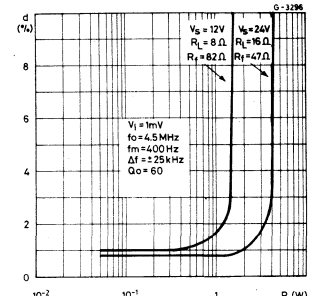


Fig. 7 - Distortion vs. frequency deviation

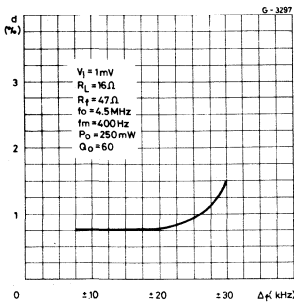


Fig. 8 - Distortion vs. tuning frequency change

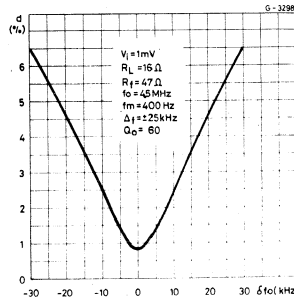
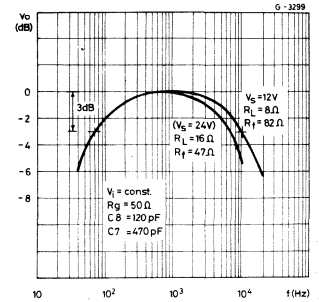


Fig. 9 - Audio amplifier frequency response



TDA 1190Z

Fig. 10 - Supply voltage ripple rejection vs. ripple frequency

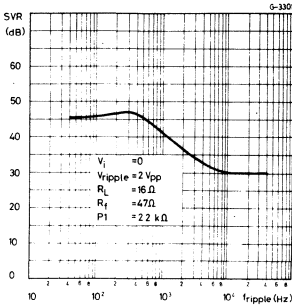


Fig. 11 - Supply voltage ripple rejection vs. volume control attenuation

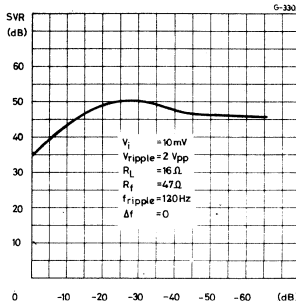


Fig. 12 - Output power vs. supply voltage

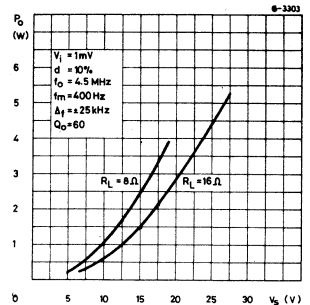


Fig. 13 - Maximum power dissipation vs. supply voltage (sine wave operation)

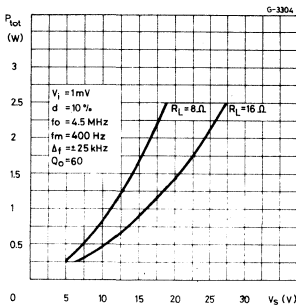


Fig. 14 - Power dissipation and efficiency vs. output power

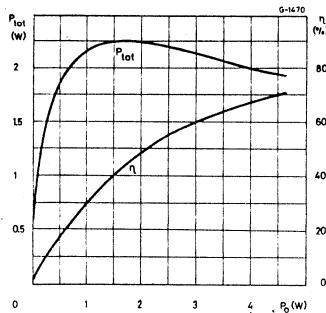
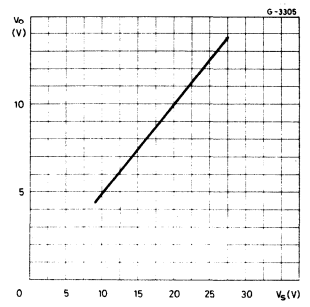


Fig. 15 - Quiescent output voltage (pin 9) vs. supply voltage



APPLICATION INFORMATION

The electrical characteristics of the TDA 1190Z remain almost constant over the frequency range of 4.5 to 6 MHz, therefore it can be used in all television standard (FM mod.). The TDA 1190Z has a high input impedance, so it can function with a ceramic filter or with a tuned circuit that provide the necessary input selectivity.

The value of the resistors connected to pin 7, determine the AC gain of the audio frequency amplifier. This enables the desired gain to be selected in relation to the frequency deviation at which the output stage of the AF amplifier must enter into clipping.

The capacitor connected between pins 9 and 8 determines the upper cut-off frequency of the audio band. If larger bandwidth is required C_{10} , C_{12} must be reduced keeping C_{12}/C_{10} as in Fig. 16.

The capacitor connected between pin 12 and ground, together with the internal resistor of 10 K Ω , forms the de-emphasis network. The Boucherot cell eliminates the high frequency oscillations caused by inductive load and the wires connecting the loudspeaker.

APPLICATION INFORMATION (continued)

Fig. 16 - Typical application circuit

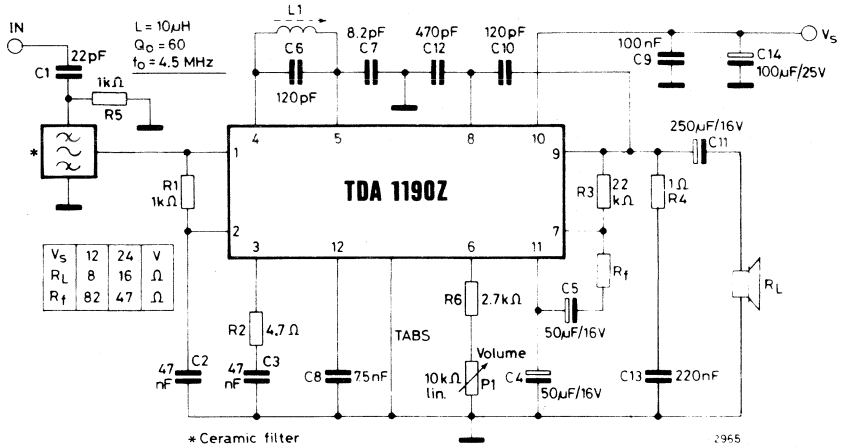
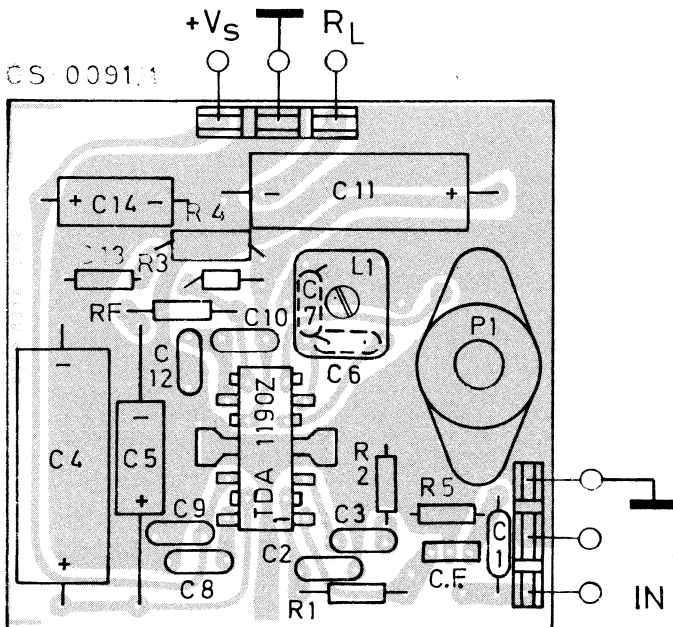


Fig. 17 - P.C. board and component layout of the circuit shown in Fig. 16



TDA 1190Z

MOUNTING INSTRUCTION

The $R_{thj-amb}$ of the TDA 1190Z can be reduced by soldering the tabs to a suitable copper area of the printed circuit board (Fig. 18) or to an external heatsink (Fig. 19).

The diagram of figure 20 shows the maximum dissippable power P_{tot} and the $R_{thj-amb}$ as a function of the side "l" of two equal square copper areas having a thickness of 35μ (1.4 mils).

During soldering the tab temperature must not exceed 260°C and the soldering time must not be longer than 12 seconds.

The external heatsink or printed circuit copper area must be connected to electrical ground.

Fig. 18 - Example of P.C. board copper area which is used as heatsink

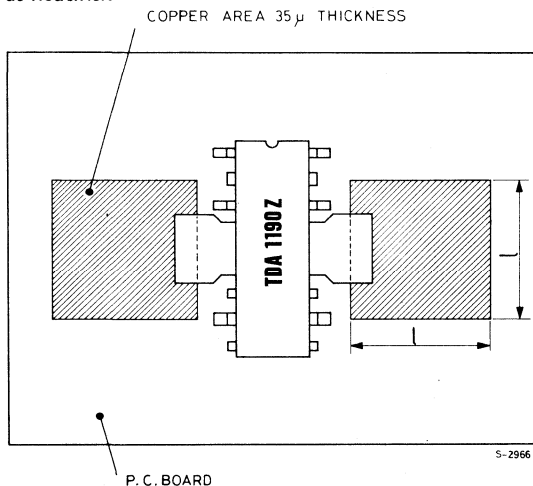


Fig. 19 - External heatsink mounting example

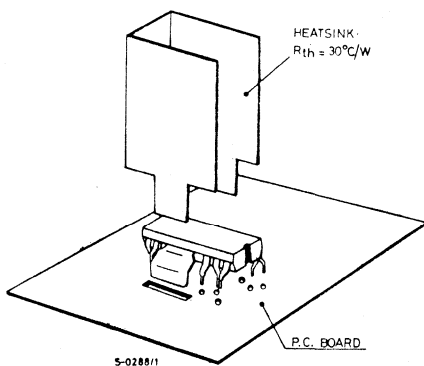


Fig. 20 - Maximum dissippable power and junction to ambient thermal resistance vs. side "l"

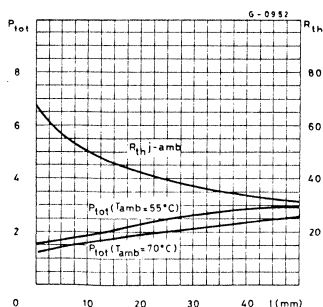
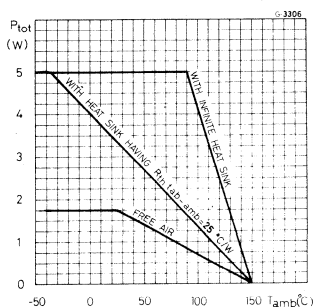


Fig. 21 - Maximum allowable power dissipation vs. ambient temperature



LINEAR INTEGRATED CIRCUIT

FM-IF RADIO SYSTEM

- HIGH LIMITING SENSITIVITY
- HIGH AMR
- HIGH RECOVERED AUDIO
- GOOD CAPTURE RATIO
- LOW DISTORTION
- MUTING CAPABILITY

The TDA 1200 is a monolithic integrated circuit in a 16-lead dual in-line plastic package. It provides a complete subsystem for amplification of FM signals.

The functions incorporated are:

- FM amplification and detection
- Interchannel controlled muting
- AFC and delayed AGC for FM tuner
- Switching of stereo decoder
- Driving of a field strength meter

The TDA 1200 can be used for FM-IF amplifier application in HI-FI, car-radios and communication receivers.

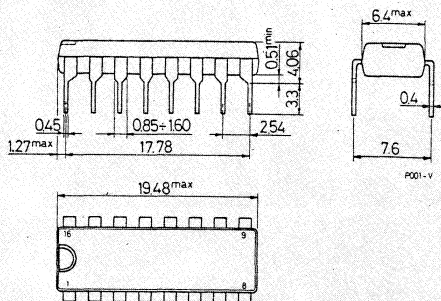
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	16	V
I_o	Output current (from pin 15)	2	mA
P_{tot}	Total power dissipation at $T_{amb} \leq 70^\circ\text{C}$	800	mW
T_{stg}	Storage temperature	-55 to 150	$^\circ\text{C}$
T_{op}	Operating temperature	-25 to 70	$^\circ\text{C}$

ORDERING NUMBER: TDA 1200

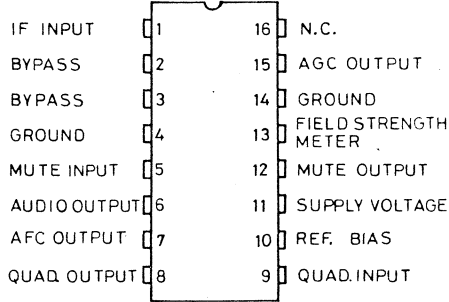
MECHANICAL DATA

Dimensions in mm



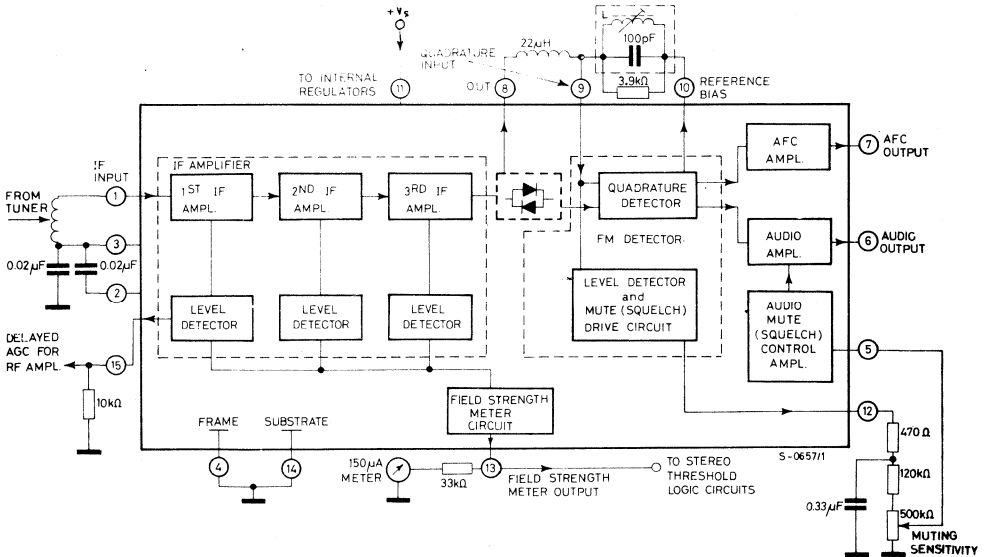
TDA 1200

CONNECTION DIAGRAM (top view)

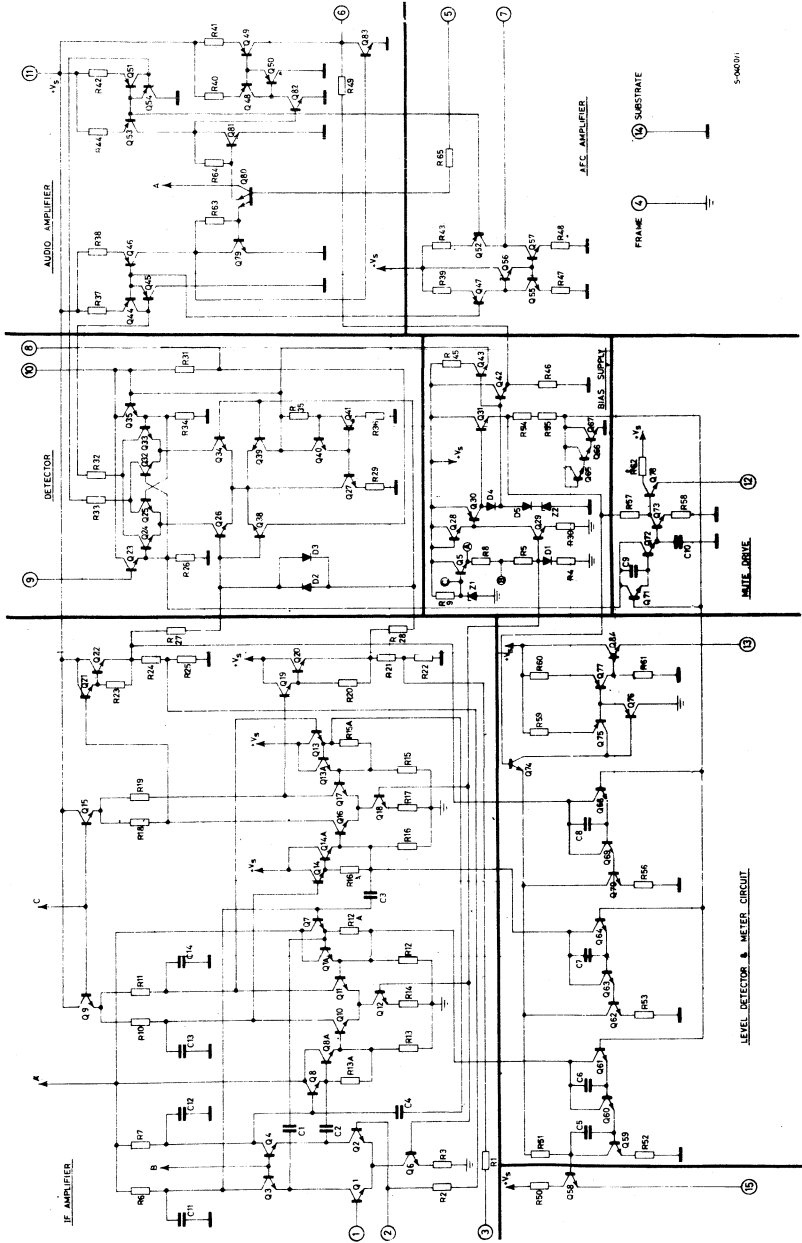


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BLOCK DIAGRAM

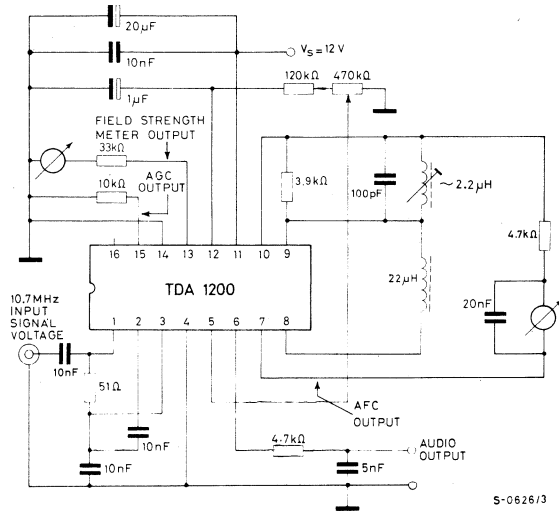


SCHEMATIC DIAGRAM



TDA 1200

TEST CIRCUIT



THERMAL DATA

$R_{th j-amb}$ Thermal resistance junction-ambient

max 100 °C/W

ELECTRICAL CHARACTERISTICS

(Refer to the test circuit; $V_s = 12\text{ V}$, $T_{amb} = 25^\circ\text{C}$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
-----------	-----------------	------	------	------	------

DC CHARACTERISTICS

I_s	Supply current		23		mA
V_1	Voltage at the IF amplifier input		1.9		V
V_2, V_3	Voltage at the input bypassing		1.9		V
V_6	Voltage at the audio output		5.6		V
V_{10}	Reference bias voltage		5.6		V

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
AC CHARACTERISTICS					
$V_{i(\text{threshold})}$ Input limiting voltage (-3 dB) at pin 1	$f_0 = 10.7 \text{ MHz}$ $f_m = 1 \text{ kHz}$ $\Delta f = \pm 25 \text{ kHz}$		12		μV
V_o Recovered audio voltage (pin 6)	$V_i \geq 50 \mu\text{V}$ $f_0 = 10.7 \text{ MHz}$ $f_m = 1 \text{ kHz}$ $\Delta T = \pm 25 \text{ kHz}$		140		mV
d Distortion	$V_i \geq 1 \text{ mV}$ $f_0 = 10.7 \text{ MHz}$ $f_m = 1 \text{ kHz}$ $\Delta f = \pm 75 \text{ kHz}$		0.5		%
$\frac{S+N}{N}$ Signal to noise ratio			60		dB
AMR Amplitude modulation rejection	$V_i \geq 1 \text{ mV}$ $f_0 = 10.7 \text{ MHz}$ $f_m = 1 \text{ kHz}$ $\Delta f = \pm 25 \text{ kHz}$ $m = 0.3$		40		dB
V_i Input voltage for delayed AGC action (pin 1)			10		mV
$\frac{\Delta V_{15}}{\Delta V_i}$ AGC control slope	$V_i \geq 10 \text{ mV}$ $f_0 = 10.7 \text{ MHz}$		40		dB
$\frac{\Delta I_7}{\delta f}$ AFC control slope			1		$\frac{\mu\text{A}}{\text{kHz}}$
$\frac{\Delta V_{13}}{\Delta V_i}$ Field strength meter output slope			42		dB
V_{13} Field strength meter output sensitivity	$V_i = 1 \text{ mV}$ $f_0 = 10.7 \text{ MHz}$		1.7		V

TDA 1200

Fig. 1 – Recovered audio and noise versus input voltage

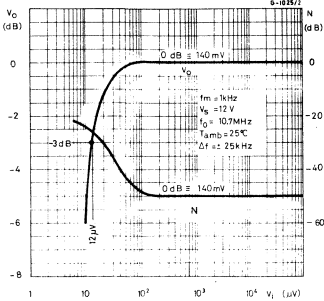


Fig. 2 – Capture ratio versus input voltage

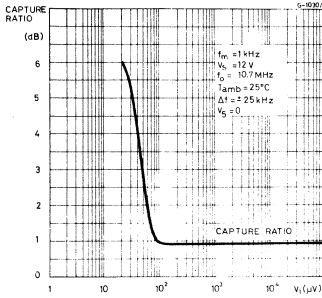


Fig. 3 – AGC (V_{15}) and field strength meter output (V_{13}) versus input signal

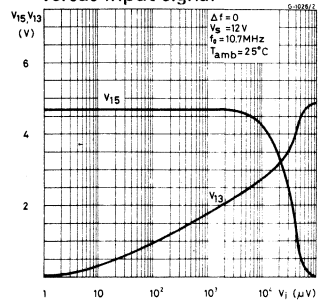


Fig. 4 – AFC output current versus change-in tuning frequency

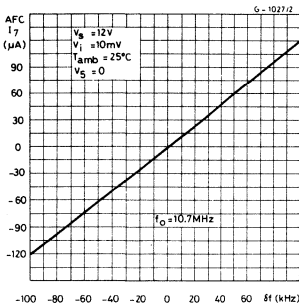


Fig. 5 – Amplitude modulation rejection versus input signal

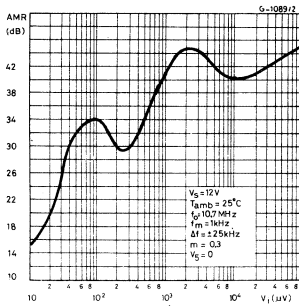


Fig. 6 – AMR (relative to the value of $f_0 = 10.7$ MHz) versus change-in tuning frequency

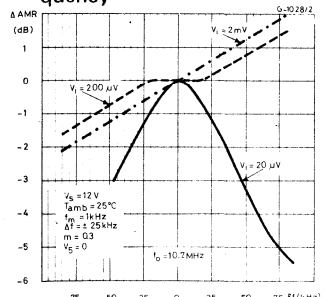
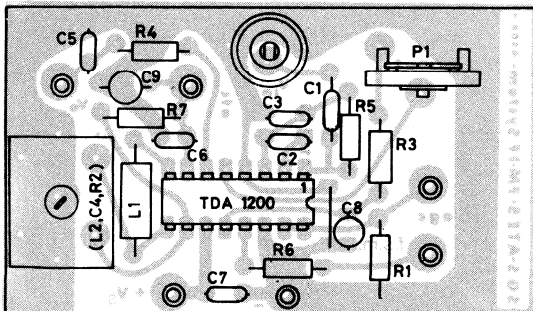
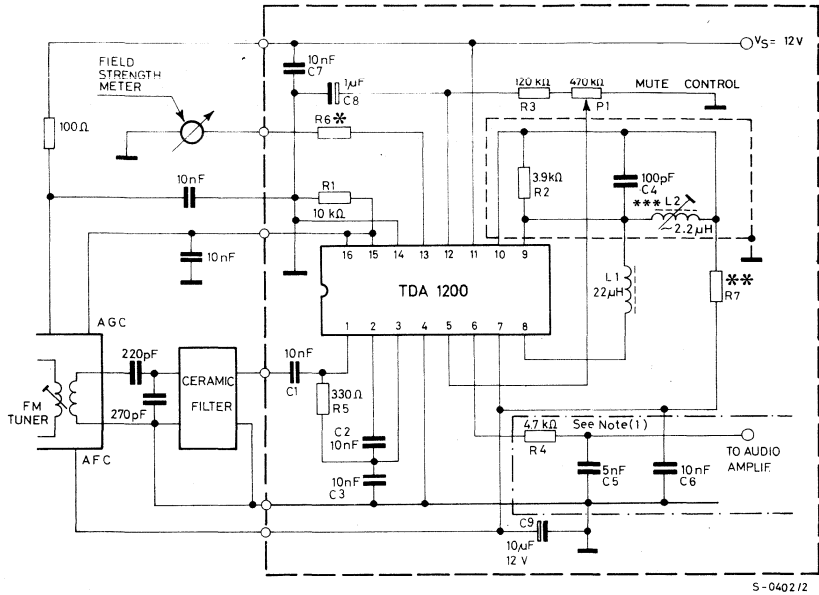


Fig. 7 – PC board and component layout of the circuit on next page (1:1 scale).

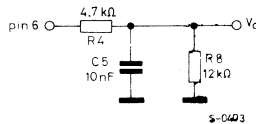


CS-0024

Fig. 8 - Typical application circuit



NOTES: (1) When V_s is less than 12V, a resistor R8 = 12 k Ω must be connected between audio output and ground, and the integrator capacitor C5 must be changed to 10 nF, as follows:



- * Dependent on field strength meter sensitivity.
- ** Dependent on the tuner's AFC circuit.
- *** L2 tunes with 100 pF at 10.7 MHz ($Q_0 = 75$).

AM-FM RADIORECEIVER SYSTEM

The TDA 1220A is a monolithic integrated circuit in a 16-lead dual in-line plastic package designed for use in portable and home AM-FM radio sets as well as in industrial communication systems.

The functions incorporated are:

AM SECTION

- Preamplifier and double balanced mixer
- Local oscillator
- IF amplifier with internal AGC
- Balanced detector
- AF preamplifier

FM SECTION

- IF amplifier
- Quadrature detector
- AF preamplifier

The TDA 1220A is suitable for all AM and FM broadcasting bands and it features:

- Very low noise
- High sensitivity
- Wide supply voltage range ($2.8 \div 16V$)
- Low quiescent current (9 mA)
- Very simple DC switching of AM-FM sections
- Minimized number of external components
- Local oscillator up to 30 MHz

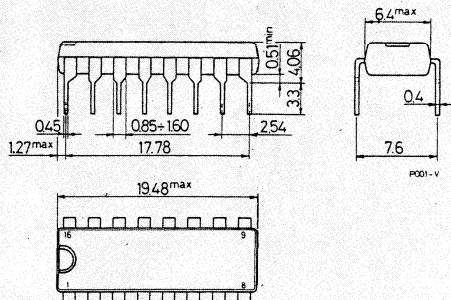
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	16	V
P_{tot}	Total power dissipation at $T_{amb} \leq 110^\circ C$	400	mW
T_{op}	Operating temperature	-20 to 85	$^\circ C$
T_{stg}, T_j	Storage and junction temperature	-55 to 150	$^\circ C$

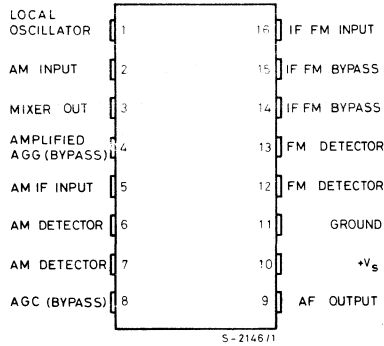
ORDERING NUMBER: TDA 1220A

MECHANICAL DATA

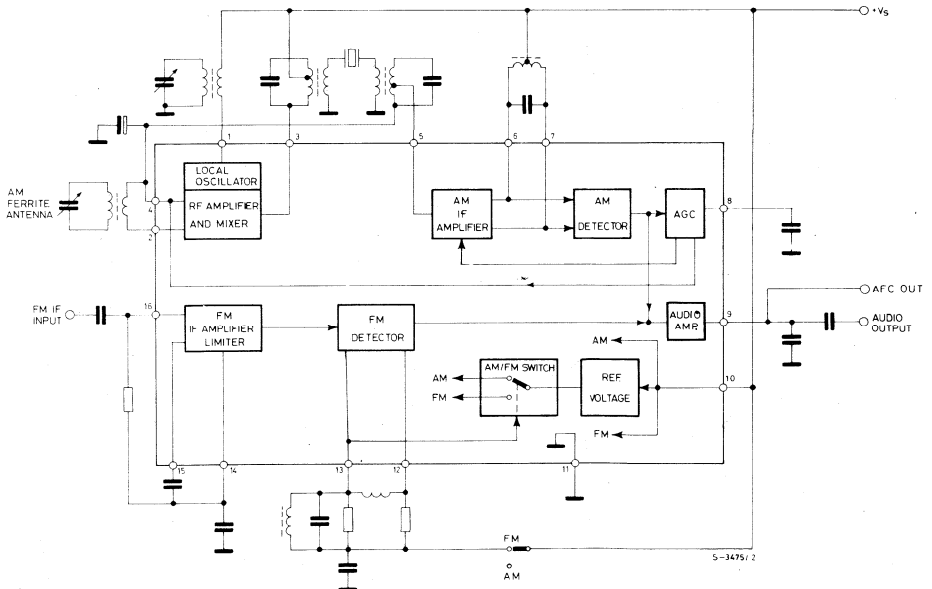
Dimensions in mm



CONNECTION DIAGRAM (top view)

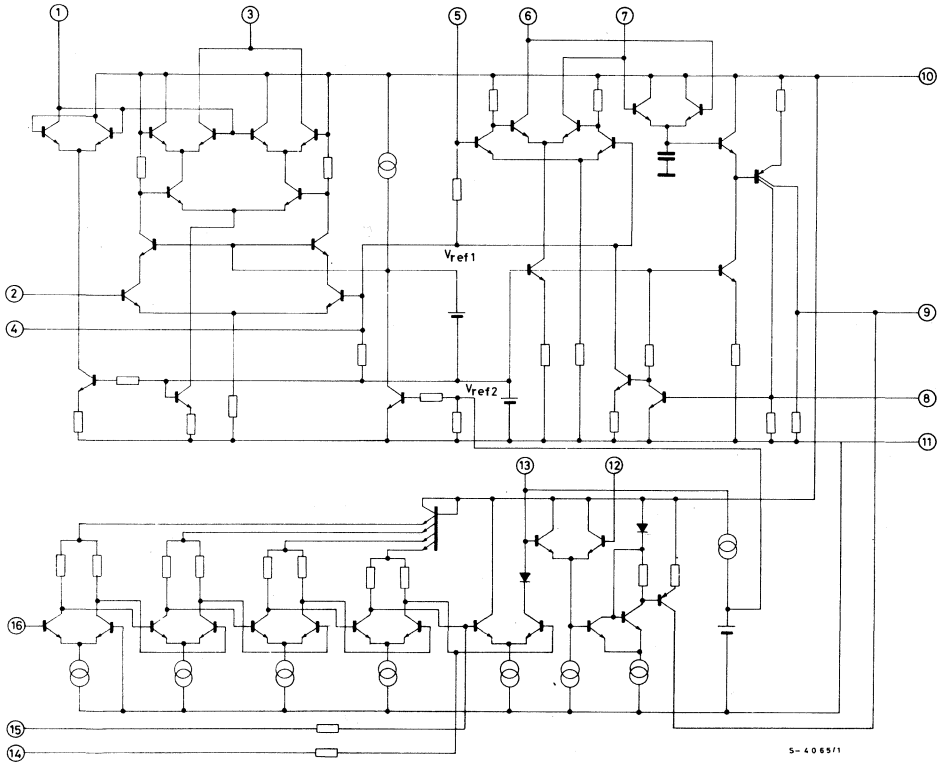


BLOCK DIAGRAM



TDA 1220A

SCHEMATIC DIAGRAM



THERMAL DATA

$R_{th\ j-amb}$ Thermal resistance junction-ambient

max 100 °C/W

ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^{\circ}\text{C}$, $V_s = 9\text{V}$ unless otherwise specified, refer to test circuit)

Parameter	Test condition	Min.	Typ.	Max.	Unit
-----------	----------------	------	------	------	------

DC CHARACTERISTICS

V_s	Supply Voltage		2.8		16	V
I_d	Drain current	AM section		9	15	mA
		FM section		9	15	

AC CHARACTERISTICS

AM SECTION ($f_o = 1\text{ MHz}$; $f_m = 1\text{ KHz}$)							
V_i	Input sensitivity	S/N = 26 dB	$m = 0.3$		12	25	μV
S/N	Ultimate quieting	$V_i = 10\text{ mV}$	$m = 0.3$	50	60		dB
ΔV_i	AGC range	$\Delta V_{out} = 10\text{ dB}$	$m = 0.3$	80			dB
V_o	Recovered audio signal (pin 9)	$V_i = 1\text{ mV}$	$m = 0.3$	40	80	160	mV
d	Distortion	$V_i = 1\text{ mV}$	$m = 0.8$		1	3	%
d	Distortion	$V_i = 1\text{ mV}$	$m = 0.3$		0.4	1	%
V_H	Max input signal handling capability	$m = 0.8$	$d = 10\%$		80		mV
R_i	Input resistance between pins 2 and 4	$m = 0$			7.5		$\text{K}\Omega$
C_i	Input capacitance between pins 2 and 4	$m = 0$			18		pF
R_o	Output resistance (pin 9)				7		$\text{K}\Omega$
FM SECTION ($f_o = 10.7\text{ MHz}$; $f_m = 1\text{ KHz}$)							
V_i	Input limiting voltage	-3 dB limiting point				36	μV
AMR	Amplitude modulation rejection	$\Delta f = \pm 22.5\text{ KHz}$ $V_i = 3\text{ mV}$		35	48		dB
S/N	Ultimate quieting	$\Delta f = \pm 22.5\text{ KHz}$ $V_i = 1\text{ mV}$		55	70		dB
d	Distortion (single tuned)	$\Delta f = \pm 75\text{ KHz}$ $V_i = 1\text{ mV}$			0.7	3	%
d	Distortion (double tuned)	$\Delta f = \pm 22.5\text{ KHz}$ $V_i = 1\text{ mV}$			0.2		
V_o	Recovered audio signal (pin 9)	$\Delta f = \pm 22.5\text{ KHz}$ $V_i = 1\text{ mV}$		40	80	160	mV
R_i	Input resistance between pin 16 and ground	$\Delta f = 0$			6.5		$\text{K}\Omega$
C_i	Input capacitance between pin 16 and ground	$\Delta f = 0$			14		pF
R_o	Output resistance (pin 9)				7		$\text{K}\Omega$

TDA 1220A

TEST CIRCUIT

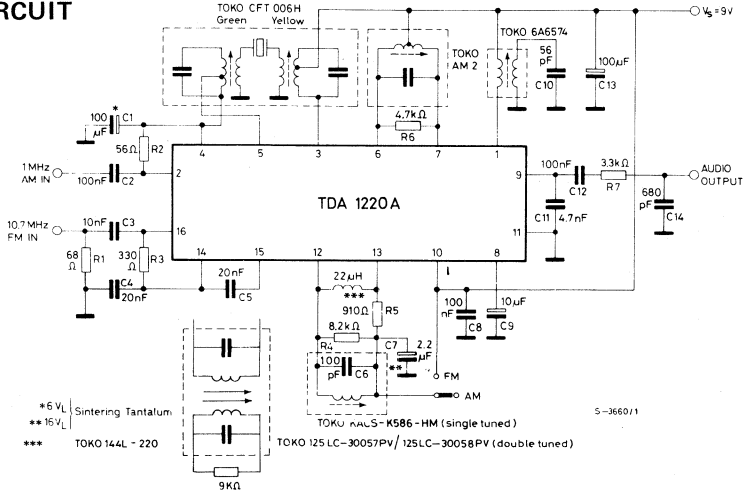


Fig. 1 - PC board and component layout (1 : 1 scale) of the test circuit

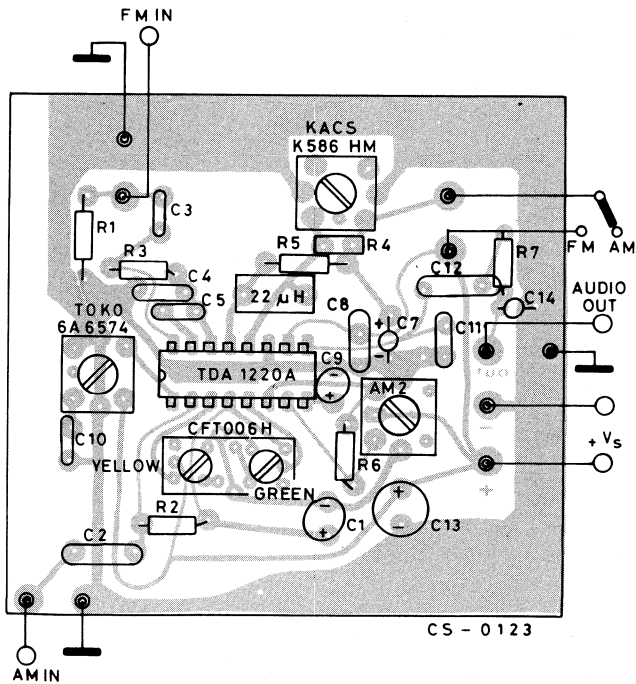


Fig. 2 - Drain current vs. supply voltage.

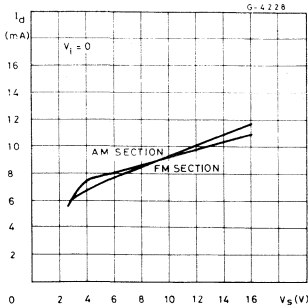


Fig. 3 - Audio output and signal to noise ratio vs. input signal (AM section)

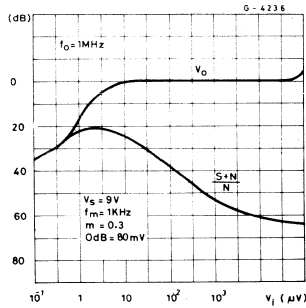


Fig. 4 - Audio output and signal to noise ratio vs. input signal (AM section)

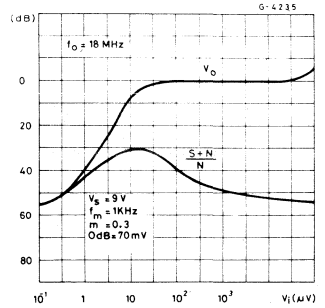


Fig. 5 - Distortion vs. input signal (AM section)

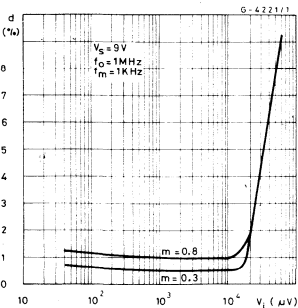


Fig. 6 - Distortion vs. modulation index (AM section)

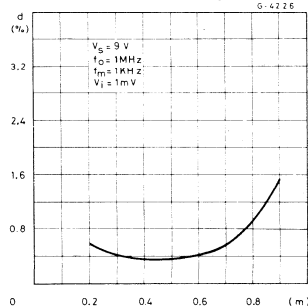


Fig. 7 - Amplified AGC voltage (pin 4) vs. input signal (AM section)

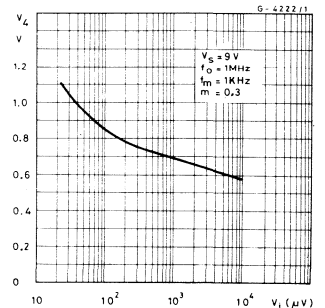


Fig. 8 - Audio output vs. supply voltage with DC level shift resistor (AM section)

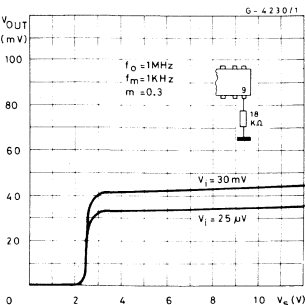


Fig. 9 - Audio output vs. supply voltage (AM section)

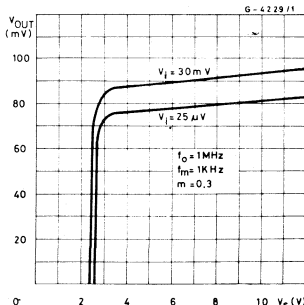
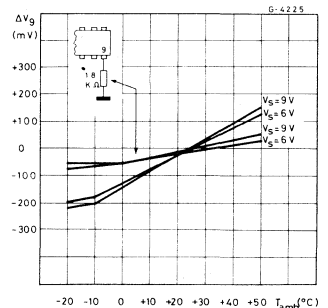


Fig. 10 - Δ DC voltage (pin 9) vs. ambient temperature (FM section)



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Fig. 11 – Audio output and signal to noise ratio vs. input signal (FM section)

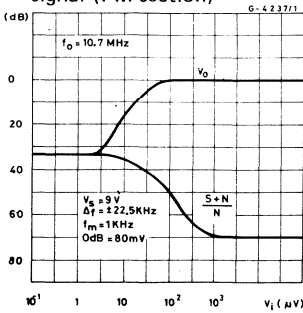


Fig. 12 – Distorsion vs. frequency deviation (FM section)

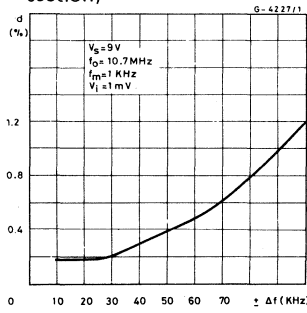


Fig. 13 – Distortion vs. input signal (FM section)

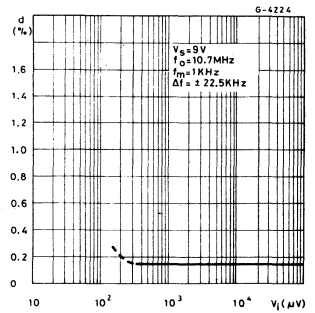


Fig. 14 – Amplitude modulation rejection vs. input signal (FM section)

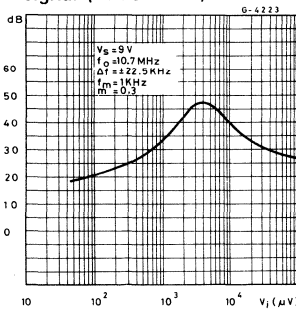


Fig. 15 – Audio output vs. supply voltage (FM section)

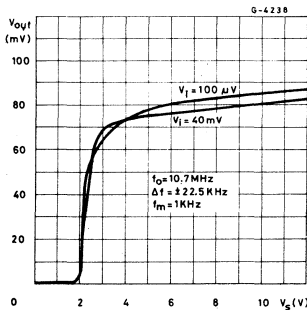


Fig. 16 – Audio output vs. supply voltage with DC level shift resistor (FM section)

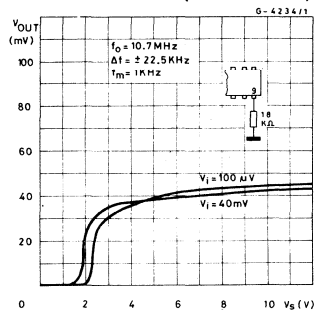


Fig. 17 – Δ DC output voltage (pin 9) vs. frequency shift (FM section)

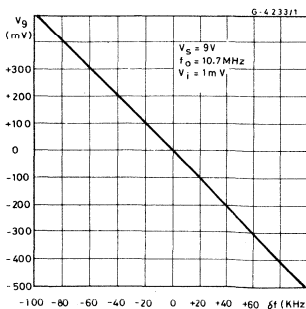


Fig. 18 -- DC output voltage (pin 9) vs. supply voltage (FM section)

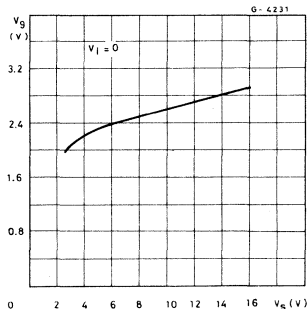
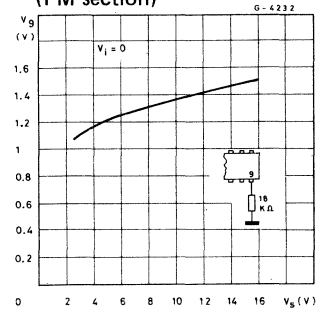


Fig. 19 – DC output voltage (pin 9) with DC level shift resistor vs. supply voltage (FM section)



APPLICATION INFORMATION (continued)

FM Section

IF Amplifier and limiter

The 10.7 MHz IF signal from the ceramic filter is amplified and limited by a chain of four differential stages.

Pin 16 is the amplifier input and has a typical input impedance of $6.5\text{ K}\Omega$ in parallel with 14 pF at 10.7 MHz.

Bias for the first stage is available at pin 14 and provides 100% DC feedback for stable operating conditions. Pin 15 is the second input to the amplifier and is decoupled to pin 14, which is grounded by a 20 nF capacitor.

An RLC network is connected to the amplifier output and gives a 90° phase shift (at the IF centre frequency) between pins 13 and 12. The signal level at pin 13 is about 150 mV rms .

FM Detector

The circuit uses a quadrature detector and the choice of component values is determined by the acceptable level of distortion at a given recovered audio level.

With a double tuned network the linearity improves (distortion is reduced) and the phase shift can be optimized; however this leads to a reduction in the level of the recovered audio. A satisfactory compromise for most FM receiver applications is shown in the test circuit.

Care should be taken with the physical layout.

The main recommendations are:

- Locate the phase shift coil as near as possible to pin 13.
- Shunt pins 14 and 16 with a low value resistor (between 56Ω and 330Ω).
- Ground the decoupling capacitor of pin 14 and the 10.7 MHz input filter at the same point.

If the supply voltage goes under 6V add a DC level shift resistor of $18\text{ K}\Omega$ from pin 9 to ground and change C11 to 8 nF .

AM-FM Switching

AM-FM switching is achieved by applying a DC voltage at pin 13, to switch the internal reference.

Typical DC Voltages (refer to the test circuit)

Pins	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	Unit
AM	9	1.3	9	1.3	1.3	9	9	0.7	2	9	0	0	0	8.4	8.4	8.4	V
FM	9	0.4	9	0.4	0	9	9	0	2.6	9	0	9	9	8.1	8.1	8.1	V

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APPLICATION INFORMATION

AM Section

RF Amplifier and mixer stages

The RF amplifier stage (pin 2) is connected directly to the secondary winding of the ferrite rod antenna or input tuned circuit. Bias is provided at pin 4 which must be adequately decoupled. The RF amplifier provides stable performance extending beyond 30 MHz.

The Mixer employed is a double - balanced multiplier and the IF output at pin 3 is connected directly to the IF filter coil.

Local oscillator

The local oscillator is a cross coupled differential stage which oscillates at the frequency determined by the load on pin 1.

The oscillator resonant circuit is transformer coupled to pin 1 to improve the **Q** factor and frequency stability.

The oscillator level at pin 1 is about 100 mV rms and the performance extends beyond 30 MHz, however to enhance the stability and reduce to a minimum pulling effects of the AGC operation or supply voltage variations, a high C/L ratio should be used above 10 MHz.

An external oscillator can be injected at pin 1. The level should be 50 mV rms and pin 1 should be connected to the supply via a 100 Ω resistor.

IF Amplifier Detector

The IF amplifier is a wide band amplifier with a tuned output stage.

The outputs are at pins 6 and 7 which drive the balanced load and the differential positive peak AM detector, which is biased to reduce distortion at high modulation levels. At the output of balanced detectors of this type there is a low level signal at double the IF frequency (about 920 KHz). To avoid feedback of this signal by radiation from the detector coil, the shield around this coil must be grounded and the ferrite antenna placed in a suitable position.

The Audio output is at pin 9 (for either AM or FM); the IF frequency is filtered by an external capacitor which is also used as the FM mono de-emphasis network. The audio output impedance is about 7 K Ω and a high impedance load (\sim 50 K Ω) must be used.

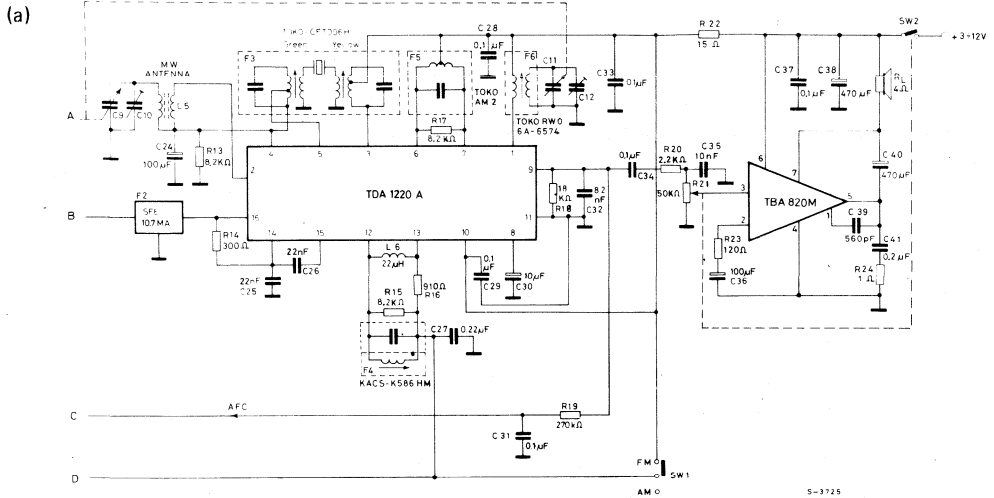
AGC

Both the RF and the first IF amplifiers have the same differential amplifier circuit configuration. The AGC action is obtained by control of the collector current of these stages.

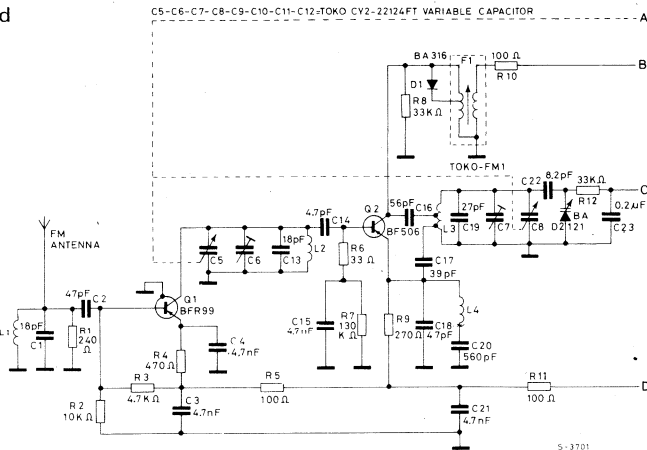
At pin 8 there is a carrier envelope signal which is filtered by an external capacitor to remove the Audio and RF content and obtain a mean DC signal to drive the AGC circuit.

APPLICATION INFORMATION (continued)

Fig. 20 - Low cost AM-FM radio



(b) FM front end



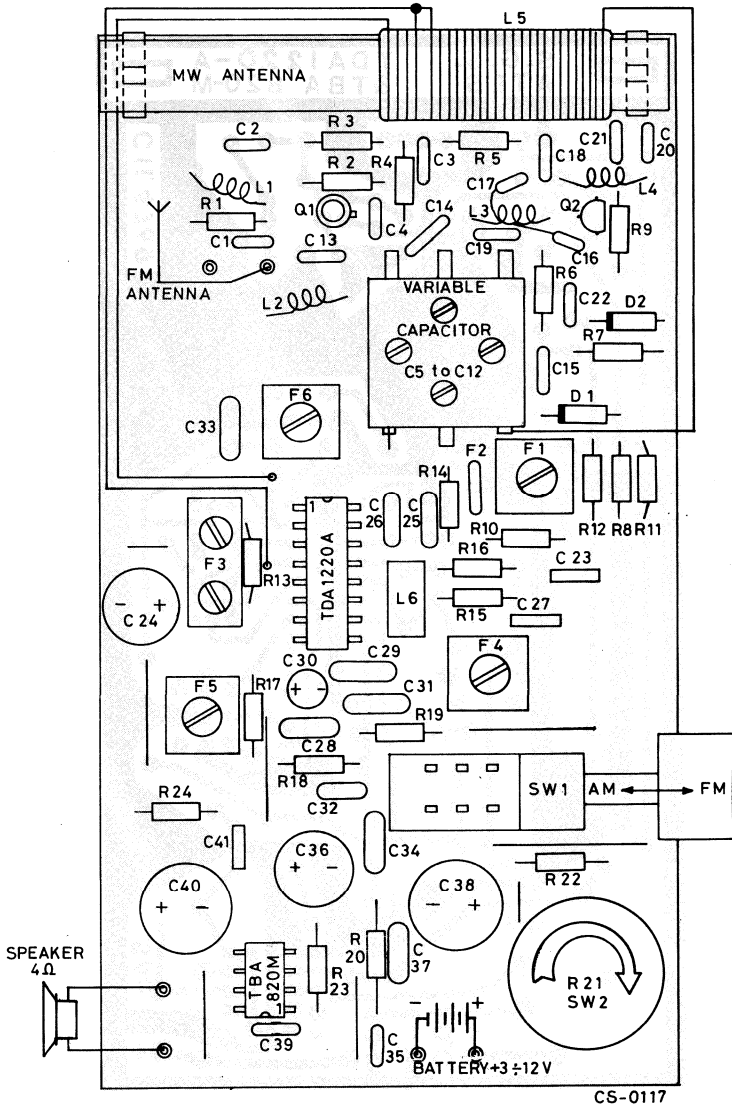
COILS

- L1** FM Antenna coil - 6 Turns copper wire 0.9 mm diameter. Inner diameter 4 mm. Winding pitch 1 mm.
- L2** FM Tuning coil - 5 Turns copper wire 0.9 mm diameter. Inner diameter 4 mm Winding pitch 0.5 mm.
- L4** - 18 Turns copper wire 0.6 mm diameter. Inner diameter 2.5 mm. Closely wound.
- L5** MW Antenna coil - Televox.
- L3** FM osc. coil - 4 Turns copper wire 0.9 mm diameter. Inner diameter 4 mm. Winding pitch 2 mm.

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APPLICATION INFORMATION (continued)

Fig. 21 - PC board and component layout (1:1 scale) of the low cost AM-FM radio in fig. 20.



APPLICATION INFORMATION (continued)

Low cost receiver performance ($V_s = 9V$)

Parameter	Test conditions	Value
Wavebands	FM	87.5 ÷ 108 MHz
	AM	510 ÷ 1620 KHz
Sensitivity	FM : 75Ω (S + N/N) = 26 dB $\Delta f = 22.5$ KHz	$\leq 2 \mu V$
	AM (S + N/N) = 6 dB $m = 0.3$	$1 \mu V$
	AM (S + N/N) = 26 dB $m = 0.3$	$10 \mu V$
Distortion $f_m = 1$ KHz	FM $V_i = 100 \mu V$ $\Delta f = 22.5$ KHz $P = 0.5W$	$\leq 0.25 \%$
	FM $V_i = 100 \mu V$ $\Delta f = 75$ KHz $P = 0.5W$	$\leq 1 \%$
	AM $V_i = 100 \mu V$ $m = 0.3$ $P = 0.5W$	$\leq 0.6 \%$
	AM $V_i = 100 \mu V$ $m = 0.8$ $P = 0.5W$	$\leq 1 \%$
$\frac{S+N}{N}$ $f_m = 1$ KHz	FM $V_i = 100 \mu V$ $\Delta f = 22.5$ KHz $P = 0.5W$	≥ 70 dB
	AM $V_i = 1000 \mu V$ $m = 0.3$ $P = 0.5W$	≥ 55 dB
Input limiting voltage	FM -3 dB point	$\leq 1.5 \mu V$
A M R	FM $V_i = 100 \mu V$ $\Delta f = 22.5$ KHz $m = 0.3$	≥ 45 dB
I F	FM	10.7 MHz
	AM	460 KHz
Quiescent current	FM	23 mA
	AM	15 mA
Supply voltage range	FM	3 ÷ 12 V
	AM	3 ÷ 12 V

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APPLICATION INFORMATION (continued)

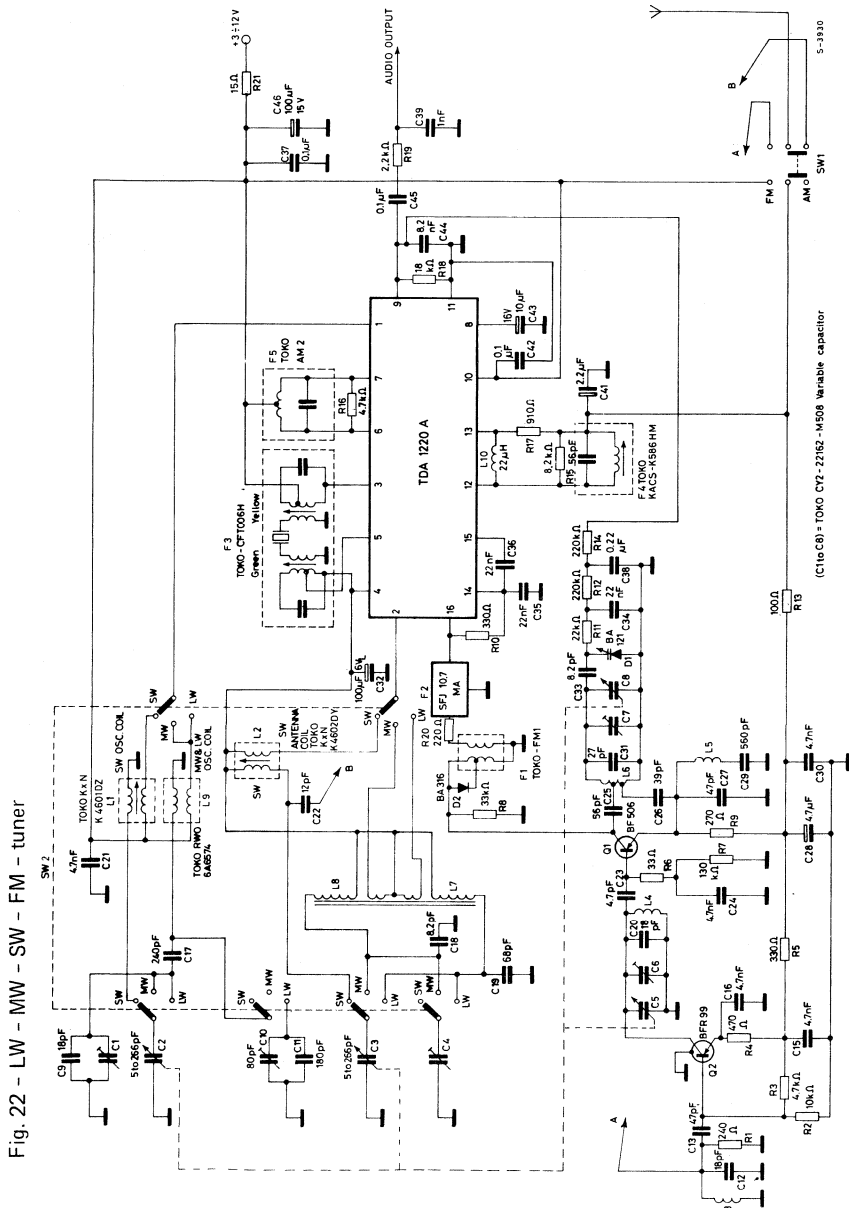


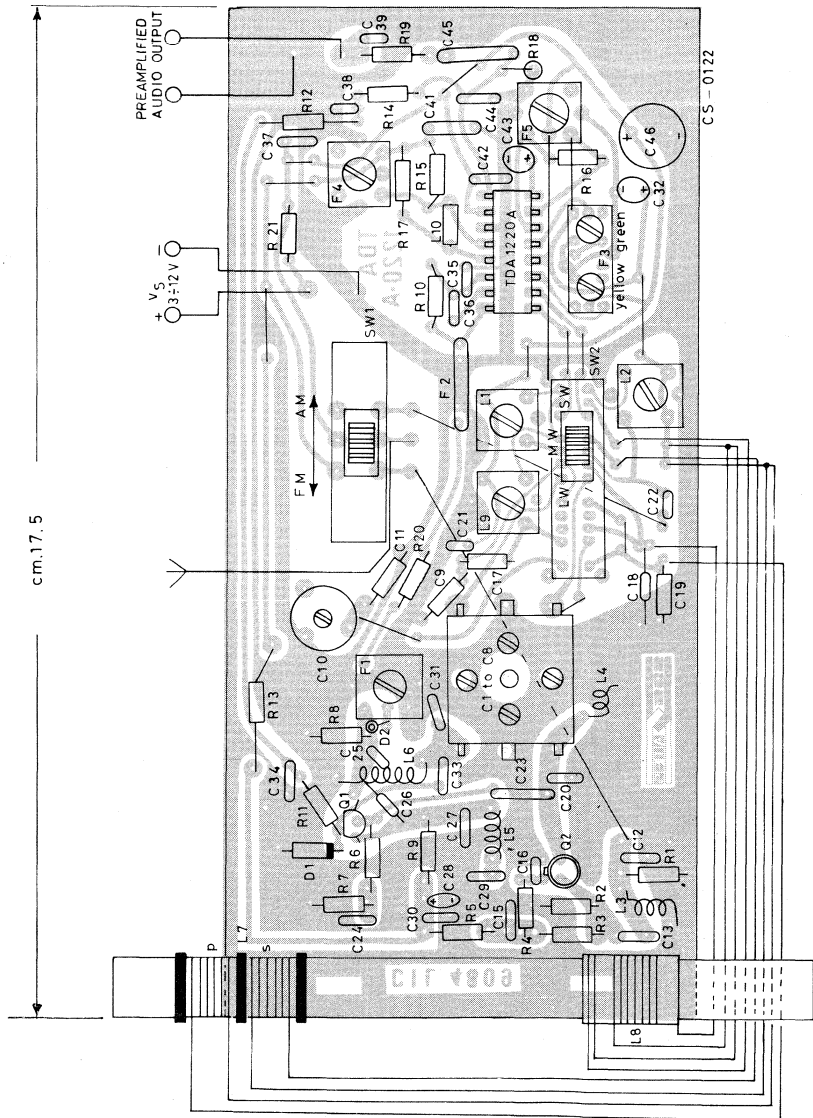
Fig. 22 - LW - MW - SW - FM - tuner

- L3 FM Antenna Coil - 6 Turns copper wire 0.9 mm diameter. Inner diameter 4 mm - winding pitch 1 mm.
- L4 FM Tuning Coil - 5 Turns copper wire 0.9 mm diameter. Inner diameter 4 mm - winding pitch 0.5 mm.
- L5 - 18 Turns copper wire 0.6 mm. diameter. Inner diameter 2.5 mm. Closely wound.
- L6 FM oscillator Coil - 4 Turns silvered copper wire 1 mm. diameter. Inner diameter 4 mm. - winding pitch 2.5 mm.
- L7 - LW antenna coil - Televox.
- L8 - MW antenna coil - Televox.
- SW3 - ALPS type SSA 0.63.

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APPLICATION INFORMATION (continued)

Fig. 23 - PC board and component layout of the four band tuner (fig. 22)



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APPLICATION INFORMATION (continued)

FOUR BAND TUNER PERFORMANCE

Parameter	Test conditions	Values
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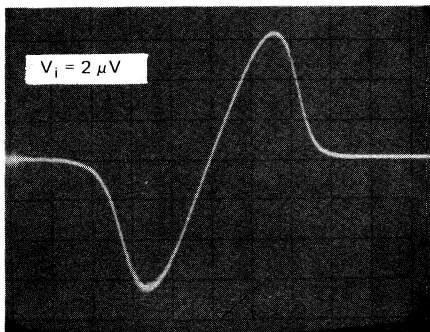
AM SECTION (*)

$\left \frac{S+N}{N} \right $	$V_i = 10 \mu\text{V}$ $m = 0.3$	26 dB
	$V_i = 1 \text{mV}$ $m = 0.3$	55 dB
BW	-3 dB	10 KHz
Distortion	$V_i = 20 \mu\text{V}$ $m = 0.3$	0.5 %
	$V_i = 100 \mu\text{V}$ $m = 0.3$	0.5 %
	$V_i = 1 \text{mV}$ $m = 0.3$	0.5 %
	$V_i = 20 \mu\text{V}$ $m = 0.8$	0.9 %
	$V_i = 1 \text{mV}$ $m = 0.8$	1 %

FM SECTION

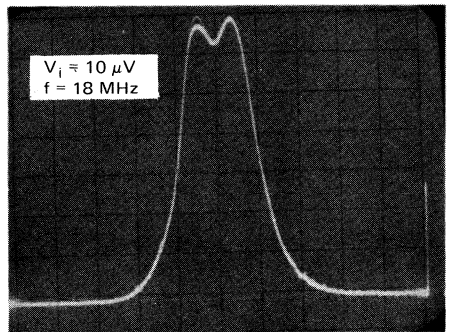
AMR	$V_i = 30 \mu\text{V}$ $\Delta f = 22.5 \text{ KHz}$ $m = 0.3$ $f_m = 1 \text{ KHz}$	45 dB
	$V_i = 100 \mu\text{V}$ $\Delta f = 22.5 \text{ KHz}$ $m = 0.3$ $f_m = 1 \text{ KHz}$	47 dB
Distortion	$V_i = 10 \mu\text{V}$ $\Delta f = 22.5 \text{ KHz}$	0.3 %
	$V_i = 100 \mu\text{V}$ $\Delta f = 22.5 \text{ KHz}$	0.2 %
	$V_i = 1 \text{mV}$ $\Delta f = 22.5 \text{ KHz}$	0.2 %
	$V_i = 10 \mu\text{V}$ $\Delta f = 75 \text{ KHz}$	1 %
	$V_i = 100 \mu\text{V}$ $\Delta f = 75 \text{ KHz}$	1 %
$\left \frac{S+N}{N} \right $	$V_i = 10 \mu\text{V}$ $\Delta f = 22.5 \text{ KHz}$	60 dB
	$V_i = 100 \mu\text{V}$ $\Delta f = 22.5 \text{ KHz}$	70 dB
	$V_i = 1 \text{mV}$ $\Delta f = 22.5 \text{ KHz}$	70 dB
Input limiting voltage	-3 dB	1 μV

(*) The performance remains substantially the same over LW, MW and SW bands.



100 KHz/div.

Fig. 24 - FM-SECTION
S curve response



5 KHz/div.

Fig. 25 - AM-SECTION
Band pass IF filter response at AGC
starting point.

APPLICATION INFORMATION (continued)

Fig. 26 - Stereo set block diagram

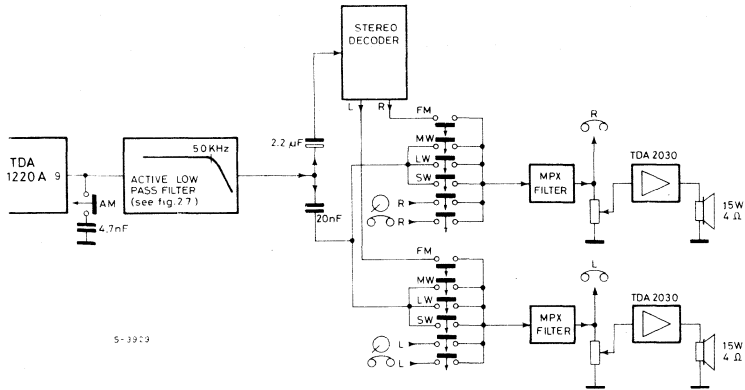


Fig. 27 - Active low-pass filter

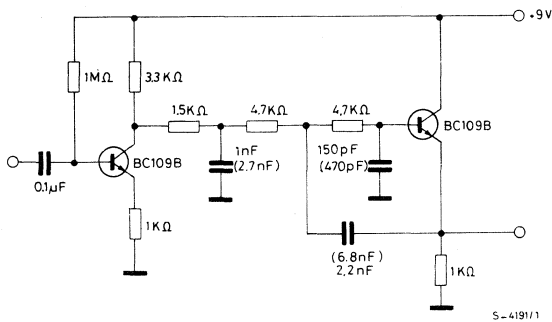
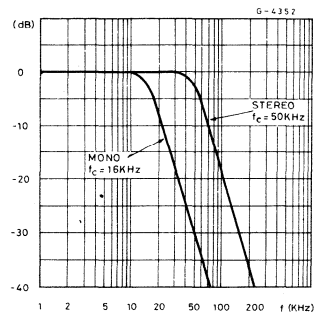


Fig. 28 - Frequency response of active low pass filter

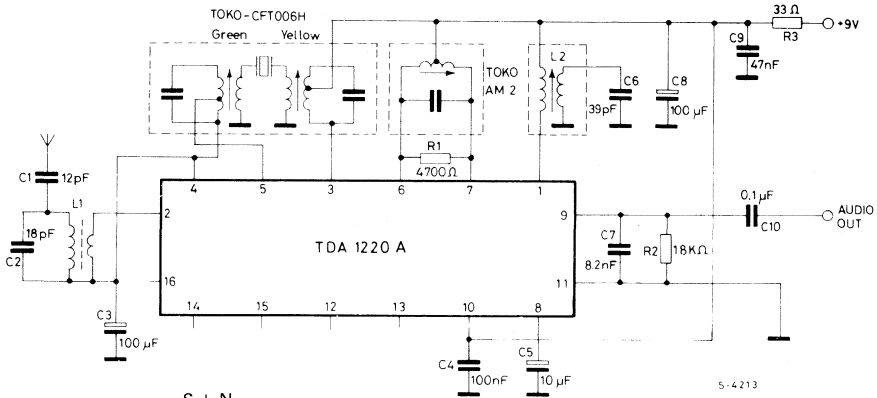


Note: Values in brackets refer to the mono application ($f_c = 16$ KHz).

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APPLICATION INFORMATION (continued)

Fig. 29 - Low cost 27 MHz receiver



Sensitivity: $10 \mu\text{V}$ for $\left(\frac{S+N}{N}\right) = 26 \text{ dB}$

Fig. 30 - PC board and component layout of the low cost 27 MHz receiver (1:1 scale)

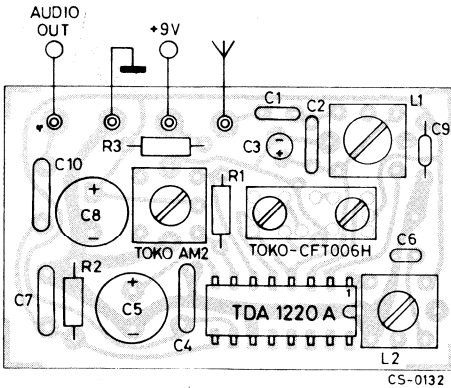
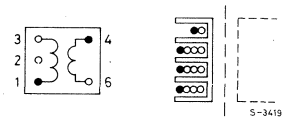
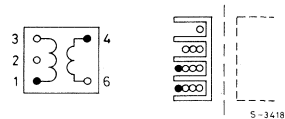


Fig. 31 - L2 Oscillator Coil



Coil support: Toko 10K.
 Primary winding: 10 Turns of enameled copper wire 0.16 mm diameter (pins 3-1).
 Secondary winding: 4 Turns copper wire 0.16 mm diameter (pins 6-4).

Fig. 32 - L1 Antenna Coil



Coil support: Toko 10K.
 Primary winding: as L2 (pins 3-1)
 Secondary winding: 2 Turns copper wire 0.16 mm diameter (pins 6-4).

APPLICATION INFORMATION (continued)

Fig. 33 - Low cost 27 MHz receiver, with external XTAL oscillator (use the same PC board of Fig. 30).

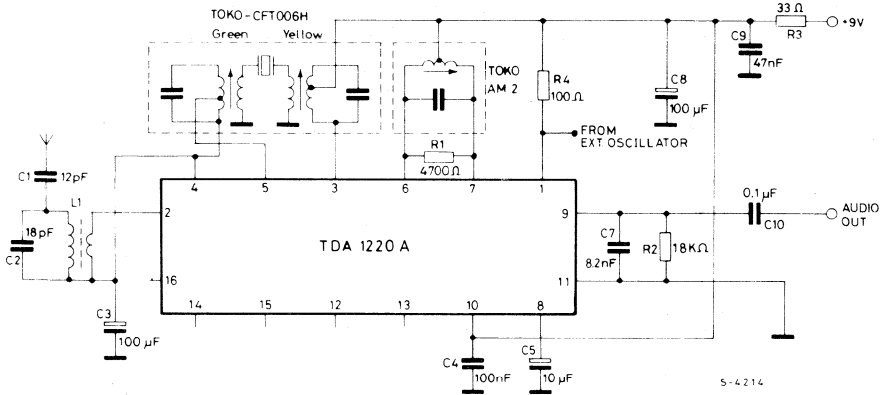


Fig. 34 - External XTAL oscillator for low cost 27 MHz receiver

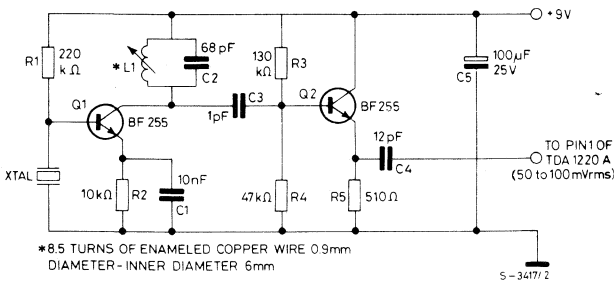
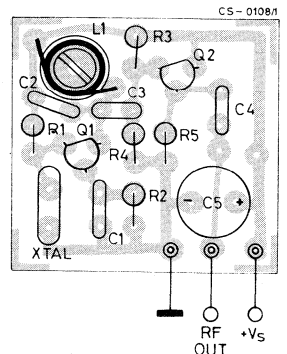


Fig. 35 - PC board component layout of the crystal oscillator circuit (1:1 scale)



TDA 1220A

APPLICATION INFORMATION (continued)

Fig. 36 - Low cost field strength meter circuit (9V)

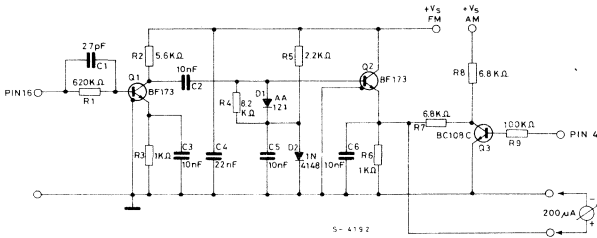
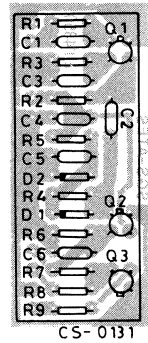


Fig. 37 -- PC board and component layout of the field strength meter circuit (1:1 scale)



LINEAR INTEGRATED CIRCUIT

TV VERTICAL DEFLECTION SYSTEM

The TDA 1270 is a monolithic integrated circuit in a 12-lead quad in-line plastic package. It is mainly designed for driving complementary vertical deflection output stages in colour TV receivers.

The functions incorporated are:

- oscillator
- voltage ramp generator
- high gain amplifier.

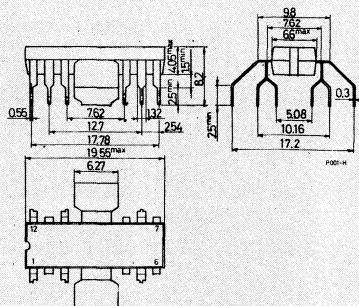
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage (pins 2 and 5)	40	V
V_4	Voltage at pin 4	41	V
V_8	Sync. input voltage	± 12	V
V_{10}	Power amplifier input voltage	$\left. \begin{array}{l} 10 \\ -0.5 \end{array} \right\}$	V
I_o	Output peak current (non-repetitive)	2	A
I_o	Output peak current (repetitive)	1.2	A
P_{tot}	Power dissipation: at $T_{tab} = 90^\circ\text{C}$	5	W
	at $T_{amb} = 80^\circ\text{C}$ (free air)	1	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBER: TDA 1270

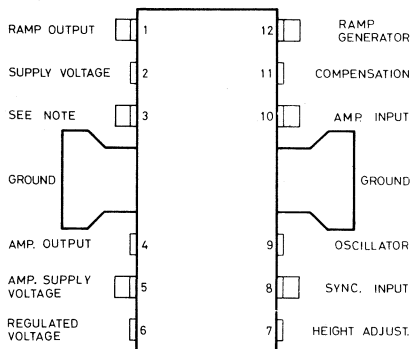
MECHANICAL DATA

Dimensions in mm



TDA 1270

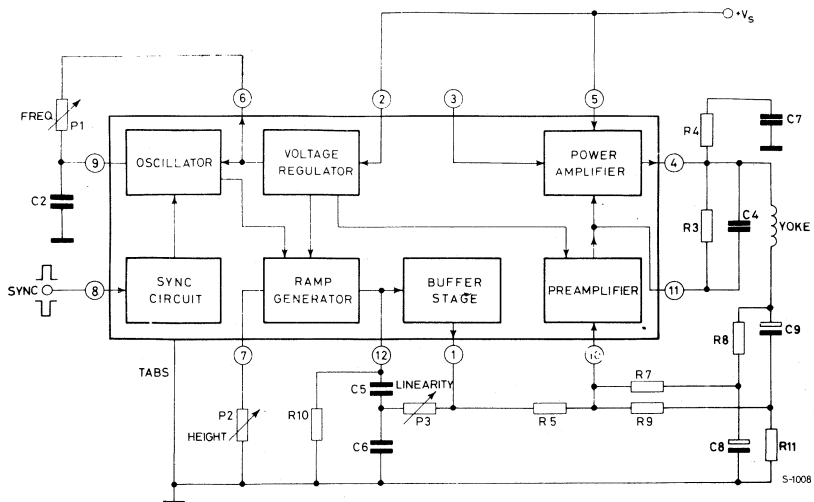
CONNECTION DIAGRAM (top view)



S-1002/1

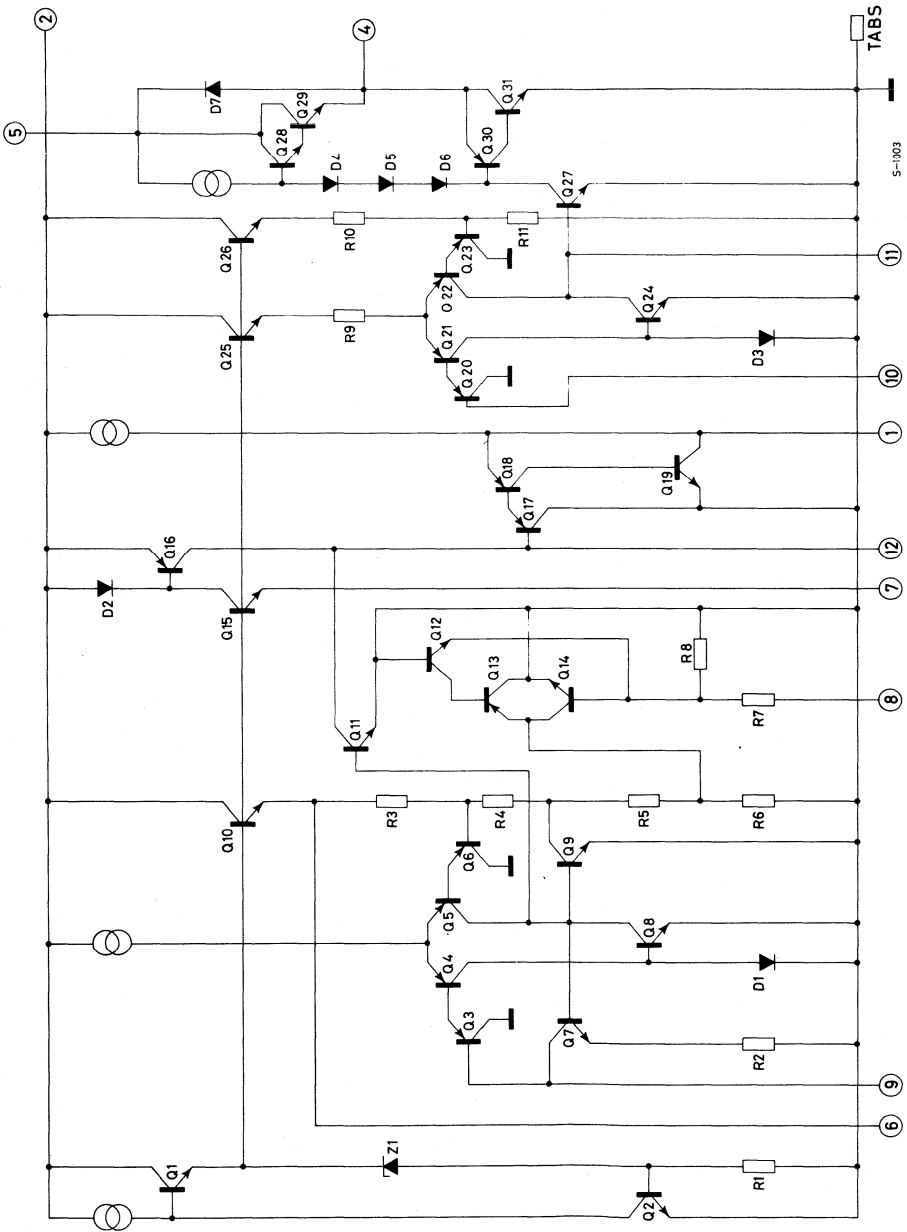
Note: PIN3 Internally connected, must be left open

BLOCK DIAGRAM



S-1008

SCHEMATIC DIAGRAM



S-1003

TDA 1270

THERMAL DATA

$R_{th\ j-tab}$	Thermal resistance junction-tab	max	12	°C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	70*	°C/W

* Obtained with tabs soldered to printed circuit with minimized copper area.

ELECTRICAL CHARACTERISTICS (Refer to the test circuits, $V_s = 32V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig.
-----------	-----------------	------	------	------	------	------

DC CHARACTERISTICS

$-I_9$	Oscillator bias current	$V_9 = 1V$		0.2	1	μA	1a	
$-I_{10}$	Amplifier input bias current	$V_{10} = 1V$		0.15	1	μA	1b	
$-I_{12}$	Ramp generator bias current			0.05	0.5	μA	1a	
V_s	Supply voltage		10		40	V	—	
V_4	Quiescent output voltage	$R_2 = 10\ k\Omega$ $V_s = 32V$ $V_s = 10V$	$R_1 = 30\ k\Omega$ $R_1 = 10\ k\Omega$	8 4	8.8 4.4	9.6 4.8	V V	1a
V_6, V_7	Regulated voltage		6	6.5	7	V	1b	
$\frac{\Delta V_6}{\Delta V_s}, \frac{\Delta V_7}{\Delta V_s}$	Line regulation	$V_s = 10\ to\ 40V$		1.5		mV/V		

AC CHARACTERISTICS (f = 50 Hz)

I_s	Supply current	$I_o = 0.5A$ peak to peak		70		mA	2
I_o	Peak to peak output current (pin 4)				1	A	
V_8	Peak sync. input voltage (positive or negative)		1			V	
V_9	Peak to peak oscillator sawtooth voltage			2.4		V	
R_8	Sync. input resistance at pin 8	$V_8 = 1V$		3.5		k Ω	

ELECTRICAL CHARACTERISTICS (continued)

Parameter		Test conditions	Min.	Typ.	Max.	Unit	Fig.
t_{fly}	Flyback time	$I_o = 0.5A$ peak to peak		0.7		ms	2
δf	Pull-in range (below 50 Hz)			7		Hz	
$\frac{\delta f}{\Delta V_s}$	Oscillator frequency shift	$V_s = 10$ to $40V$		0.01		$\frac{Hz}{V}$	
$\frac{\delta f}{\Delta T_{tab}}$	Oscillator frequency drift	$T_{tab} = 40$ to $120^\circ C$		0.015		$\frac{Hz}{^\circ C}$	

TEST CIRCUITS

Fig. 1a - DC test circuit for measurement of $-I_g$, $-I_{12}$ and V_4

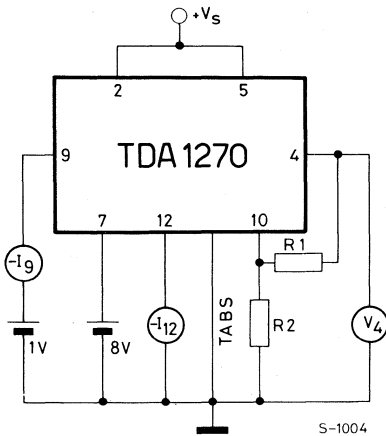
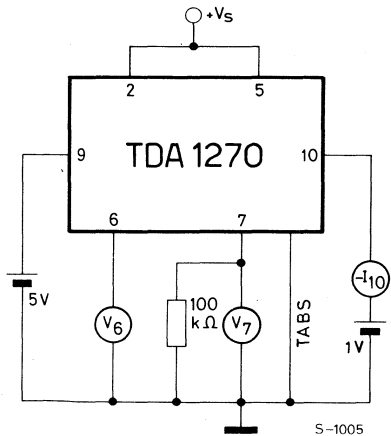


Fig. 1b - DC test circuit for measurement of $-I_{10}$, V_6 , V_7 , $\Delta V_6/\Delta V_s$ and $\Delta V_7/\Delta V_s$



TDA 1270

Fig. 2 - AC test circuit

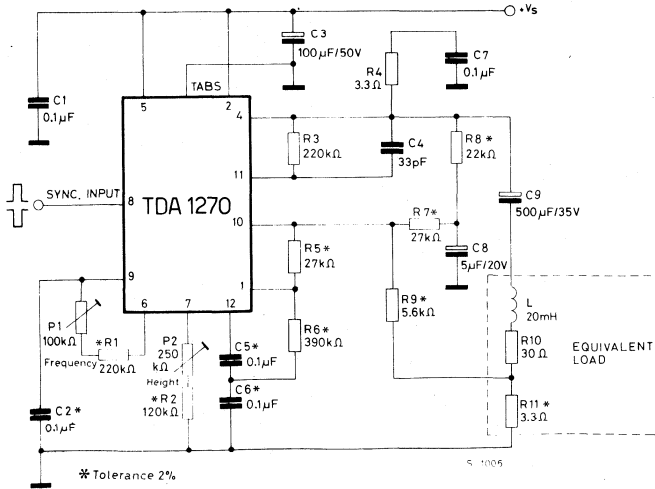


Fig. 3 - Quiescent voltage variation vs. supply voltage

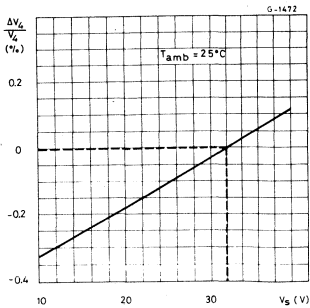


Fig. 4 - Quiescent voltage variation vs. tab temperature

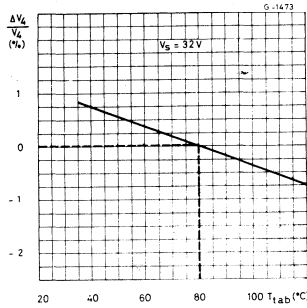


Fig. 5 - Regulated voltage vs. supply voltage

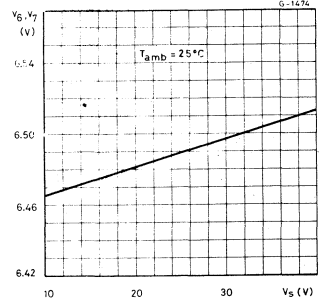


Fig. 6 - Regulated voltage vs. tab temperature

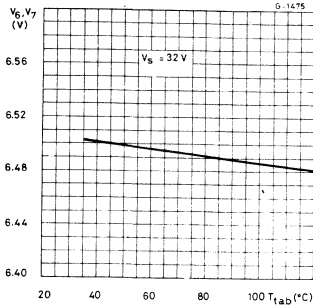


Fig. 7 - Frequency variation of unsynchronized oscillator vs. supply voltage

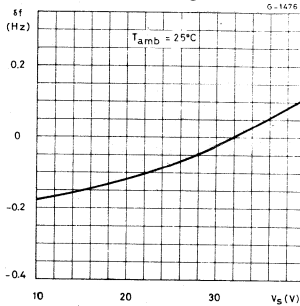
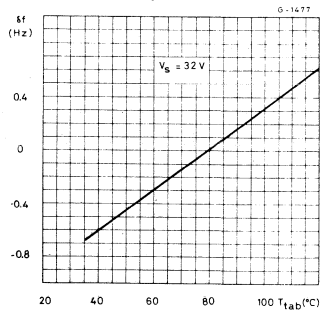


Fig. 8 - Frequency variation of unsynchronized oscillator vs. tab temperature



APPLICATION INFORMATION

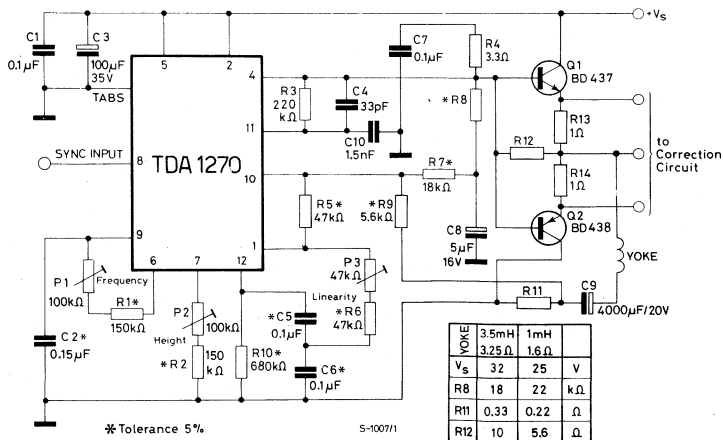
The high current capability of the TDA 1270 allows low current gain transistors to be used in driving low impedance yokes. The oscillator is directly synchronized by the sync. pulses, therefore its free frequency must be lower than the sync. frequency. The sync. input (pin 8) can be driven by positive or negative pulses.

The quiescent output voltage is fixed by the voltage feedback network R7, R8, and R9 (refer to fig. 9) according to:

$$V_o = V_{10} \frac{R7 + R8 + R9}{R9}$$

Pin 10 is the inverting input of the amplifier and its voltage is $V_{10} \cong 2V$.

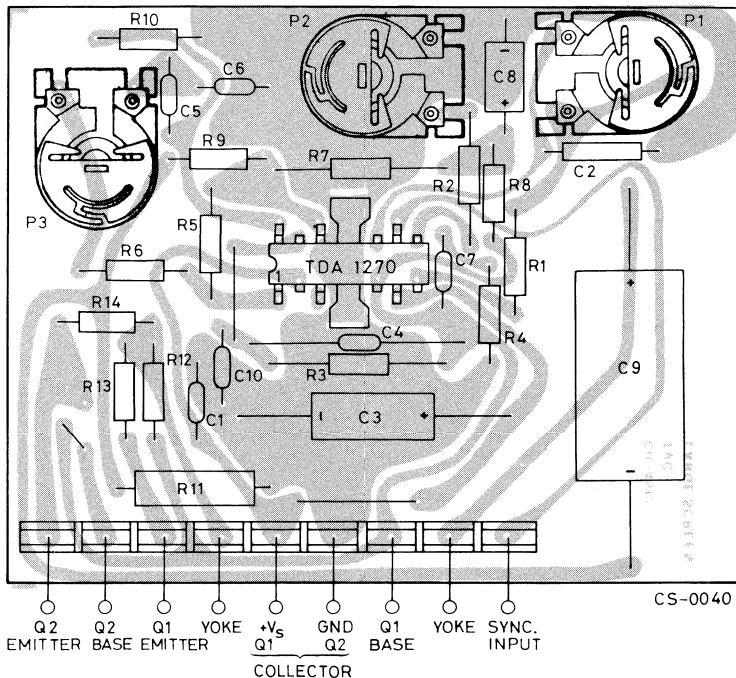
Fig. 9 - Application circuit for large screen colour TV sets



TDA 1270

APPLICATION INFORMATION (continued)

Fig. 10 - P.C. board and component layout for the circuit of fig. 9 (1:1 scale)

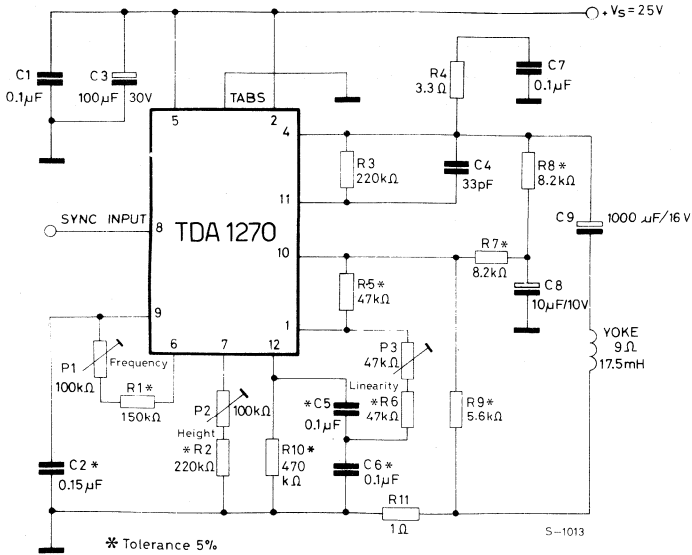


Performance of circuit in fig. 9

		YOKE	
		3.5 mH	1 mH
		3.25 Ω	1.6 Ω
I_s	Supply current	0.5 A	0.8 A
t_{fly}	Flyback time	0.7 ms	0.6 ms
I_Y	Maximum scanning current (peak to peak)	4 A	7.5 A
V_s	Operating supply voltage	28 to 36V	23 to 27V
P_{tot}	TDA 1270 power dissipation	1.5 W	2 W
P_{tot}	Output transistors power dissipation	11 W	13 W
$R_{th \text{ tab-amb}}$	Heatsink R_{th} required for TDA 1270	35 $^{\circ}\text{C}/\text{W}$	30 $^{\circ}\text{C}/\text{W}$
$R_{th \text{ case-amb}}$	R_{th} of output transistors heatsink (total)	6 $^{\circ}\text{C}/\text{W}$	5 $^{\circ}\text{C}/\text{W}$

Stable continuous operation is ensured up to an ambient temperature of 55 $^{\circ}\text{C}$.

Fig. 11 - Application circuit for 12" to 17" (110°, 20 mm neck) B & W TV sets



Performance of circuit in fig. 11

I_s	Supply current	110	mA
t_{fly}	Flyback time	0.8	ms
I_Y	Maximum scanning current (peak to peak)	0.9	A
V_s	Operating supply voltage	23 to 27	V
P_{tot}	TDA 1270 power dissipation	2.4	W

For safe working up to $T_{amb} = 50^\circ\text{C}$ a heatsink of $R_{th} = 30^\circ\text{C/W}$ is required and each tab of the TDA 1270 must be soldered to 1 cm² copper area of the printed circuit board.

TDA 1270

APPLICATION INFORMATION (continued)

Fig. 12 - P.C. board and component layout for the circuit of fig. 11 (1:1 scale)

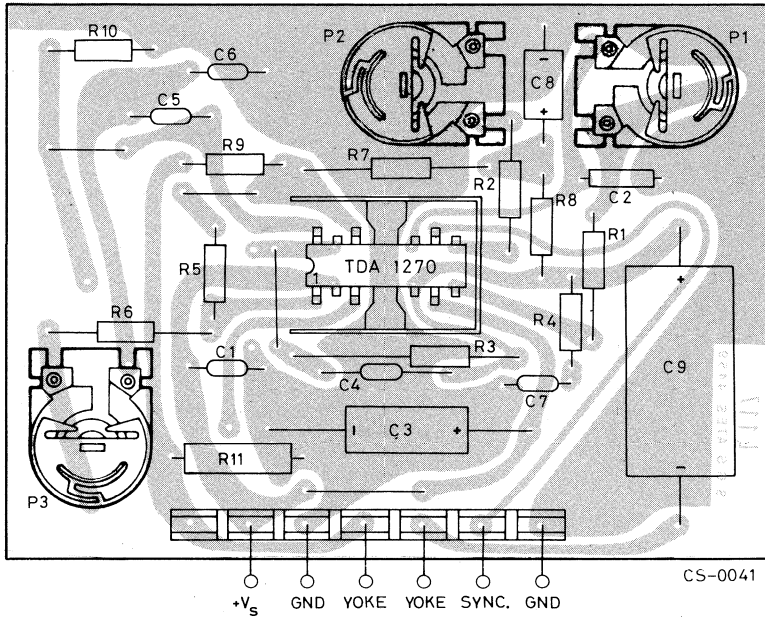
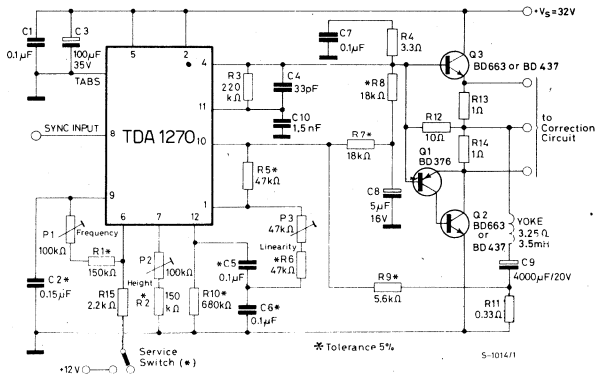


Fig. 13 - Vertical deflection circuit employing two NPN output power transistors



* The service switch stops the vertical deflection during convergence adjustment.

MOUNTING INSTRUCTION

The thermal resistance junction to ambient of the TDA 1270 can be reduced by soldering the tabs to a suitable copper area of the printed circuit board (fig. 14) or to an external heatsink (fig. 15).

Fig. 16 gives the maximum power that can be dissipated (for $T_{amb} = 55$ to 70 °C) as a function of the side "s" of two equal square copper areas having a thickness of 35μ (1.4 mil).

During soldering the tab temperature must not exceed 260 °C and the soldering time must not be longer than 12 seconds.

The external heatsink or printed circuit copper area must be connected to electrical ground.

Fig. 14 - Example of TDA 1270 with external heatsink

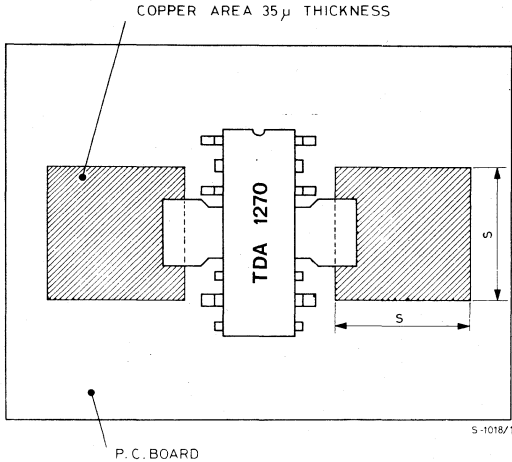


Fig. 15 - Example of P.C. board copper area used as heatsink

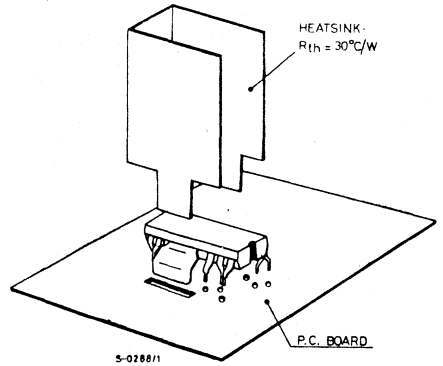


Fig. 16 - Maximum power dissipation and thermal resistance junction-ambient vs. "s"

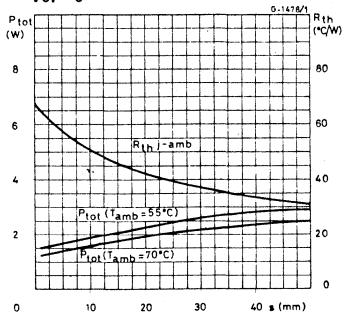
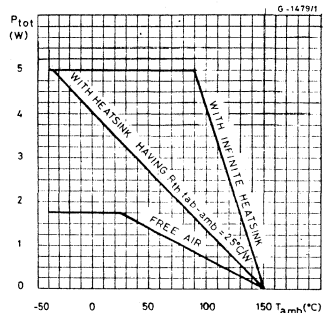


Fig. 17 - Maximum allowable power dissipation vs. ambient temperature



MONOLITHIC QUASI-COMPLEMENTARY DUAL DARLINGTONS

The TDA 1410A, TDA 1420A and 1420L are monolithic integrated circuits in Pentawatt[®] plastic package consisting of a pair of quasi-complementary (NPN-PNP) darlington with the associated biasing system. Each darlington can deliver a current in excess of 3A and can withstand a supply voltage of 36V for TDA 1410A, 40V for TDA 1420L and 44V for TDA 1420A. The devices are intended for application as:

- booster for operational amplifier
- DC motor driver
- stepping motor driver
- output stage for AC power amplifier up to 12W
- output stage for vertical deflection systems in colour TV etc.

ABSOLUTE MAXIMUM RATINGS

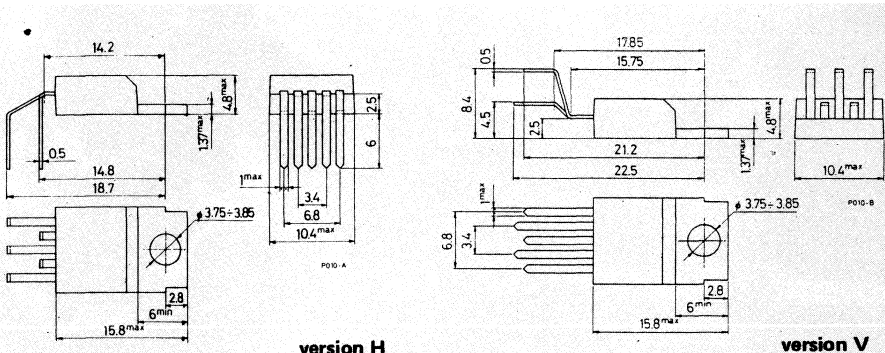
V_{CEO}	Collector-emitter voltage ($I_B = 0$)	TDA 1410A	36	V
		TDA 1420L	40	V
		TDA 1420A	44	V
V_{CBO}	Collector-base voltage ($I_E = 0$)	TDA 1410A	50	V
		TDA 1420A/L	55	V
I_o	Output peak current (repetitive)		3.5	A
I_o	DC output current		3	A
$I_{F D1} (*)$	D1 forward current		0.3	A
$I_{F D2} (*)$	D2 forward current		3	A
P_{tot}	Total power dissipation at $T_{case} = 60^\circ C$		30	W
T_j, T_{stg}	Junction and storage temperature		-40 to 150	$^\circ C$

(*) See schematic diagram.

ORDERING NUMBERS: TDA 1410AH - TDA 1420AH - TDA 1420LH
TDA 1410AV - TDA 1420AV - TDA 1420LV

MECHANICAL DATA

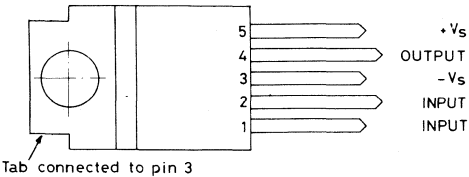
Dimensions in mm



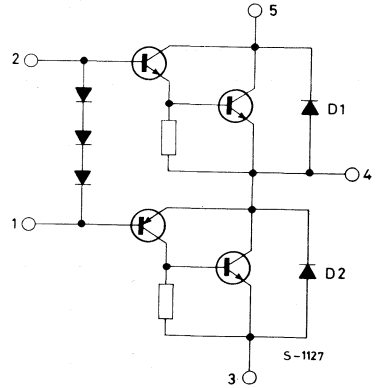
TDA 1410A TDA 1420A TDA 1420L

CONNECTION AND SCHEMATIC DIAGRAMS

(top view)



S-1128/1



THERMAL DATA

$R_{th\ j-case}$	Thermal resistance junction-case	max. 3 °C/W
------------------	----------------------------------	-------------

ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^{\circ}C$)

Parameter	Test conditions		Min.	Typ.	Max.	Unit
V_{CEO} Collector-emitter breakdown voltage	$I_C = 500\ \mu A$	TDA 1410A	36			V
		TDA 1420L	40			
		TDA 1420A	44			
V_{CBO} Collector-base breakdown voltage	$I_C = 500\ \mu A$	TDA 1410A	50			V
		TDA 1420A/L	55			
$V_{(BR)}$ Collector-substrate breakdown voltage	$I_C = 500\ \mu A$	TDA 1410A	50			V
		TDA 1420A/L	60			
$h_{FE(NPN)}$ DC forward current transfer ratio	$V_{CE} = 5V$	TDA 1410A $I_C = 2A$	2000	5000		—
		TDA 1420L $I_C = 2A$	2000			
		TDA 1420A $I_C = 3A$	1000	2500		
$h_{FE(PNP)}$ DC forward current transfer ratio	$V_{CE} = 5V$	TDA 1410A $I_C = 2A$	800	2500		—
		TDA 1420L $I_C = 2A$	800			
		TDA 1420A $I_C = 3A$	500	1000		
I_d Quiescent drain current	$I_{2-1} = 5mA$	$V_s = 34V$		20		mA

TDA 1410A TDA 1420A TDA 1420L

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
$V_{CE(sat)}$ Collector-emitter saturation voltage (NPN-PNP)	$h_{FE} = 200$ TDA 1410A $I_C = 2A $ TDA 1420L $I_C = 2A $ TDA 1420A $I_C = 3A $		1.7 2.3	2.3 1.8 2.7	V
$V_{BE(NPN)}$ Base-emitter voltage (pins 2-4)	$I_C = 2A$ $I_C = 3A$	TDA 1410A TDA 1420A/L	2 2.5		V
$V_{BE(PNP)}$ Base-emitter voltage (pins 1-4)	$I_C = -2A$ $I_C = -3A$	TDA 1410A TDA 1420A/L	-0.9 -1.2		V
$V_{F(D1)}$ D1 forward voltage	$V_{3-5} = -34V$ $I_{F(D1)} = 0.3A$		1.5		V
$V_{F(D2)}$ D2 forward voltage	$I_{F(D2)} = 3A$		5		V
$f_T(NPN)$ Cutoff frequency	$I_C = 2A$ $V_{CE} = 10V$		10		MHz
$f_T(PNP)$ Cutoff frequency	$I_C = -2A$ $V_{CE} = -10V$		5		MHz

Fig. 1 - Quiescent drain current vs. I_{2-1}

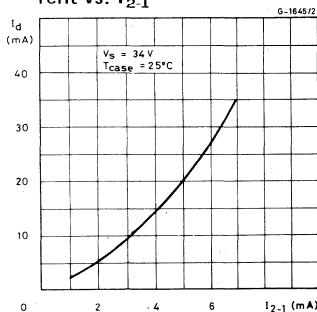


Fig. 2 - Quiescent drain current vs. case temperature

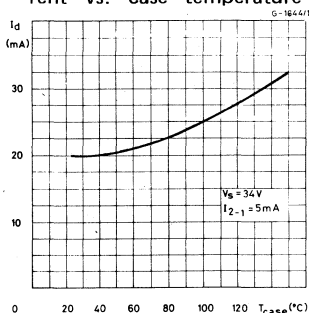


Fig. 3 - Quiescent drain current vs. supply voltage

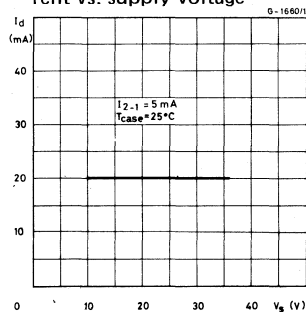


Fig. 4 - DC current gain vs. collector current

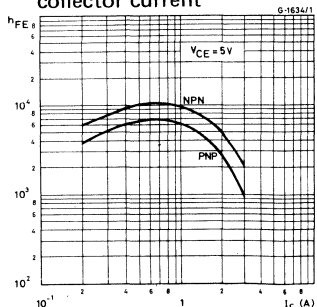


Fig. 5 - $V_{CE(sat)}$ vs. collector current

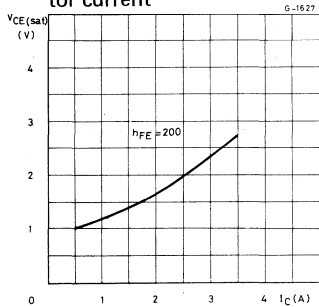
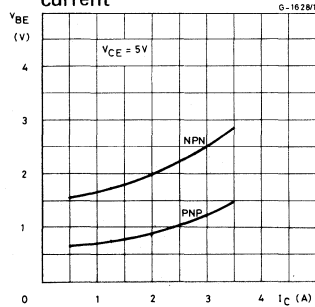


Fig. 6 - V_{BE} vs. collector current



TDA 1410A TDA 1420A TDA 1420L

Fig. 7 - Pulse response (rising edge)

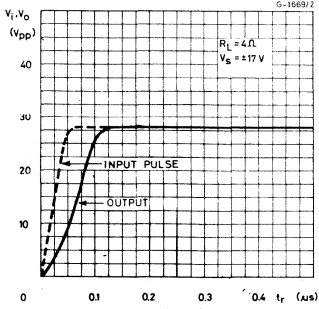


Fig. 8 - Pulse response (falling edge)

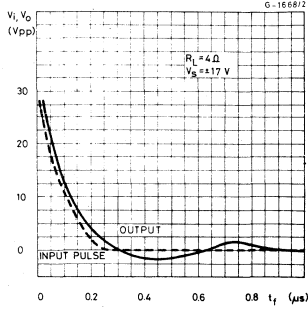


Fig. 9 - Output voltage swing vs. frequency

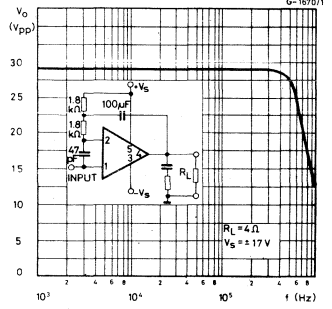


Fig. 10 - Safe operating areas (TDA 1410A)

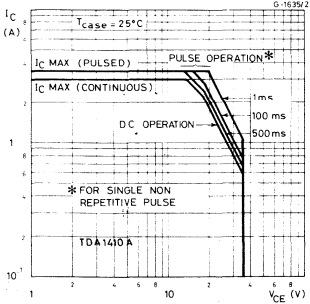


Fig. 11 - Safe operating areas (TDA 1420A)

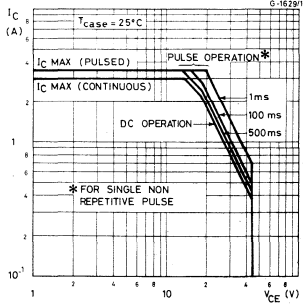
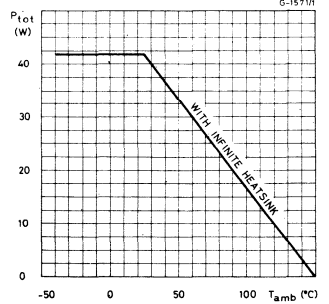
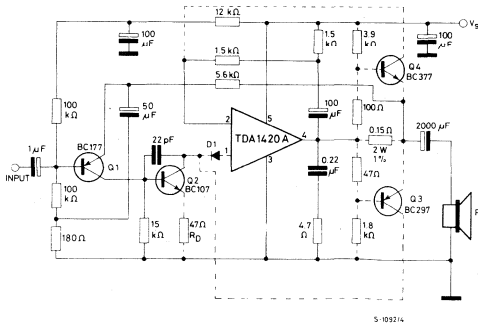


Fig. 12 - Derating characteristic



APPLICATION INFORMATION

Fig. 13 - Audio amplifier with short circuit protection



S-109214

TDA 1410A TDA 1420A TDA 1420L

Typical performance of circuit in fig. 13

Parameter	Test conditions	Min.	Typ.	Max.	Unit
P_o Output power	$d = 1\%$ $G_v = 30\text{dB}$ $f = 40 \text{ to } 15,000 \text{ Hz}$ $V_s = 34\text{V}$ $R_L = 4 \Omega$ $V_s = 36\text{V}$ $R_L = 8 \Omega$	20 15	22 17		W W
	$d = 10\%$ $G_v = 30\text{dB}$ $f = 1\text{KHz}$ $V_s = 34\text{V}$ $R_L = 4 \Omega$ $V_s = 36\text{V}$ $R_L = 8 \Omega$		30 20		W W
B Frequency response (-3dB)	$V_s = 34\text{V}$ $R_L = 4 \Omega$ $G_v = 30\text{dB}$	20 Hz to 100 KHz			
I_d Drain current	$V_s = 34\text{V}$ $R_L = 4 \Omega$ $P_o = 30\text{W}$		1.3		A
	$V_s = 36\text{V}$ $R_L = 8 \Omega$ $P_o = 20\text{W}$		720		mA

Fig. 14 - Output characteristics of the protected class B stage

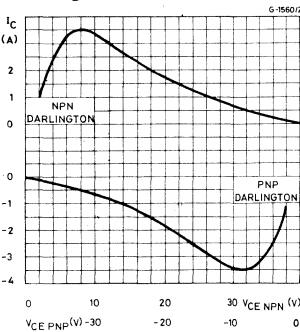


Fig. 15 - Distortion vs. output power ($R_L = 4\Omega$)

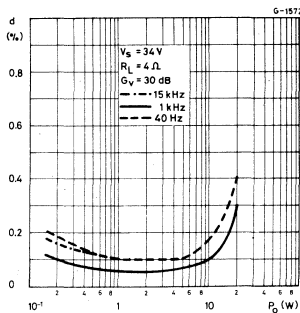
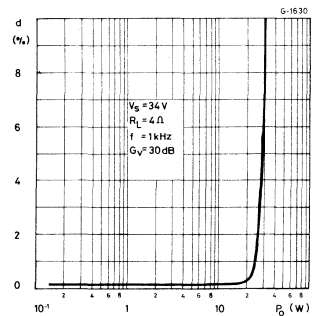


Fig. 16 - Distortion vs. output power ($R_L = 4\Omega$, $f = 1 \text{ KHz}$)



TDA 1410A TDA 1420A TDA 1420L

Fig. 17 - Sensitivity vs. output power

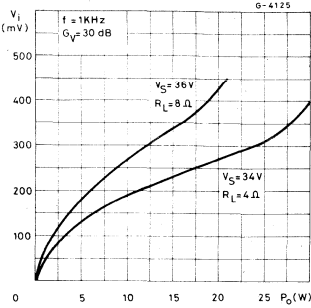


Fig. 18 - Power dissipation and efficiency vs. output power ($R_L = 4\Omega$)

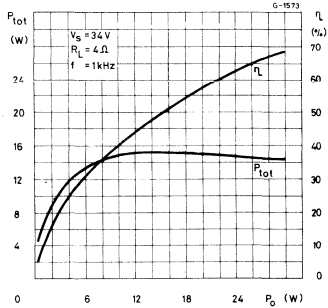


Fig. 19 - Distortion vs. output power ($R_L = 8\Omega$)

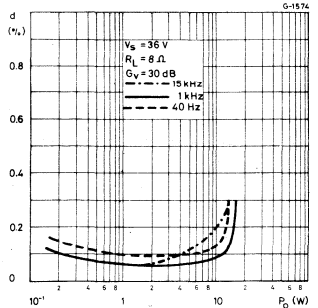


Fig. 20 - Distortion vs. output power ($R_L = 8\Omega$, $f = 1\text{ KHz}$)

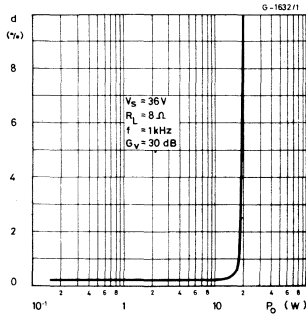


Fig. 21 - Power dissipation and efficiency vs. output power ($R_L = 8\Omega$)

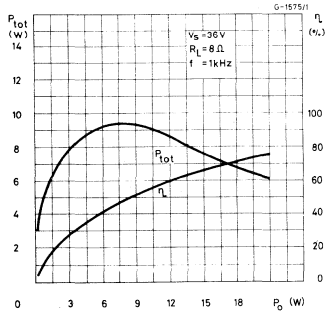


Fig. 22 - Output power vs. supply voltage

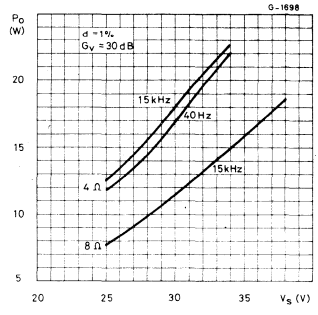
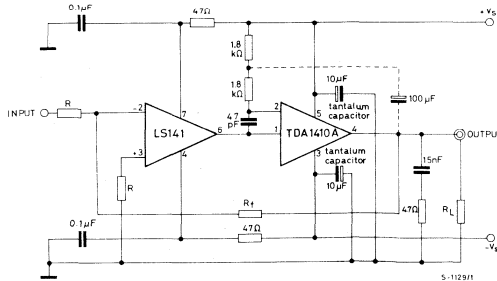


Fig. 23 - Booster for operational amplifier



TDA 1410A TDA 1420A TDA 1420L

Fig. 24 - LS141+TDA 1410A
output voltage swing vs. frequency

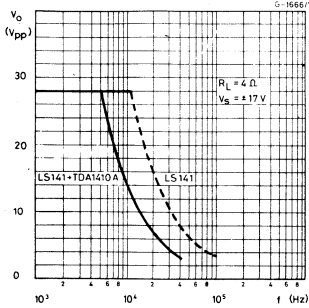
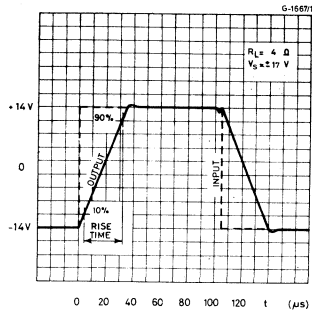


Fig. 25 - LS141+TDA 1410A
transient response



Performance of circuit in fig. 23

	LS 141 + TDA 1410A
Supply voltage	$\pm 15V$
Max. power dissipation	30W at $T_{case} = 60^\circ C$
Input offset voltage	$\leq 5 mV$
Input offset current	$\leq 200 nA$
Input bias current	$\leq 500 nA$
Voltage gain	$\geq 86 dB$ ($R_L = 4\Omega$)
Max. DC output current	3A

Fig. 26 - Position control of DC motor

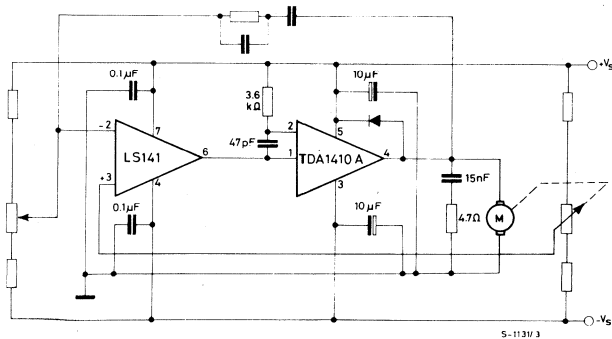


Fig. 27 - Stepping motor driver

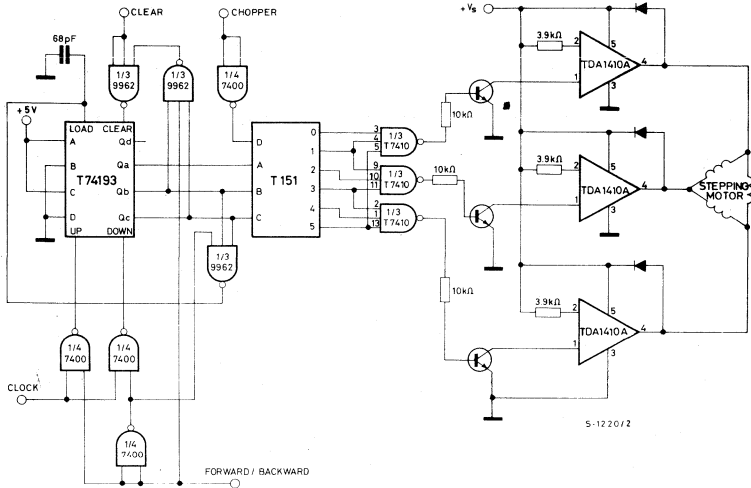
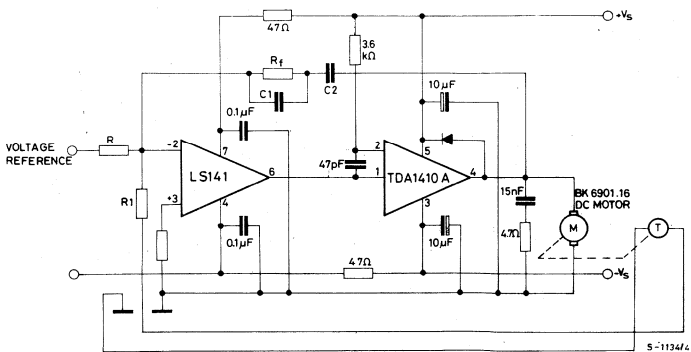
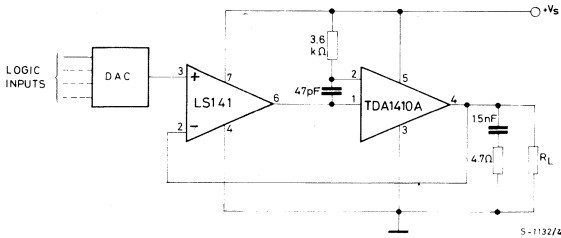


Fig. 28 - Bidirectional speed control of DC motor



TDA 1410A TDA 1420A TDA 1420L

Fig. 29 – Programmable supply voltage



LINEAR INTEGRATED CIRCUIT

COLOUR TV VERTICAL DEFLECTION SYSTEM

The TDA 1470 is a monolithic integrated circuit in a 16-lead dual in-line plastic package with or without external bar. It is intended for direct driving of colour TV yokes, but it offers a wide application range also in BW TVs, monitors and displays.

The functions incorporated are:

- Synchronization circuit
- Oscillator and ramp generator
- Power amplifier with high current capability
- Flyback generator
- Voltage regulator

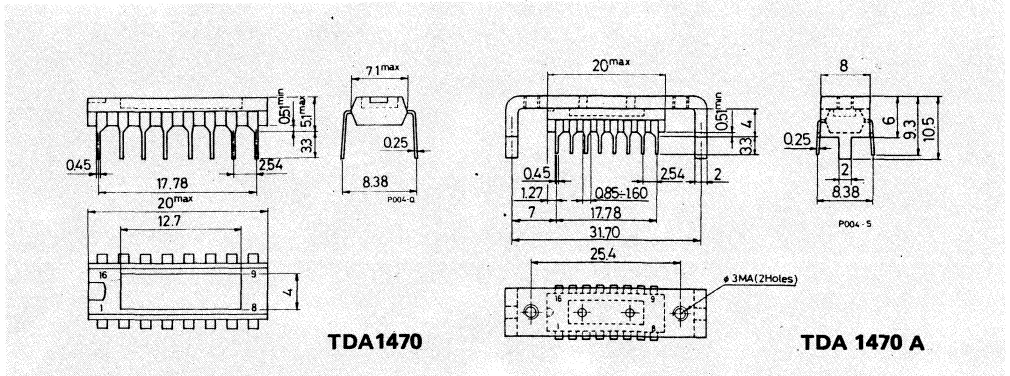
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage at pin 3	35	V
V_{14}, V_{16}	Flyback peak voltage	60	V
V_7, V_8	Power amplifier input voltage	+10	V
		-0.5	V
I_o	Output peak current (non repetitive) at $t = 2$ ms	3	A
I_o	Output peak current at $f = 50$ Hz, $t \leq 10 \mu s$	3.5	A
I_o	Output peak current at $f = 50$ Hz, $t > 10 \mu s$	2	A
I_2	Pin 2 D.C. current at $V_{16} < V_3$	100	mA
I_2	Pin 2 peak to peak flyback current for $f = 50$ Hz, $t_{fly} \leq 1.5$ ms	3	A
I_{11}	Pin 11 current	20	mA
P_{tot}	Maximum power dissipation at $T_{case} \leq 75^\circ C$ (TDA 1470)	25	W
	(TDA 1470A)	15	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ C$

ORDERING NUMBER: TDA 1470A (with external bar)
TDA 1470 (without external bar)

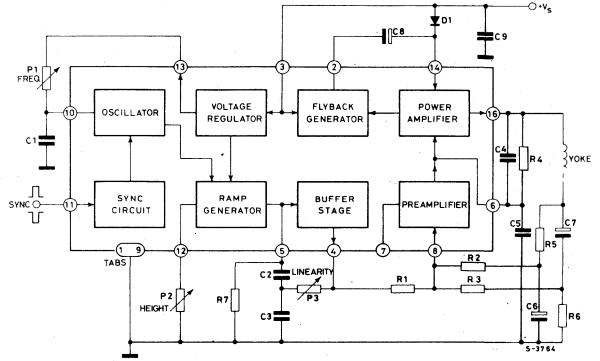
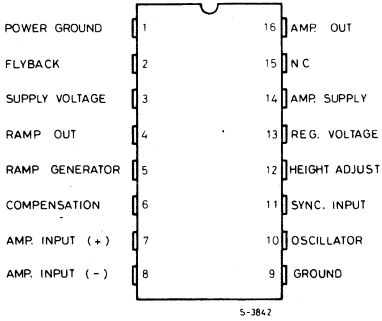
MECHANICAL DATA

Dimensions in mm



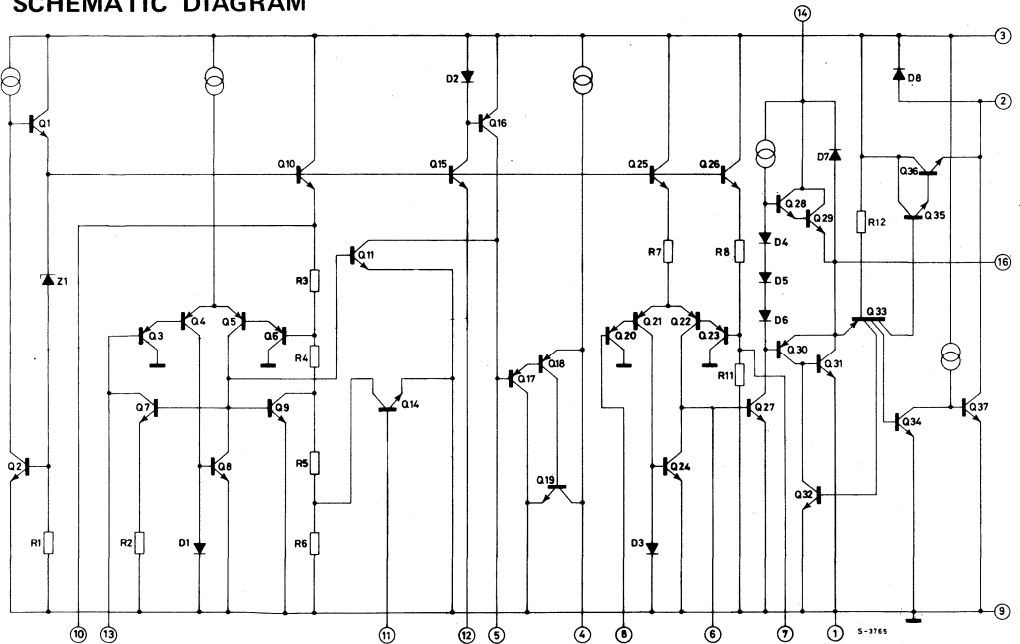
TDA 1470

CONNECTION AND BLOCK DIAGRAMS (top view)



The copper slug is electrically connected to pin 9 (substrate)

SCHEMATIC DIAGRAM



THERMAL DATA

$R_{th\ j-case}$	Thermal resistance junction–case TDA 1470 TDA 1470A	max	3	°C/W
$R_{th\ j-amb}$	Thermal resistance junction–ambient TDA 1470A	max	5	°C/W
		max	40	°C/W

DC ELECTRICAL CHARACTERISTICS (Refer to the DC test circuits, $V_s = 35V$, $T_{amb} = 25^\circ C$, unless otherwise specified)

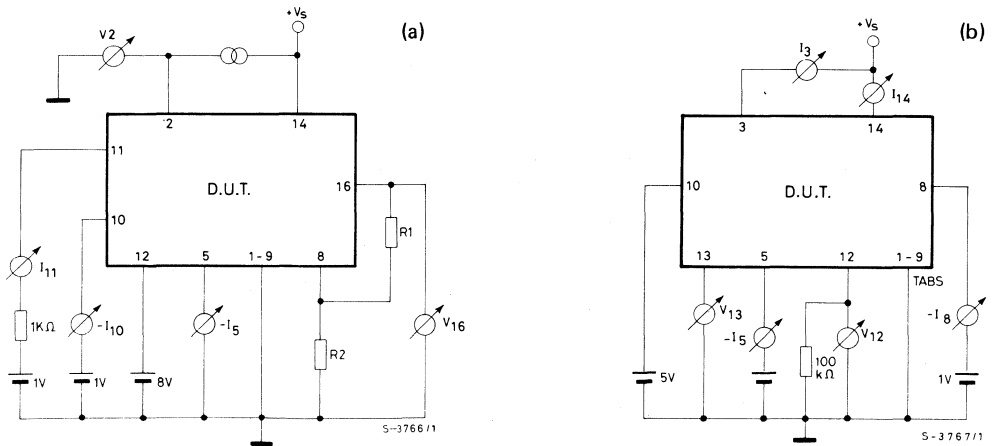
Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig.	
I_3	Pin 3 quiescent current	$I_2 = 0$	7		mA	1b	
I_{14}	Pin 14 quiescent current	$I_{16} = 0$	10		mA	1b	
$-I_{10}$	Oscillator bias current	$V_{10} = 1V$	0.1		μA	1a	
$-I_8$	Amplifier input bias current	$V_8 = 1V$	1		μA	1b	
$-I_5$	Ramp generator bias current	$V_5 = 0V$	0.02		μA	1a	
$-I_5$	Ramp generator current	$V_5 = 0V$ $I_{12} = 20\ \mu A$	20		μA	1b	
$\frac{\Delta I_5}{I_5}$	Ramp generator linearity	$\Delta V_5 = 0$ to 12V $I_{12} = 20\ \mu A$	0.2	1	%	1b	
V_s	Supply voltage range (pin 3)	10		35	V	—	
V_4	Pin 4 saturation voltage to ground	$I_4 = 1\ mA$	1	1.4	V	—	
V_2	Pin 2 saturation voltage to ground	$I_2 = 10\ mA$	0.5		V	1a	
V_{16}	Quiescent output voltage	$V_s = 10V$ $R_1 = 10K\Omega$ $R_2 = 10\ K\Omega$	4.15	4.45	4.73	V	1a
		$V_s = 35V$ $R_1 = 30\ K\Omega$ $R_2 = 10\ K\Omega$	8.3	8.9	9.45	V	1a
V_{16L}	Output saturation voltage to ground	$-I_{16} = 0.8A$		1.3		V	1c
		$-I_{16} = 1.5A$		1.7		V	1c

TDA 1470

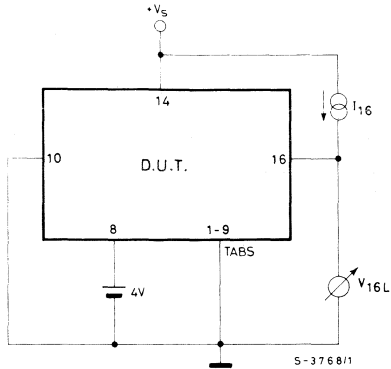
D.C. ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	Fig.
V_{16H} Output saturation voltage to supply	$I_{16} = 0.8A$		1.9		V	1d
	$I_{16} = 1.5A$		2.3		V	1d
V_{13} Regulated voltage at pin 13		6.1	6.5	6.9	V	1b
V_{12} Regulated voltage at pin 12	$I_{12} = 20 \mu A$	6.2	6.5	7	V	1b
$\frac{\Delta V_{13}}{\Delta V_s}; \frac{\Delta V_{12}}{\Delta V_s}$ Regulated voltages drift	$\Delta V_s = 10$ to $35V$		1		mV/V	1b
V_7 Amplifier input reference voltage		2.07	2.2	2.3	V	

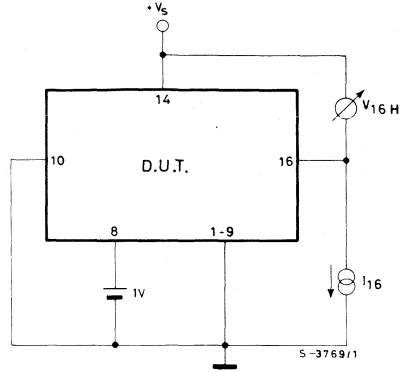
Fig. 1 - DC test circuits



(c)



(d)



AC ELECTRICAL CHARACTERISTICS (Refer to the AC test circuit $f = 50 \text{ Hz}$, $V_s = 24\text{V}$, unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s	Operating supply voltage		24		V
I_s	Supply current		270		mA
I_{11}	Sync. input current	500			μA
V_{16}	Flyback voltage		49		V
V_{10}	Peak to peak oscillator sawtooth voltage		2.4		V
t_{fly}	Flyback time		0.6		ms
f_o	Free running frequency	$R_1 + P_1 = 300 \text{ K}\Omega$ $C_2 = 100 \text{ nF}$	44		Hz
		$R_1 + P_1 = 260 \text{ K}\Omega$ $C_2 = 100 \text{ nF}$	52		Hz
Δf	Synchronization range	$I_{11} = 500 \mu\text{A}$	14		Hz
$\frac{\Delta f}{\Delta V_s}$	Frequency drift vs. supply voltage	$V_s = 10 \text{ to } 35\text{V}$	0.005		Hz/V
$\frac{\Delta f}{\Delta T_{\text{tab}}}$	Frequency drift vs. tab temperature	$T_{\text{amb}} = 40 \text{ to } 120^\circ\text{C}$	0.01		Hz/ $^\circ\text{C}$

TDA 1470

Fig. 2 - AC Test circuit

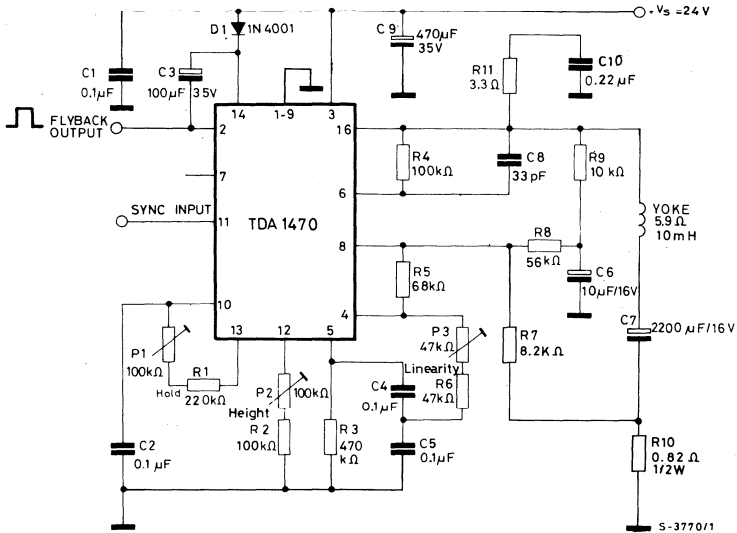


Fig. 3 - Relative output voltage drift vs. supply voltage

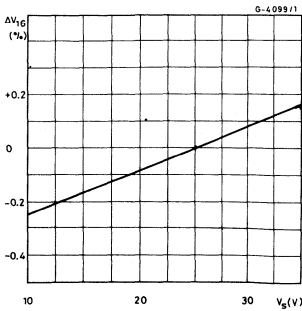


Fig. 4 - Relative output voltage drift vs. case temperature

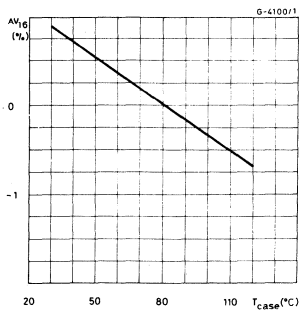
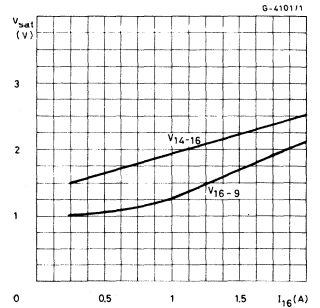
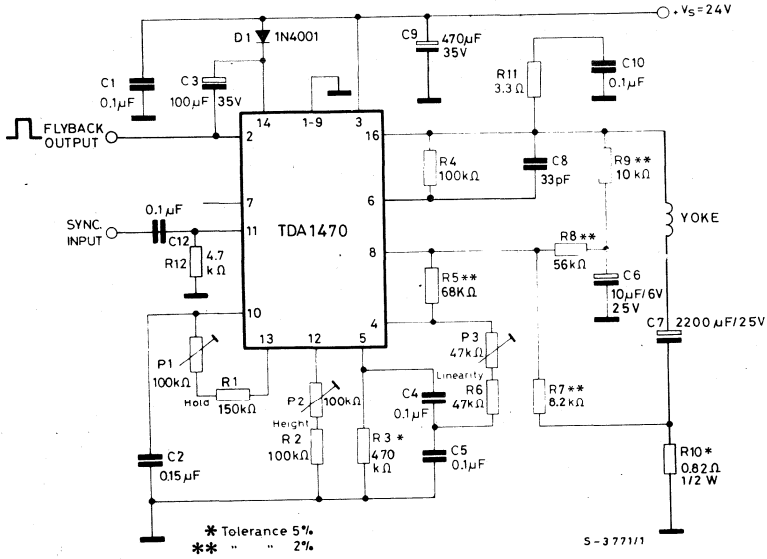


Fig. 5 - Output saturation voltage vs. output current



TDA 1470

Fig. 6 - Application circuit for large screen 110° TVC set ($R_y = 5.9\Omega$; $L_y = 10\text{ mH}$; $I_y = 1.95\text{ App}$)



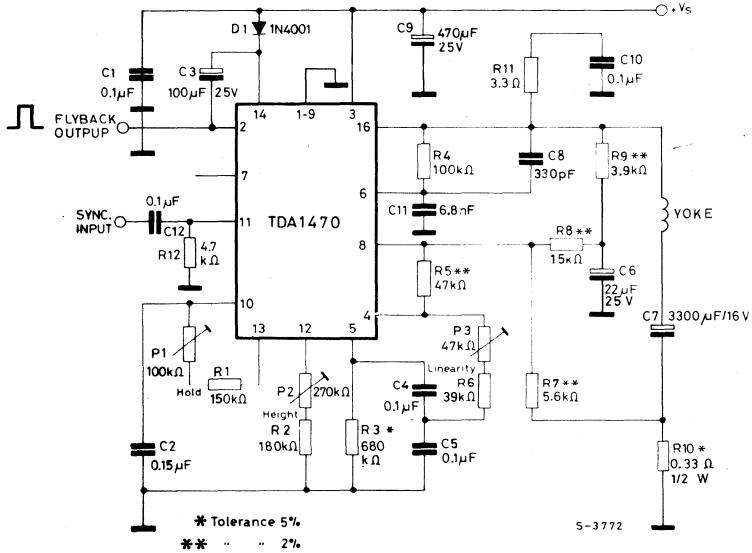
Typical performance

V_s	Operating supply voltage	24	V
I_s	Supply current	300	mA
t_{fly}	Flyback time	0.7	ms
P_d	TDA 1470 power dissipation	4	W
I_y	Maximum scanning current	2.3	App

For safe operation up to $T_{amb} = 60^\circ\text{C}$ a heatsink of $R_{th} = 7^\circ\text{C/W}$ is required.

TDA 1470

Fig. 7 – Application circuit for PIL 26" -110° parallel connected ($R_y = 2.5\Omega$; $L_y = 6.6\text{ mH}$; $I_y = 2.36\text{ App}$)

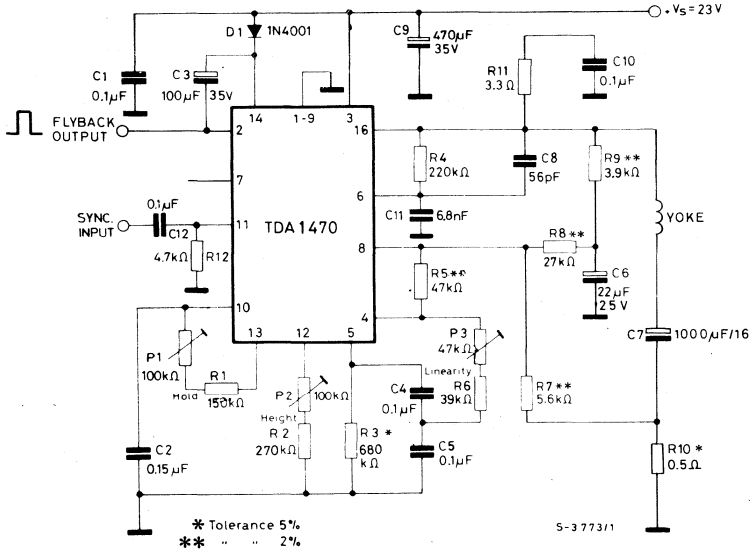


Typical performance

V_s	Operating supply voltage	16	V
I_s	Supply current	345	mA
t_{fly}	Flyback time	0.85	ms
P_d	TDA 1470 power dissipation	3.5	W
I_y	Maximum scanning current	2.5	App

For safe operation up to $T_{amb} = 60^\circ\text{C}$ a heatsink of $R_{th} = 8^\circ\text{C/W}$ is required.

Fig. 8 - Application circuit for PIL 26" -110° series connected ($R_y=9.7\Omega$; $L_y=26.4\text{ mH}$; $I_y=1.18\text{ App}$)



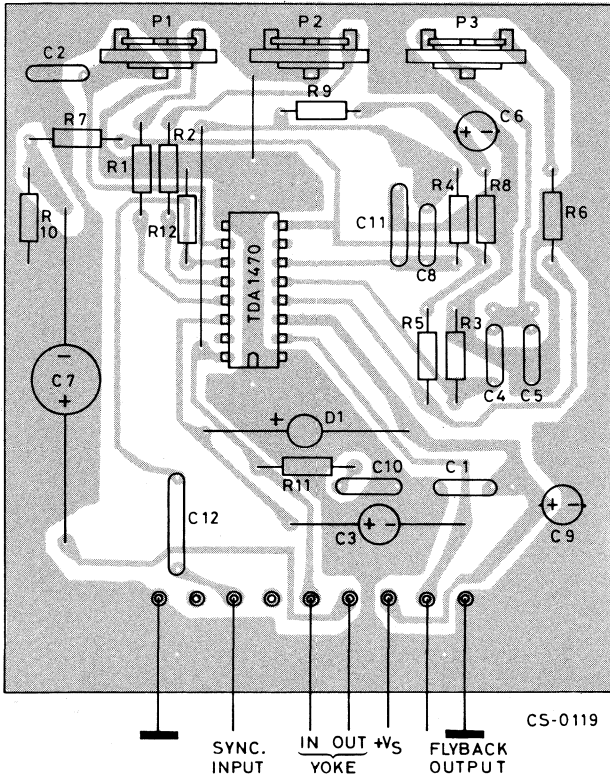
Typical performance

V_s	Operating supply voltage	23	V
I_s	Supply current	185	mA
t_{fly}	Flyback time	1	ms
P_d	TDA 1470 power dissipation	2.8	W
I_y	Maximum scanning current	1.4	App

For safe operation up to $T_{amb} = 60^\circ\text{C}$ a heatsink of $R_{th} = 10^\circ\text{C/W}$ is required.

TDA 1470

Fig. 9 - P.C. board and component layout (Application circuits of fig. 6, 7 and 8)



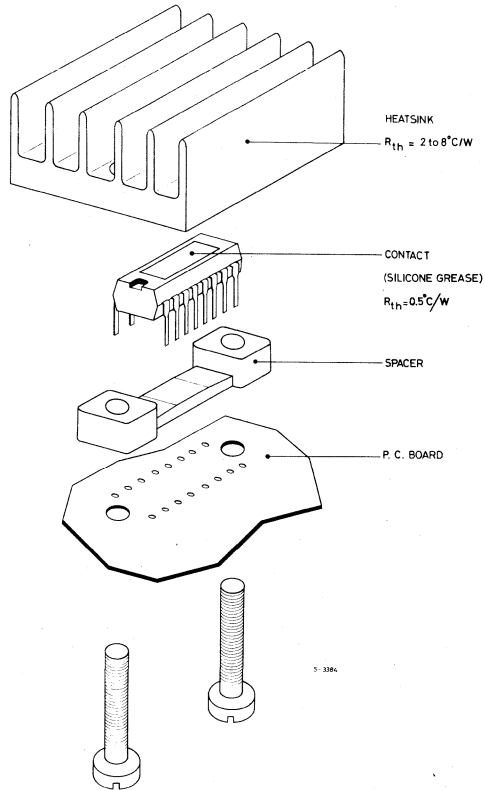
MOUNTING INSTRUCTIONS

The power dissipated in the circuit must be removed by adding an external heatsink as shown in fig. 10. The system for attaching the heatsink is very simple; it uses a plastic spacer which is supplied with the device on request (TDA 1470 F2).

Thermal contact between the copper slug (of the package) and the heatsink is guaranteed by the pressure which the screws exert via the printed circuit board, this is due to the particular shape of the spacer.

Note: The most negative supply voltage is connected to the copper slug, hence to the heatsink (because it is in contact with the slug).

Fig. 10 - Mounting system example (TDA 1470)



It is also possible to add an external heatsink to the TDA 1470A.
The external bar provides two threaded holes in order to allow the heatsink fixing.

TDA 1905

LINEAR INTEGRATED CIRCUIT

5W AUDIO POWER AMPLIFIER WITH MUTING

The TDA 1905 is a monolithic integrated circuit in POWERDIP package, intended for use as low frequency power amplifier in a wide range of applications in radio and TV sets. Its main features are:

- muting facility
- protection against chip over temperature
- very low noise
- high supply voltage rejection
- low "switch-on" noise
- voltage range 4V to 30V

The TDA 1905 is assembled in a new plastic package, the POWERDIP, that offers the same assembly ease, space and cost saving of a normal dual in-line package but with a power dissipation of up to 6W and a thermal resistance of 15°C/W (junction to pins).

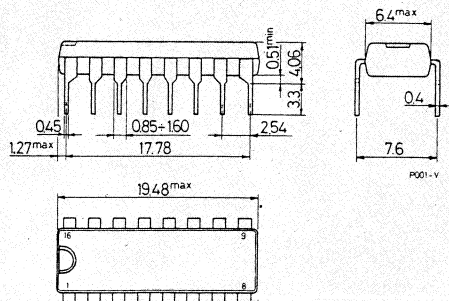
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	30	V
I_o	Output peak current (non repetitive)	3	A
I_o	Output peak current (repetitive)	2.5	A
V_i	Input voltage	0 to + V_s	V
V_i	Differential input voltage	± 7	V
V_{11}	Muting threshold voltage	V_s	V
P_{tot}	Power dissipation at $T_{amb} = 80^\circ\text{C}$	1	W
	$T_{case} = 60^\circ\text{C}$	6	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBER: TDA 1905

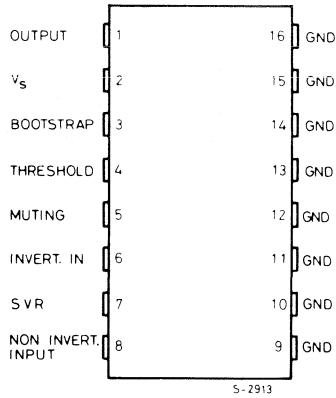
MECHANICAL DATA

Dimensions in mm

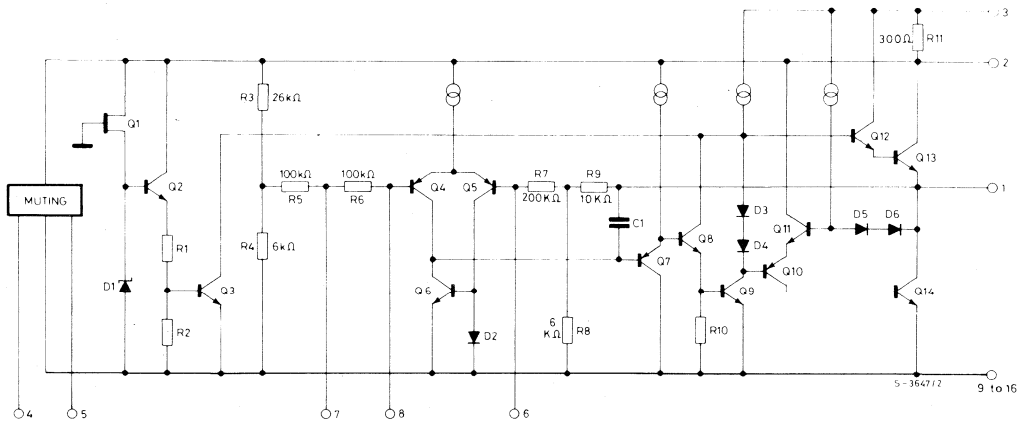


CONNECTION DIAGRAM

(Top view)



SCHEMATIC DIAGRAM

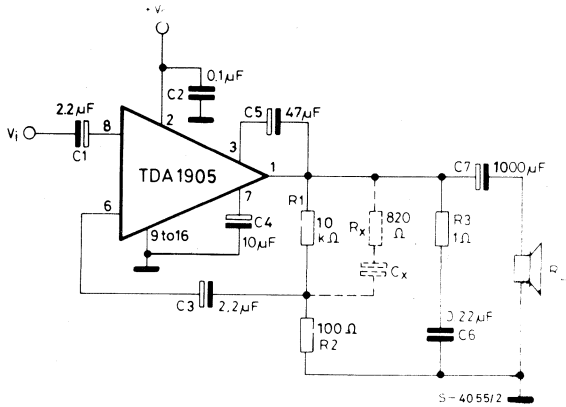


THERMAL DATA

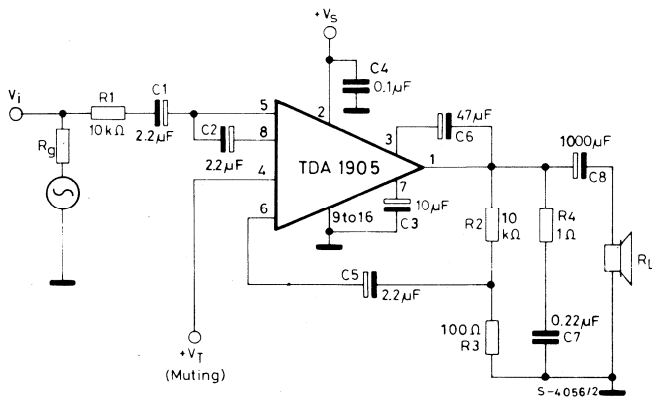
$R_{thj-case}$	Thermal resistance junction-pins	max	15 °C/W
$R_{thj-amb}$	Thermal resistance junction-amb	max	70 °C/W

TDA 1905

TEST CIRCUIT



MUTING CIRCUIT



TDA 1905

ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $T_{amb} = 25^{\circ}\text{C}$, R_{th} (heatsink) = 20°C/W , unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s Supply voltage		4		30	V
V_o Quiescent output voltage	$V_s = 4\text{V}$ $V_s = 14\text{V}$ $V_s = 30\text{V}$	1.6 6.7 14.4	2.1 7.2 15.5	2.5 7.8 16.8	V
I_d Quiescent drain current	$V_s = 4\text{V}$ $V_s = 14\text{V}$ $V_s = 30\text{V}$		15 17 21	35	mA
$V_{CE\ sat}$ Output stage saturation voltage	$I_C = 1\text{A}$ $I_C = 2\text{A}$		0.5 1		V
P_o Output power	$d = 10\%$ $f = 1\text{KHz}$ $V_s = 9\text{V}$ $R_L = 4\Omega$ (*) $V_s = 14\text{V}$ $R_L = 4\Omega$ $V_s = 18\text{V}$ $R_L = 8\Omega$ $V_s = 24\text{V}$ $R_L = 16\Omega$	2.2 5 5 4.5	2.5 5.5 5.5 5.3		W
d Harmonic distortion	$f = 1\text{KHz}$ $V_s = 9\text{V}$ $R_L = 4\Omega$ $P_o = 50\text{ mW to } 1.5\text{W}$ $V_s = 14\text{V}$ $R_L = 4\Omega$ $P_o = 50\text{ mW to } 3\text{W}$ $V_s = 18\text{V}$ $R_L = 8\Omega$ $P_o = 50\text{ mW to } 3\text{W}$ $V_s = 24\text{V}$ $R_L = 16\Omega$ $P_o = 50\text{ mW to } 3\text{W}$		0.1 0.1 0.1 0.1		%
V_i Input sensitivity	$f = 1\text{KHz}$ $V_s = 9\text{V}$ $R_L = 4\Omega$ $P_o = 2.5\text{W}$ $V_s = 14\text{V}$ $R_L = 4\Omega$ $P_o = 5.5\text{W}$ $V_s = 18\text{V}$ $R_L = 8\Omega$ $P_o = 5.5\text{W}$ $V_s = 24\text{V}$ $R_L = 16\Omega$ $P_o = 5.3\text{W}$		37 49 73 100		mV
V_i Input saturation voltage (rms)	$V_s = 9\text{V}$ $V_s = 14\text{V}$ $V_s = 18\text{V}$ $V_s = 24\text{V}$		0.8 1.3 1.8 2.4		V
R_i Input resistance (pin 8)	$f = 1\text{KHz}$	60	100		$\text{K}\Omega$
I_d Drain current	$f = 1\text{KHz}$ $V_s = 9\text{V}$ $R_L = 4\Omega$ $P_o = 2.5\text{W}$ $V_s = 14\text{V}$ $R_L = 4\Omega$ $P_o = 5.5\text{W}$ $V_s = 18\text{V}$ $R_L = 8\Omega$ $P_o = 5.5\text{W}$ $V_s = 24\text{V}$ $R_L = 16\Omega$ $P_o = 5.3\text{W}$		380 550 410 295		mA
η Efficiency	$f = 1\text{KHz}$ $V_s = 9\text{V}$ $R_L = 4\Omega$ $P_o = 2.5\text{W}$ $V_s = 14\text{V}$ $R_L = 4\Omega$ $P_o = 5.5\text{W}$ $V_s = 18\text{V}$ $R_L = 8\Omega$ $P_o = 5.5\text{W}$ $V_s = 24\text{V}$ $R_L = 16\Omega$ $P_o = 5.3\text{W}$		73 71 74 75		%

(*) With an external resistor of 100Ω between pin 3 and $+V_s$.

TDA 1905

ELECTRICAL CHARACTERISTICS (continued)

Parameter		Test conditions	Min.	Typ.	Max.	Unit
BW	Small signal bandwidth (-3dB)	$V_s = 14V$ $R_L = 4\Omega$ $P_o = 1W$	40 to 40,000			Hz
G_v	Voltage gain (open loop)	$V_s = 14V$ $f = 1KHz$		75		dB
G_v	Voltage gain (closed loop)	$V_s = 14V$ $R_L = 4\Omega$ $f = 1KHz$ $P_o = 1W$	39.5	40	40.5	dB
e_N	Total input noise	$R_g = 50\Omega$ $R_g = 1K\Omega$ $(^\circ)$ $R_g = 10K\Omega$		1.2 1.3 1.5	4.0	μV
		$R_g = 50\Omega$ $R_g = 1K\Omega$ $(^{\circ\circ})$ $R_g = 10K\Omega$		2.0 2.0 2.2	6.0	μV
S/N	Signal to noise ratio	$V_s = 14V$ $R_g = 10K\Omega$ $P_o = 5.5W$ $R_g = 0$ $(^\circ)$ $R_L = 4\Omega$		90 92		dB
		$R_g = 10K\Omega$ $(^{\circ\circ})$ $R_g = 0$		87 87		dB
SVR	Supply voltage rejection	$V_s = 18V$ $R_L = 8\Omega$ $f_{ripple} = 100 Hz$ $R_g = 10K\Omega$ $V_{ripple} = 0.5V_{rms}$	40	50		dB
T_{sd}	Thermal shut-down case temperature (*)	$P_{tot} = 2.5W$		115		$^\circ C$

MUTING FUNCTION (Refer to Muting circuit)

V_{TOFF}	Muting-off threshold voltage (pin 4)		1.9		4.7	V
V_{TON}	Muting-on threshold voltage (pin 4)		0		1.3	V
			6.2		V_s	
R_5	Input resistance (pin 5)	Muting off	80	200		$K\Omega$
		Muting on		10	30	Ω
R_4	Input resistance (pin 4)		150			$K\Omega$
A_T	Muting attenuation	$R_g + R_1 = 10K\Omega$	50	60		dB

Note:

- ($^\circ$) Weighting filter = curve A.
- ($^{\circ\circ}$) Filter with noise bandwidth: 22 Hz to 22 KHz.
- (*) See fig. 30 and fig. 31

Fig. 1 - Quiescent output voltage vs. supply voltage

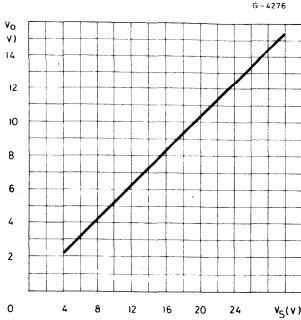


Fig. 2 - Quiescent drain current vs. supply voltage

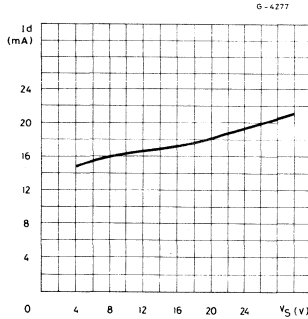


Fig. 3 - Output power vs. supply voltage

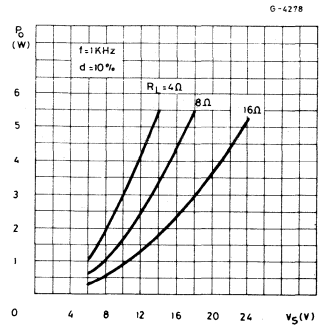


Fig. 4 - Distortion vs. output power ($R_L = 16\Omega$)

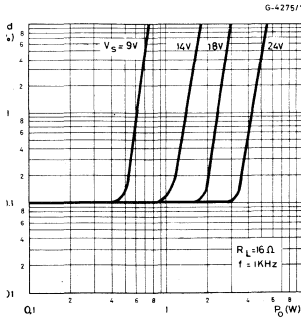


Fig. 5 - Distortion vs. output power ($R_L = 8\Omega$)

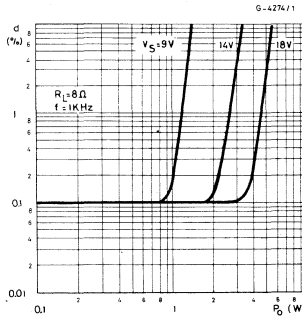


Fig. 6 - Distortion vs. output power ($R_L = 4\Omega$)

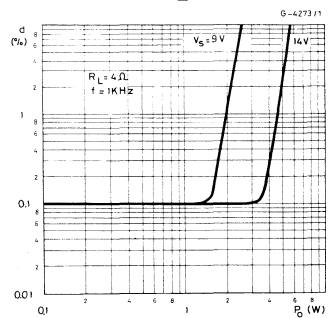


Fig. 7 - Distortion vs. frequency ($R_L = 16\Omega$)

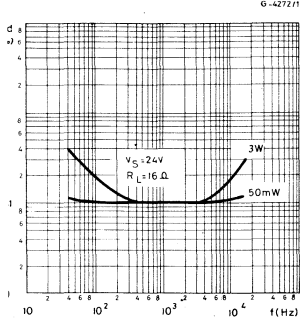


Fig. 8 - Distortion vs. frequency ($R_L = 8\Omega$)

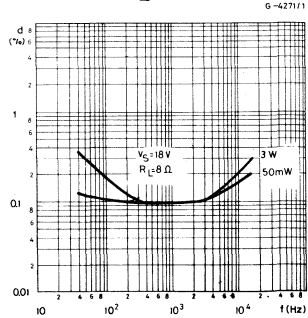
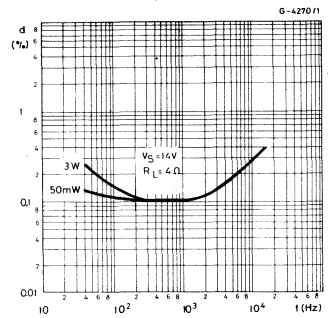


Fig. 9 - Distortion vs. frequency ($R_L = 4\Omega$)



TDA 1905

Fig. 10 - Open loop frequency response

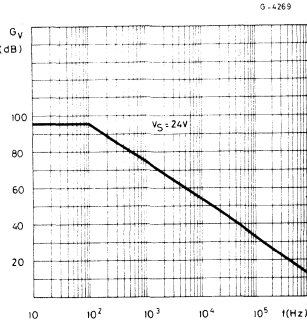


Fig. 11 - Output power vs. input voltage

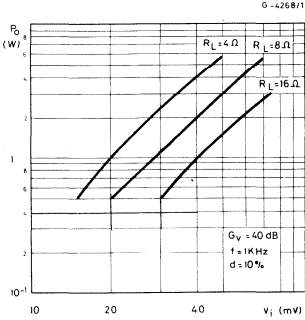


Fig. 12 - Value of capacitor C_x vs. bandwidth (BW) and gain (G_v)

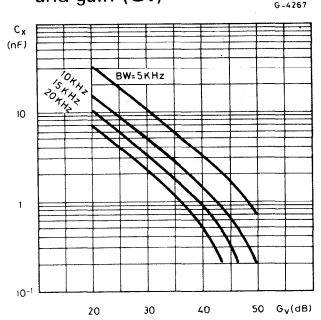


Fig. 13 - Supply voltage rejection vs. voltage gain (ref. to the Muting circuit)

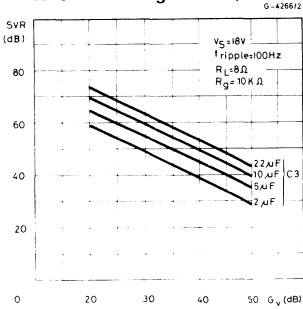


Fig. 14 - Supply voltage rejection vs. source resistance

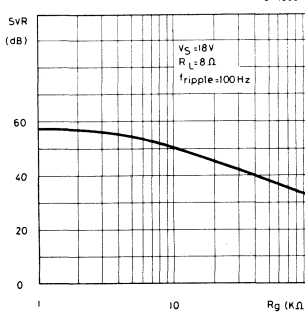


Fig. 15 - Max power dissipation vs. supply voltage (sine wave operation)

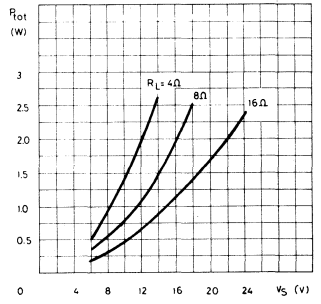


Fig. 16 - Power dissipation and efficiency vs. output power

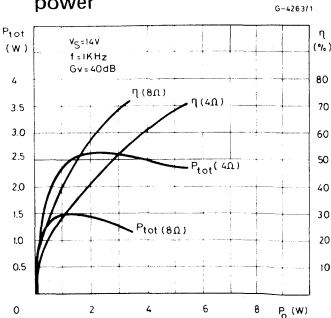


Fig. 17 - Power dissipation and efficiency vs. output power

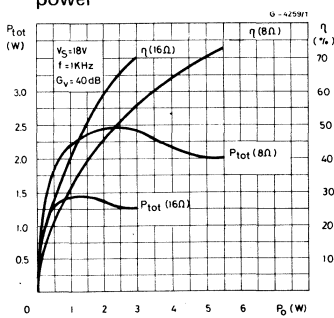
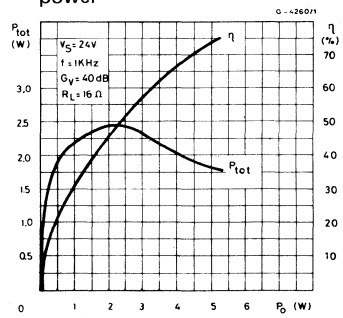
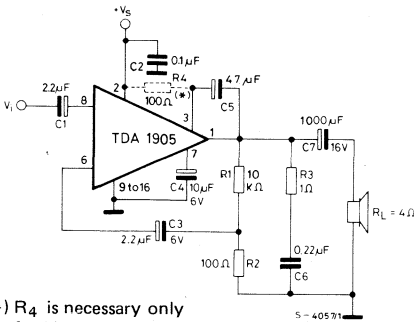


Fig. 18 - Power dissipation and efficiency vs. output power



APPLICATION INFORMATION

Fig. 19 - Application circuit without muting



(*) R₄ is necessary only for V_s < 10V.

P_O = 5.5W (d = 10%)
 V_s = 14V
 I_d = 0.55A
 G_v = 40 dB

Fig. 20 - PC board and components lay-out of the circuit of fig. 19 (1:1 scale)

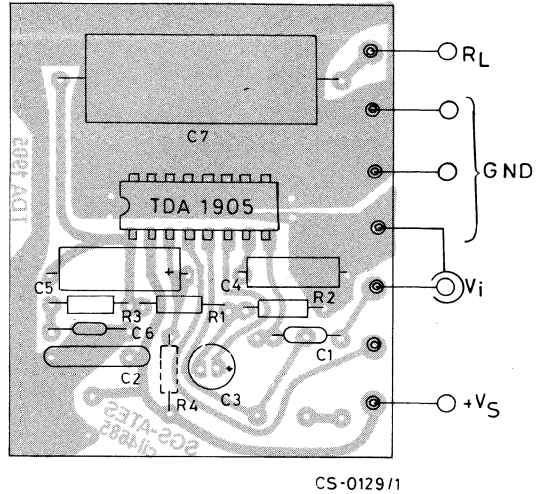


Fig. 21 - Application circuit with muting

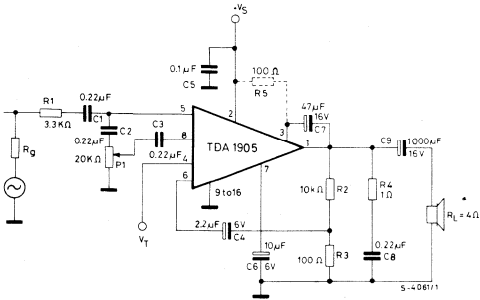
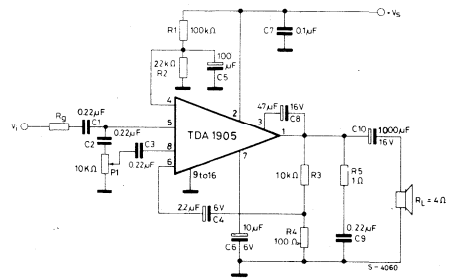


Fig. 22 - Delayed muting circuit



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APPLICATION INFORMATION (continued)

Fig. 23 - Low-cost application circuit without bootstrap.

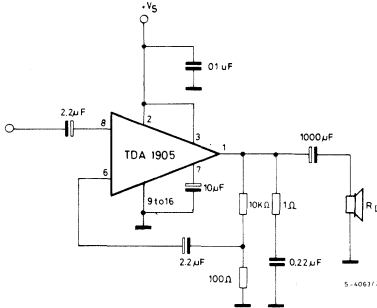


Fig. 25 - Two position DC tone control using change of pin 5 resistance (muting function)

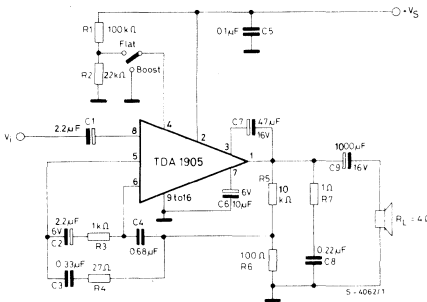


Fig. 27 - Bass Bomb tone control using change of pin 5 resistance (muting function)

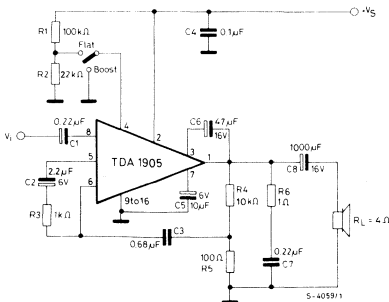


Fig. 24 - Output power vs. supply voltage (circuit of fig. 23)

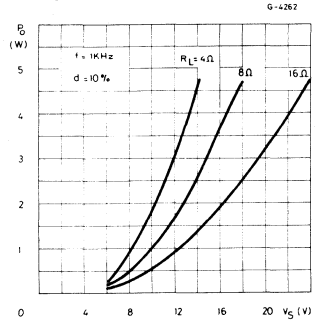


Fig. 26 - Frequency response of the circuit of fig. 25

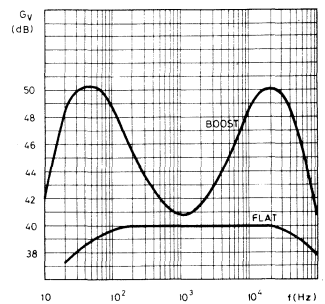
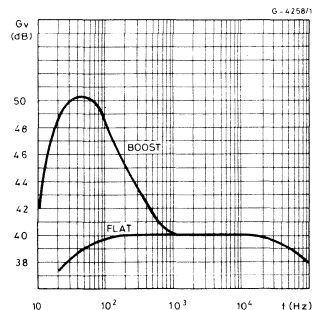


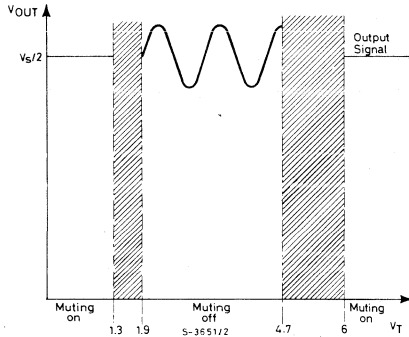
Fig. 28 - Frequency response of the circuit of fig. 27



MUTING FUNCTION

The output signal can be inhibited applying a DC voltage V_T to pin 4, as shown in fig. 29

Fig. 29

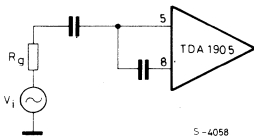


The input resistance at pin 5 depends on the threshold voltage V_T at pin 4 and is typically:

$$R_5 = 200 \text{ K}\Omega \quad @ \quad 1.9V \leq V_T \leq 4.7V \quad \text{muting-off}$$

$$R_5 = 10\Omega \quad @ \quad \begin{matrix} 0V \leq V_T \leq 1.3V \\ 6V \leq V_T \leq V_s \end{matrix} \quad \text{muting-on}$$

Referring to the following input stage, the possible attenuation of the input signal and therefore of the output signal can be found using the following expression:



$$A_T = \frac{V_i}{V_8} = \frac{R_g + \left(\frac{R_8 \cdot R_5}{R_8 + 5}\right)}{\left(\frac{R_8 \cdot R_5}{R_8 + R_5}\right)}$$

where $R_8 \approx 100 \text{ K}\Omega$

Considering $R_g = 10 \text{ K}\Omega$ the attenuation in the muting-on condition is typically $A_T = 60 \text{ dB}$. In the muting-off condition, the attenuation is very low, typically 1.2 dB .

A very low current is necessary to drive the threshold voltage V_T because the input resistance at pin 4 is greater than $150 \text{ K}\Omega$. The muting function can be used in many cases, when a temporary inhibition of the output signal is requested, for example:

- in switch-on condition, to avoid preamplifier power-on transients (see fig. 22)
- during switching at the input stages.
- during the receiver tuning.

The variable impedance capability at pin 5 can be useful in many application and two examples are shown in fig. 25 and 27, where it has been used to change the feedback network, obtaining 2 different frequency response.

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APPLICATION SUGGESTION

The recommended values of the external components are those shown on the application circuit of fig. 21. When the supply voltage V_s is less than 10V, a 100Ω resistor must be connected between pin 2 and pin 3 in order to obtain the maximum output power.

Different values can be used. The following table can help the designer.

Component	Raccom. value	Purpose	Larger than recommended value	Smaller than recommended value	Allowed range	
					Min.	Max.
$R_g + R_1$	10K Ω	Input signal impeded, for muting operation	Increase of the attenuation in muting-on condition. Decrease of the input sensitivity.	Decrease of the attenuation in muting on condition.		
R_2	10K Ω	Feedback resistors	Increase of gain.	Decrease of gain. Increase quiescent current.	$9 R_3$	
R_3	100 Ω		Decrease of gain.	Increase of gain.		1K Ω
R_4	1 Ω	Frequency stability	Danger of oscillation at high frequencies with inductive loads.			
R_5	100 Ω	Increase of the output swing with low supply voltage.			47	330
P_1	20K Ω	Volume potentiometer	Increase of the switch-on noise.	Decrease of the input impedance and of the input level.	10K Ω	100K Ω
C_1 C_2 C_3	0.22 μ F	Input DC decoupling.	Higher cost lower noise.	Higher low frequency cutoff. Higher noise		
C_4	2.2 μ F	Inverting input DC decoupling.	Increase of the switch-on noise.	Higher low frequency cutoff.	0.1 μ F	
C_5	0.1 μ F	Supply voltage bypass.		Danger of oscillations.		
C_6	10 μ F	Ripple rejection	Increase of SVR increase of the switch-on time	Degradation of SVR	2.2 μ F	100 μ F
C_7	47 μ F	Bootstrap.		Increase of the distortion at low frequency.	10 μ F	100 μ F
C_8	0.22 μ F	Frequency stability.		Danger of oscillation.		
C_9	1000 μ F	Output DC decoupling.		Higher low frequency cutoff.		

THERMAL SHUT-DOWN

The presence of a thermal limiting circuit offers the following advantages:

- 1) An overload on the output (even if it is permanent), or an above limit ambient temperature can be easily tolerated since the T_j cannot be higher than 150°C .
- 2) The heatsink can have a smaller factor of safety compared with that of a conventional circuit. There is no possibility of device damage due to high junction temperature. If for any reason, the junction temperature increases up to 150°C , the thermal shut-down simply reduces the power dissipation and the current consumption.

The maximum allowable power dissipation depends upon the size of the external heatsink (i.e. its thermal resistance); fig. 32 shows this dissipable power as a function of ambient temperature for different thermal resistance.

Fig. 30 - Output power and drain current vs. case temperature.

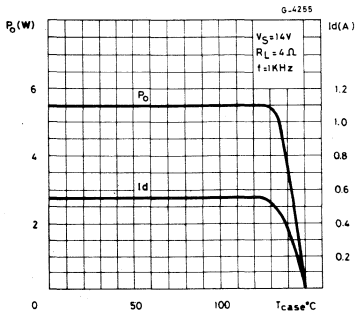


Fig. 31 - Output power and drain current vs. case temperature

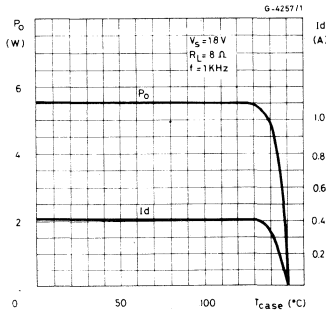
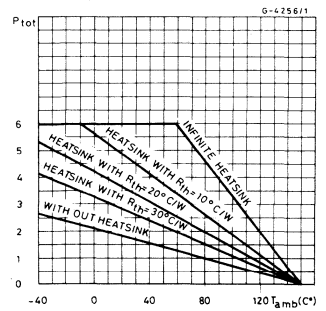


Fig. 32 - Maximum allowable power dissipation vs. ambient temperature.



TDA 1905

MOUNTING INSTRUCTION

The TDA 1905 is assembled in a new plastic package, the Powerdip, in which 8 pins (from 9 to 16) are attached to the frame and remove the heat produced by the chip.

Figure 33 and 34 show two ways of heatsinking. In the first case, a PC board copper area is used as a heatsink $l = 65$ mm, while in the second case, the device is soldered to an external heatsink. In both examples, the thermal resistance junction-ambient is 35°C/W .

Fig. 33 - Example of heatsink using PC board copper ($l = 65$ mm)

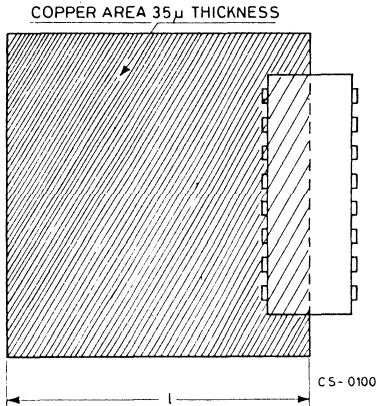
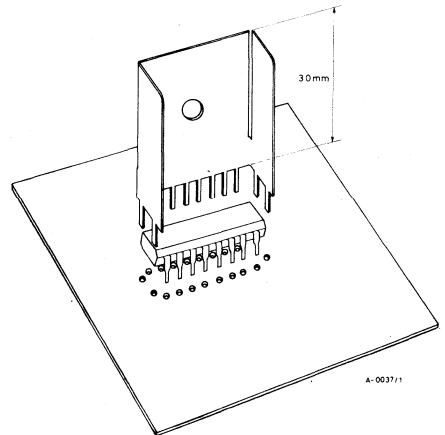


Fig. 34 - Example of an external heatsink



LINEAR INTEGRATED CIRCUITS

8W AUDIO POWER AMPLIFIER

The TDA 1908 is a monolithic integrated circuit in 12 lead quad in-line plastic package intended for low frequency power applications. The mounting is compatible with SGS-ATES TBA 800, TBA 810S, TCA 830S and TCA 940N. Its main features are:

- flexibility in use with a max output current of 3A and an operating supply voltage range of 4V to 30V
- protection against chip overtemperature
- soft limiting in saturation conditions
- low "switch-on" noise
- low number of external components
- high supply voltage rejection
- very low noise

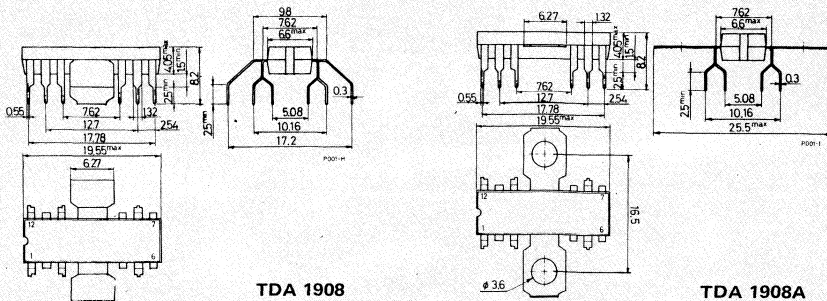
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	30	V
I_o	Output peak current (non repetitive)	3.5	A
I_{oR}	Output peak current (repetitive)	3	A
P_{tot}	Power dissipation: at $T_{amb} = 80^\circ\text{C}$ (TDA 1908)	1	W
	at $T_{tab} = 100^\circ\text{C}$ (TDA 1908A)	5	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBERS: TDA 1908, TDA 1908A

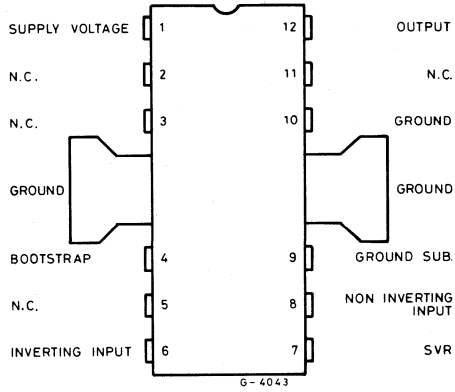
MECHANICAL DATA

Dimensions in mm

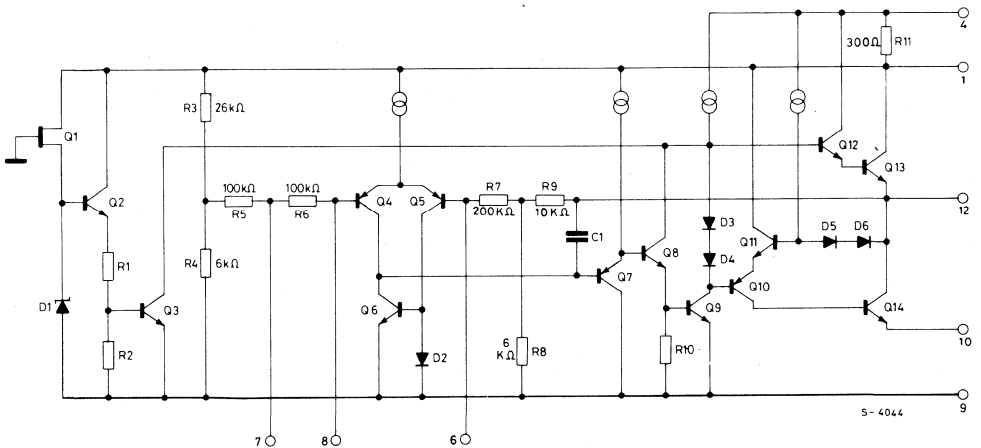


TDA 1908 TDA 1908A

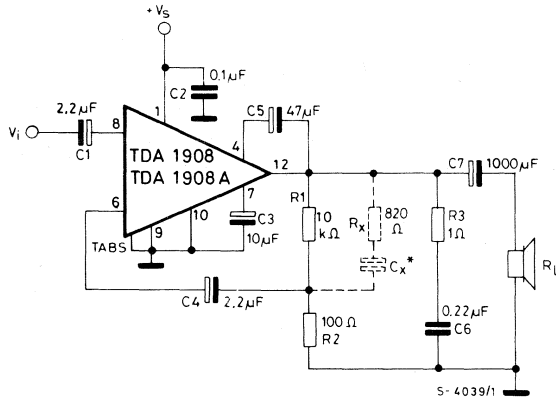
CONNECTION DIAGRAM (top view)



SCHEMATIC DIAGRAM



TEST CIRCUIT



* See fig. 12.

THERMAL DATA

			TDA 1908	TDA 1908A
$R_{th\ j-tab}$	Thermal resistance junction-tab	max	12 °C/W	10 °C/W
$R_{th\ j-amb}$	Thermal resistance junction-amb	max	(°) 70 °C/W	80 °C/W

(°) Obtained with tabs soldered to printed circuit board with min copper area.

ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $T_{amb} = 25^{\circ}\text{C}$, $R_{th}(\text{heatsink}) = 8^{\circ}\text{C/W}$, unless otherwise specified)

Parameter	Test condition	Min.	Typ.	Max.	Unit	
V_s	Supply voltage	4		30	V	
V_o	Quiescent output voltage	$V_s = 4\text{V}$ $V_s = 18\text{V}$ $V_s = 30\text{V}$	1.6 8.2 14.4	2.1 9.2 15.5	2.5 10.2 16.8	V
I_d	Quiescent drain current	$V_s = 4\text{V}$ $V_s = 18\text{V}$ $V_s = 30\text{V}$		15 17.5 21	35	mA
V_{CEsat}	Output stage saturation voltage (each output transistor)	$I_C = 1\text{A}$ $I_C = 2.5\text{A}$		0.5 1.3		V
P_o	Output power	$d = 10\%$ $f = 1\text{ KHz}$ $V_s = 9\text{V}$ $V_s = 14\text{V}$ $V_s = 18\text{V}$ $V_s = 22\text{V}$ $V_s = 24\text{V}$ $R_L = 4\Omega$ $R_L = 4\Omega$ $R_L = 4\Omega$ $R_L = 8\Omega$ $R_L = 16\Omega$		2.5 5.5 7 6.5 4.5		W

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ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test condition	Min.	Typ.	Max	Unit
d Harmonic distortion	$f = 1 \text{ KHz}$ $V_s = 9\text{V}$ $R_L = 4\Omega$ $P_o = 50 \text{ mW to } 1.5\text{W}$ $V_s = 18\text{V}$ $R_L = 4\Omega$ $P_o = 50 \text{ mW to } 4\text{W}$ $V_s = 24\text{V}$ $R_L = 16\Omega$ $P_o = 50 \text{ mW to } 3\text{W}$		0.1 0.1 0.1		%
V_i Input sensitivity	$V_s = 9\text{V}$ $R_L = 4\Omega$ $P_o = 2.5\text{W}$ $V_s = 14\text{V}$ $R_L = 4\Omega$ $P_o = 5.5\text{W}$ $V_s = 18\text{V}$ $R_L = 4\Omega$ $P_o = 9\text{W}$ $V_s = 22\text{V}$ $R_L = 8\Omega$ $P_o = 8\text{W}$ $V_s = 24\text{V}$ $R_L = 16\Omega$ $P_o = 5.3\text{W}$		37 52 64 90 110		mV
V_i Input saturation voltage (rms)	$V_s = 9\text{V}$ $V_s = 14\text{V}$ $V_s = 18\text{V}$ $V_s = 24\text{V}$	0.8 1.3 1.8 2.4			V
R_i Input resistance (pin 8)	$f = 1 \text{ KHz}$	60	100		K Ω
I_s Drain current	$f = 1 \text{ KHz}$ $V_s = 14\text{V}$ $R_L = 4\Omega$ $P_o = 5.5\text{W}$ $V_s = 18\text{V}$ $R_L = 4\Omega$ $P_o = 9\text{W}$ $V_s = 22\text{V}$ $R_L = 8\Omega$ $P_o = 8\text{W}$ $V_s = 24\text{V}$ $R_L = 16\Omega$ $P_o = 5.3\text{W}$		570 730 500 310		mA
η Efficiency	$V_s = 18\text{V}$ $f = 1 \text{ KHz}$ $R_L = 4\Omega$ $P_o = 9\text{W}$		72		%
BW Small signal bandwidth (-3 dB)	$V_s = 18\text{V}$ $R_L = 4\Omega$ $P_o = 1\text{W}$	40 to 40 000			Hz
G_v Voltage gain (open loop)	$f = 1 \text{ KHz}$		75		dB
G_v Voltage gain (closed loop)	$V_s = 18\text{V}$ $R_L = 4\Omega$ $f = 1 \text{ KHz}$ $P_o = 1\text{W}$	39.5	40	40.5	dB
e_N Total input noise	(°)	$R_g = 50\Omega$ $R_g = 1\text{K}\Omega$ $R_g = 10\text{K}\Omega$	1.2 1.3 1.5	4.0	μV
	(°°)	$R_g = 50\Omega$ $R_g = 1\text{K}\Omega$ $R_g = 10\text{K}\Omega$	2.0 2.0 2.2	6.0	μV
S/N Signal to noise ratio	$V_s = 18\text{V}$ $P_o = 9\text{W}$ $R_L = 4\Omega$	$R_g = 10\text{K}\Omega$ (°) $R_g = 0$	92 94		dB
		$R_g = 10\text{K}\Omega$ (°°) $R_g = 0$	88 90		dB
SVR Supply voltage rejection	$V_s = 18\text{V}$ $R_L = 4\Omega$ $f_{\text{ripple}} = 100 \text{ Hz}$ $R_g = 10\text{K}\Omega$	40	50		dB
T_{sd} Thermal shut-down case temperature (*)	$P_{\text{tot}} = 4\text{W}$		110		°C

Note:

(°) Weighting filter = curve A.

(°°) Filter with noise bandwidth: 22 Hz to 22 KHz.

(*) See fig. 24 and fig. 25.

Fig. 1 - Quiescent output voltage vs. supply voltage

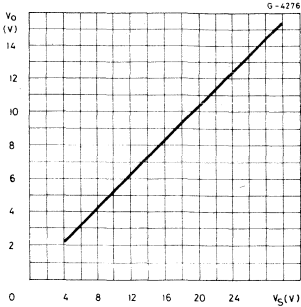


Fig. 2 - Quiescent drain current vs. supply voltage

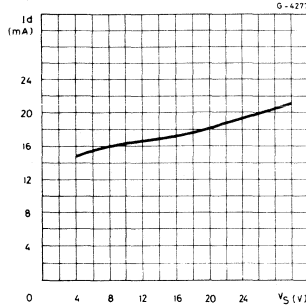


Fig. 3 - Output power vs. supply voltage

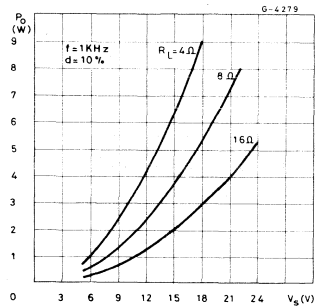


Fig. 4 - Distortion vs. output power ($R_L = 16\Omega$)

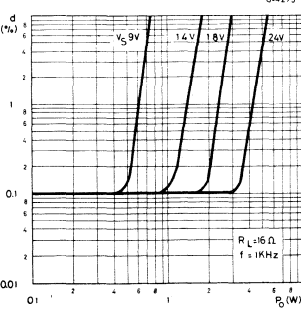


Fig. 5 - Distortion vs. output power ($R_L = 8\Omega$)

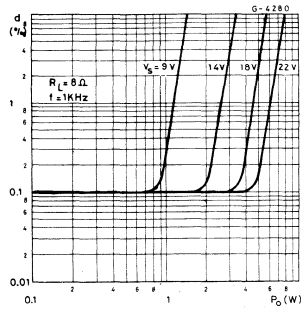


Fig. 6 - Distortion vs. output power ($R_L = 4\Omega$)

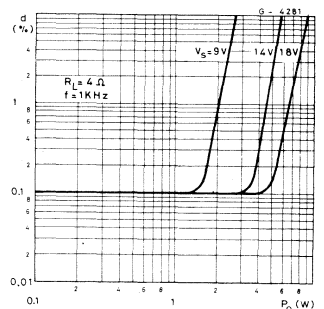


Fig. 7 - Distortion vs. frequency ($R_L = 16\Omega$)

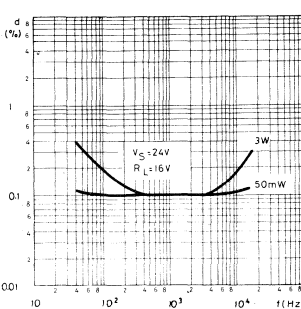


Fig. 8 - Distortion vs. frequency ($R_L = 8\Omega$)

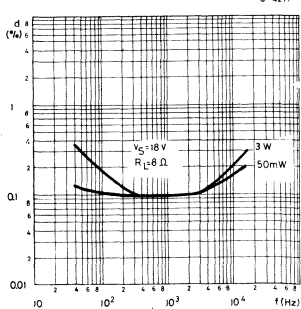
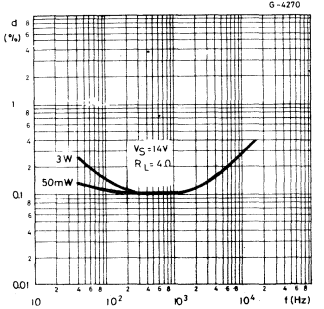


Fig. 9 - Distortion vs. frequency ($R_L = 4\Omega$)



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Fig. 10 - Open loop frequency response

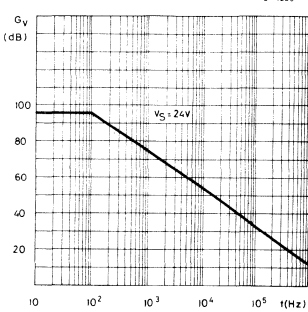


Fig. 11 - Output power vs. input voltage

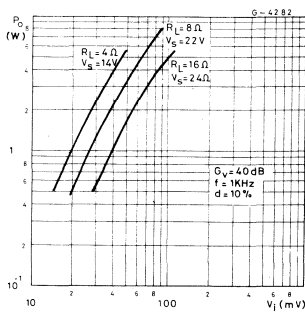


Fig. 12 - Values of capacitor C_x versus gain and B_w

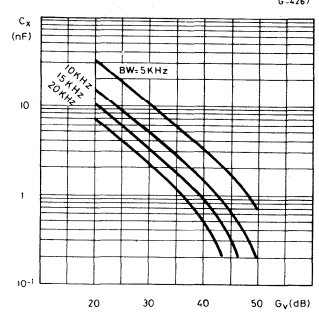


Fig. 13 - Supply voltage rejection vs. voltage gain

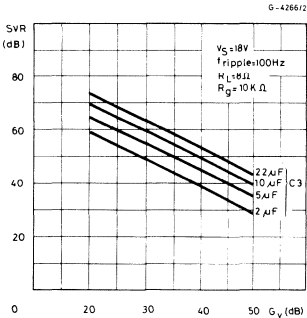


Fig. 14 - Supply voltage rejection vs. source resistance

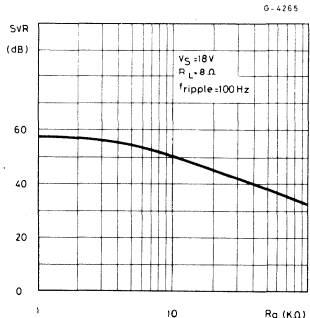


Fig. 15 - Max power dissipation vs. supply voltage

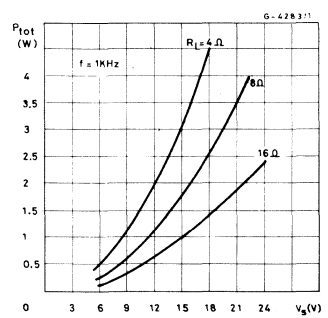


Fig. 16 - Power dissipation and efficiency vs. output power ($V_S = 14V$)

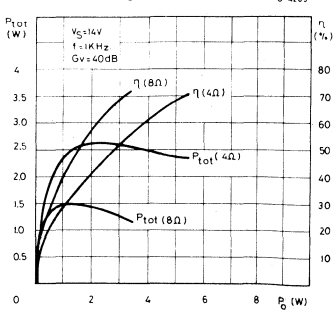


Fig. 17 - Power dissipation and efficiency vs. output power ($V_S = 18V$)

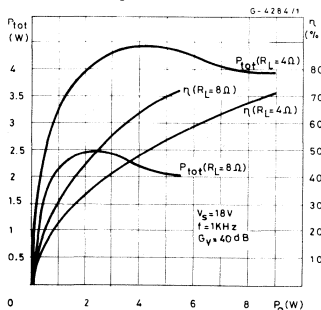
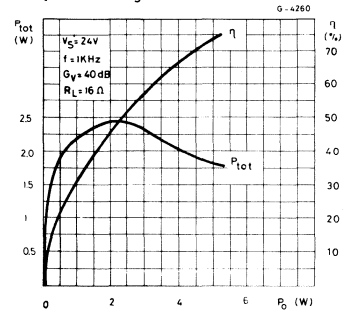
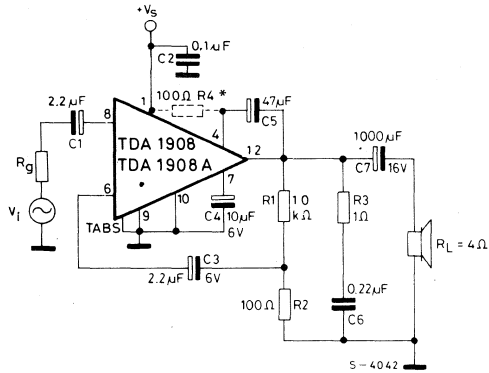


Fig. 18 - Power dissipation and efficiency vs. output power ($V_S = 24V$)



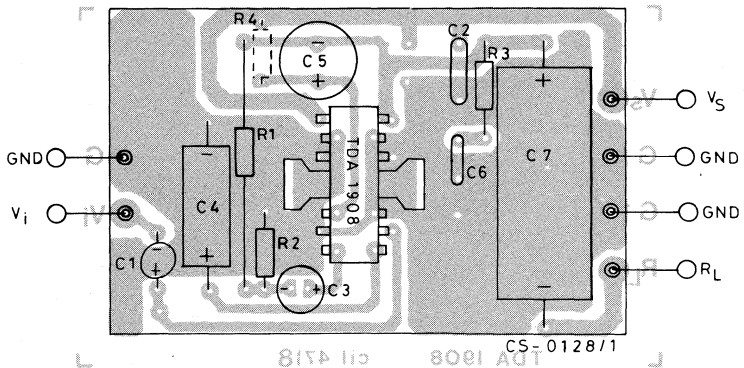
APPLICATION INFORMATION

Fig. 19 - Application circuit with bootstrap



* R4 is necessary when V_S is less than 10V.

Fig. 20 - P.C. board and component lay-out of the circuit of fig. 19 (1:1 scale)



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APPLICATION INFORMATION (continued)

Fig. 21 - Application circuit without bootstrap

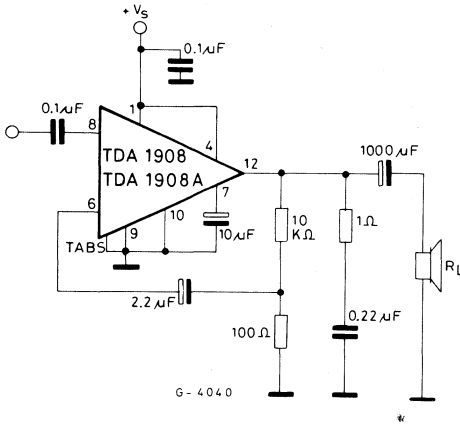


Fig. 22 - Output power vs. supply voltage (circuit of fig. 21)

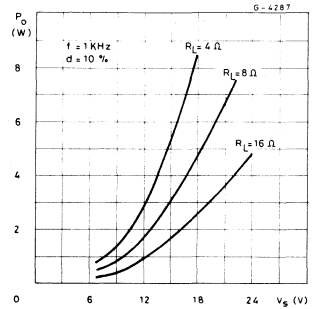
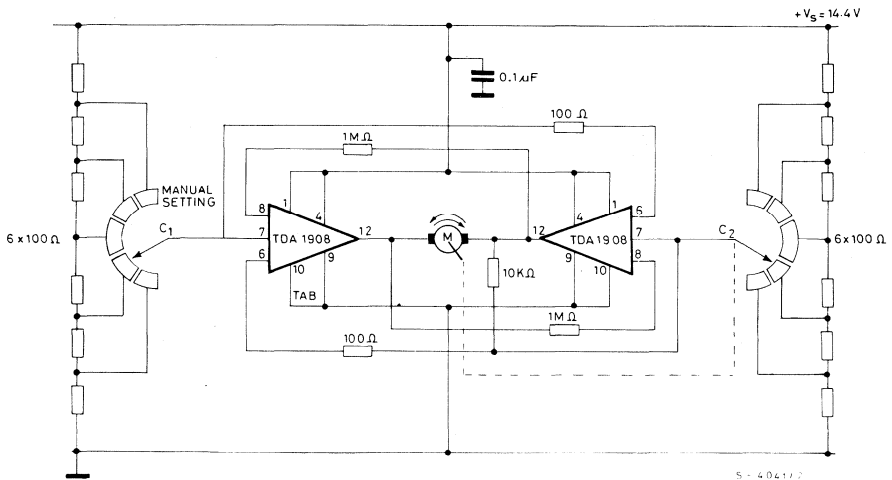


Fig. 23 - Position control for car headlights



APPLICATION SUGGESTION

The recommended values of the external components are those shown on the application circuit of fig. 19.

When the supply voltage V_s is less than 10V, a 100 Ω resistor must be connected between pin 1 and pin 4 in order to obtain the maximum output power.

Different values can be used. The following table can help the designer.

Component	Raccom. value	Purpose	Larger than raccomanded value	Smaller than raccomanded value	Allowed range	
					Min.	Max.
R ₁	10 K Ω	Close loop gain setting.	Increase of gain.	Decrease of gain. Increase quiescent current.	9 R ₂	
R ₂	100 Ω	Close loop gain setting.	Decrease of gain.	Increase of gain.		R ₁ /9
R ₃	1 Ω	Frequency stability	Danger of oscillation at high frequencies with inductive loads.			
R ₄	100 Ω	Increasing of output swing with low V_s .			47 Ω	330 Ω
C ₁	2.2 μ F	Input DC decoupling.	Lower noise	Higher low frequency cutoff. Higher noise.	0.1 μ F	
C ₂	0.1 μ F	Supply voltage bypass.		Danger of oscillations.		
C ₃	2.2 μ F	Inverting input DC decoupling.	Increase of the switch-on noise	Higher low frequency cutoff.	0.1 μ F	
C ₄	10 μ F	Ripple Rejection.	Increase of SVR. Increase of the switch-on time.	Degradation of SVR.	2.2 μ F	100 μ F
C ₅	47 μ F	Bootstrap		Increase of the distortion at low frequency	10 μ F	100 μ F
C ₆	0.22 μ F	Frequency stability.		Danger of oscillation.		
C ₇	1000 μ F	Output DC decoupling.		Higher low frequency cutoff.		

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THERMAL SHUT-DOWN

The presence of a thermal limiting circuit offers the following advantages:

- 1) An overload on the output (even if it is permanent), or an above limit ambient temperature can be easily supported since the T_j cannot be higher than 150°C .
- 2) The heatsink can have a smaller factor of safety compared with that of a conventional circuit. There is no possibility of device damage due to high junction temperature.
If, for any reason, the junction temperature increases up to 150°C , the thermal shut-down simply reduces the power dissipation and the current consumption.

The maximum allowable power dissipation depends upon the size of the external heatsink (i.e. its thermal resistance); fig. 26 shows this dissipable power as a function of ambient temperature for different thermal resistance.

Fig. 24 - Output power and drain current vs. case temperature

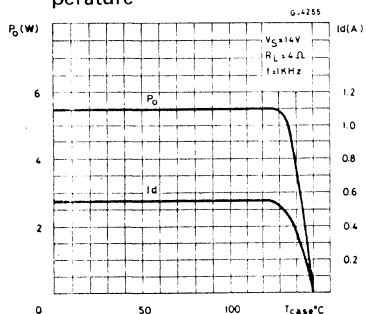


Fig. 25 - Output power and drain current vs. case temperature

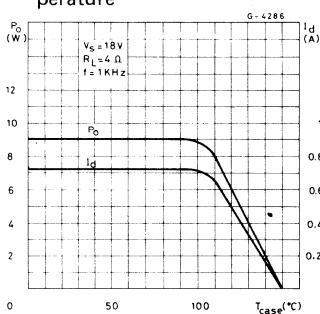
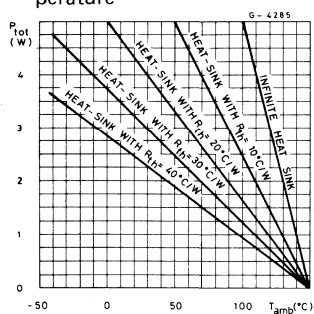


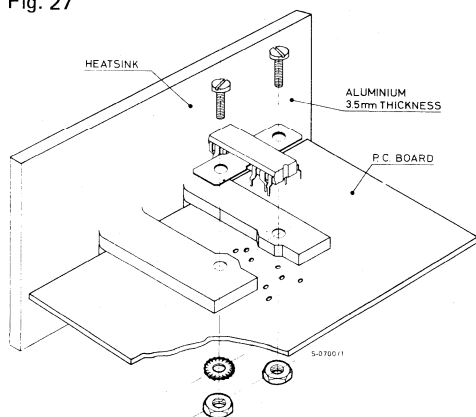
Fig. 26 - Maximum power dissipation vs. ambient temperature



MOUNTING INSTRUCTIONS

The thermal power dissipated in the circuit may be removed by connecting the tabs to an external heatsink (TDA 1908A see fig. 27), or by soldering them to a copper area on the PC board (TDA 1908 see fig. 28). During soldering, tab temperature must not exceed 260°C and the soldering time must not be longer than 12 seconds.

Fig. 27



MOUNTING INSTRUCTIONS (continued)

Fig. 28 - Mounting example (TDA 1908)

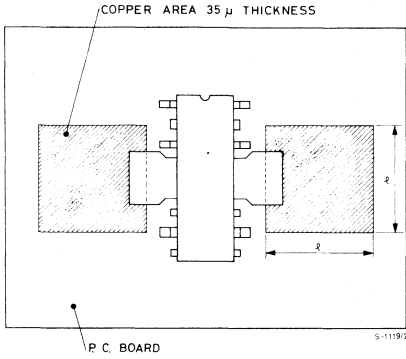
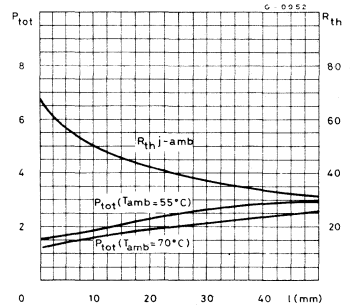


Fig. 29 - Maximum power dissipation and thermal resistance vs. side "l" (TDA 1908)



TDA 1910

LINEAR INTEGRATED CIRCUIT

10W Hi-Fi AUDIO POWER AMPLIFIER WITH MUTING

The TDA 1910 is a monolithic integrated circuit in MULTIWATT[®] package, intended for use in Hi-Fi audio power applications, as **high quality TV sets**.

The TDA 1910 meets the DIN 45500 ($d = 0.5\%$) guaranteed output power of 10W when used at 24V/4 Ω . At 24V/8 Ω the output power is 7W min. Features:

- muting facility
- protection against chip over temperature
- very low noise
- high supply voltage rejection
- low "switch-on" noise.

The TDA 1910 is assembled in MULTIWATT[®] package that offers:

- easy assembly
- simple heatsink
- space and cost saving
- high reliability.

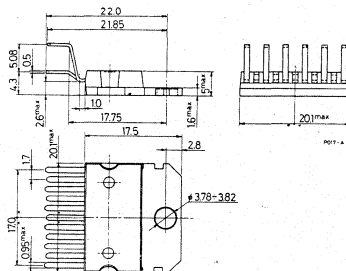
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	30	V
I_o	Output peak current (non repetitive)	3.5	A
I_o	Output peak current (repetitive)	3.0	A
V_i	Input voltage	0 to + V_s	V
V_i	Differential input voltage	± 7	V
V_{11}	Muting threshold voltage	V_s	V
P_{tot}	Power dissipation at $T_{case} = 90^\circ\text{C}$	20	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBER: TDA 1910

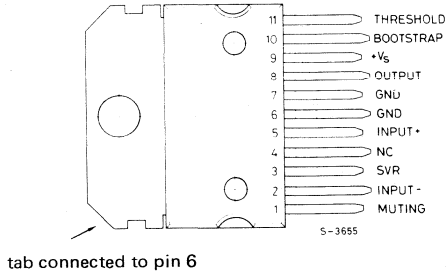
MECHANICAL DATA

Dimensions in mm

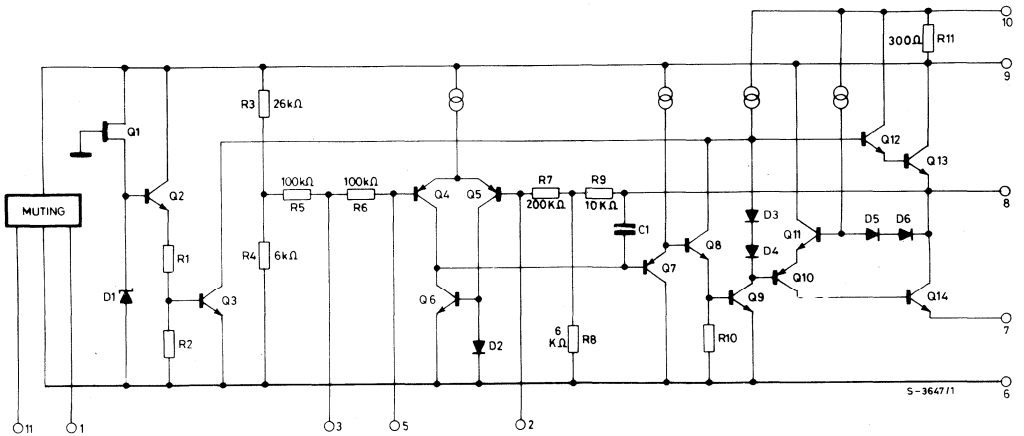


TDA 1910

CONNECTION DIAGRAM (Top view)

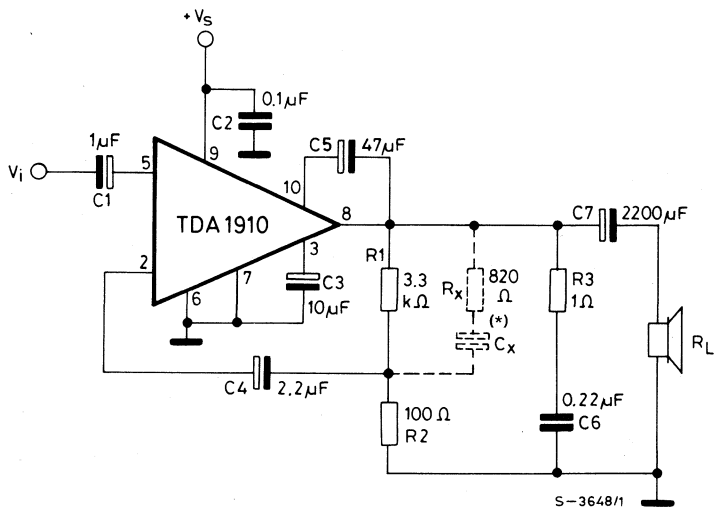


SCHEMATIC DIAGRAM



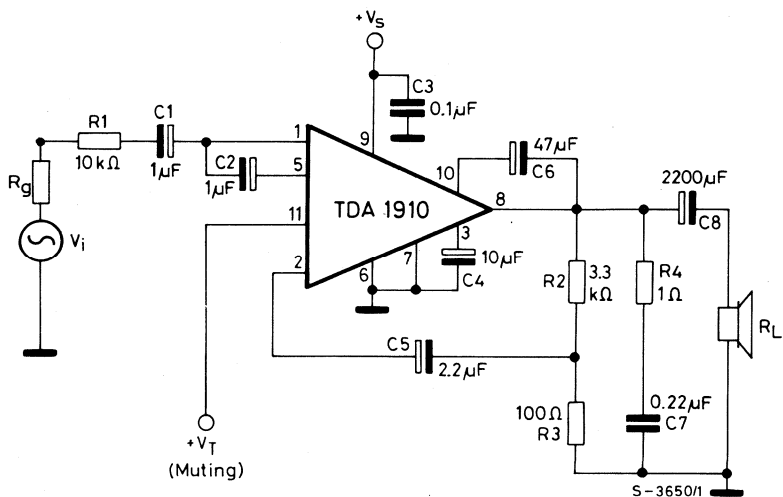
TDA 1910

TEST CIRCUIT



(*) See fig. 13.

MUTING CIRCUIT



THERMAL DATA

$R_{th\ j-c}$ Thermal resistance junction-case	max 3 °C/W
--	------------

ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $T_{amb} = 25^{\circ}\text{C}$, R_{th} (heatsink) = 4°C/W , unless otherwise specified)

Parameter	Test condition	Min.	Typ.	Max.	Unit
V_s Supply voltage		8		30	V
V_o Quiescent output voltage	$V_s = 18\text{V}$ $V_s = 24\text{V}$	8.3 11.5	9.2 12.4	10 13.4	V
I_d Quiescent drain current	$V_s = 18\text{V}$ $V_s = 24\text{V}$		19 21	32 35	mA
$V_{CE\ sat}$ Output stage saturation voltage	$I_C = 2\text{A}$		1		V
	$I_C = 3\text{A}$		1.6		
P_o Output power	$d = 0.5\%$ $f = 40$ to $15,000\text{Hz}$ $V_s = 18\text{V}$ $R_L = 4\Omega$ $V_s = 24\text{V}$ $R_L = 4\Omega$ $V_s = 24\text{V}$ $R_L = 8\Omega$	6.5 10 7	7 12 7.5		W
	$d = 10\%$ $f = 1\text{KHz}$ $V_s = 18\text{V}$ $R_L = 4\Omega$ $V_s = 24\text{V}$ $R_L = 4\Omega$ $V_s = 24\text{V}$ $R_L = 8\Omega$	8.5 15 9	9.5 17 10		W
d Harmonic distortion	$f = 40$ to $15,000\text{ Hz}$ $V_s = 18\text{V}$ $R_L = 4\Omega$ $P_o = 50\text{ mW}$ to 6.5W $V_s = 24\text{V}$ $R_L = 4\Omega$ $P_o = 50\text{ mW}$ to 10W $V_s = 24\text{V}$ $R_L = 8\Omega$ $P_o = 50\text{ mW}$ to 7W		0.2 0.2 0.2	0.5 0.5 0.5	%
d Intermodulation distortion	$V_s = 24\text{V}$ $R_L = 4\Omega$ $P_o = 10\text{W}$ $f_1 = 250\text{ Hz}$ $f_2 = 8\text{ KHz}$ (DIN 45500)		0.2		%
V_i Input sensitivity	$f = 1\text{ KHz}$ $V_s = 18\text{V}$ $R_L = 4\Omega$ $P_o = 7\text{W}$ $V_s = 24\text{V}$ $R_L = 4\Omega$ $P_o = 12\text{W}$ $V_s = 24\text{V}$ $R_L = 8\Omega$ $P_o = 7.5\text{W}$		170 220 245		mV
V_j Input saturation voltage (rms)	$V_s = 18\text{V}$ $V_s = 24\text{V}$	1.8 2.4			V
R_i Input resistance (pin 5)	$f = 1\text{ KHz}$	60	100		K Ω
I_d Drain current	$V_s = 24\text{V}$ $f = 1\text{ KHz}$ $R_L = 4\Omega$ $P_o = 12\text{W}$ $R_L = 8\Omega$ $P_o = 7.5\text{W}$		820 475		mA

TDA 1910

ELECTRICAL CHARACTERISTICS (continued)

Parameter		Test condition		Min.	Typ.	Max.	Unit
η	Efficiency	$V_s = 24V$ $R_L = 4\Omega$ $R_L = 8\Omega$	$f = 1\text{ KHz}$ $P_o = 12W$ $P_o = 7.5W$		62 65		%
BW	Small signal bandwidth	$V_s = 24V$	$R_L = 4\Omega$	$P_o = 1W$		10 to 120,000	Hz
BW	Power bandwidth	$V_s = 24V$ $P_o = 12W$	$R_L = 4\Omega$ $d \leq 0.5\%$			40 to 15,000	Hz
G_v	Voltage gain (open loop)	$f = 1\text{ KHz}$			75		dB
G_v	Voltage gain (closed loop)	$V_s = 24V$ $f = 1\text{ KHz}$	$R_L = 4\Omega$ $P_o = 1W$	29.5	30	30.5	dB
e_N	Total input noise	$R_g = 50\Omega$ $R_g = 1K\Omega$ ($^{\circ}$) $R_g = 10K\Omega$			1.2 1.3 1.5	3.0 3.2 4.0	μV
		$R_g = 50\Omega$ $R_g = 1K\Omega$ ($^{\infty}$) $R_g = 10K\Omega$			2.0 2.0 2.2	5.0 5.2 6.0	μV
S/N	Signal to noise ratio	$V_s = 24V$ $P_o = 12W$ $R_L = 4\Omega$	$R_g = 10K\Omega$ ($^{\circ}$) $R_g = 0$	97	103 105		dB
			$R_g = 10K\Omega$ ($^{\infty}$) $R_g = 0$	93	100 100		dB
SVR	Supply voltage rejection	$V_s = 24V$ $f_{\text{ripple}} = 100\text{ Hz}$	$R_L = 4\Omega$ $R_g = 10K\Omega$	50	60		dB
T_{sd}	Thermal shut-down case temperature (*)	$P_{\text{tot}} = 8W$		110	125		$^{\circ}C$

MUTING FUNCTION (Refer to Muting circuit)

V_T	Muting-off threshold voltage (pin 11)		1.9		4.7	V
V_T	Muting-on threshold voltage (pin 11)		0		1.3	V
			6		V_s	
R_1	Input resistance (pin 1)	Muting off	80	200		$K\Omega$
		Muting on		10	30	Ω
R_{11}	Input resistance (pin 11)		150			$K\Omega$
A_T	Muting attenuation	$R_g + R_1 = 10\text{ K}\Omega$	50	60		dB

Note:

($^{\circ}$) Weighting filter = curve A.

($^{\infty}$) Filter with noise bandwidth: 22 Hz to 22 KHz.

(*) See fig. 29 and fig. 30.

Fig. 1 - Quiescent output voltage vs. supply voltage

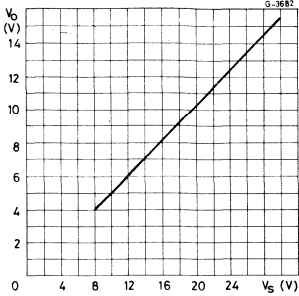


Fig. 2 - Quiescent drain current vs. supply voltage

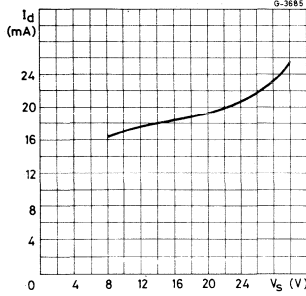


Fig. 3 - Open loop frequency response

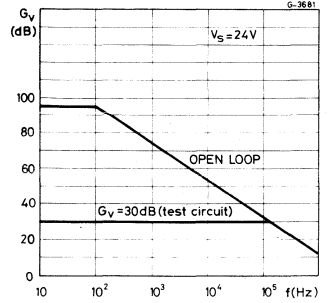


Fig. 4 - Output power vs. supply voltage

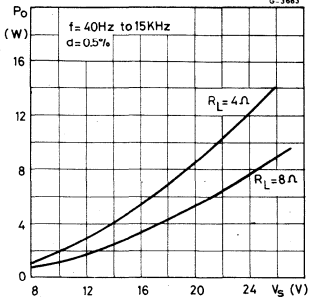


Fig. 5 - Output power vs. supply voltage

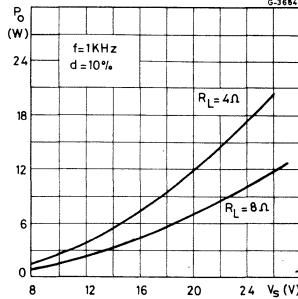


Fig. 6 - Distortion vs. output power

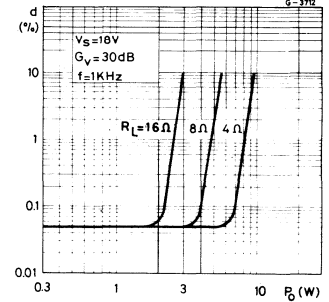


Fig. 7 - Distortion vs. output power

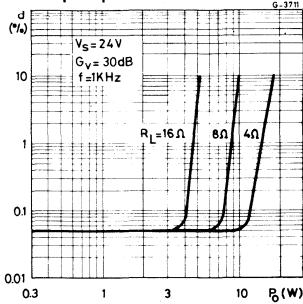


Fig. 8 - Output power vs. frequency

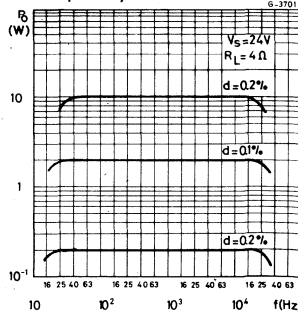
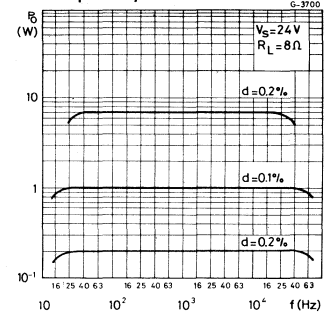


Fig. 9 - Output power vs. frequency



TDA 1910

Fig. 10 - Output power vs. input voltage

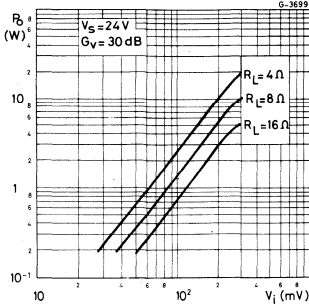


Fig. 11 - Output power vs. input voltage

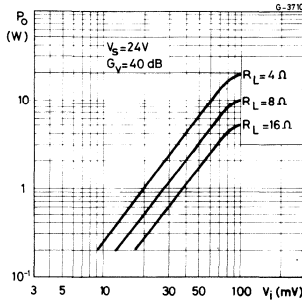


Fig. 12 - Total input noise vs. source resistance

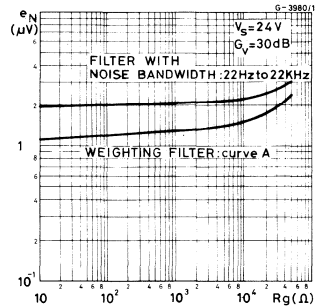


Fig. 13 - Values of capacitor C_x vs. bandwidth (BW) and gain (G_v)

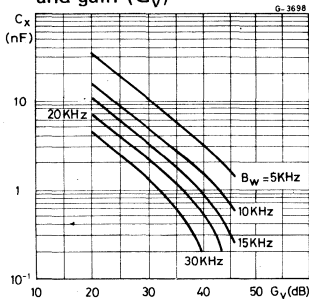


Fig. 14 - Supply voltage rejection vs. voltage gain

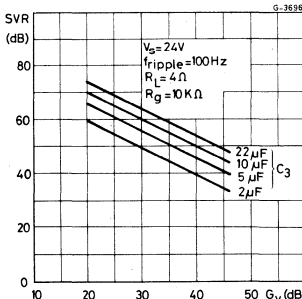


Fig. 15 - Supply voltage rejection vs. source resistance

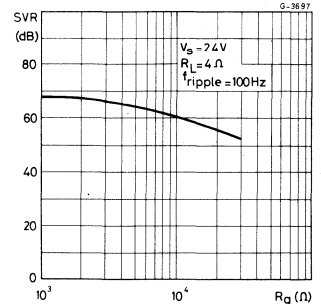


Fig. 16 - Power dissipation and efficiency vs. output power

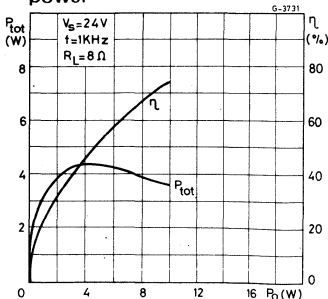


Fig. 17 - Power dissipation and efficiency vs. output power

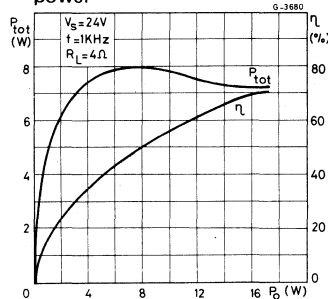
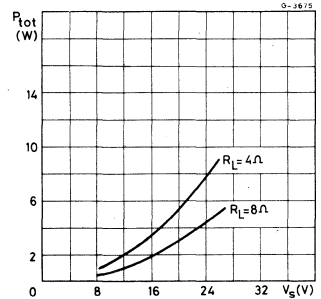


Fig. 18 - Max power dissipation vs. supply voltage



APPLICATION INFORMATION

Fig. 19 - Application circuit without muting

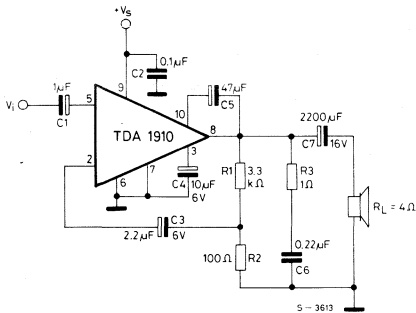


Fig. 20 - PC board and component lay-out of the circuit of fig. 19 (1:1 scale)

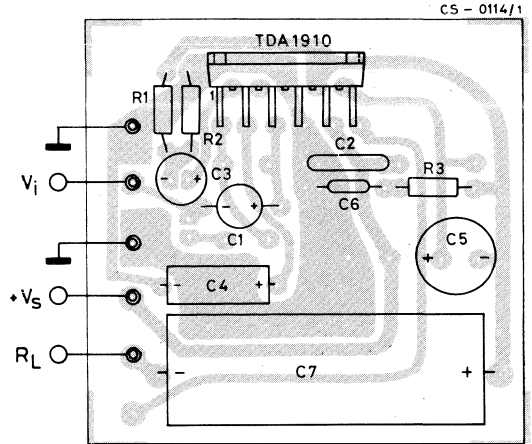
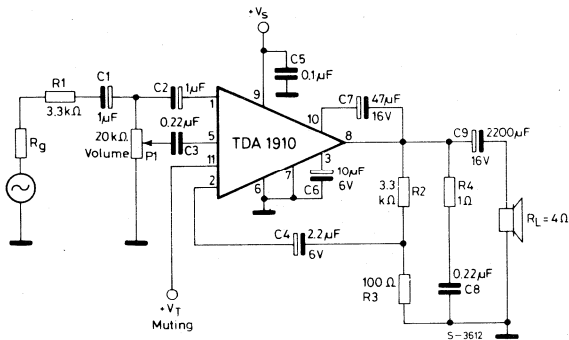


Fig. 21 - Application circuit with muting



Performance (circuits of fig. 19 and 21)

$P_o = 12W$ (40 to 15000 Hz, $d \leq 0.5\%$)

$V_s = 24V$

$I_d = 0.82A$

$G_v = 30 dB$

TDA 1910

APPLICATION INFORMATION (continued)

Fig. 22 - Two position DC tone control (10 dB boost 50 Hz and 20 KHz) using change of pin 1 resistance (muting function)

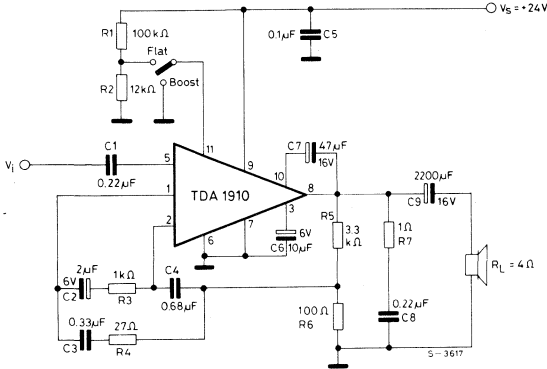


Fig. 23 - Frequency response of the circuit of Fig. 22

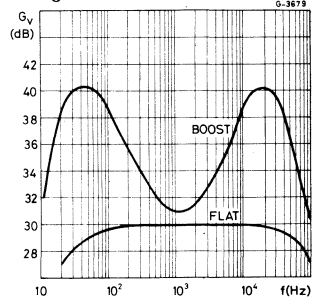


Fig. 24 - 10 dB 50 Hz boost tone control using change of pin 1 resistance (muting function)

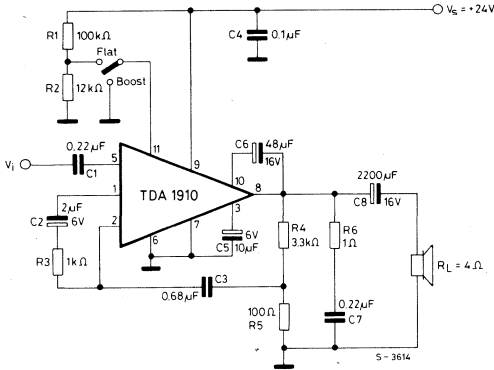


Fig. 25 - Frequency response of the circuit of Fig. 24

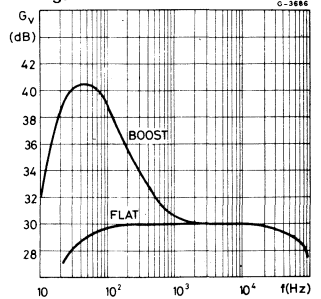


Fig. 26 - Squelch function in TV applications

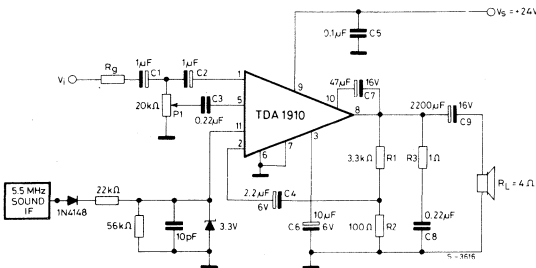
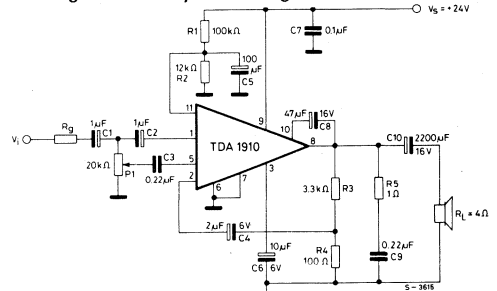


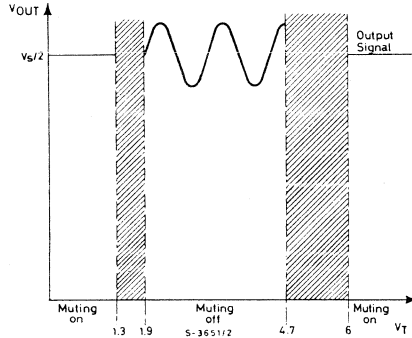
Fig. 27 - Delayed muting circuit



MUTING FUNCTION

The output signal can be inhibited applying a DC voltage V_T to pin 11, as shown in fig. 28

Fig. 28

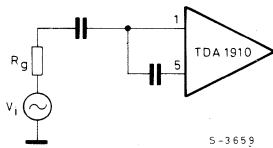


The input resistance at pin 1 depends on the threshold voltage V_T at pin 11 and is typically.

$$R_1 = 200 \text{ K}\Omega \quad @ \quad 1.9\text{V} \leq V_T \leq 4.7\text{V} \quad \text{muting-off}$$

$$R_1 = 10 \text{ }\Omega \quad @ \quad \begin{matrix} 0\text{V} \leq V_T \leq 1.3\text{V} \\ 6\text{V} \leq V_T \leq V_s \end{matrix} \quad \text{muting-on}$$

Referring to the following input stage, the possible attenuation of the input signal and therefore of the output signal can be found using the following expression.



$$A_T = \frac{V_i}{V_5} = \frac{R_g + R_5 // R_1}{R_5 // R_1}$$

where $R_5 \cong 100 \text{ K}\Omega$

Considering $R_g = 10 \text{ K}\Omega$ the attenuation in the muting-on condition is typically $A_T = 60 \text{ dB}$. In the muting-off condition, the attenuation is very low, typically 1.2 dB.

A very low current is necessary to drive the threshold voltage V_T because the input resistance at pin 11 is greater than $150 \text{ K}\Omega$. The muting function can be used in many cases, when a temporary inhibition of the output signal is requested, for example:

- in switch-on condition, to avoid preamplifier power-on transients (see fig. 27)
- during commutations at the input stages.
- during the receiver tuning.

The variable impedance capability at pin 1 can be useful in many applications and we have shown 2 examples in fig. 22 and 24, where it has been used to change the feedback network, obtaining 2 different frequency responses.

APPLICATION SUGGESTION

The recommended values of the components are those shown on application circuit of fig. 21. Different values can be used.

The following table can help the designer.

Component	Recomm. value	Purpose	Larger than recommended value	Smaller than recommended value	Allowed range	
					Min.	Max.
$R_g + R_1$	10K Ω	Input signal imped. for muting operation	Increase of the attenuation in muting-on condition. Decrease of the input sensitivity.	Decrease of the attenuation in muting on condition.		
R_2	3.3K Ω	Close loop gain setting.	Increase of gain.	Decrease of gain. Increase quiescent current.	$9 R_3$	
R_3	100 Ω	Close loop gain setting.	Decrease of gain.	Increase of gain.		$R_2/9$
R_4	1 Ω	Frequency stability	Danger of oscillation at high frequencies with inductive loads.			
P_1	20K Ω	Volume potentiometer.	Increase of the switch-on noise.	Decrease of the input impedance and the input level.	10K Ω	100K Ω
C_1 C_2 C_3	1 μ F 1 μ F 0.22 μ F	Input DC decoupling.		Higher low frequency cutoff.		
C_4	2.2 μ F	Inverting input DC decoupling.	Increase of the switch-on noise.	Higher low frequency cutoff.	0.1 μ F	
C_5	0.1 μ F	Supply voltage bypass.		Danger of oscillations.		
C_6	10 μ F	Ripple Rejection.	Increase of SVR. Increase of the switch-on time.	Degradation of SVR.	2.2 μ F	100 μ F
C_7	47 μ F	Bootstrap.		Increase of the distortion at low frequency.	10 μ F	100 μ F
C_8	0.22 μ F	Frequency stability.		Danger of oscillation.		
C_9	2200 μ F ($R_L = 4\Omega$) 1000 μ F ($R_L = 8\Omega$)	Output DC decoupling.		Higher low frequency cutoff.		

THERMAL SHUT-DOWN

The presence of a thermal limiting circuit offers the following advantages:

- 1) An overload on the output (even if it is permanent), or an above limit ambient temperature can be easily supported since the T_j cannot be higher than 150°C .
- 2) The heatsink can have a smaller factor of safety compared with that of a conventional circuit. There is no possibility of device damage due to high junction temperature.
If for any reason, the junction temperature increases up to 150°C , the thermal shut-down simply reduces the power dissipation and the current consumption.

The maximum allowable power dissipation depends upon the size of the external heatsink (i.e. its thermal resistance); fig. 31 shows this dissipable power as a function of ambient temperature for different thermal resistance.

Fig. 29 - Output power and drain current vs. case temperature

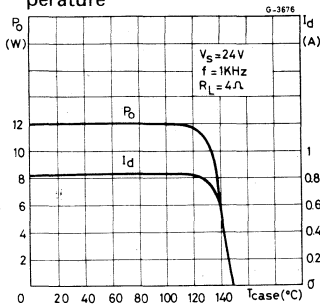


Fig. 30 - Output power and drain current vs. case temperature

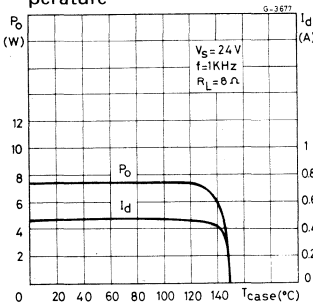
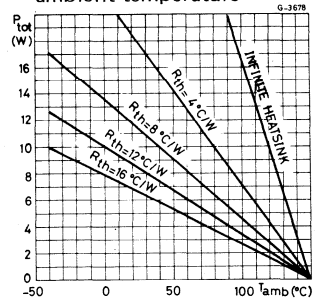


Fig. 31 - Maximum allowable power dissipation vs. ambient temperature

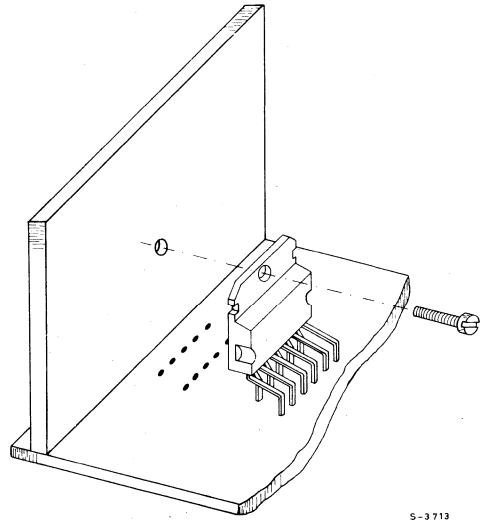
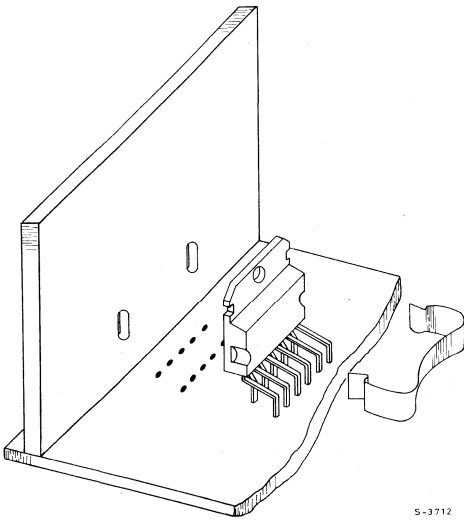


TDA 1910

MOUNTING INSTRUCTIONS

The power dissipated in the circuit must be removed by adding an external heatsink. Thanks to the Multiwatt[®] package attaching the heatsink is very simple, a screw or a compression spring (clip) being sufficient. Between the heatsink and the package it is better to insert a layer of silicon grease, to optimize the thermal contact; no electrical isolation is needed between the two surfaces.

Fig. 34 - Mounting examples



LINEAR INTEGRATED CIRCUIT

8W CAR RADIO AUDIO AMPLIFIER

The TDA 2002 is a class B audio power amplifier in Pentawatt[®] package designed for driving low impedance loads (down to 1.6Ω). The device provides a high output current capability (up to 3.5A), very low harmonic and cross-over distortion. In addition, the device offers the following features:

- very low number of external components
- assembly ease, due to Pentawatt[®] power package with no electrical insulation requirement
- space and cost saving
- high reliability
- flexibility in use
- complete safety during operation due to protection against:
 - a) short circuit; b) thermal over range; c) fortuitous open ground; d) polarity inversion (V_s max= 12V); e) load dump voltage surge.

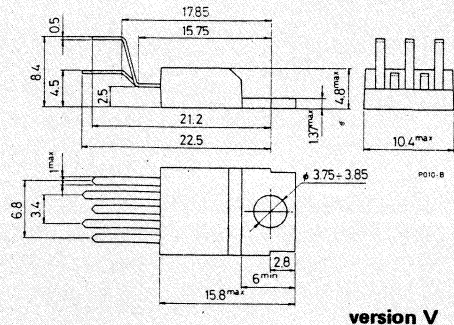
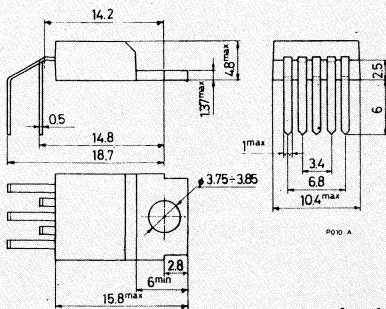
ABSOLUTE MAXIMUM RATINGS

V_s	Peak supply voltage (50 ms)	40	V
V_s	DC supply voltage	28	V
V_s	Operating supply voltage	18	V
I_o	Output peak current (repetitive)	3.5	A
I_o	Output peak current (non repetitive)	4.5	A
P_{tot}	Power dissipation at $T_{case} = 90^\circ\text{C}$	15	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBERS: TDA 2002 H
TDA 2002 V

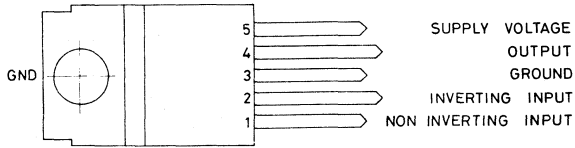
MECHANICAL DATA

Dimensions in mm



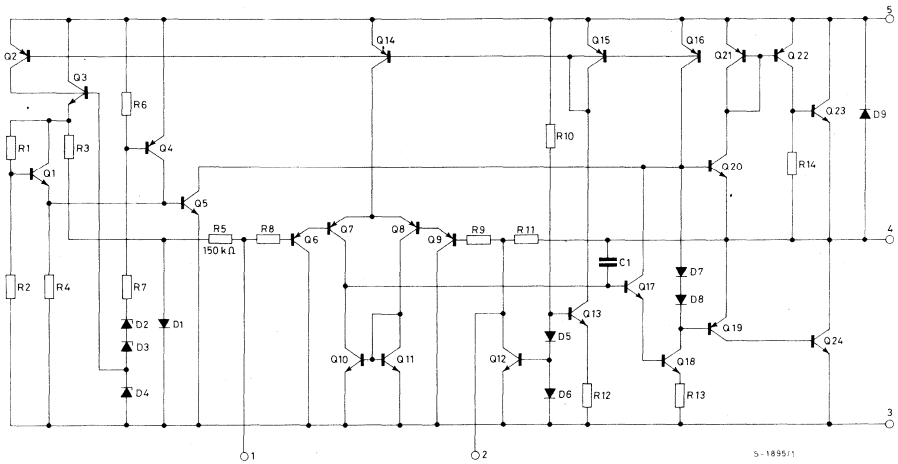
TDA 2002

CONNECTION DIAGRAM (top view)

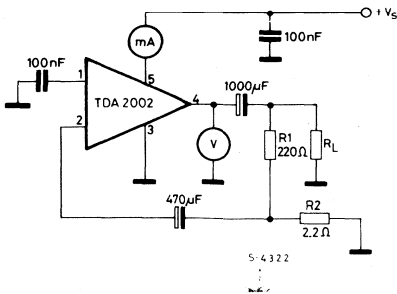


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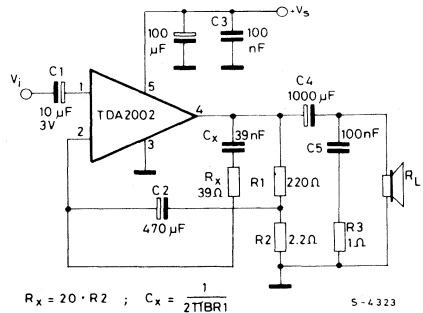
SCHEMATIC DIAGRAM



DC TEST CIRCUIT



AC TEST CIRCUIT



$$R_x = 20 \cdot R_2 ; C_x = \frac{1}{2TfBR_1}$$

S-4323

THERMAL DATA

$R_{th\ j-case}$	Thermal resistance junction-case	max	4	$^{\circ}C/W$
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ELECTRICAL CHARACTERISTICS ($V_s = 14.4V$, $T_{amb} = 25^{\circ}C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
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DC CHARACTERISTICS (Refer to DC test circuit)

V_s	Supply voltage		8		18	V
V_o	Quiescent output voltage (pin 4)		6.4	7.2	8	V
I_d	Quiescent drain current (pin 5)			45	80	mA

AC CHARACTERISTICS (Refer to AC test circuit, $G_v = 40\text{ dB}$)

P_o	Output power	$d = 10\%$ $V_s = 16V$	$f = 1\text{ kHz}$ $R_L = 4\Omega$ $R_L = 2\Omega$ $R_L = 4\Omega$ $R_L = 2\Omega$	4.8 7	5.2 8 6.5 10	W W W W	
$V_{i(rms)}$	Input saturation voltage			600		mV	
V_i	Input sensitivity	$P_o = 0.5W$ $P_o = 0.5W$ $P_o = 5.2W$ $P_o = 8W$	$f = 1\text{ kHz}$ $R_L = 4\Omega$ $R_L = 2\Omega$ $R_L = 4\Omega$ $R_L = 2\Omega$		15 11 55 50	mV mV mV mV	
B	Frequency response (-3 dB)	$R_L = 4\Omega$	$P_o = 1W$	40 to 15 000		Hz	
d	Distortion		$f = 1\text{ kHz}$ $P_o = 0.05\text{ to }3.5W$ $P_o = 0.05\text{ to }5W$		0.2 0.2	% %	
R_i	Input resistance (pin 1)	$f = 1\text{ kHz}$		70	150	k Ω	
G_v	Voltage gain (open loop)	$R_L = 4\Omega$	$f = 1\text{ kHz}$		80	dB	
G_v	Voltage gain (closed loop)	$R_L = 4\Omega$	$f = 1\text{ kHz}$	39.5	40	40.5	dB
e_N	Input noise voltage (*)				4	μV	
i_N	Input noise current (*)				60	pA	
η	Efficiency	$P_o = 5.2W$ $P_o = 8W$	$f = 1\text{ kHz}$ $R_L = 4\Omega$ $R_L = 2\Omega$		68 58	% %	
SVR	Supply voltage rejection	$R_L = 4\Omega$ $R_g = 10\text{ k}\Omega$ $f_{ripple} = 100\text{ Hz}$		30	35	dB	

(*) Filter with noise bandwidth: 22 Hz to 22 KHz.

TDA 2002

Fig. 1 - Quiescent output voltage vs. supply voltage

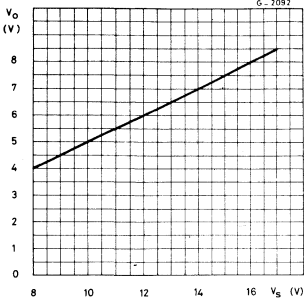


Fig. 2 - Quiescent drain current vs. supply voltage

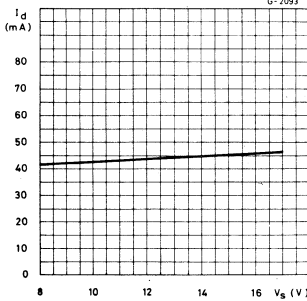


Fig. 3 - Output power vs. supply voltage

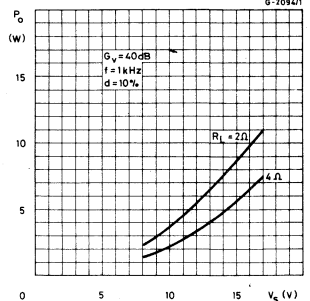


Fig. 4 - Output power vs. load resistance R_L

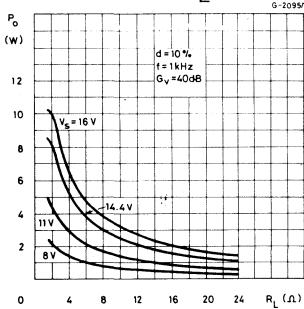


Fig. 5 - Input voltage vs. voltage gain ($R_L = 4 \Omega$)

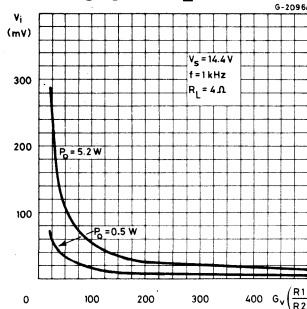


Fig. 6 - Input voltage vs. voltage gain ($R_L = 2 \Omega$)

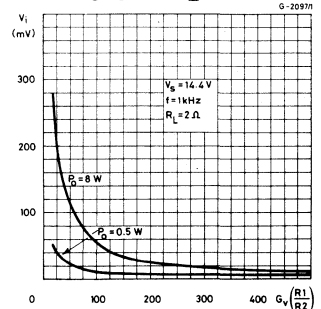


Fig. 7 - Distortion vs. output power

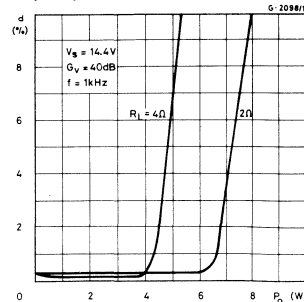


Fig. 8 - Distortion vs. frequency

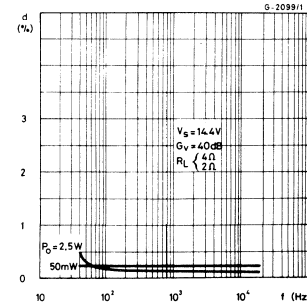


Fig. 9 - Supply voltage rejection vs. voltage gain

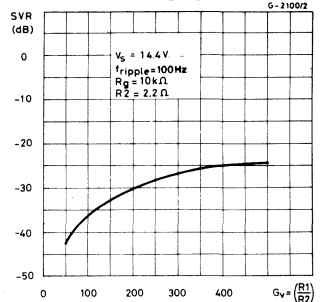


Fig. 10 - Supply voltage rejection vs. frequency

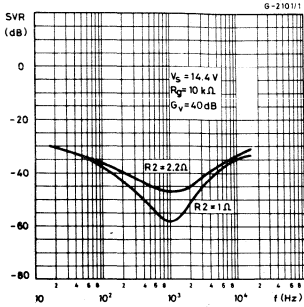


Fig. 11 - Power dissipation and efficiency vs. output power ($R_L = 4\Omega$)

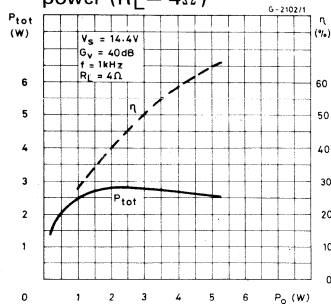


Fig. 12 - Power dissipation and efficiency vs. output power ($R_L = 2\Omega$)

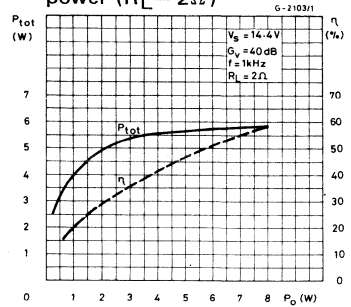


Fig. 13 - Maximum power dissipation vs. supply voltage (sine wave operation)

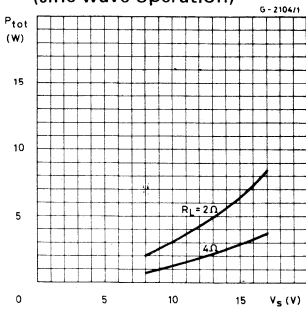


Fig. 14 - Maximum allowable power dissipation vs. ambient temperature

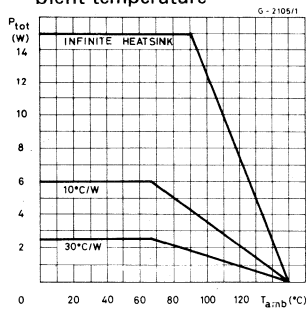
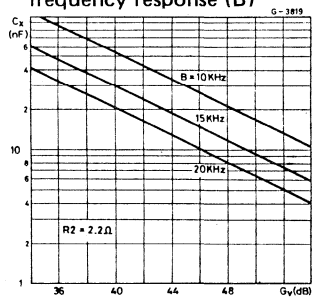


Fig. 15 - Values of capacitor (C_x) for different values of frequency response (B)



APPLICATION INFORMATION

Fig. 16 - Application circuit

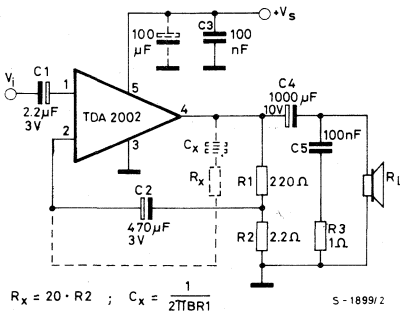
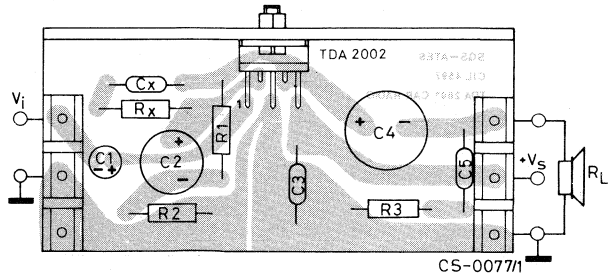


Fig. 17 - P.C. board and component layout for the circuit of fig. 16 (1:1 scale)



TDA 2002

APPLICATION INFORMATION (continued)

Fig. 18 - Low cost application circuit

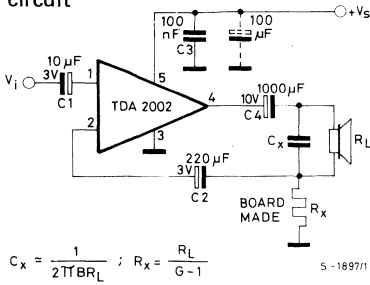


Fig. 19 - P.C. board and component layout for the circuit of fig. 18 (1:1 scale)

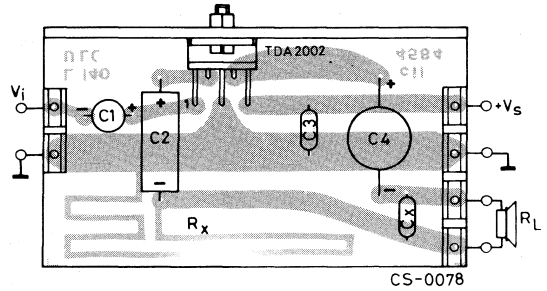


Fig. 20 - 15W application circuit-bridge configuration

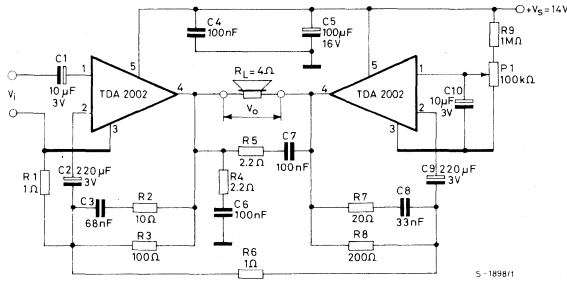
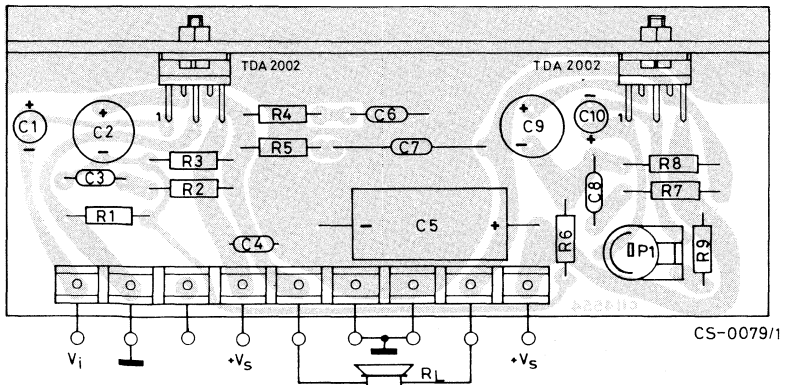


Fig. 21 - P.C. board and component layout for the circuit of fig. 20 (1:1 scale)



LOAD DUMP VOLTAGE SURGE PROTECTION

The TDA 2002 has a circuit which enables it to withstand a voltage pulse train, on pin 5, of the type shown in fig. 22. If the supply voltage peaks to more than 40V, then an LC filter must be inserted between the supply and pin 5, in order to assure that the pulses at pin 5 will be held within the limits shown in fig. 22.

A suggested LC network is shown in fig. 23. With this network, a train of pulses with amplitude up to 120V and width of 2 ms can be applied at point A. This type of protection is ON when the supply voltage (pulsed or DC) exceeds 18V. For this reason the maximum operating supply voltage is 18V.

Fig. 22

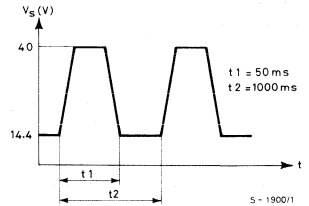
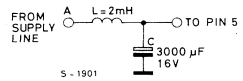


Fig. 23



THERMAL SHUT-DOWN

The presence of a thermal limiting circuit offers the following advantages:

- 1) an overload on the output (even if it is permanent), or an excessive ambient temperature can be easily withstood
- 2) the heat-sink can have a smaller factor of safety compared with that of a conventional circuit. There is no device damage in the case of excessive junction temperature: all that happens is that P_o (and therefore P_{tot}) and I_d are reduced (figs. 24 and 25).

Fig. 24 - Output power and drain current vs. case temperature ($R_L = 4\Omega$)

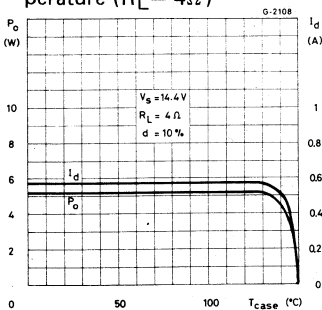
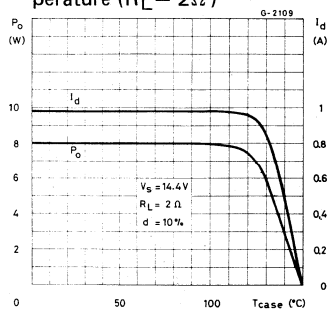


Fig. 25 - Output power and drain current vs. case temperature ($R_L = 2\Omega$)



PRACTICAL CONSIDERATIONS

Printed circuit board

The layout shown in fig. 17 is recommended. If different layouts are used, the ground points of input 1 and input 2 must be well decoupled from the ground of the output through which a rather high current flows.

Assembly suggestion

No electrical insulation is needed between the package and the heat-sink. Pin length should be as short as possible. The soldering temperature must not exceed 260°C for 12 seconds.

Application suggestions

The recommended component values are those shown in the application circuits of fig. 16. Different values can be used. The following table is intended to aid the car-radio designer.

Component	Recommended value	Purpose	Larger than recommended value	Smaller than recommended value
C1	2.2 μ F	Input DC decoupling		Noise at switch-on, switch-off
C2	470 μ F	Ripple rejection		Degradation of SVR
C3	0.1 μ F	Supply bypassing		Danger of oscillation
C4	1000 μ F	Output coupling to load		Higher low frequency cutoff
C5	0.1 μ F	Frequency stability		Danger of oscillation at high frequencies with inductive loads
C _X	$\cong \frac{1}{2\pi B R1}$	Upper frequency cutoff	Lower bandwidth	Larger bandwidth
R1	$(G_V - 1) \cdot R2$	Setting of gain		Increase of drain current
R2	2.2 Ω	Setting of gain and SVR	Degradation of SVR	
R3	1 Ω	Frequency stability	Danger of oscillation at high frequencies with inductive loads	
R _X	$\cong 20 R2$	Upper frequency cutoff	Poor high frequency attenuation	Danger of oscillation

LINEAR INTEGRATED CIRCUIT

10W CAR RADIO AUDIO AMPLIFIER

The TDA 2003 has improved performance with the same pin configuration as the TDA 2002. The additional features of TDA 2002, very low number of external components, ease of assembly, space and cost saving, are maintained.

The device provides a high output current capability (up to 3.5A) very low harmonic and cross-over distortion.

Completely safe operation is guaranteed due to protection against DC and AC short circuit between all pins and ground, thermal over-range, load dump voltage surge up to 40V, polarity inversion and fortuitous open ground.

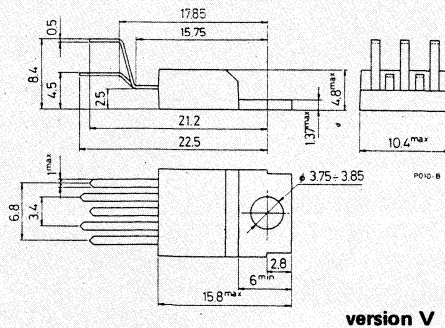
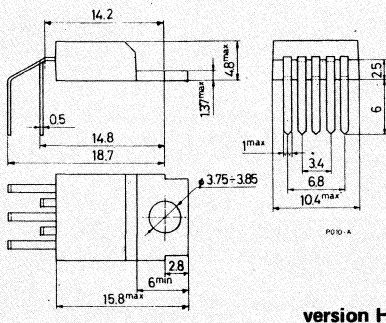
ABSOLUTE MAXIMUM RATINGS

V_s	Peak supply voltage (50 ms)	40	V
V_s	DC supply voltage	28	V
V_s	Operating supply voltage	18	V
I_o	Output peak current (repetitive)	3.5	A
I_o	Output peak current (non repetitive)	4.5	A
P_{tot}	Power dissipation at $T_{case} = 90^\circ\text{C}$	20	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBERS: TDA 2003H
TDA 2003V

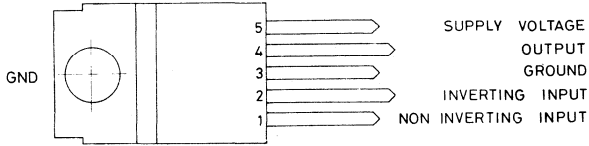
MECHANICAL DATA

Dimensions in mm



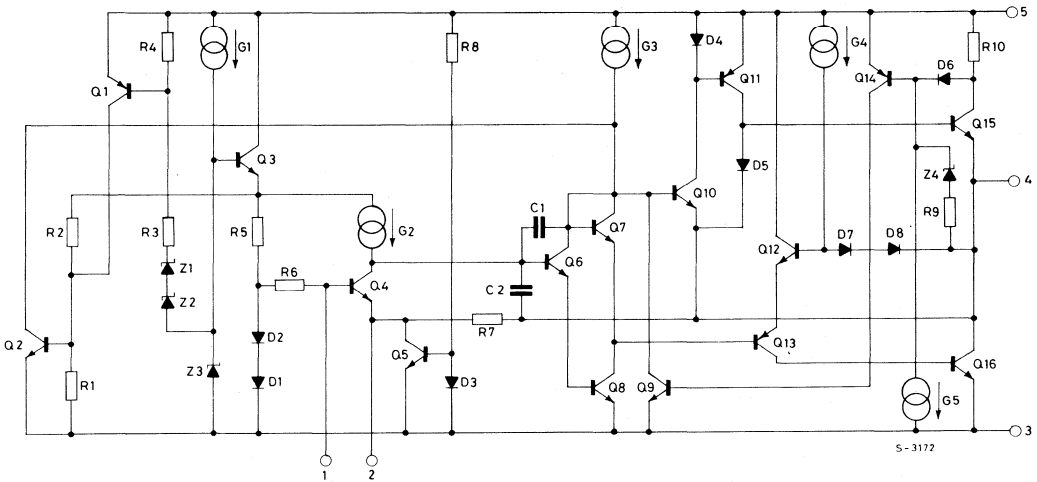
TDA 2003

CONNECTION DIAGRAM (top view)



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SCHEMATIC DIAGRAM

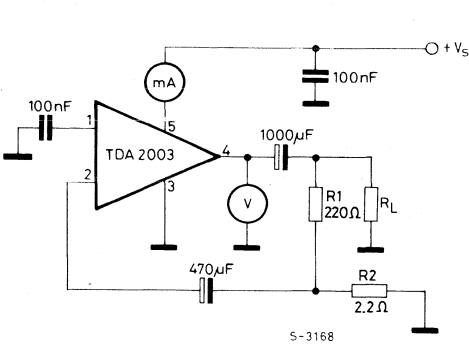


THERMAL DATA

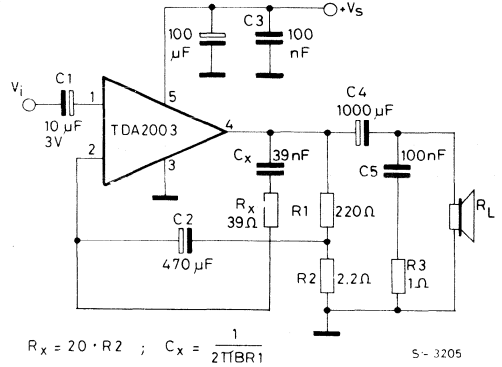
$R_{th\ j-case}$ Thermal resistance junction-case

max 3 °C/W

DC TEST CIRCUIT



AC TEST CIRCUIT



$$R_x = 20 \cdot R_2 ; C_x = \frac{1}{2\pi f R_1}$$

ELECTRICAL CHARACTERISTICS ($V_s = 14.4V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
-----------	-----------------	------	------	------	------

DC CHARACTERISTICS (Refer to DC test circuit)

V_s	Supply voltage	8		18	V
V_o	Quiescent output voltage (pin 4)	6.1	6.9	7.7	V
I_d	Quiescent drain current (pin 5)		44	50	mA

AC CHARACTERISTICS (Refer to AC test circuit, $G_v = 40$ dB)

P_o	Output power	$d = 10\%$ $f = 1$ kHz $R_L = 4\Omega$ $R_L = 2\Omega$ $R_L = 3.2\Omega$ $R_L = 1.6\Omega$	5.5 9	6 10 7.5 12		W W W W
$V_{i(rms)}$	Input saturation voltage		300			mV
V_i	Input sensitivity	$f = 1$ kHz $P_o = 0.5W$ $P_o = 6W$ $P_o = 0.5W$ $P_o = 10W$ $R_L = 4\Omega$ $R_L = 4\Omega$ $R_L = 2\Omega$ $R_L = 2\Omega$		14 55 10 50		mV mV mV mV

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
B Frequency response (-3 dB)	$P_O = 1W$ $R_L = 4\Omega$	40 to 15,000			Hz
d Distortion	$f = 1 \text{ kHz}$ $P_O = 0.05 \text{ to } 4.5W$ $R_L = 4\Omega$ $P_O = 0.05 \text{ to } 7.5W$ $R_L = 2\Omega$		0.15 0.15		% %
R_i Input resistance (pin 1)	$f = 1 \text{ kHz}$	70	150		$k\Omega$
G_v Voltage gain (open loop)	$f = 1 \text{ kHz}$ $f = 10 \text{ kHz}$		80 60		dB dB
G_v Voltage gain (closed loop)	$f = 1 \text{ kHz}$ $R_L = 4\Omega$	39.5	40	40.5	dB
e_N Input noise voltage (0)			1	5	μV
i_N Input noise current (0)			60	200	pA
η Efficiency	$f = 1 \text{ kHz}$ $P_O = 6W$ $R_L = 4\Omega$ $P_O = 10W$ $R_L = 2\Omega$		69 65		% %
SVR Supply voltage rejection	$f = 100 \text{ Hz}$ $V_{ripple} = 0.5V$ $R_g = 10 \text{ k}\Omega$ $R_L = 4\Omega$	30	36		dB

(0) Filter with noise bandwidth: 22 Hz to 22 kHz

Fig. 1 - Quiescent output voltage vs. supply voltage

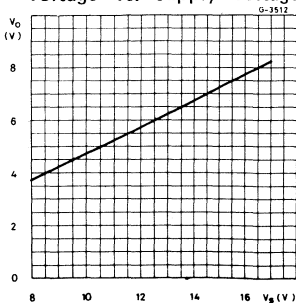


Fig. 2 - Quiescent drain current vs. supply voltage

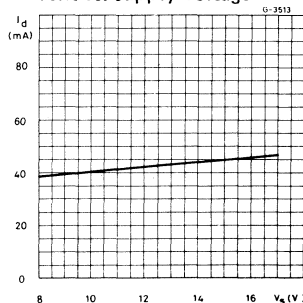


Fig. 3 - Output power vs. supply voltage

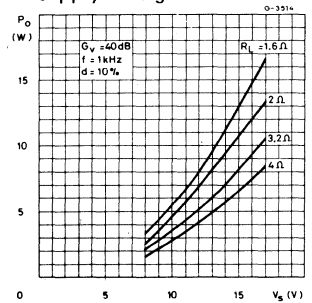


Fig. 4 - Output power vs. load resistance R_L

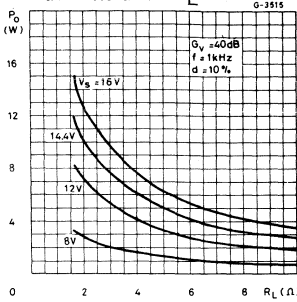


Fig. 5 - Gain vs. input sensitivity

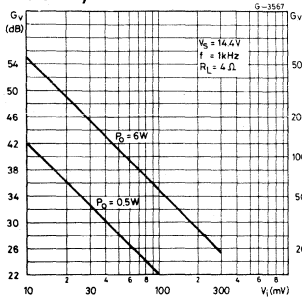


Fig. 6 - Gain vs. input sensitivity

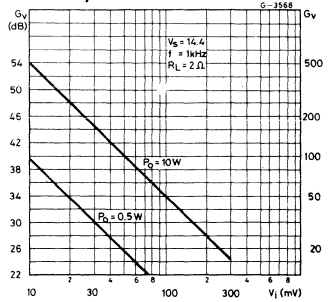


Fig. 7 - Distortion vs. output power

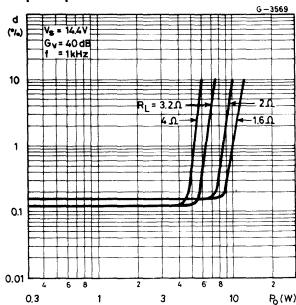


Fig. 8 - Distortion vs. frequency

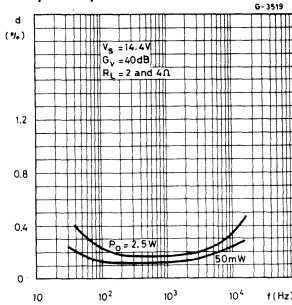


Fig. 9 - Supply voltage rejection vs. voltage gain

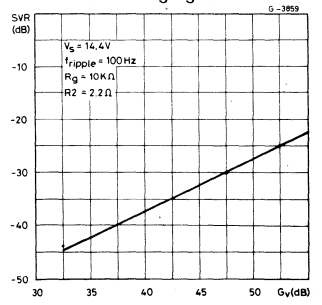


Fig. 10 - Supply voltage rejection vs. frequency

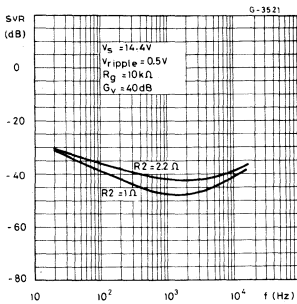


Fig. 11 - Power dissipation and efficiency vs. output power ($R_L = 4\ \Omega$)

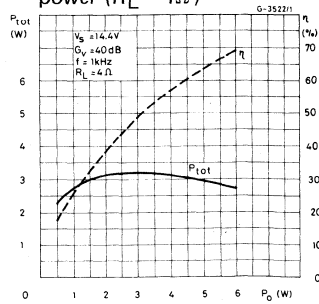
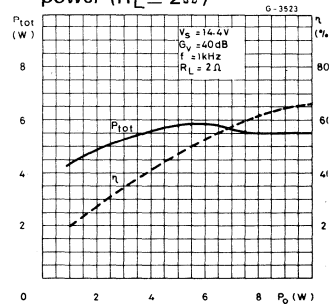


Fig. 12 - Power dissipation and efficiency vs. output power ($R_L = 2\ \Omega$)



TDA 2003

Fig. 13 - Maximum power dissipation vs. supply voltage (sine wave operation)

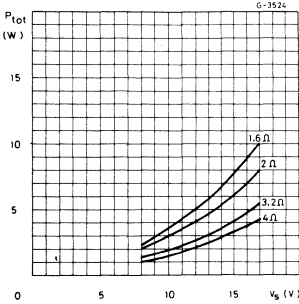


Fig. 14 - Maximum allowable power dissipation vs. ambient temperature

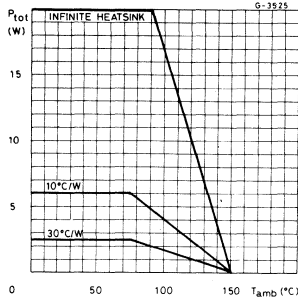
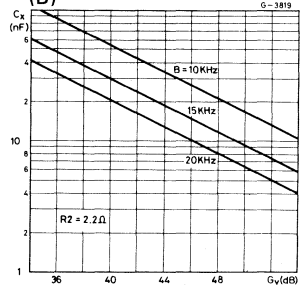


Fig. 15 - Typical values of capacitor (C_x) for different values of frequency response (B)



APPLICATION INFORMATION

Fig. 16 - Typical application circuit

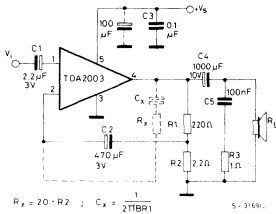


Fig. 17 - P.C. board and component layout for the circuit of fig. 16 (1:1 scale)

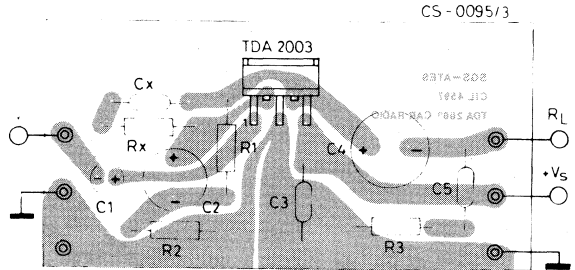
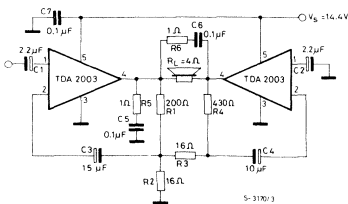
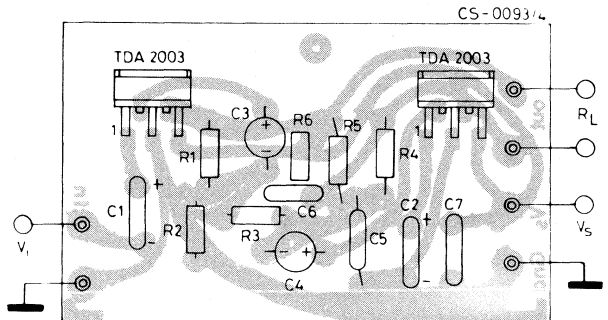


Fig. 18 - 20W bridge configuration application circuit (*)



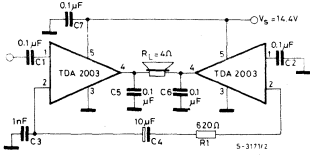
(*) The values of the capacitors C_3 and C_4 are different to optimize the SVR ($T_{yp} = 40$ dB)

Fig. 19 - P.C. board and component layout for the circuit of fig. 18 (1:1 scale)



APPLICATION INFORMATION (continued)

Fig. 20 - Low cost bridge configuration application circuit (*) ($P_o = 18W$)



(*) In this application the device can support a short circuit between every side of the loudspeaker and ground.

Fig. 21 - P.C. board and component layout for the circuit of fig. 20 (1:1 scale)

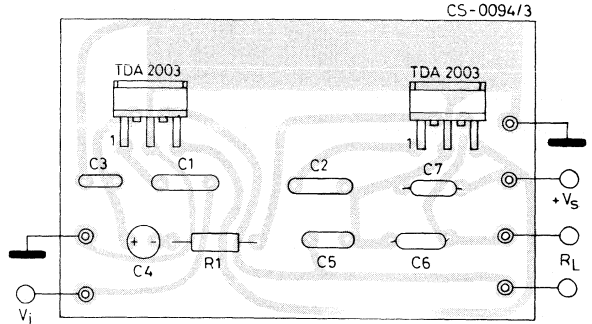
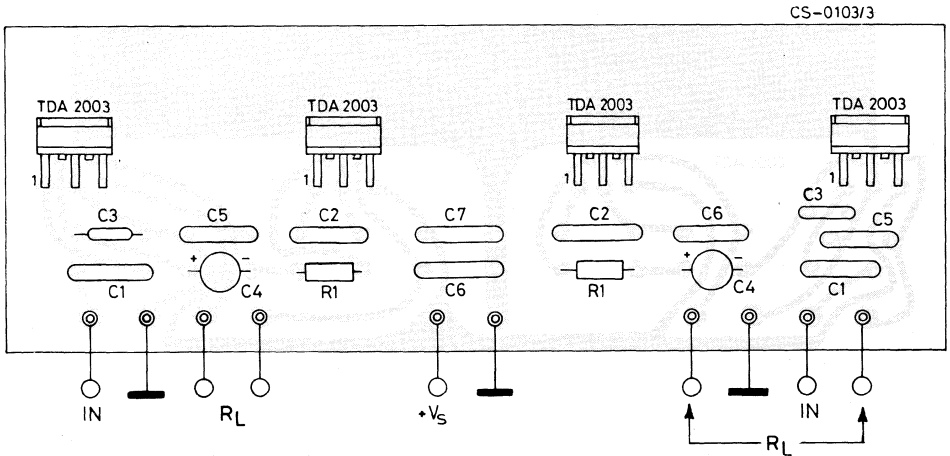


Fig. 22 - P.C. board and component layout for the low-cost bridge amplifier of fig. 20, in stereo version (1:1 scale)



BUILT-IN PROTECTION SYSTEMS

Load dump voltage surge

The TDA 2003 has a circuit which enables it to withstand a voltage pulse train, on pin 5, of the type shown in fig. 23.

If the supply voltage peaks to more than 40V, then an LC filter must be inserted between the supply and pin 5, in order to assure that the pulses at pin 5 will be held within the limits shown in fig. 23. A suggested LC network is shown in fig. 24. With this network, a train of pulses with amplitude up to 120V and width of 2 ms can be applied at point A. This type of protection is ON when the supply voltage (pulsed or DC) exceeds 18V. For this reason the maximum operating supply voltage is 18V.

Fig. 23

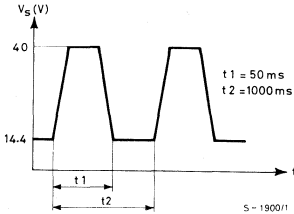
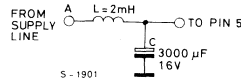


Fig. 24



Short-circuit (AC and DC conditions)

The TDA 2003 can withstand a permanent short-circuit on the output for a supply voltage up to 16V.

Polarity inversion

High current (up to 5A) can be handled by the device with no damage for a longer period than the blow-out time of a quick 1A fuse (normally connected in series with the supply).

This feature is added to avoid destruction if, during fitting to the car, a mistake on the connection of the supply is made.

Open ground

When the radio is in the ON condition and the ground is accidentally opened, a standard audio amplifier will be damaged. On the TDA 2003 protection diodes are included to avoid any damage.

Inductive load

A protection diode is provided between pin 4 and 5 (see the internal schematic diagram) to allow use of the TDA 2003 with inductive loads.

In particular, the TDA 2003 can drive a coupling transformer for audio modulation.

DC voltage

The maximum operating DC voltage on the TDA 2003 is 18V.

However the device can withstand a DC voltage up to 28V with no damage. This could occur during winter if two batteries were series connected to crank the engine.

Thermal shut-down

The presence of a thermal limiting circuit offers the following advantages:

- 1) an overload on the output (even if it is permanent), or an excessive ambient temperature can be easily withstood.
- 2) the heat-sink can have a smaller factor of safety compared with that of a conventional circuit. There is no device damage in the case of excessive junction temperature: all that happens is that P_o (and therefore P_{tot}) and I_d are reduced (figs. 25 and 26).

Fig. 25 - Output power and drain current vs. case temperature ($R_L = 4 \Omega$)

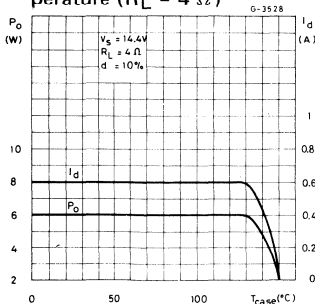
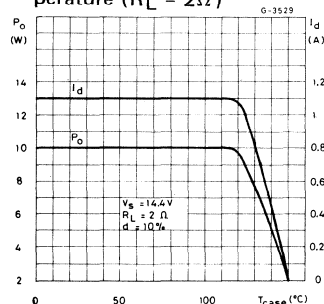


Fig. 26 - Output power and drain current vs. case temperature ($R_L = 2 \Omega$)



PRATICAL CONSIDERATIONS

Printed circuit board

The layout shown in fig. 17 is recommended. If different layouts are used, the ground points of input 1 and input 2 must be well decoupled from the ground of the output through which a rather high current flows.

Assembly suggestion

No electrical insulation is required between the package and the heat-sink. Pin length should be as short as possible. The soldering temperature must not exceed 260°C for 12 seconds.

Application suggestions

The recommended component values are those shown in the application circuits of fig. 16. Different values can be used. The following table is intended to aid the car-radio designer.

Component	Recommended value	Purpose	Larger than recommended value	Smaller than recommended value
C1	2.2 μ F	Input DC decoupling		Noise at switch-on, switch-off
C2	470 μ F	Ripple rejection		Degradation of SVR
C3	0.1 μ F	Supply bypassing		Danger of oscillation
C4	1000 μ F	Output coupling to load		Higher low frequency cutoff
C5	0.1 μ F	Frequency stability		Danger of oscillation at high frequencies with inductive loads
C _X	$\cong \frac{1}{2 \pi B R 1}$	Upper frequency cutoff	Lower bandwidth	Larger bandwidth
R1	(G _v -1) • R2	Setting of gain		Increase of drain current
R2	2.2 Ω	Setting of gain and SVR	Degradation of SVR	
R3	1 Ω	Frequency stability	Danger of oscillation at high frequencies with inductive loads	
R _X	$\cong 20 R 2$	Upper frequency cutoff	Poor high frequency attenuation	Danger of oscillation

10 + 10W STEREO AMPLIFIER FOR CAR RADIO

The TDA 2004 is a class B dual audio power amplifier in MULTIWATT[®] package specifically designed for car radio applications: stereo amplifiers are easily designed using this device that provides a high current capability (up to 3.5A) and that can drive very low impedance loads (down to 1.6Ω). Its main features are:

Low distortion.

Low noise.

High reliability of the chip and of the package with additional complete safety during operation thanks to protections against:

- output AC short circuit to ground
- very inductive loads
- overrating chip temperature
- load dump voltage surge
- fortuitous open ground
- polarity inversion

Space and cost saving: very low number of external components, very simple mounting system with no electrical isolation between the package and the heatsink (one screw only).

ABSOLUTE MAXIMUM RATINGS

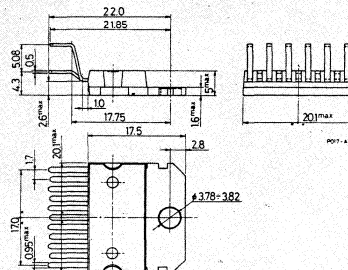
V_s	Operating supply voltage	18	V
V_s	DC supply voltage	28	V
V_s	Peak supply voltage (for 50 ms)	40	V
I_o (*)	Output peak current (non repetitive $t = 0.1$ ms)	4.5	A
I_o (*)	Output peak current (repetitive $f \geq 10$ Hz)	3.5	A
P_{tot}	Power dissipation at $T_{case} = 60$ °C	30	W
T_j, T_{stg}	Storage and junction temperature	-40 to 150	°C

(*) The max. output current is internally limited.

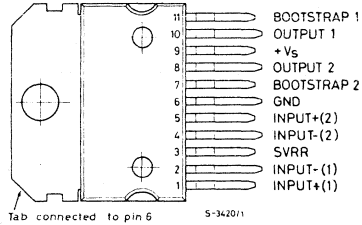
ORDERING NUMBER: TDA 2004

MECHANICAL DATA

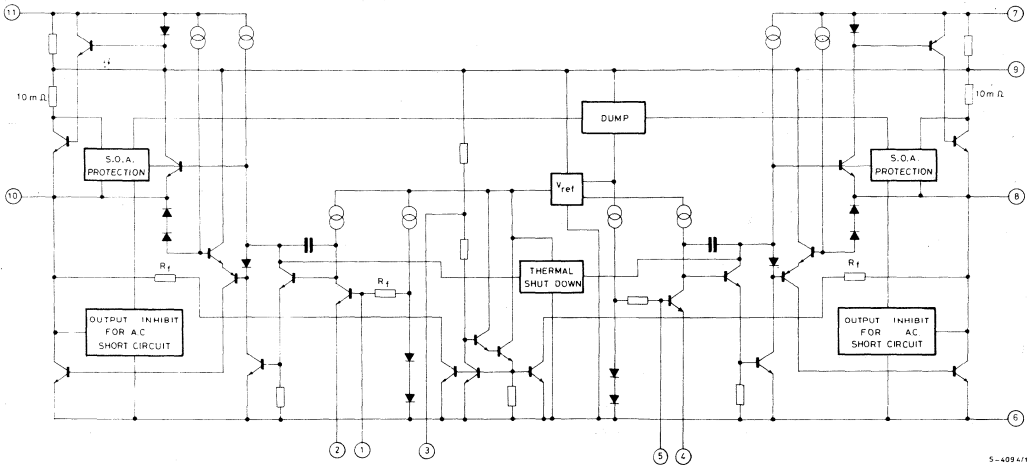
Dimensions in mm



CONNECTION DIAGRAM (top view)



SCHEMATIC DIAGRAM



THERMAL DATA

$R_{th\ j\text{-case}}$ Thermal resistance junction-case

max 3 °C/W

TDA 2004

Fig. 1 - Test circuit

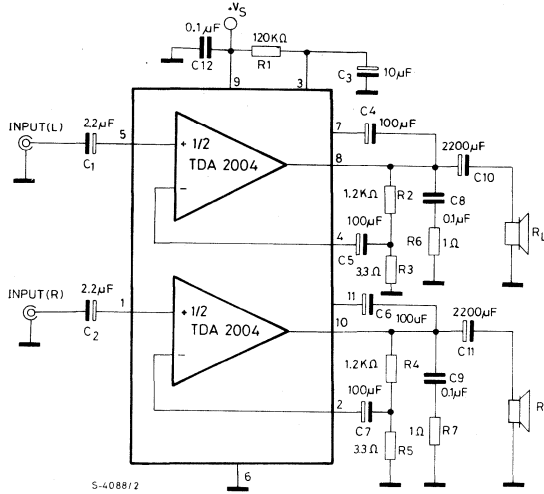
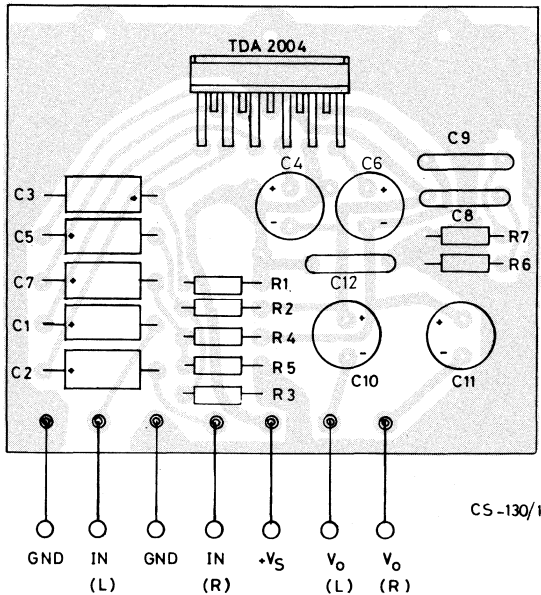


Fig. 2 - PC board and components layout (scale 1:1)



ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $T_{amb} = 25^{\circ}\text{C}$, $G_v = 50 \text{ dB}$, $R_{th}(\text{heatsink}) = 4^{\circ}\text{C/W}$, unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s Supply voltage		8		18	V
V_o Quiescent output voltage	$V_s = 14.4\text{V}$ $V_s = 13.2\text{V}$	6.6 5.0	7.2 6.6	7.8 7.2	V V
I_d Total quiescent drain current	$V_s = 14.4\text{V}$ $V_s = 13.2\text{V}$		65 62	120 120	mA mA
I_{SB} Stand-by current	Pin 3 grounded		5		mA
P_o Output power (each channel)	$f = 1 \text{ KHz}$ $d = 10\%$ $V_s = 14.4\text{V}$ $R_L = 4\Omega$ $R_L = 3.2\Omega$ $R_L = 2\Omega$ $R_L = 1.6\Omega$ $V_s = 13.2\text{V}$ $R_L = 3.2\Omega$ $R_L = 1.6\Omega$ $V_s = 16\text{V}$ $R_L = 2\Omega$	6 7 9 10 6 9	6.5 8 10(*) 11 6.5 10 12		W W W W W W W
d Distortion (each channel)	$f = 1 \text{ KHz}$ $V_s = 14.4\text{V}$ $R_L = 4\Omega$ $P_o = 50 \text{ mW}$ to 4W $V_s = 14.4\text{V}$ $R_L = 2\Omega$ $P_o = 50 \text{ mW}$ to 6W $V_s = 13.2\text{V}$ $R_L = 3.2\Omega$ $P_o = 50 \text{ mW}$ to 3W $V_s = 13.2\text{V}$ $R_L = 1.6\Omega$ $P_o = 50 \text{ mW}$ to 6W		0.2 0.3 0.2 0.3	1 1 1 1	% % % %
CT Cross talk	$V_s = 14.4\text{V}$ $V_o = 4 \text{ V}_{rms}$ $R_L = 4\Omega$ $f = 1 \text{ KHz}$ $f = 10 \text{ KHz}$	50 40	60 45		dB dB
V_i Input sensitivity	$f = 1 \text{ KHz}$ $P_o = 1\text{W}$ $R_L = 4\Omega$ $R_L = 3.2\Omega$		6 5.5		mV mV
V_i Input saturation voltage		300			mV
R_i Input resistance (non inverting input)	$f = 1 \text{ KHz}$	70	200		K Ω
R_i Input resistance (inverting input)	$f = 1 \text{ KHz}$		10		K Ω
f_L Low frequency roll off (-3 dB)	$R_L = 4\Omega$ $R_L = 2\Omega$ $R_L = 3.2\Omega$ $R_L = 1.6\Omega$			35 50 40 55	Hz Hz Hz Hz
f_H High frequency roll off (-3 dB)	$R_L = 4\Omega$ $R_L = 2\Omega$ $R_L = 3.2\Omega$ $R_L = 1.6\Omega$	15 15 15 15			KHz KHz KHz KHz

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ELECTRICAL CHARACTERISTICS (continued)

Parameters	Test conditions	Min.	Typ.	Max.	Unit
G_V	Voltage gain (open loop)		90		dB
G_V	Voltage gain (closed loop)		48	51	dB
	Closed loop gain matching		0.5		dB
e_N	Total input noise voltage	$R_g = 10 \text{ K}\Omega$	1.5	5	μV
SVR	Supply voltage rejection	$f_{\text{ripple}} = 100 \text{ Hz}$ $R_g = 10 \text{ K}\Omega$ $C_3 = 10 \mu\text{F}$ $V_{\text{ripple}} = 0.5 \text{ V}_{\text{rms}}$	35	45	dB
η	Efficiency	$V_s = 14.4 \text{ V}$ $f = 1 \text{ KHz}$ $R_L = 4 \Omega$ $P_o = 6.5 \text{ W}$ $R_L = 2 \Omega$ $P_o = 10 \text{ W}$ $V_s = 13.2 \text{ V}$ $f = 1 \text{ KHz}$ $R_L = 3.2 \Omega$ $P_o = 6.5 \text{ W}$ $R_L = 1.6 \Omega$ $P_o = 10 \text{ W}$		70 60 70 60	% % % %
T_{sd}	Thermal shut down case temperature	$V_s = 14.4 \text{ V}$ $R_L = 4 \Omega$ $f = 1 \text{ KHz}$ $P_{\text{tot}} = 5.5 \text{ W}$	125	135	$^{\circ}\text{C}$

(*) 9.3W without bootstrap.

(°) Bandwidth filter: 22 Hz to 22 KHz.

Fig. 3 - Quiescent output voltage vs. supply voltage

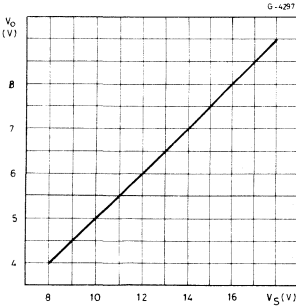


Fig. 4 - Quiescent drain current vs. supply voltage

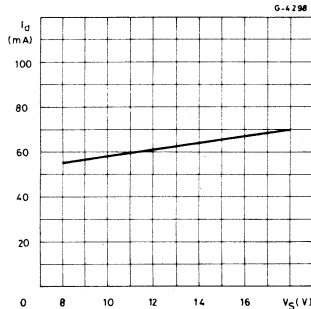


Fig. 5 - Distortion vs. output power

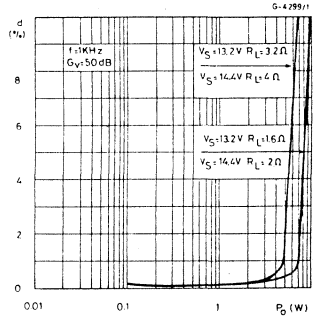


Fig. 6 - Output power vs. supply voltage

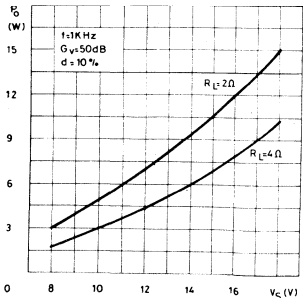


Fig. 7 - Output power vs. supply voltage

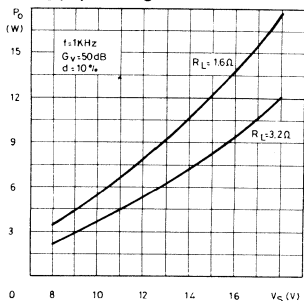


Fig. 8 - Distortion vs. frequency

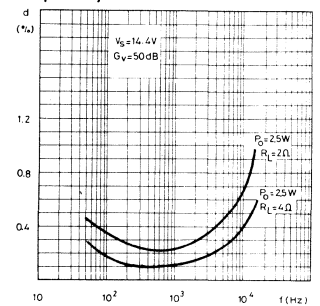


Fig. 9 - Distortion vs. frequency

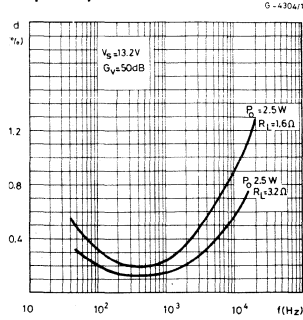


Fig. 10 - Supply voltage rejection vs. C_3

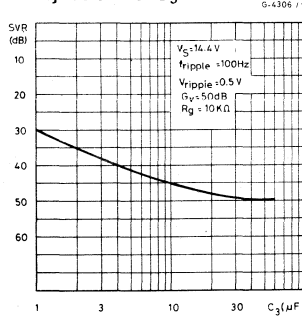


Fig. 11 - Supply voltage rejection vs. frequency

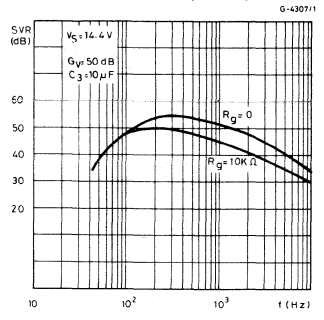


Fig. 12 - Supply voltage rejection vs. values of capacitors C_2 and C_3

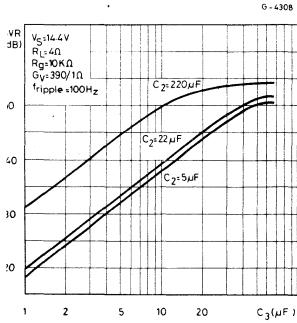


Fig. 13 - Supply voltage rejection vs. values of capacitors C_2 and C_3

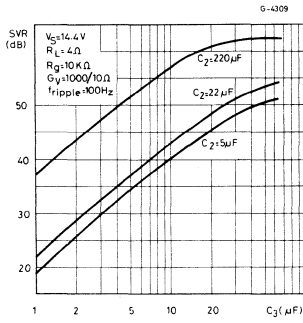


Fig. 14 - Gain vs. input sensitivity

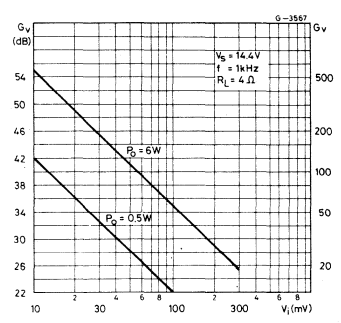


Fig. 15 - Gain vs. input sensitivity

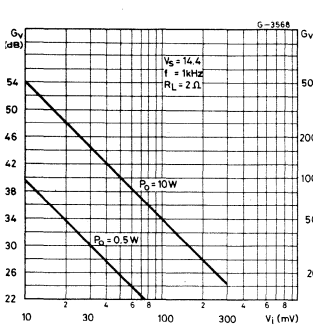


Fig. 16 - Total power dissipation and efficiency vs. output power

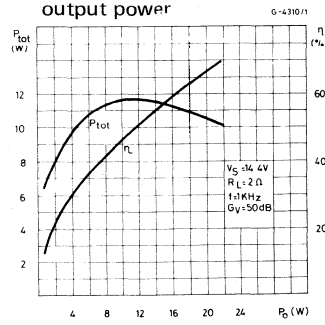
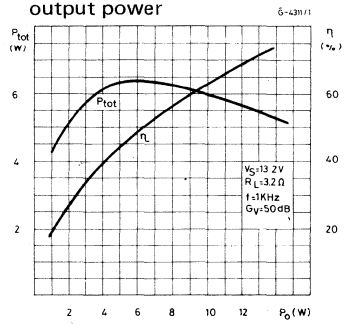


Fig. 17 - Total power dissipation and efficiency vs. output power



TDA 2004

APPLICATION INFORMATION

Fig. 18 - Typical application circuit

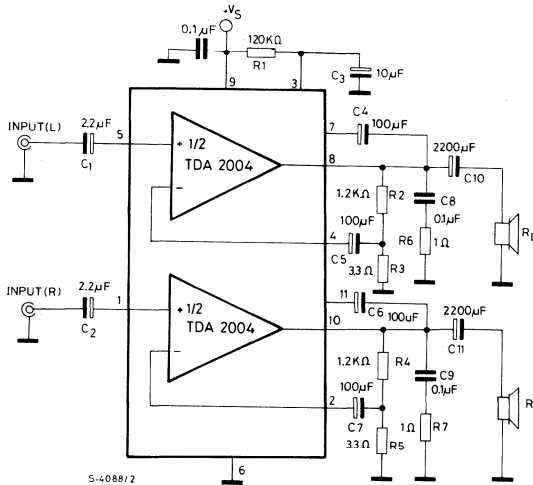


Fig. 19 - Application circuit without bootstrap ($G_v = 40$ dB)

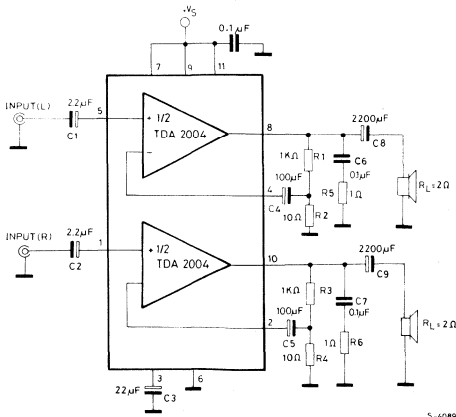


Fig. 20 - 18W low-cost bridge application ($G_v \cong 30$ dB)

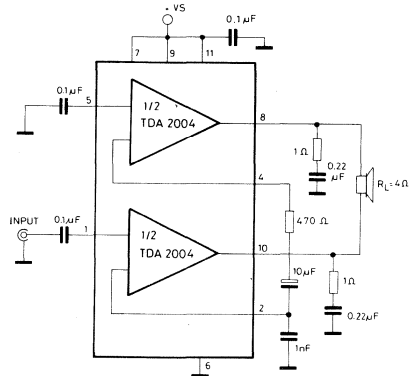


Fig. 21 - 10 + 10W stereo amplifier with tone, balance and loudness control

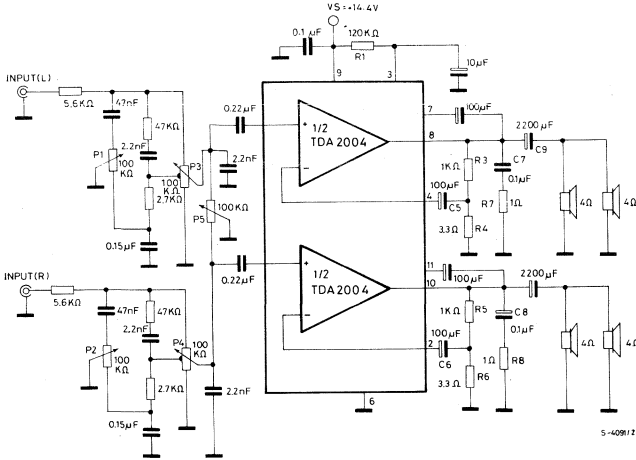


Fig. 22 - Tone control response (circuit of fig. 21)

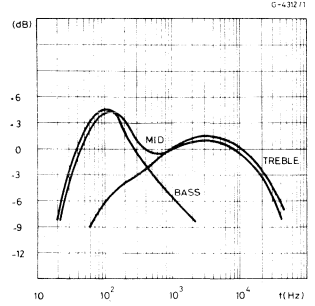
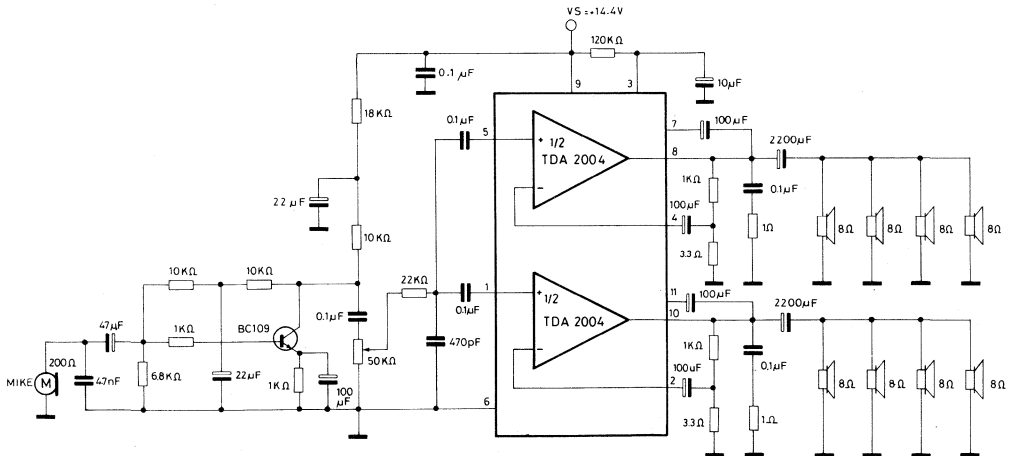


Fig. 23 - 20W Bus amplifier



TDA 2004

Fig. 24 - Simple two way amplifier ($f_c = 2 \text{ KHz}$)

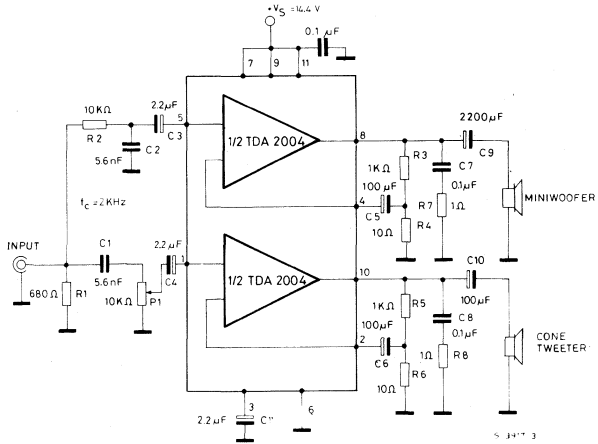
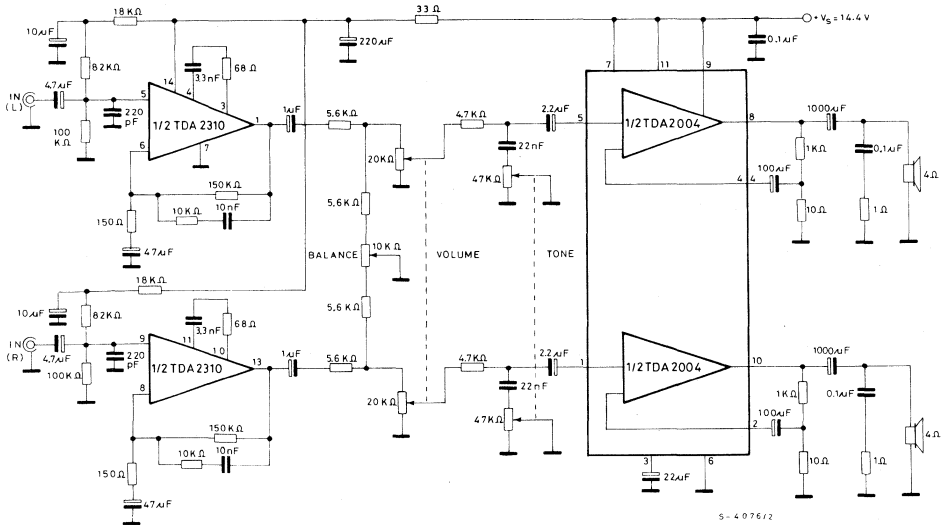


Fig. 25 - High quality, 10 + 10W cassette player



APPLICATION SUGGESTION

The recommended values of the components are those shown on application circuit of fig. 18. Different values can be used; the following table can help the designer.

Component	Recomm. value	Purpose	Larger than	Smaller than
R ₁	120 K Ω	Optimisation of the output signal symmetry	Smaller P _O max	Smaller P _O max
R ₂ and R ₄	1 K Ω	Close loop gain setting	Increase of gain	Decrease of gain
R ₃ and R ₅	3.3 Ω		Decrease of gain	Increase of gain
R ₆ and R ₇	1 Ω	Frequency stability	Danger of oscillation at high frequency with inductive load	
C ₁ and C ₂	2.2 μ F	Input DC decoupling	High turn-on delay	High turn-on pop Higher low frequency cutoff. Increase of noise.
C ₃	10 μ F	Ripple rejection	Increase of SVR. Increase of the switch-on time.	Degradation of SVR.
C ₄ and C ₆	100 μ F	Bootstrapping		Increase of distortion at low frequency.
C ₅ and C ₇	100 μ F	Feedback Input DC decoupling.		
C ₈ and C ₉	0.1 μ F	Frequency stability.		Danger of oscillation.
C ₁₀ and C ₁₁	1000 μ F to 2200 μ F	Output DC decoupling.		Higher low-frequency cut-off.

BUILT-IN PROTECTION SYSTEMS

Load dump voltage surge

The TDA 2004 has a circuit which enables it to withstand a voltage pulse train, on pin 9, of the type shown in fig. 27.

If the supply voltage peaks to more than 40V, then an LC filter must be inserted between the supply and pin 9, in order to assure that the pulses at pin 9 will be held within the limits shown.

A suggested LC network is shown in fig. 26. With this network, a train of pulses with amplitude up to 120V and width of 2 ms can be applied to point A. This type of protection is ON when the supply voltage (pulse or DC) exceeds 18V. For this reason the maximum operating supply voltage is 18V.

Fig. 26

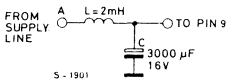
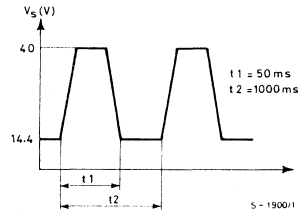


Fig. 27



Short circuit (AC conditions)

The TDA 2004 can withstand a permanent short-circuit on the output for a supply voltage up to 16V.

Polarity inversion

High current (up to 10A) can be handled by the device with no damage for a longer period than the blow-out time of a quick 2A fuse (normally connected in series with the supply). This feature is added to avoid destruction, if during fitting to the car, a mistake on the connection of the supply is made.

Open ground

When the radio is the ON condition and the ground is accidentally opened, a standard audio amplifier will be damaged. On the TDA 2004 protection diodes are included to avoid any damage.

Inductive load

A protection diode is provided to allow use of the TDA 2004 with inductive loads.

DC voltage

The maximum operating DC voltage on the TDA 2004 is 18V.

However the device can withstand a DC voltage up to 28V with no damage. This could occur during winter if two batteries are series connected to crank the engine.

BUILD-IN PROTECTION SYSTEMS (continued)

Thermal shut-down

The presence of a thermal limiting circuit offers the following advantages:

- 1) an overload on the output (even if it is permanent), or an excessive ambient temperature can be easily withstood.
- 2) the heatsink can have a smaller factor of safety compared with that of a conventional circuit. There is no device damage in the case of excessive junction temperature: all that happens is that P_o (and therefore P_{tot}) and I_d are reduced.

The maximum allowable power dissipation depends upon the size of the external heatsink (i.e. its thermal resistance); fig. 28 shows this dissipable power as a function of ambient temperature for different thermal resistance.

Fig. 28 - Maximum allowable power dissipation vs. ambient temperature

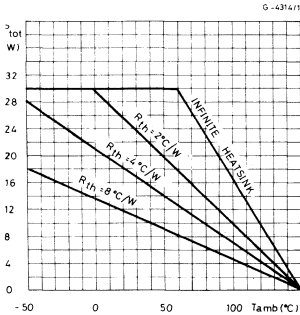


Fig. 29 - Output power and drain current vs. case temperature

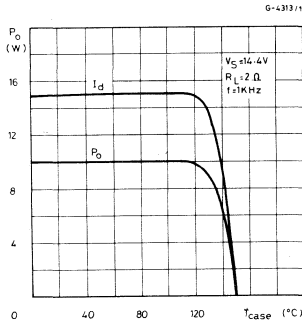
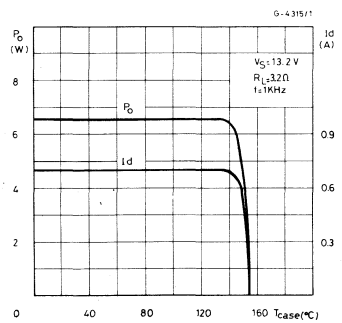


Fig. 30 - Output power and drain current vs. case temperature



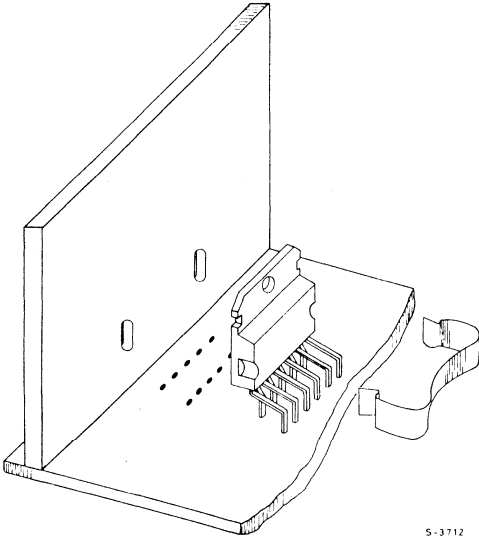
MOUNTING INSTRUCTIONS

The power dissipated in the circuit must be removed by adding an external heatsink.

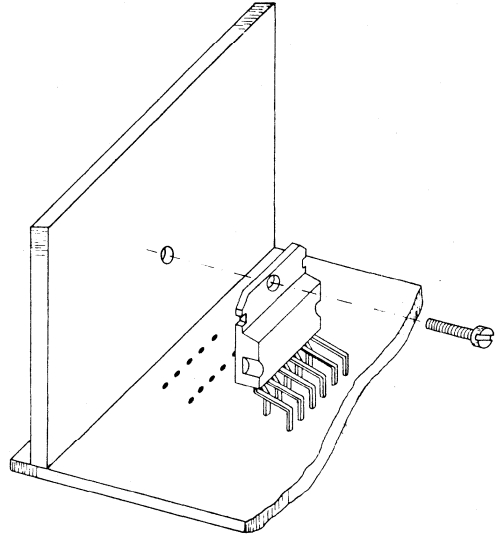
Thanks to the MULTIWATT[®] package attaching the heatsink is very simple, a screw or a compression spring (clip) being sufficient. Between the heatsink and the package it is better to insert a layer of silicon grease, to optimize the thermal contact; no electrical isolation is needed between the two surfaces.

MOUNTING INSTRUCTIONS (continued)

Fig. 31 - Mounting examples



S-3712



LINEAR INTEGRATED CIRCUIT

PRELIMINARY DATA

20 W BRIDGE BOOSTER FOR CAR RADIO

The TDA 2005 is a class B dual audio power amplifier in MULTIWATT® package specifically designed for car radio application: **power booster amplifiers** are easily designed using this device that provides a high current capability (up to 3.5A) and that can drive very low impedance loads (down to 1.6 Ω in stereo applications) obtaining an output power of more than 20W (bridge configuration).

High output power: $P_o = 10 + 10W @ R_L = 2\Omega, d = 10\%$; $P_o = 20W @ R_L = 4\Omega, d = 10\%$

High reliability of the chip and package with additional complete safety during operation thanks to protection against:

- output DC and AC short circuit to ground or across the load.
- overrating chip temperature (150°C)
- load dump voltage surge.
- fortuitous open ground.
- polarity inversion.
- very inductive loads.

Flexibility in use: bridge or stereo booster amplifiers with or without bootstrap and with programmable gain and bandwidth.

Space and cost saving: very low number of external components, very simple mounting system with no electrical isolation between the package and the heatsink (one screw only).

In addition, the circuit offers **loudspeaker protection** during short circuit for one wire to ground.

ABSOLUTE MAXIMUM RATINGS

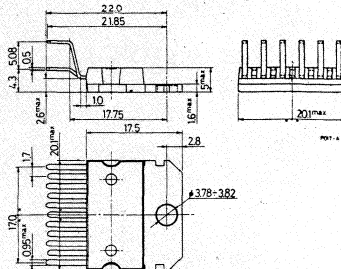
V_s	Operating supply voltage	18	V
V_s	DC supply voltage	28	V
V_s	Peak supply voltage (for 50 ms)	40	V
I_o (*)	Output peak current (non repetitive $t = 0.1$ ms)	4.5	A
I_o (*)	Output peak current (repetitive $f \geq 10$ Hz)	3.5	A
P_{tot}	Power dissipation at $T_{case} = 60^\circ C$	30	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150°	C

(*) The max. output current is internally limited

ORDERING NUMBERS: TDA 2005 M - Bridge application
TDA 2005 S - Stereo application

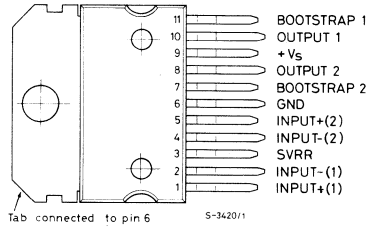
MECHANICAL DATA

Dimensions in mm.

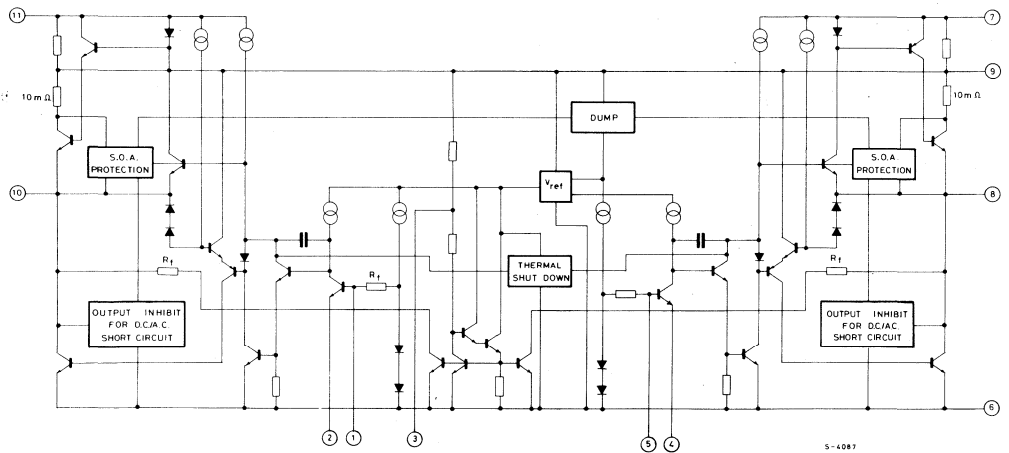


TDA 2005

CONNECTION DIAGRAM (top view)



SCHEMATIC DIAGRAM



THERMAL DATA

$R_{th\ j-case}$ Thermal resistance junction-case

max 3 °C/W

BRIDGE AMPLIFIER APPLICATION (TDA 2005M)

Fig. 1 - Test and application circuit (Bridge amplifier)

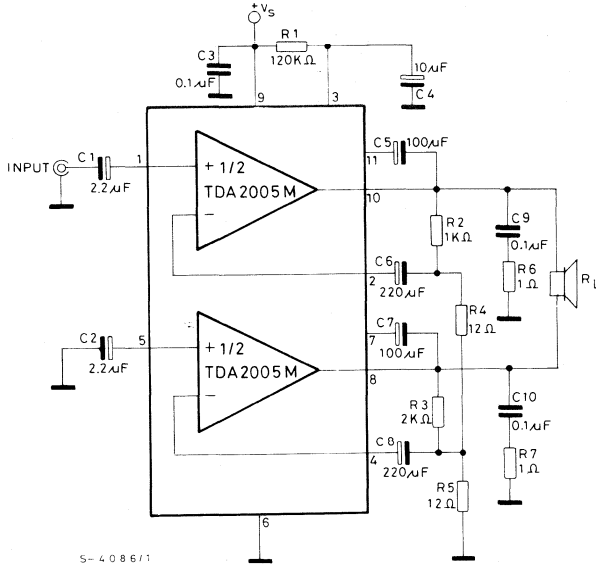
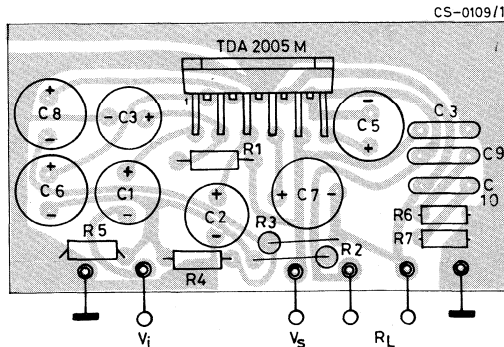


Fig. 2 - P.C. board and component layout (scale 1:1)



TDA 2005

ELECTRICAL CHARACTERISTICS (Refer to the **bridge** application circuit, $T_{amb} = 25^{\circ}\text{C}$, $G_v = 50\text{ dB}$, $R_{th}(\text{heatsink}) = 4^{\circ}\text{C/W}$, unless otherwise specified).

Parameters		Test conditions	Min.	Typ.	Max.	Unit
V_s	Supply voltage		8		18	V
V_{OS}	Output offset voltage ^(*) (between pin 8 and 10)	$V_s = 14.4\text{V}$ $V_s = 13.2\text{V}$			150 150	mV mV
I_d	Total quiescent drain current	$V_s = 14.4\text{V}$ $R_L = 4\Omega$		75	150	mA
		$V_s = 13.2\text{V}$ $R_L = 3.2\Omega$		70	160	mA
P_O	Output power	$d = 10\%$ $f = 1\text{ KHz}$				
		$V_s = 14.4\text{V}$ $R_L = 4\Omega$ $R_L = 3.2\Omega$	18 20	20 22		W W
		$V_s = 13.2\text{V}$ $R_L = 3.2\Omega$	17	19		W
d	Distortion	$f = 1\text{ KHz}$ $V_s = 14.4\text{V}$ $R_L = 4\Omega$ $P_O = 50\text{ mW to } 15\text{W}$			1	%
		$V_s = 13.2\text{V}$ $R_L = 3.2\Omega$ $P_O = 50\text{ mW to } 13\text{W}$			1	%
V_i	Input sensitivity	$f = 1\text{ KHz}$ $P_O = 2\text{W}$ $R_L = 4\Omega$ $P_O = 2\text{W}$ $R_L = 3.2\Omega$		9 8		mV mV
R_i	Input resistance	$f = 1\text{ KHz}$	70			K Ω
f_L	Low frequency roll off (-3 dB)	$R_L = 3.2\Omega$			40	Hz
f_H	High frequency roll off (-3 dB)	$R_L = 3.2\Omega$	20			KHz
G_v	Closed loop voltage gain	$f = 1\text{ KHz}$		50		dB
e_N	Total input noise voltage	$R_g = 10\text{ K}\Omega$ ^(**)		3	10	μV
SVR	Supply voltage rejection	$R_g = 10\text{ K}\Omega$ $C_4 = 10\mu\text{F}$ $f_{\text{ripple}} = 100\text{ Hz}$ $V_{\text{ripple}} = 0.5\text{ V}$	45	55		dB
η	Efficiency	$V_s = 14.4\text{V}$ $f = 1\text{ KHz}$ $P_O = 20\text{W}$ $R_L = 4\Omega$		60		%
		$P_O = 22\text{W}$ $R_L = 3.2\Omega$		60		%
		$V_s = 13.2\text{V}$ $f = 1\text{ KHz}$ $P_O = 19\text{W}$ $R_L = 3.2\Omega$		58		%
T_{SD}	Thermal shut-down case temperature	$V_s = 14.4\text{V}$ $R_L = 4\Omega$ $f = 1\text{ KHz}$ $P_{\text{tot}} = 13\text{W}$	100	110		$^{\circ}\text{C}$
V_{OSH}	Output voltage with one side of the speaker shorted to ground	$V_s = 14.4\text{V}$ $R_L = 4\Omega$ $V_s = 13.2\text{V}$ $R_L = 3.2\Omega$			2	V

(*) For TDA 2005M only.

(**) Bandwidth filter: 22 Hz to 22 KHz.

Fig. 3 - Output offset voltage vs. supply voltage

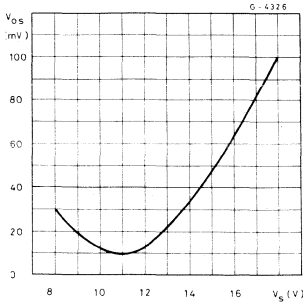


Fig. 4 - Distortion vs. output power (Bridge amplifier)

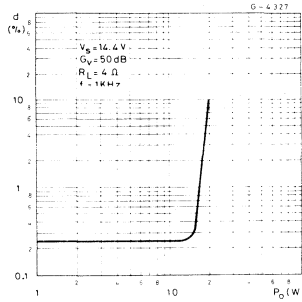
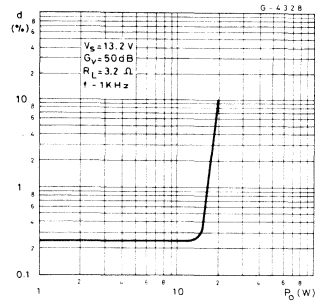


Fig. 5 - Distortion vs. output power (Bridge amplifier)



BRIDGE AMPLIFIER DESIGN

The following considerations can be useful when designing a bridge amplifier.

Parameter		Single ended	Bridge
$V_o \text{ max}$	Peak output voltage (before clipping)	$\frac{1}{2} (V_s - 2 V_{CE \text{ sat}})$	$V_s - 2 V_{CE \text{ sat}}$
$I_o \text{ max}$	Peak output current (before clipping)	$\frac{1}{2} \frac{(V_s - 2 V_{CE \text{ sat}})}{R_L}$	$\frac{V_s - 2 V_{CE \text{ sat}}}{R_L}$
$P_o \text{ max}$	rms output power (before clipping)	$\frac{1}{4} \frac{(V_s - 2 V_{CE \text{ sat}})^2}{2 R_L}$	$\frac{(V_s - 2 V_{CE \text{ sat}})^2}{2 R_L}$

where: $V_{CE \text{ sat}}$ = output transistors saturation voltage
 V_s = allowable supply voltage
 R_L = load impedance.

Voltage and current swings are twice for a bridge amplifier in comparison with single ended amplifier. In other words, with the same R_L the bridge configuration can deliver an output power that is four times the output power of a single ended amplifier, while, with the same max output current the bridge configuration can deliver an output power that is twice the output power of a single ended amplifier. Care must be taken when selecting V_s and R_L in order to avoid an output peak current above the absolute maximum rating.

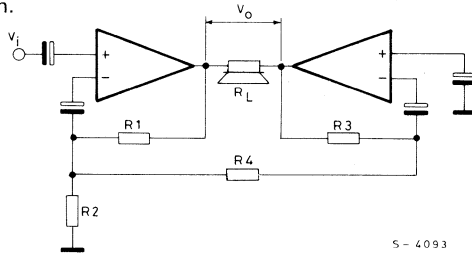
From the expression for $I_o \text{ max}$, assuming $V_s = 14.4V$ and $V_{CE \text{ sat}} = 2V$, the minimum load that can be driven by TDA 2005 in bridge configuration is:

$$R_{L \text{ min}} = \frac{V_s - 2 V_{CE \text{ sat}}}{I_o \text{ max}} = \frac{14.4 - 4}{3.5} = 2.97 \Omega$$

TDA 2005

BRIDGE AMPLIFIER DESIGN (continued)

Fig. 6 - Bridge configuration.



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The voltage gain of the bridge configuration is given by (see fig. 6):

$$G_v = \frac{V_o}{V_i} = 1 + \frac{R_1}{\left(\frac{R_2 \cdot R_4}{R_2 + R_4}\right)} + \frac{R_3}{R_4}$$

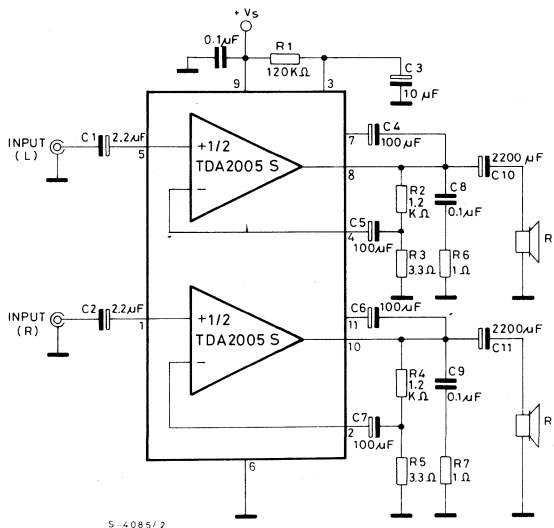
For sufficiently high gains (40 ÷ 50 dB) it is possible to put $R_2 = R_4$ and $R_3 = 2 R_1$, simplifying the formula in:

$$G_v = 4 \frac{R_1}{R_2}$$

G_v (dB)	R_1 (Ω)	$R_2 = R_4$ (Ω)	R_3 (Ω)
30	1000	130	2000
40	1000	39	2000
50	1000	12	2000

STEREO AMPLIFIER APPLICATION (TDA 2005S)

Fig. 7 - Typical application circuit



S - 4085/2

ELECTRICAL CHARACTERISTICS (Refer to the **stereo** application circuit, $T_{amb} = 25^{\circ}\text{C}$, $G_v = 50\text{ dB}$, $R_{th(\text{heatsink})} = 4^{\circ}\text{C/W}$, unless otherwise specified).

Parameters	Test conditions	Min.	Typ.	Max.	Unit
V_s Supply voltage		8		18	V
V_o Quiescent output voltage	$V_s = 14.4\text{V}$ $V_s = 13.2\text{V}$	6.6 6	7.2 6.6	7.8 7.2	V V
I_d Total quiescent drain current	$V_s = 14.4\text{V}$ $V_s = 13.2\text{V}$		65 62	120 120	mA mA
P_o Output power (each channel)	$f = 1\text{ KHz}$ $d = 10\%$ $V_s = 14.4\text{V}$ $R_L = 4\Omega$ $R_L = 3.2\Omega$ $R_L = 2\Omega$ $R_L = 1.6\Omega$ $V_s = 13.2\text{V}$ $R_L = 3.2\Omega$ $R_L = 1.6\Omega$ $V_s = 16\text{V}$ $R_L = 2\Omega$	6 7 9 10 6 9	6.5 8 10 11 6.5 10 12		W W W W W W W
d Distortion (each channel)	$f = 1\text{ KHz}$ $V_s = 14.4\text{V}$ $R_L = 4\Omega$ $P_o = 50\text{ mW to } 4\text{W}$ $V_s = 14.4\text{V}$ $R_L = 2\Omega$ $P_o = 50\text{ mW to } 6\text{W}$ $V_s = 13.2\text{V}$ $R_L = 3.2\Omega$ $P_o = 50\text{ mW to } 3\text{W}$ $V_s = 13.2\text{V}$ $R_L = 1.6\Omega$ $P_o = 40\text{ mW to } 6\text{W}$		0.2 0.3 0.2 0.3	1 1 1 1	% % % %
CT Cross talk ($^{\circ}$)	$V_s = 14.4\text{V}$ $R_L = 4\Omega$ $V_o = 4\text{V}_{\text{rms}}$ $R_g = 10\text{ K}\Omega$	$f = 1\text{ KHz}$ $f = 10\text{ KHz}$	60 45		dB dB
V_i Input saturation voltage		300			mV
V_i Input sensitivity	$f = 1\text{ KHz}$ $P_o = 1\text{W}$ $R_L = 4\Omega$ $R_L = 3.2\Omega$		6 5.5		mV
R_i Input resistance	$f = 1\text{ KHz}$	non inverting input inverting input	70 10	200	K Ω K Ω
f_L Low frequency roll off (-3 dB)	$R_L = 2\Omega$			50	Hz
f_H High frequency roll off (-3 dB)	$R_L = 2\Omega$		15		KHz
G_v Voltage gain (open loop)	$f = 1\text{ KHz}$		90		dB
G_v Voltage gain (closed loop)	$f = 1\text{ KHz}$		48	51	dB
ΔG_v Closed loop gain matching			0.5		dB
e_N Total input noise voltage	$R_g = 10\text{ K}\Omega$ ($^{\circ\circ}$)		1.5	5	μV

($^{\circ}$) For TDA 2005S only.

($^{\circ\circ}$) Bandwidth filter: 22 Hz to 22 KHz.

ELECTRICAL CHARACTERISTICS (continued)

Parameters	Test conditions	Min.	Typ.	Max.	Unit
SVR Supply voltage rejection	$R_G = 10\text{ K}\Omega$ $f_{\text{ripple}} = 100\text{ Hz}$ $C_3 = 10\text{ }\mu\text{F}$ $V_{\text{ripple}} = 0.5\text{ V}$	35	45		dB
η Efficiency	$V_S = 14.4\text{ V}$ $f = 1\text{ KHz}$				
	$R_L = 4\Omega$ $P_O = 6.5\text{ W}$		70		%
	$R_L = 2\Omega$ $P_O = 10\text{ W}$		60		%
	$V_S = 13.2\text{ V}$ $f = 1\text{ KHz}$		70		%
	$R_L = 3.2\Omega$ $P_O = 6.5\text{ W}$		60		%
	$R_L = 1.6\Omega$ $P_O = 10\text{ W}$		60		%
T_{sd} Thermal shut-down case temperature	$V_S = 14.4\text{ V}$ $R_L = 2\Omega$ $P_{\text{tot}} = 6.6\text{ W}$	120	130		$^{\circ}\text{C}$

Fig. 8 - Quiescent output voltage vs. supply voltage

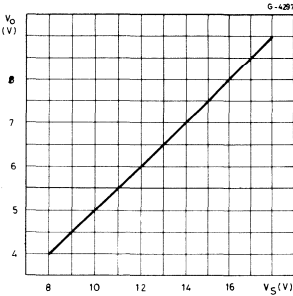


Fig. 9 - Quiescent drain current vs. supply voltage

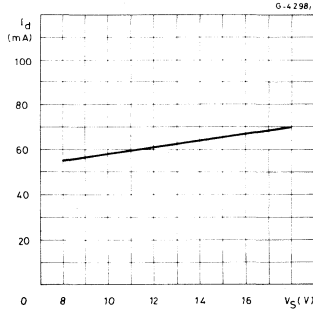


Fig. 10 - Distortion vs. output power

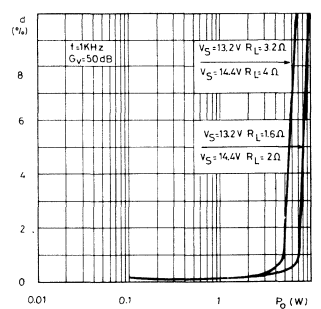


Fig. 11 - Output power vs. supply voltage

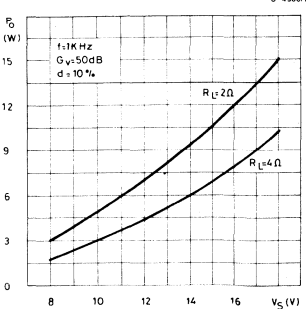


Fig. 12 - Output power vs. supply voltage

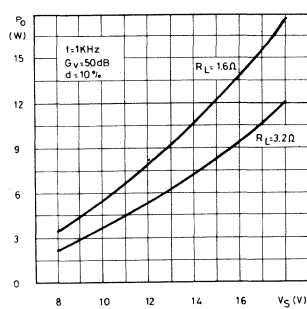


Fig. 13 - Distortion vs. frequency

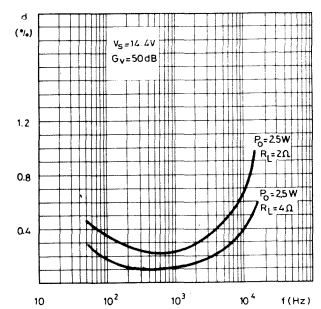


Fig. 14 - Distorsion vs. frequency

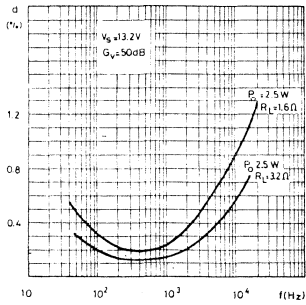


Fig. 15 - Supply voltage rejection vs. C_3

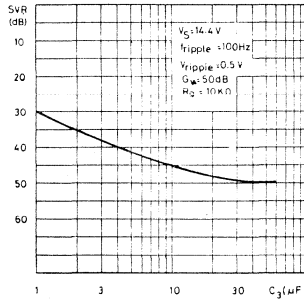


Fig. 16 - Supply voltage rejection vs. frequency

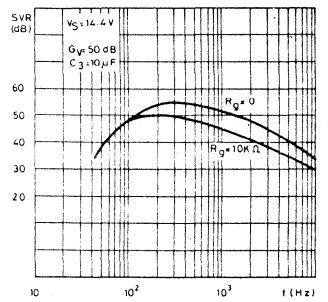


Fig. 17 - Supply voltage rejection vs. values of capacitors C_2 and C_3

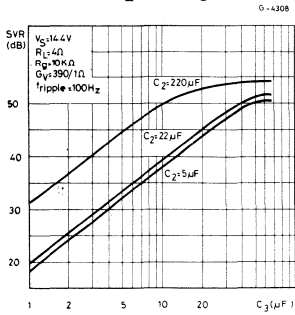


Fig. 18 - Supply voltage rejection vs. values of capacitors C_2 and C_3

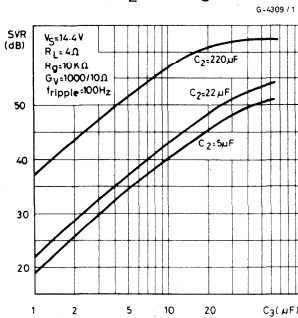


Fig. 19 - Gain vs. input sensitivity

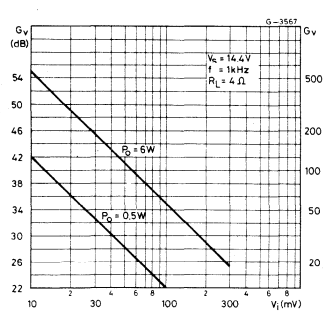


Fig. 20 - Gain vs. input sensitivity

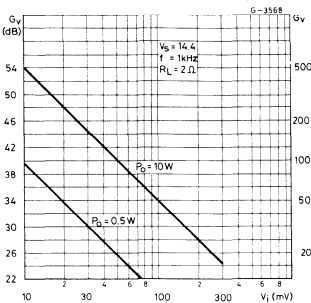


Fig. 21 - Total power dissipation and efficiency vs. output power (bridge)

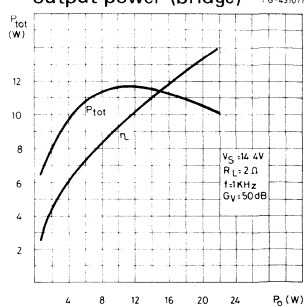
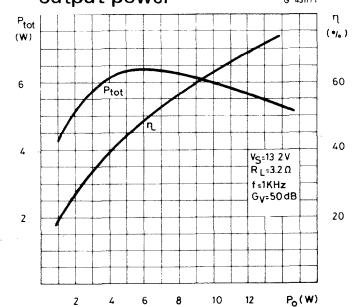


Fig. 22 - Total power dissipation and efficiency vs. output power



TDA 2005

APPLICATION INFORMATION

Fig. 23 - 10 + 10W stereo amplifier with tone balance and loudness control

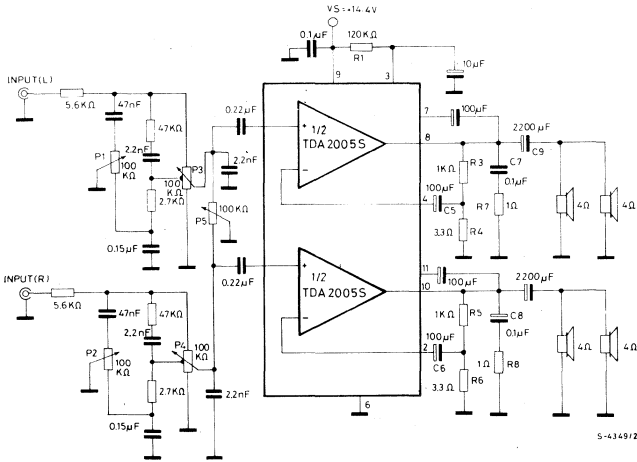


Fig. 24 - Tone control response (circuit of fig. 23)

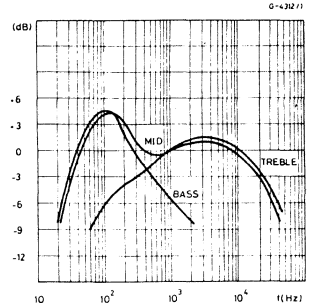


Fig. 25 - 20W Bus amplifier

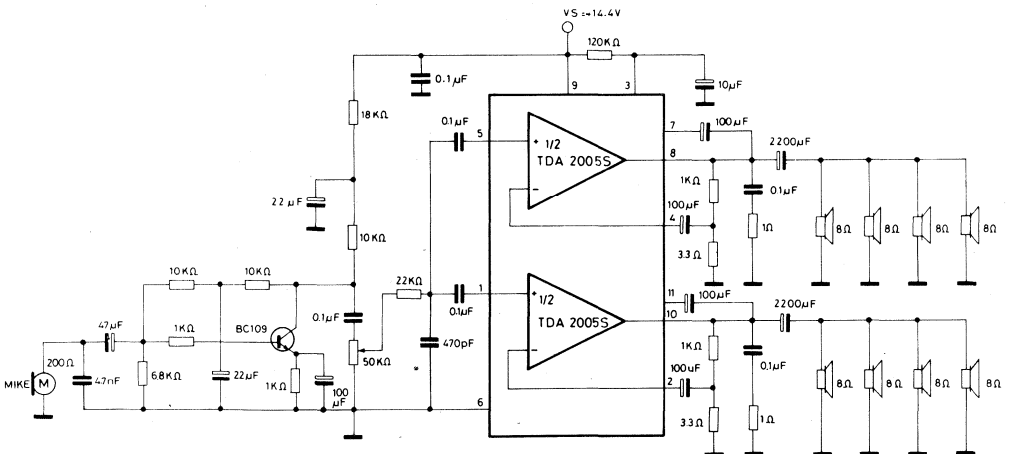


Fig. 26 - Simple 20W two way amplifier ($f_c = 2$ KHz)

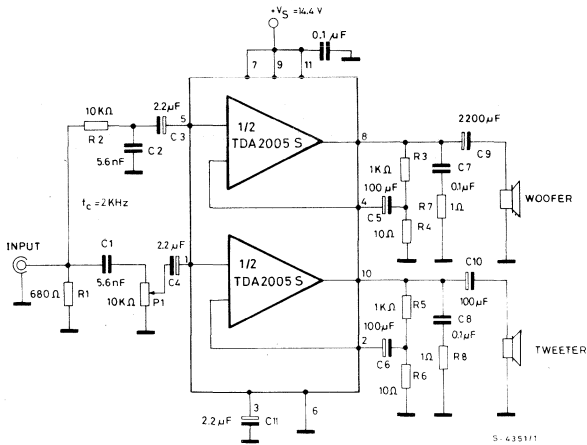
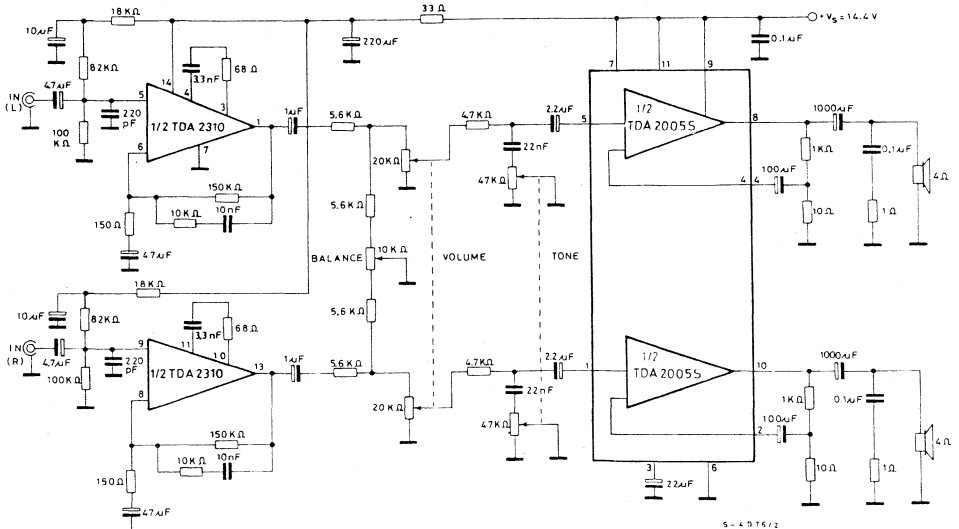


Fig. 27 - High quality, 10 + 10W cassette player



APPLICATION SUGGESTION

The recommended values of the components are those shown on Bridge application circuit of fig. 1. Different values can be used, the following table can help the designer.

Component	Recommended Value	Purpose	Larger than	Smaller than
R ₁	120 KΩ	Optimization of the output symmetry	Smaller P _O max	Smaller P _O max
R ₂	1 KΩ	Closed loop gain setting (see BRIDGE AMPLIFIER DESIGN)		
R ₃	2 KΩ			
R ₄ and R ₅	12 Ω			
R ₆ and R ₇	1 Ω	Frequency stability	Danger of oscillation at high frequency with inductive loads	
C ₁	2.2 μF	Input DC decoupling	High turn on delay	Higher turn on pop. Higher low frequency cutoff. Increase of noise.
C ₂	2.2 μF	Optimization of turn on pop and turn on delay.		
C ₃	0.1 μF	Supply by pass		Danger of oscillation.
C ₄	10 μF	Ripple Rejection	Increase of SVR. Increase of the switch-on time.	Degradation of SVR.
C ₅ and C ₇	100 μF	Bootstrapping		Increase of distortion at low frequency.
C ₆ and C ₈	220 μF	Feedback input DC decoupling, low frequency cutoff.		Higher low frequency cutoff.
C ₉ and C ₁₀	0.1 μF	Frequency stability.		Danger of oscillation.

BUILT-IN PROTECTION SYSTEMS

Load dump voltage surge

The TDA 2005 has a circuit which enables it to withstand a voltage pulse train, on pin 9, of the type shown in fig. 29.

If the supply voltage peaks to more than 40V, then an LC filter must be inserted between the supply and pin 9, in order to assure that the pulses at pin 9 will be held within the limits shown.

A suggested LC network is shown in fig. 28. With this network, a train of pulses with amplitude up to 120V and width of 2 ms can be applied at point A. This type of protection is ON when the supply voltage (pulse or DC) exceeds 18V. For this reason the maximum operating supply voltage is 18V.

Fig. 28

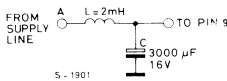
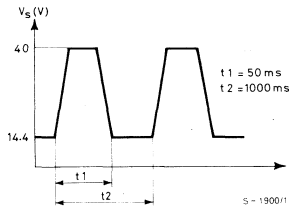


Fig. 29



Short circuit (AC and DC conditions)

The TDA 2005 can withstand a permanent short-circuit on the output for a supply voltage up to 16V.

Polarity inversion

High current (up to 10A) can be handled by the device with no damage for a longer period than the blow-out time of a quick 2A fuse (normally connected in series with the supply). This feature is added to avoid destruction, if during fitting to the car, a mistake on the connection of the supply is made.

Open ground

When the radio is in the ON condition and the ground is accidentally opened, a standard audio amplifier will be damaged. On the TDA 2005 protection diodes are included to avoid any damage.

Inductive load

A protection diode is provided to allow use of the TDA 2005 with inductive loads.

DC voltage

The maximum operating DC voltage for the TDA 2005 is 18V.

However the device can withstand a DC voltage up to 28V with no damage. This could occur during winter if two batteries are series connected to crank the engine.

Thermal shut-down

The presence of a thermal limiting circuit offers the following advantages:

- 1) an overload on the output (even if it is permanent), or an excessive ambient temperature can be easily withstood.
- 2) the heatsink can have a smaller factor of safety compared with that of a conventional circuit. There is no device damage in the case of excessive junction temperature: all that happens is that P_o (and therefore P_{tot}) and I_d are reduced.

The maximum allowable power dissipation depends upon the size of the external heatsink (i.e. its thermal resistance); fig. 30 shows this dissippable power as a function of ambient temperature for different thermal resistance.

TDA 2005

Fig. 30 - Maximum allowable power dissipation vs. ambient temperature

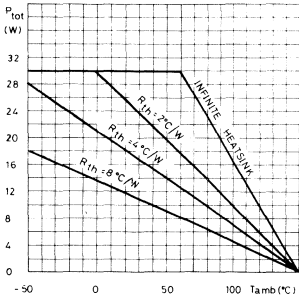


Fig. 31 - Output power and drain current vs. case temperature

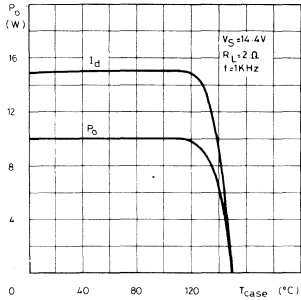
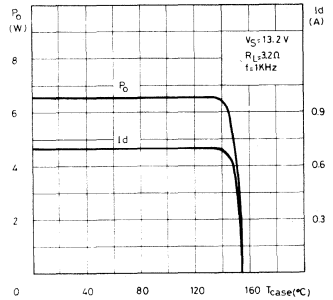


Fig. 32 - Output power and drain current vs. case temperature



Loudspeaker protection

The circuit offers loudspeaker protection during short circuit for one wire to ground.

MOUNTING INSTRUCTIONS

The power dissipated in the circuit must be removed by adding an external heatsink. Thanks to the MULTIWATT® package attaching the heatsink is very simple, a screw or a compression spring (clip) being sufficient. Between the heatsink and the package it is better to insert a layer of silicon grease, to optimize the thermal contact; no electrical isolation is needed between the two surfaces.

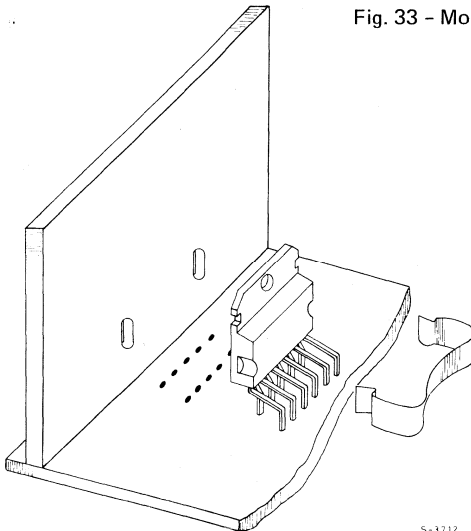
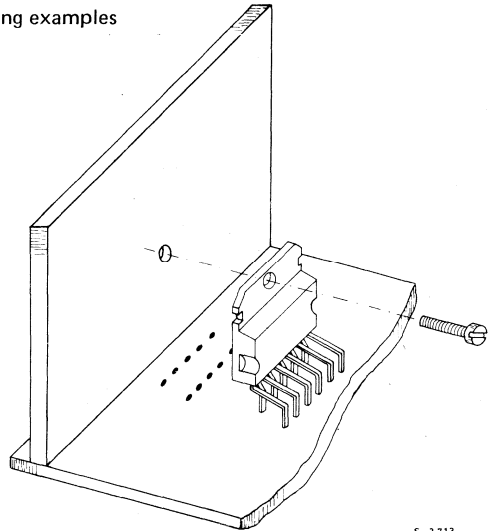


Fig. 33 - Mounting examples



S-3712

S-3713

LINEAR INTEGRATED CIRCUIT

10W-AUDIO POWER AMPLIFIER WITH SHORT CIRCUIT PROTECTION AND THERMAL SHUT-DOWN

The TDA 2006 is a monolithic integrated circuit in Pentawatt[®] package, intended for use as a low frequency class "AB" amplifier. At $\pm 12V$, $d = 10\%$ typically it provides 12W output power on a 4Ω load and 8W on a 8Ω . The TDA 2006 provides high output current and has very low harmonic and cross-over distortion. Further the device incorporates an original (and patented) short circuit protection system comprising an arrangement for automatically limiting the dissipated power so as to keep the working point of the output transistors within their safe operating area. A conventional thermal shutdown system is also included. The TDA 2006 is pin to pin equivalent to the TDA 2030.

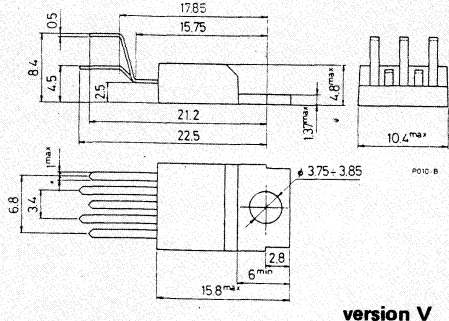
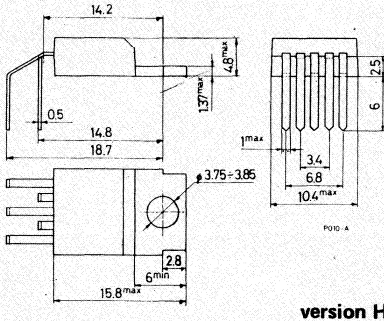
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	± 15	V
V_i	Input voltage	V_s	
V_i	Differential input voltage	± 12	V
I_o	Output peak current (internally limited)	3	A
P_{tot}	Power dissipation at $T_{case} = 90^\circ C$	20	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ C$

ORDERING NUMBERS: TDA 2006H; TDA 2006V

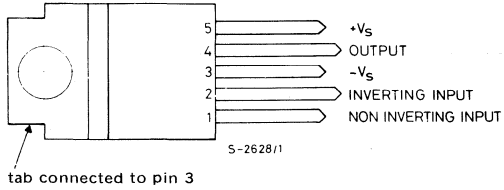
MECHANICAL DATA

Dimensions in mm

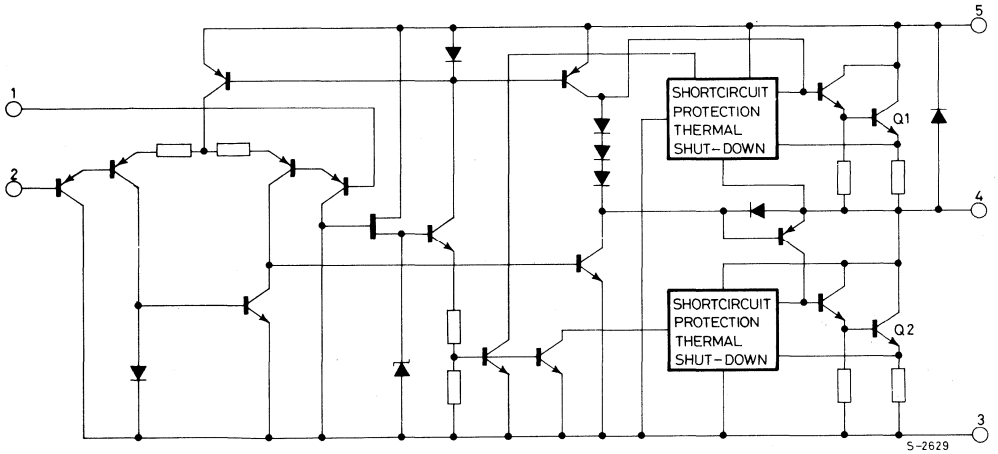


TDA 2006

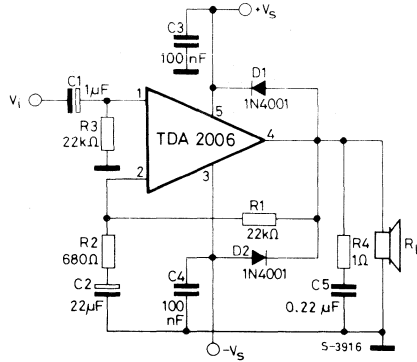
CONNECTION DIAGRAM



SCHEMATIC DIAGRAM



TEST AND APPLICATION CIRCUIT



THERMAL DATA

$R_{th-j case}$	Thermal resistance junction-case	max	3	°C/W
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ELECTRICAL CHARACTERISTICS (Refer to the test circuit; $V_s = \pm 12V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameters	Test conditions	Min.	Typ.	Max.	Unit
V_s Supply voltage		± 6		± 15	V
I_d Quiescent drain current	$V_s = \pm 15V$		40	80	mA
I_b Input bias current			0.2	3	μA
V_{OS} Input offset voltage				± 8	mV
I_{OS} Input offset current				± 80	nA
V_{OS} Output offset voltage				± 10	± 100
P_o Output power	$d = 10\%$ $f = 1 KHz$ $R_L = 4\Omega$ $R_L = 8\Omega$	6	12 8		W W

TDA 2006

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Units
d	Distortion $P_o = 0.1$ to $8W$ $R_L = 4\Omega$ $f = 1$ KHz		0.2		%
		$P_o = 0.1$ to $4W$ $R_L = 8\Omega$ $f = 1$ KHz		0.1	1
V_i	Input sensitivity $f = 1$ KHz $P_o = 10W$ $R_L = 4\Omega$ $P_o = 6W$ $R_L = 8\Omega$		200 220		mV mV
B	Frequency response (-3 dB) $P_o = 8W$ $R_L = 4\Omega$	10 to 140,000			Hz
R_i	Input resistance (pin 1)	0.5	5		M Ω
G_v	Voltage gain (open loop)		75		dB
G_v	Voltage gain (closed loop)	29.5	30	30.5	dB
e_N	Input noise voltage	B (-3 dB) = 22Hz to 22kHz $R_L = 4\Omega$			μV
i_N	Input noise current		80	200	pA
SVR	Supply voltage rejection $R_L = 4\Omega$ $R_g = 22$ K Ω $f_{ripple} = 100$ Hz (*)	40	50		dB
I_d	Drain current $P_o = 12W$ $R_L = 4\Omega$ $P_o = 8W$ $R_L = 8\Omega$		850 500		mA mA
T_{sd}	Thermal shut down case temperature temperature	$P_{tot} = 9W$	110		$^{\circ}C$

(*) Referring to fig. 15, single supply.

Fig. 1 - Output power vs. supply voltage

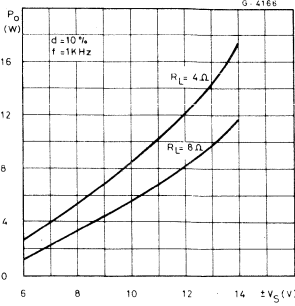


Fig. 2 - Distortion vs. output power

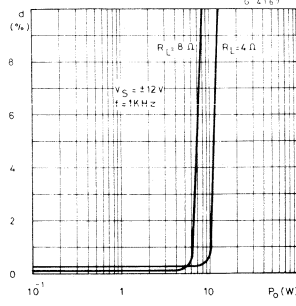


Fig. 3 - Distortion vs. frequency

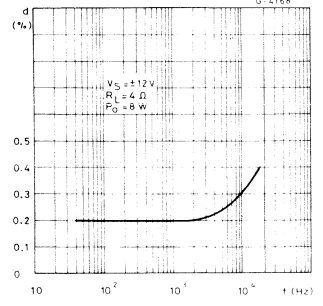


Fig. 4 - Distortion vs. frequency

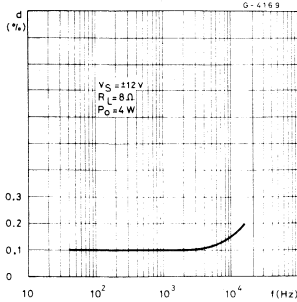


Fig. 5 - Sensitivity vs. output power

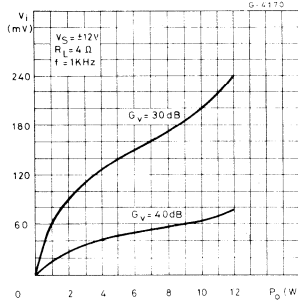


Fig. 6 - Sensitivity vs. output power

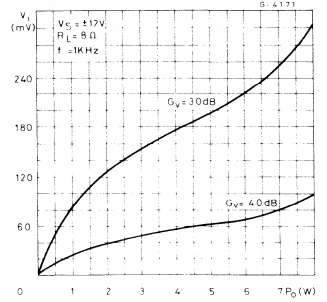


Fig. 7 - Frequency response with different values of the rolloff capacitor C₈ (see fig. 13)

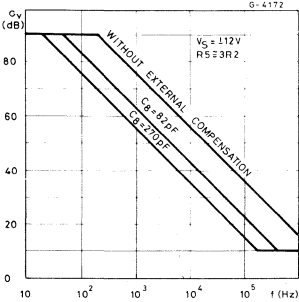


Fig. 8 - Value of C₈ vs. voltage gain for different bandwidths (see fig. 13)

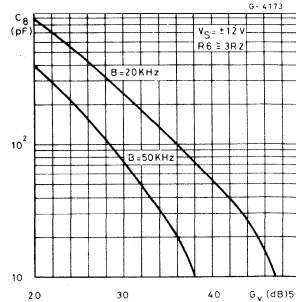
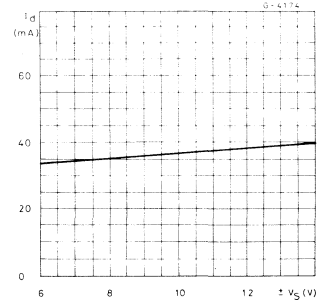


Fig. 9 - Quiescent current vs. supply voltage



TDA 2006

Fig. 10 - Supply voltage rejection vs. voltage gain

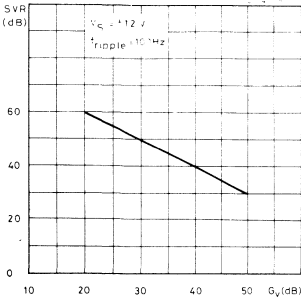


Fig. 11 - Power dissipation and efficiency vs. output power

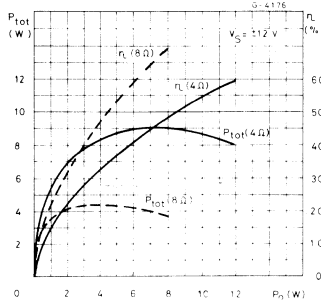


Fig. 12 - Maximum power dissipation vs. supply voltage (sine wave operation)

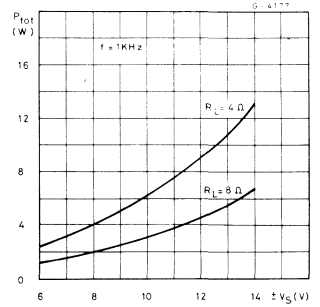


Fig. 13 - Application circuit with split power supply

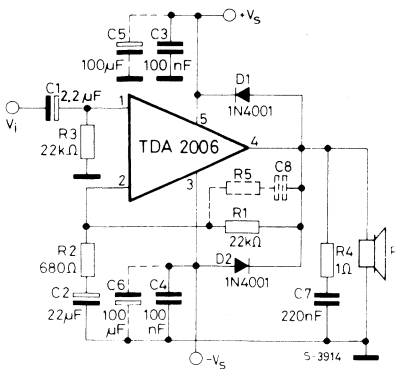


Fig. 14 - P.C. board and component layout for the circuit of fig. 13

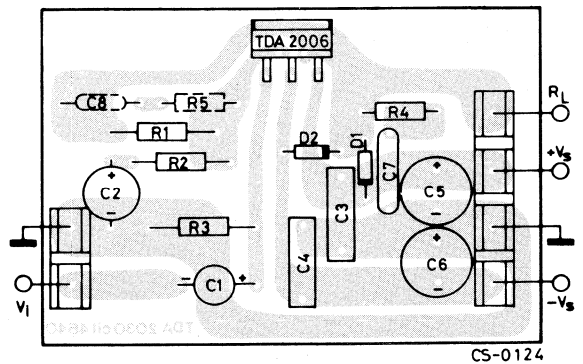


Fig. 15 – Application circuit with single power supply

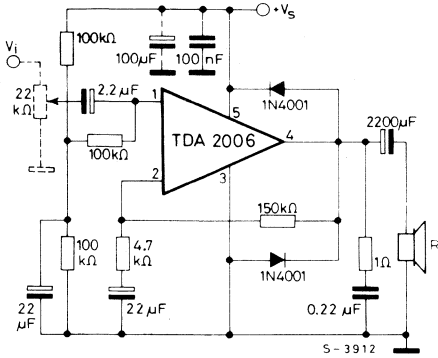


Fig. 16 – P.C. board and component layout for the circuit of fig. 15

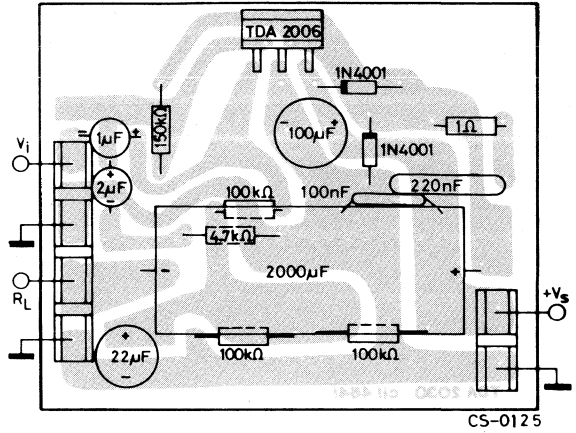
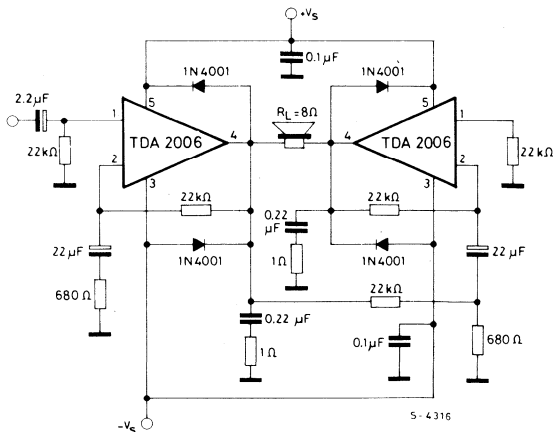


Fig. 17 – Bridge amplifier configuration with split power supply ($P_o = 24\text{W}$, $V_S = \pm 12\text{V}$)



PRACTICAL CONSIDERATION

Printed circuit board

The layout shown in fig. 14 should be adopted by the designers. If different layout are used, the ground points of input 1 and input 2 must be well decoupled from ground of the output on which a rather high current flows.

Assembly suggestion

No electrical isolation is needed between the package and the heat-sink with single supply voltage configuration.

Application suggestion

The recommended values of the components are the ones shown on application circuits of fig. 13. Different values can be used. The following table can help the designers.

Component	Recommended value	Purpose	Larger than recommended value	Smaller than recommended value
R ₁	22 KΩ	Closed loop gain setting	Increase of gain	Decrease of gain
R ₂	680Ω	Closed loop gain setting	Decrease of gain	Increase pf gain
R ₃	22 KΩ	Non inverting input biasing	Increase of input impedance	Decrease of input impedance
R ₄	1Ω	Frequency stability	Danger of oscillation at high frequencies with inductive loads	
R ₅	3 R ₂	Upper frequency cutoff	Poor high frequencies attenuation	Danger of oscillation
C ₁	2.2 μF	Input DC decoupling		Increase of low frequencies cut off
C ₂	22 μF	Inverting input DC decoupling		Increase of low frequencies cutoff
C ₃ C ₄	0.1 μF	Supply voltage by pass		Danger of oscillation
C ₅ C ₆	100 μF	Supply voltage by pass		Danger of oscillation
C ₇	0.22 μF	Frequency stability		Danger of oscillation
C ₈	$\frac{1}{2\pi BR_1}$	Upper frequency cutoff	Lower bandwidth	Larger bandwidth
D ₁ D ₂	1N4001	To protect the device against output voltage spikes.		

SHORT CIRCUIT PROTECTION

The TDA 2006 has an original circuit which limits the current of the output transistors. Fig. 18 shows that the maximum output current is a function of the collector emitter voltage; hence the output transistors work within their safe operating area (fig. 19).

This function can therefore be considered as being peak power limiting rather than simple current limiting. The TDA 2006 is thus protected against temporary overloads or short circuit. Should the short circuit exist for a longer time, the thermal shutdown protection keeps the junction temperature within safe limits.

Fig. 18 - Maximum output current vs. voltage $V_{CE(sat)}$ across each output transistor

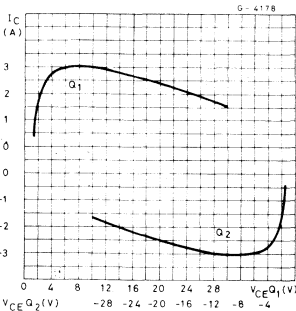
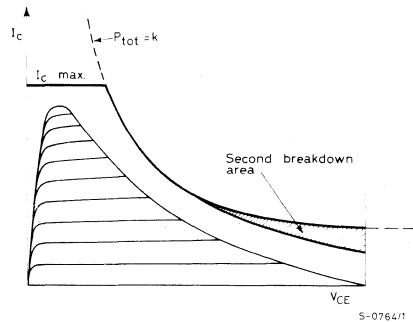


Fig. 19 - Safe operating area and collector characteristics of the protected power transistor



THERMAL SHUT-DOWN

The presence of a thermal limiting circuit offers the following advantages:

- 1) An overload on the output (even if it is permanent), or an above limit ambient temperature can be easily supported since the T_j cannot be higher than 150°C .
- 2) The heatsink can have a smaller factor of safety compared with that of a conventional circuit. There is no possibility of device damage due to high junction temperature.

If for any reason, the junction temperature increases up to 150°C , the thermal shutdown simply reduces the power dissipation and the current consumption.

Fig. 20 – Output power and drain current vs. case temperature ($R_L = 4\Omega$)

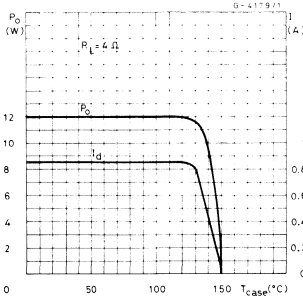
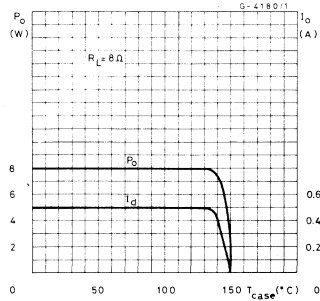


Fig. 21 – Output power and drain current vs. case temperature ($R_L = 8\Omega$)



The maximum allowable power dissipation depends upon the size of the external heatsink (i.e. its thermal resistance); fig. 22 shows this dissippable power as a function of ambient temperature for different thermal resistances.

Fig. 22 – Maximum allowable power dissipation vs. ambient temperature

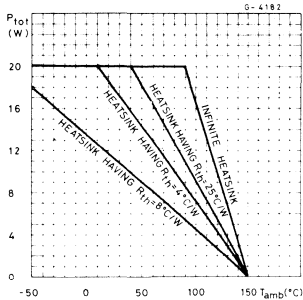
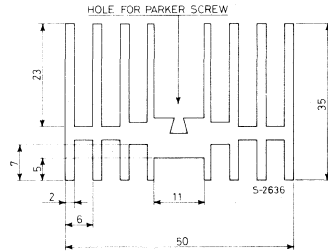


Fig. 23 – Example of heatsink



Dimension suggestion

The following table shows the lenght of the heatsink in fig. 23 for several values of P_{tot} and R_{th} .

P_{tot} (W)	12	8	6
Lenght of heatsink (mm)	60	40	30
R_{th} of heatsink ($^{\circ}C/W$)	4.2	6.2	8.3

LINEAR INTEGRATED CIRCUIT

PRELIMINARY DATA

12W AUDIO AMPLIFIER ($V_s = 22V$, $R_L = 4\Omega$)

The TDA 2008 is a monolithic class B audio power amplifier in Pentawatt[®] package designed for driving low impedance loads (down to 3.2Ω). The device provides a high output current capability (up to 3A), very low harmonic and crossover distortion.

In addition, the device offers the following features:

- very low number of external components
- assembly ease, due to Pentawatt[®] power package with no electrical insulation requirement
- space and cost saving
- high reliability
- flexibility in use
- thermal protection

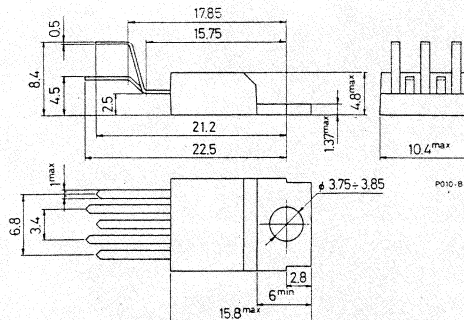
ABSOLUTE MAXIMUM RATINGS

V_s	DC supply voltage	28	V
I_o	Output peak current (repetitive)	3	A
I_o	Output peak current (non repetitive)	4	A
P_{tot}	Power dissipation at $T_{case} = 90^\circ C$	20	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ C$

ORDERING NUMBERS: TDA 2008V

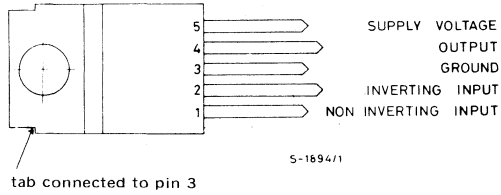
MECHANICAL DATA

Dimensions in mm

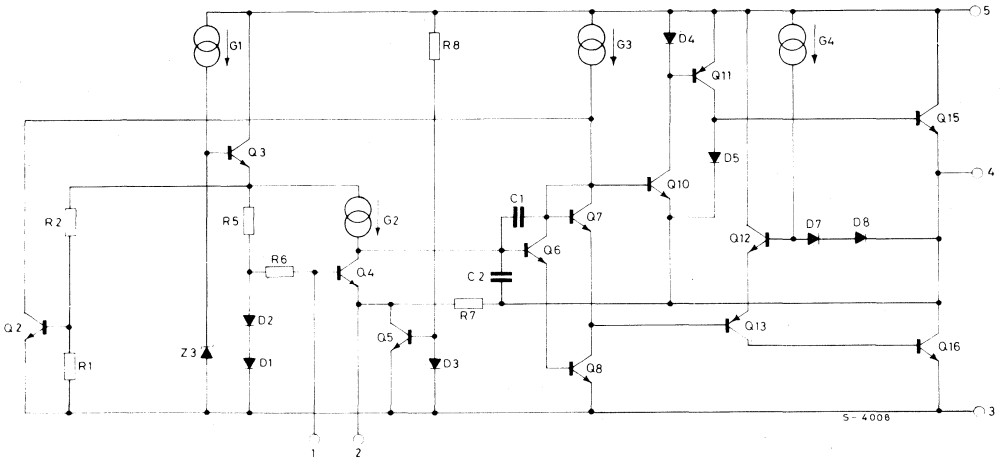


TDA 2008

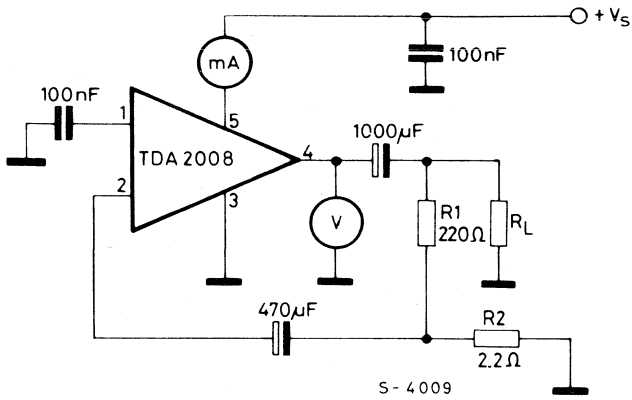
CONNECTION DIAGRAM (top view)



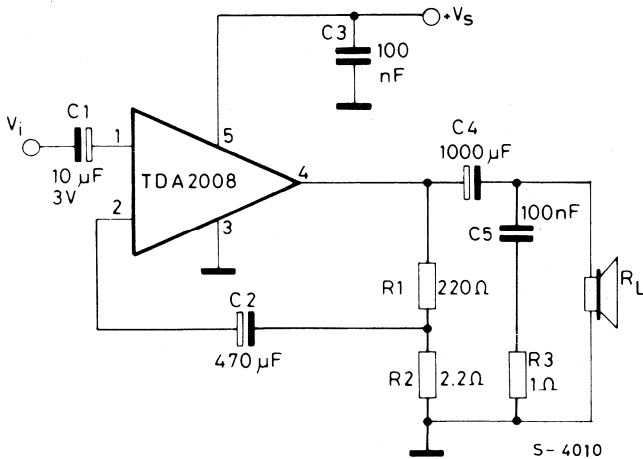
SCHEMATIC DIAGRAM



DC TEST CIRCUIT



AC TEST CIRCUIT



TDA 2008

THERMAL DATA

$R_{th\ j-case}$	Thermal resistance junction-case	max	3	$^{\circ}C/W$
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ELECTRICAL CHARACTERISTICS (Refer to the test circuits, $V_s = 22V$, $T_{amb} = 25^{\circ}C$ unless otherwise specified)

Parameter		Test conditions		Min.	Typ.	Max.	Unit
V_s	Supply voltage			10		28	V
V_o	Quiescent output voltage (pin 4)				10.5		V
I_d	Quiescent drain current (pin 5)				65	115	mA
P_o	Output power	d = 10%	$R_L = 8\Omega$		8		W
			f = 1 KHz	$R_L = 4\Omega$	10	12	W
V_i (RMS)	Input saturation voltage			300			mV
V_i	Input sensitivity	f = 1 KHz	$P_o = 0.5W$	$R_L = 8\Omega$		20	mV
			$P_o = 8W$	$R_L = 8\Omega$		80	mV
			$P_o = 0.5W$	$R_L = 4\Omega$		14	mV
			$P_o = 12W$	$R_L = 4\Omega$		70	mV
B	Frequency response (-3 dB)	$P_o = 1W$ $R_L = 4\Omega$	40 to 15 000				Hz
d	Distortion	f = 1 KHz	$P_o = 0.05$ to 4W	$R_L = 8\Omega$		0.15	%
			$P_o = 0.05$ to 6W	$R_L = 4\Omega$		0.15	%
R_i	Input resistance (pin 1)	f = 1 KHz		70	150		$K\Omega$
G_v	Voltage gain (open loop)	f = 1 KHz $R_L = 8\Omega$			80		dB
G_v	Voltage gain (closed loop)			39.5	40	40.5	dB
e_N	Input noise voltage	BW = 22Hz to 22 KHz			1	5	μV
i_N	Input noise current				60	200	pA
SVR	Supply voltage rejection	$V_{ripple} = 0.5V$ $R_g = 10K\Omega$ $R_L = 4\Omega$	f = 100 Hz	30	36		dB
			f = 15 KHz		36		dB

APPLICATION INFORMATION

Fig. 1 - Typical application circuit

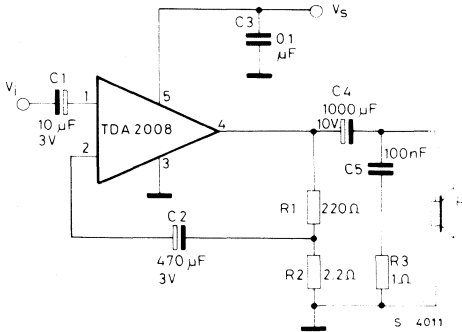


Fig. 2 - P.C. board and component layout for the circuit of fig. 1 (1:1 scale)

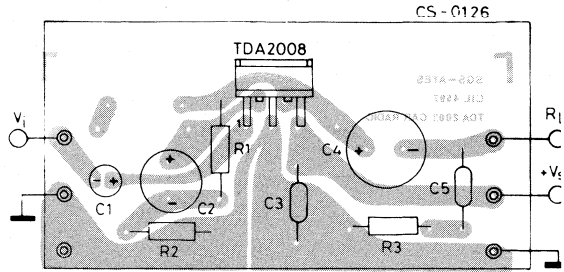


Fig. 3 - 25W bridge configuration application circuit (°)

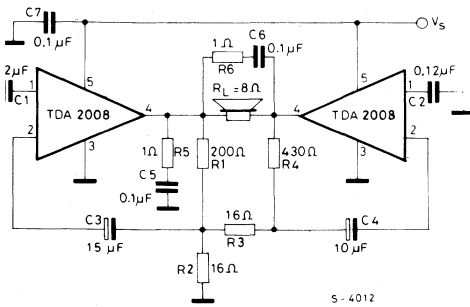
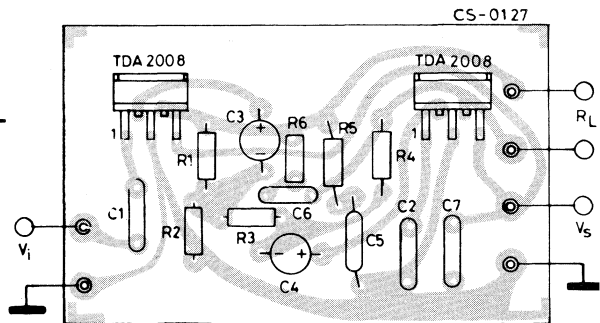


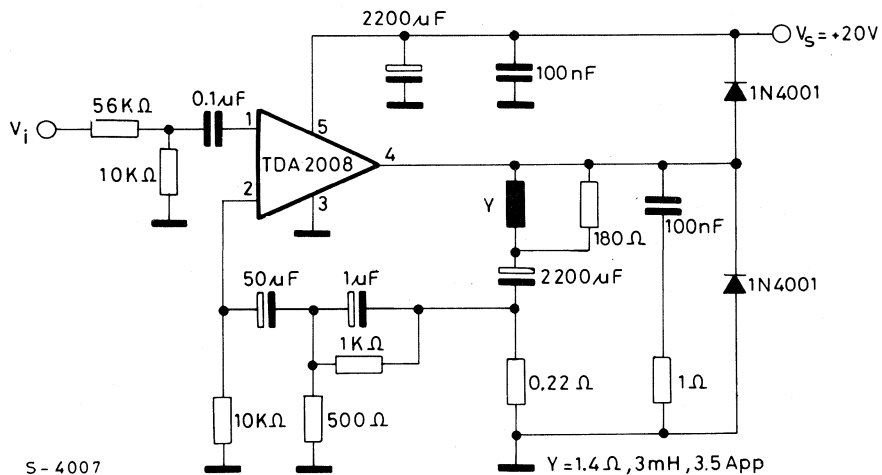
Fig. 4 - P.C. board and component layout for the circuit of fig. 3 (1:1 scale)



(°) The value of the capacitors C3 and C4 are different to optimize the SVR (Typ. = 40 dB)

TDA 2008

VERTICAL DEFLECTION FOR COUNT-DOWN CIRCUITS



LINEAR INTEGRATED CIRCUIT

12W Hi-Fi AUDIO POWER AMPLIFIER WITH SHORT CIRCUIT PROTECTION AND THERMAL SHUT-DOWN

The TDA 2010 is a monolithic integrated operational amplifier in a 14-lead quad in-line plastic package, intended for use as a low frequency class B power amplifier. Typically it provides 12W output power ($d = 1\%$) at $\pm 14V/4\Omega$; at $V_s = \pm 14V$ the guaranteed output power is 10W on a 4Ω load and 8W on a 8Ω load (DIN norm 45500). The TDA 2010 provides high output current (up to 3.5 A) and has very low harmonic and cross-over distortion. Further, the device incorporates an original (and patented) short circuit protection system, comprising an arrangement for automatically limiting the dissipated power so as to keep to working point of the output transistors within their safe operating area. A conventional thermal shut-down system is also included. The TDA 2010 is pin to pin equivalent to TDA 2020.

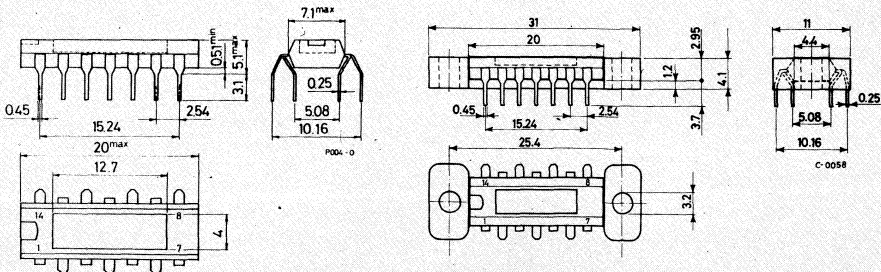
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	± 18	V
V_i	Input voltage	V_s	
V_d	Differential input voltage	± 15	V
I_o	Output peak current (internally limited)	3.5	A
P_{tot}	Power dissipation at $T_{case} \leq 95^\circ C$	18	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ C$

ORDERING NUMERS:	TDA 2010 B82	dual in-line plastic package
	TDA 2010 B92	quad in-line plastic package
	TDA 2010 BC2	dual in-line plastic package with spacer
	TDA 2010 BD2	quad in-line plastic package with spacer

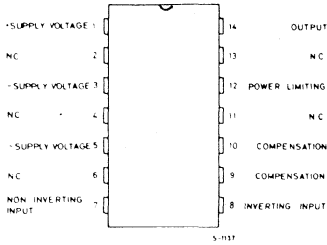
MECHANICAL DATA

Dimensions in mm

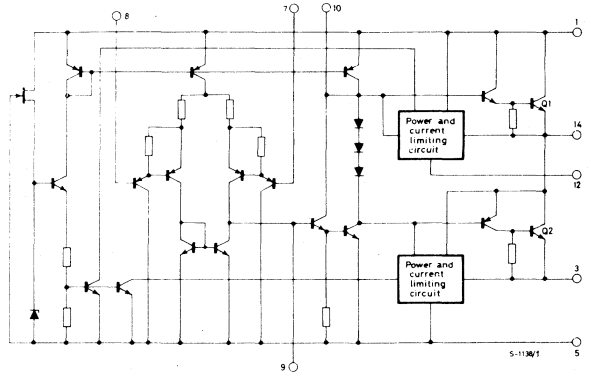


TDA 2010

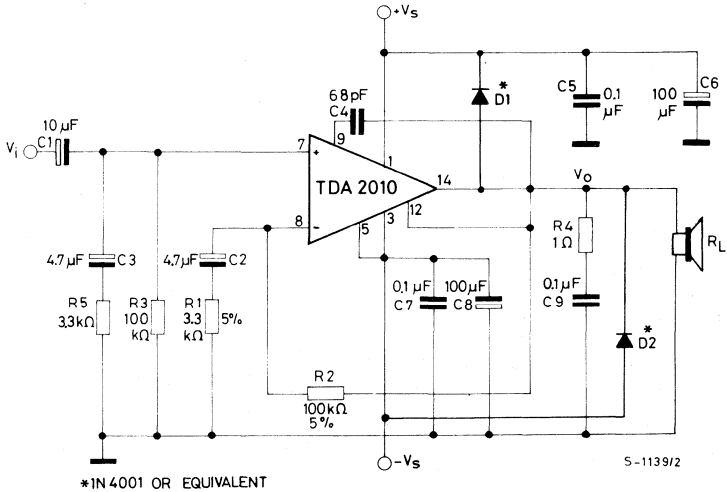
CONNECTION AND SCHEMATIC DIAGRAMS (top view)



The copper slug is electrically connected to pin 5 (substrate)



TEST CIRCUIT



THERMAL DATA

$R_{th\ j-case}$	Thermal resistance junction-case	max	3	$^{\circ}C/W$
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ELECTRICAL CHARACTERISTICS

(Refer to the test circuit, $V_s = \pm 14V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	
V_s	Supply voltage	± 5		± 18	V	
I_d	Quiescent drain current	$V_s = \pm 18V$	45		mA	
I_b	Input bias current	$V_s = \pm 17V$	0.15		μA	
V_{os}	Input offset voltage		5		mV	
I_{os}	Input offset current		0.05		μA	
V_{os}	Output offset voltage		10	100	mV	
P_o	Output power	$d = 1\%$ $T_{case} \leq 70^\circ C$ $f = 40$ to $15,000$ Hz $R_L = 4 \Omega$ $R_L = 8 \Omega$	10 8	12 9		W W
		$d = 10\%$ $T_{case} \leq 70^\circ C$ $f = 1$ kHz $R_L = 4 \Omega$ $R_L = 8 \Omega$		15 12		W W
V_i	Input sensitivity	$f = 1$ kHz $P_o = 10$ W $R_L = 4 \Omega$ $P_o = 8$ W $R_L = 8 \Omega$		220 250		mV mV
B	Frequency response (-3dB)	$R_L = 4 \Omega$ $C4 = 68$ pF	10 to 160 000			Hz
d	Distortion	$P_o = 100$ mW to 10 W $R_L = 4 \Omega$ $T_{case} \leq 70^\circ C$ $f = 1$ kHz $f = 40$ to $15\ 000$ Hz		0.1 0.3	1	% %
		$P_o = 100$ mW to 8 W $R_L = 8 \Omega$ $T_{case} \leq 70^\circ C$ $f = 1$ kHz $f = 40$ to $15\ 000$ Hz		0.1 0.2	1	% %
R_i	Input resistance (pin 7)		5		M Ω	
G_v	Voltage gain (open loop)	$R_L = 4 \Omega$ $f = 1$ kHz	100		dB	
G_v	Voltage gain (closed loop)		29.5	30	30.5	dB
e_N	Input noise voltage	$R_L = 4 \Omega$	4		μV	
i_N	Input noise current	B (-3 dB) = 22 Hz to 22 KHz	0.1		nA	

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
SVR	Supply voltage rejection $R_L = 4 \Omega$ $f_{\text{ripple}} = 100 \text{ Hz}$		50		dB
I_d	Drain current $P_O = 12 \text{ W}$ $R_L = 4 \Omega$ $P_O = 9 \text{ W}$ $R_L = 8 \Omega$		0.8 0.5		A A
T_{sd}	Thermal shut-down junction temperature		145		$^{\circ}\text{C}$
T_{sd}	(*) Thermal shut-down case temperature $P_{\text{tot}} = 10.5 \text{ W}$		120		$^{\circ}\text{C}$

(*) See fig. 14.

Fig. 1 - Output power vs. supply voltage

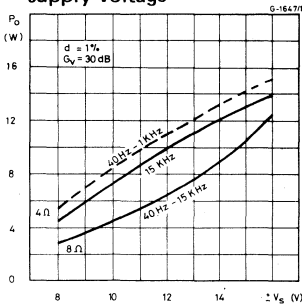


Fig. 2 - Output power vs. supply voltage

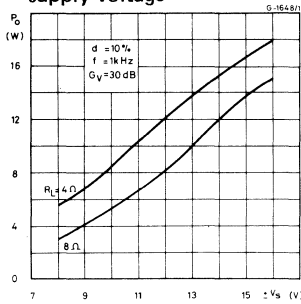


Fig. 3 - Distortion vs. output power

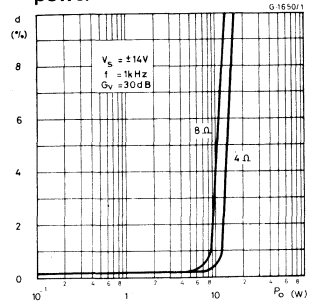


Fig. 4 - Distortion vs. output power ($R_L = 4 \Omega$)

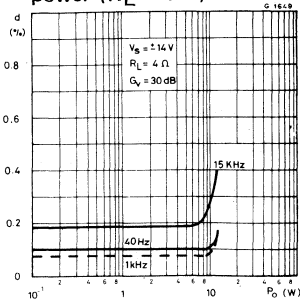


Fig. 5 - Distortion vs. output power ($R_L = 8 \Omega$)

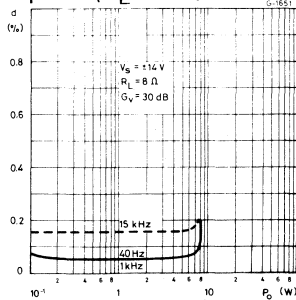


Fig. 6 - Distortion vs. frequency

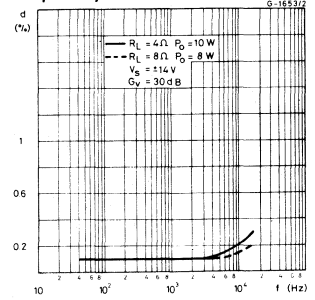


Fig. 7 - Output power vs. frequency

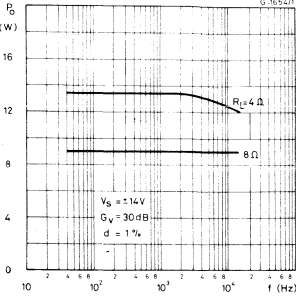


Fig. 8 - Sensitivity vs. output power ($R_L = 4 \Omega$)

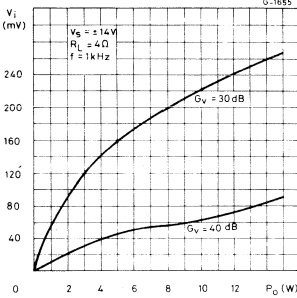


Fig. 9 - Sensitivity vs. output power ($R_L = 8 \Omega$)

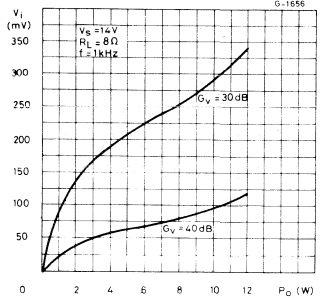


Fig. 10 - Open loop frequency response with different values of the rolloff capacitor C4

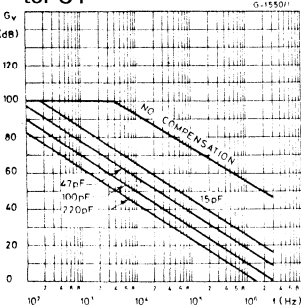


Fig. 11 - Value of C4 vs. voltage gain for different bandwidths

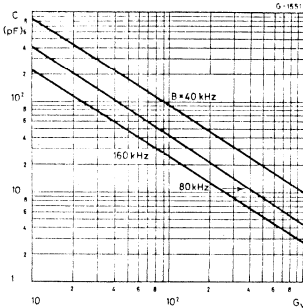


Fig. 12 - Quiescent current vs. supply voltage

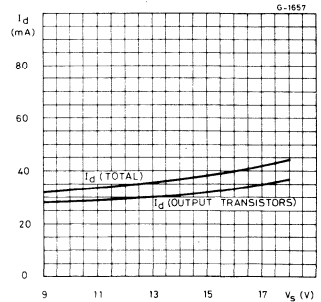


Fig. 13 - Supply voltage rejection vs. voltage gain

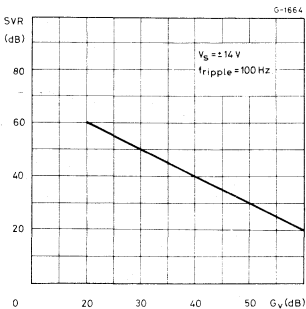


Fig. 14 - Power dissipation and efficiency vs. output power

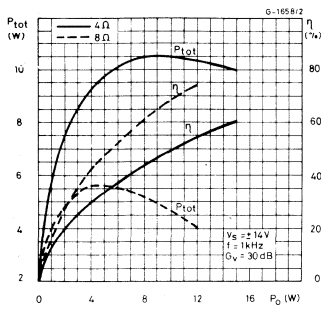
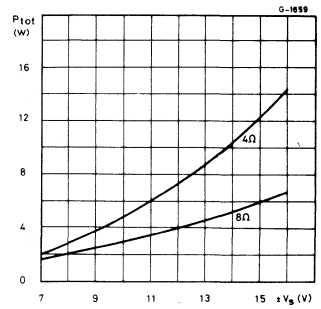


Fig. 15 - Maximum power dissipation vs. supply voltage (sine wave operation)



APPLICATION INFORMATION

Fig. 16 - Application circuit with split power supply

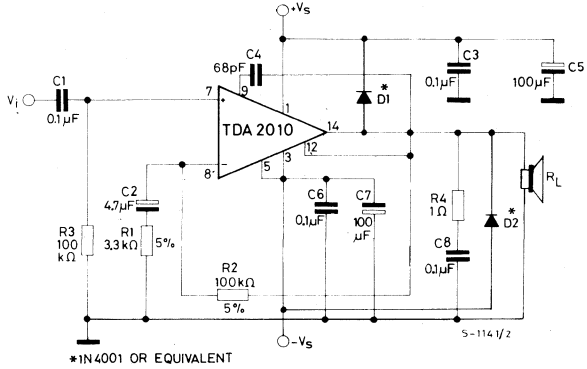
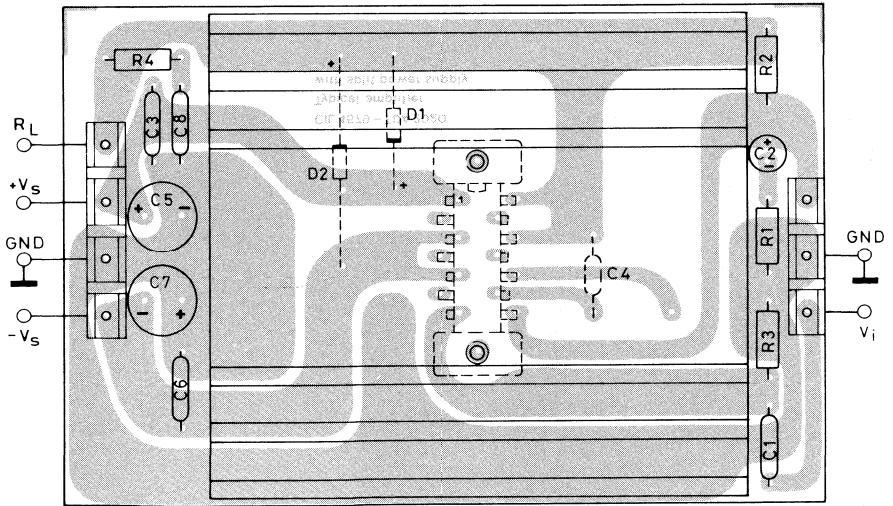


Fig. 17 - P.C. board and component layout for the circuit of fig. 17 (1:1 scale)



CS-0074

APPLICATION INFORMATION (continued)

Fig. 18 - 10W Hi-Fi stereo amplifier with preamplifier-equalizer for ceramic pick-ups

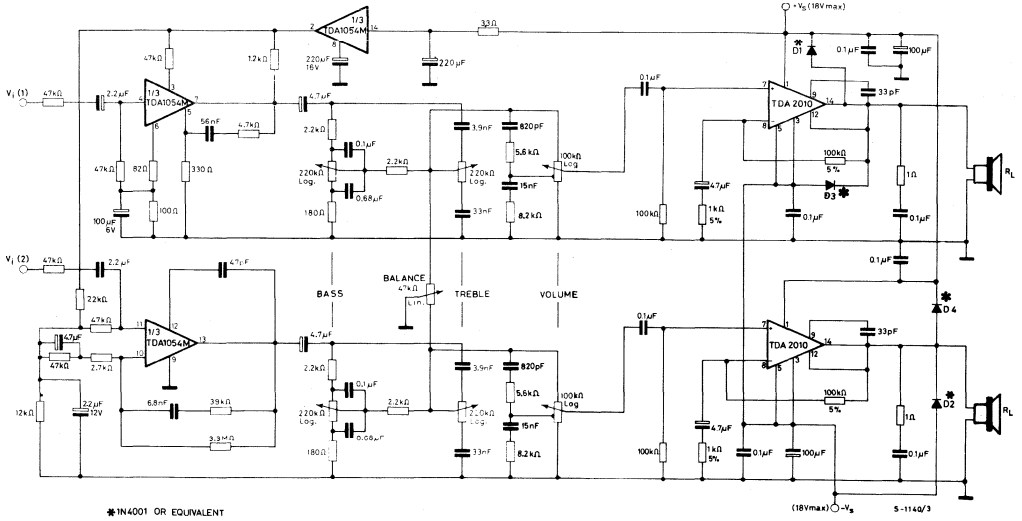
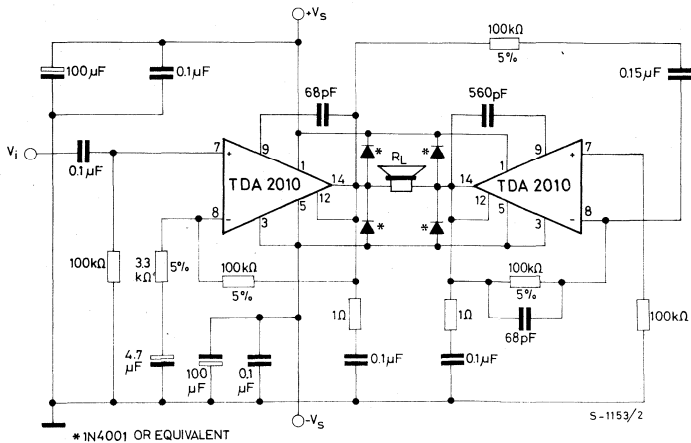


Fig. 19 - Bridge amplifier configuration with split power supply ($P_o = 24W$, $V_s = \pm 14V$, $R_L = 8 \Omega$, $d \leq 1\%$)



SHORT CIRCUIT PROTECTION

The most important innovation in the TDA 2010 is an original circuit which limits the current of the output transistors. Fig. 20 shows that the maximum output current is a function of the collector-emitter voltage; hence the output transistors work within their safe operating area (fig. 21). This function can therefore be considered as being peak power limiting rather than simple current limiting. The TDA 2010 is thus protected against temporary overloads or short circuit. Should the short circuit exist for a longer time, the thermal shut-down comes into action and keeps the junction temperature within safe limits.

Fig. 20 - Maximum output current vs. voltage (V_{CE}) across each output transistor

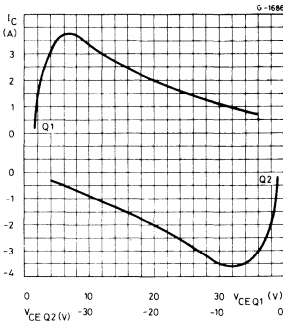
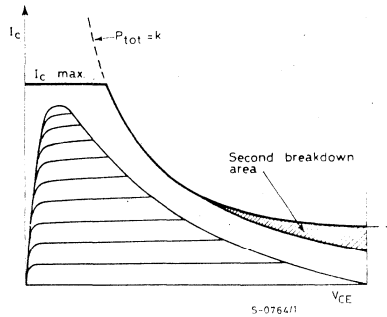


Fig. 21 - Safe operating area and collector characteristics of the protected power transistor.



THERMAL SHUT-DOWN

The presence of a thermal limiting circuit offers the following advantages:

- 1) an overload on the output (even if it is permanent), or an above-limit ambient temperature can be easily supported since the T_j cannot be higher than 150°C
- 2) the heatsink can have a smaller factor of safety compared with that of a conventional circuit. There is no possibility of device damage due to high junction temperature.

If, for any reason, the junction temperature increases up to 150°C , the thermal shut-down simply reduces the power dissipation and the current consumption.

Fig. 22 - Output power and drain current vs. case temperature ($R_L = 8 \Omega$)

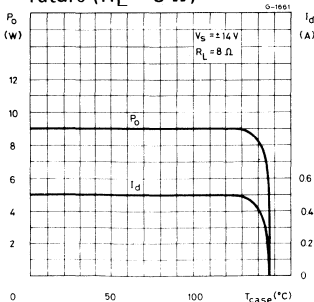
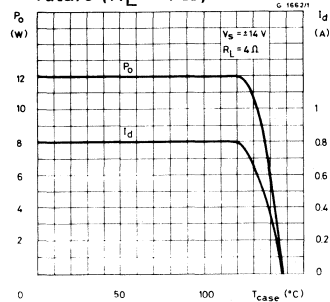


Fig. 23 - Output power and drain current vs. case temperature ($R_L = 4 \Omega$)



MOUNTING INSTRUCTIONS

The power dissipated in the circuit must be removed by adding an external heatsink as shown in figs. 24 and 25.

The system for attaching the heatsink is very simple: it uses a plastic spacer which is supplied with the device.

Thermal contact between the copper slug (of the package) and the heatsink is guaranteed by the pressure which the screws exert via the spacer and the printed circuit board; this is due to the particular shape of the spacer.

Note: The most negative supply voltage is connected to the copper slug, hence to the heatsink (because it is in contact with the slug).

Fig. 24 - Mounting system of TDA 2010

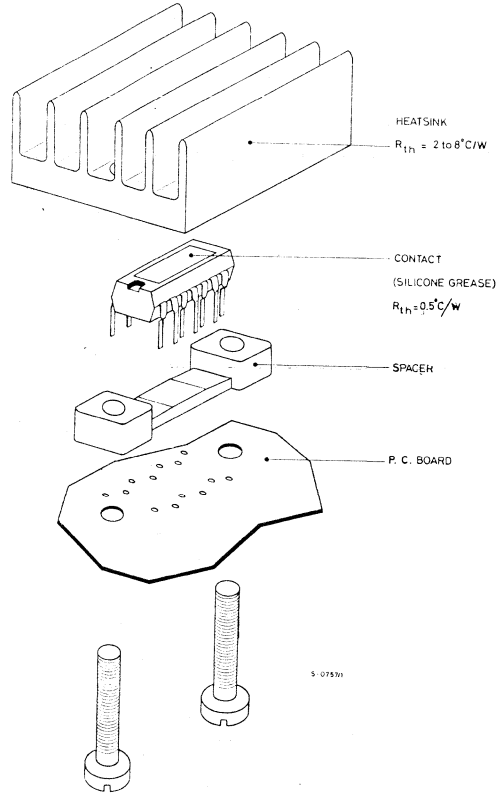
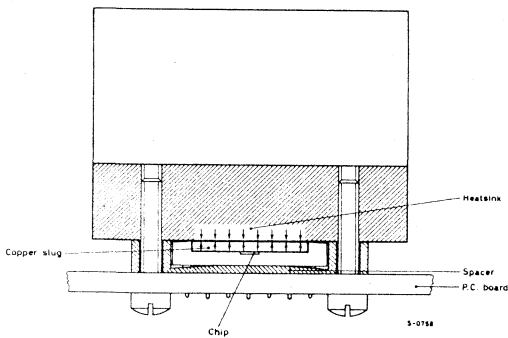


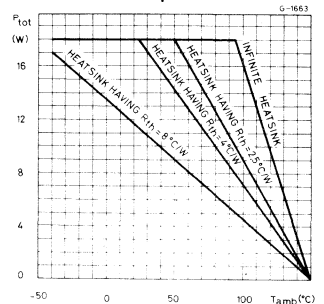
Fig. 25 - Cross-section of mounting system



The maximum allowable power dissipation depends upon the size of the external heatsink (i.e. its thermal resistance); fig. 26 shows this dissippable power as a function of ambient temperature for different thermal resistance.

For a more detailed description of the TDA 2010 and related performance refer to SGS-ATES Application Note n. 130.

Fig. 26 - Maximum allowable power dissipation vs. ambient temperature



TDA 2020

LINEAR INTEGRATED CIRCUIT

20W Hi-Fi AUDIO POWER AMPLIFIER WITH SHORT CIRCUIT PROTECTION AND THERMAL SHUT-DOWN

The TDA 2020 is a monolithic integrated **operational amplifier** in a 14-lead quad in-line plastic package, intended for use as a low frequency class B power amplifier. Typically it provides 20W output power ($d = 1\%$) at $\pm 18V/4\Omega$; the guaranteed output power at $\pm 17V/4\Omega$ is 15W (DIN norm 45500). The TDA 2020 provides high output current (up to 3.5 A) and has very low harmonic and cross-over distortion. Further, the device incorporates an original (and patented) short circuit protection system, comprising an arrangement for automatically limiting the dissipated power so as to keep to working point of the output transistors within their safe operating area. A conventional thermal shut-down system is also included.

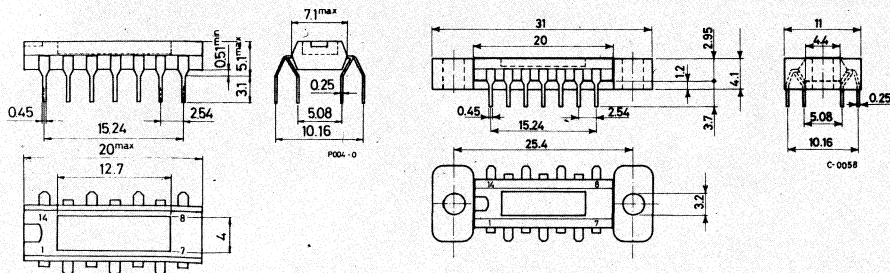
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	± 22	V
V_i	Input voltage	V_s	
V_i	Differential input voltage	± 15	V
I_o	Output peak current (internally limited)	3.5	A
P_{tot}	Power dissipation at $T_{case} \leq 75^\circ C$	25	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ C$

ORDERING NUMBERS: TDA 2020 A82 dual in-line plastic package
 TDA 2020 A92 quad in-line plastic package
 TDA 2020 AC2 dual in-line plastic package with spacer
 TDA 2020 AD2 quad in-line plastic package with spacer

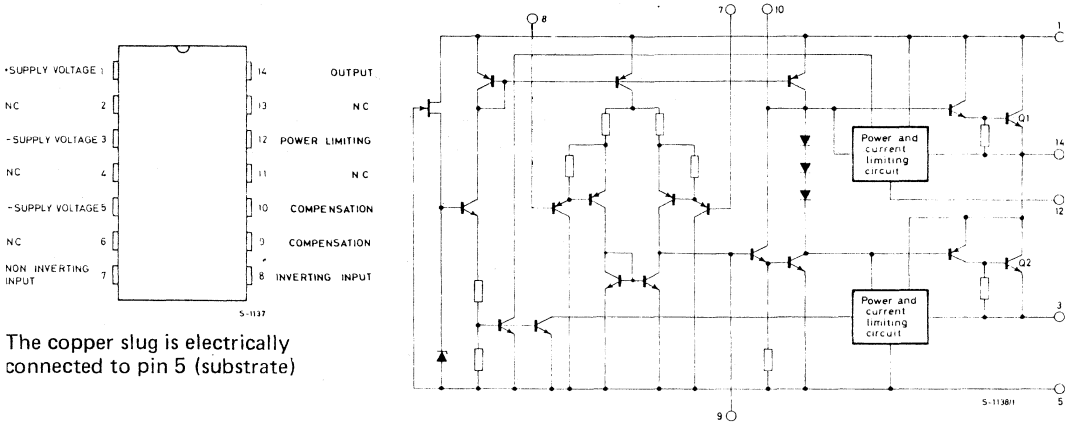
MECHANICAL DATA

Dimensions in mm



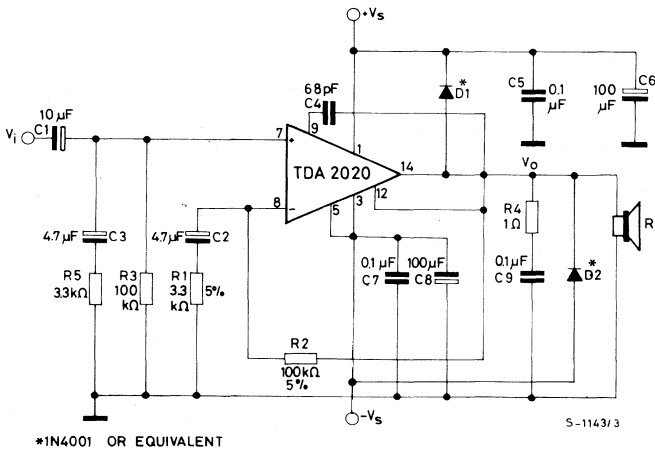
TDA 2020

CONNECTION AND SCHEMATIC DIAGRAMS (top view)



The copper slug is electrically connected to pin 5 (substrate)

TEST CIRCUIT



THERMAL DATA

$R_{th\ j-case}$	Thermal resistance junction-case	max	3	$^{\circ}\text{C/W}$
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TDA 2020

ELECTRICAL CHARACTERISTICS

(Refer to the test circuit, $V_s = \pm 17V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	
V_s	Supply voltage	± 5		± 22	V	
I_d	Quiescent drain current	$V_s = \pm 22 V$	60		mA	
I_b	Input bias current		0.15		μA	
V_{os}	Input offset voltage		5		mV	
I_{os}	Input offset current		0.05		μA	
V_{os}	Output offset voltage		10	100	mV	
P_o	Output power	$d = 1\%$ $G_v = 30 \text{ dB}$ $T_{case} \leq 70^\circ C$ $f = 40 \text{ to } 15\,000 \text{ Hz}$	15	18.5		W
		$V_s = \pm 17V$ $R_L = 4 \Omega$ $V_s = \pm 18V$ $R_L = 4 \Omega$ $V_s = \pm 18V$ $R_L = 8 \Omega$		20		W
$d = 10\%$ $G_v = 30 \text{ dB}$ $T_{case} \leq 70^\circ C$ $f = 1 \text{ kHz}$	16.5	W				
P_o	Output power	$d = 10\%$ $G_v = 30 \text{ dB}$ $T_{case} \leq 70^\circ C$ $f = 1 \text{ kHz}$		24		W
		$V_s = \pm 17V$ $R_L = 4 \Omega$ $V_s = \pm 18V$ $R_L = 8 \Omega$		20		W
V_i	Input sensitivity	$G_v = 30 \text{ dB}$ $f = 1 \text{ kHz}$ $P_o = 15 \text{ W}$		260 380	mV mV	
B	Frequency response (-3 dB)	$R_L = 4 \Omega$ $C_4 = 68 \text{ pF}$	10 to 160 000			Hz
d	Distortion	$P_o = 150 \text{ mW to } 15W$ $R_L = 4 \Omega$ $G_v = 30 \text{ dB}$ $T_{case} \leq 70^\circ C$ $f = 1 \text{ kHz}$ $f = 40 \text{ to } 15\,000 \text{ Hz}$		0.2 0.3	1	% %
		$P_o = 150 \text{ mW to } 15W$ $V_s = \pm 18V$ $R_L = 8 \Omega$ $G_v = 30 \text{ dB}$ $T_{case} \leq 70^\circ C$ $f = 1 \text{ kHz}$ $f = 40 \text{ to } 15\,000 \text{ Hz}$		0.1 0.25		% %
R_i	Input resistance (pin 7)		5		M Ω	
G_v	Voltage gain (open loop)		100		dB	
G_v	Voltage gain (closed loop)	$R_L = 4 \Omega$ $f = 1 \text{ kHz}$	29.5	30	30.5	dB

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
e_N	Input noise voltage		4		μV
i_N	Input noise current		0.1		nA
SVR	Supply voltage rejection	$R_L = 4 \Omega$ $f_{ripple} = 100 \text{ Hz}$	$G_V = 30 \text{ dB}$	50	dB
I_d	Drain current	$P_O = 18.5 \text{ W}$ $R_L = 4 \Omega$		1	A
		$P_O = 16.5 \text{ W}$ $R_L = 8 \Omega$	$V_S = \pm 18 \text{ V}$	0.7	A
T_{sd}	Thermal shut-down junction temperature		140		$^{\circ}C$
T_{sd}	Thermal shut-down case temperature	$P_{tot} = 15.5 \text{ W}$	105		$^{\circ}C$

Fig. 1 - Output power vs. supply voltage

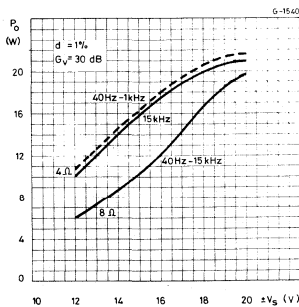


Fig. 2 - Output power vs. supply voltage

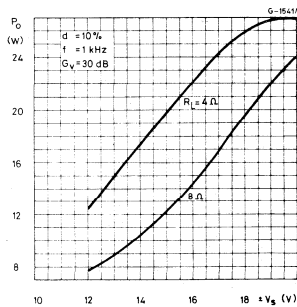


Fig. 3 - Distortion vs. output power

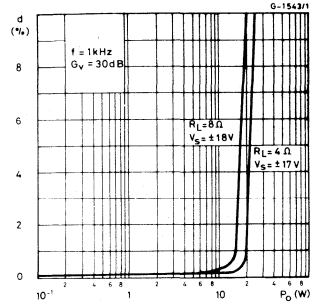


Fig. 4 - Distortion vs. output power ($R_L = 4 \Omega$)

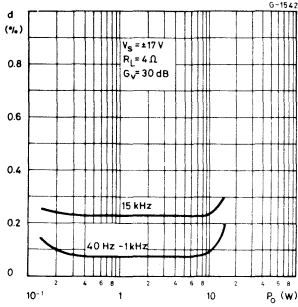


Fig. 5 - Distortion vs. output power ($R_L = 8 \Omega$)

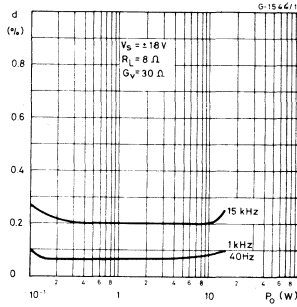


Fig. 6 - Distortion vs. frequency

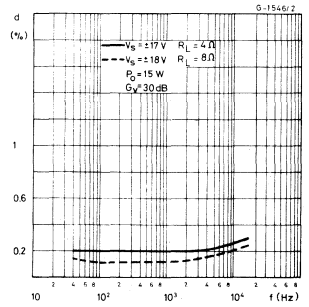


Fig. 7 - Output power vs. frequency

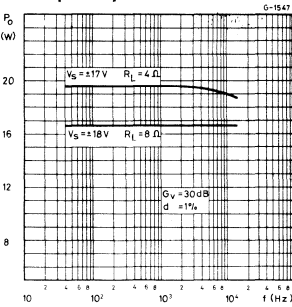


Fig. 8 - Sensitivity vs. output power ($R_L = 4 \Omega$)

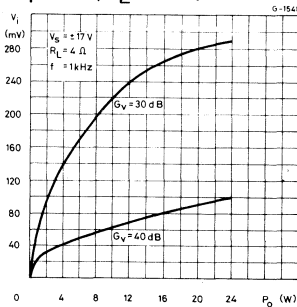


Fig. 9 - Sensitivity vs. output power ($R_L = 8 \Omega$)

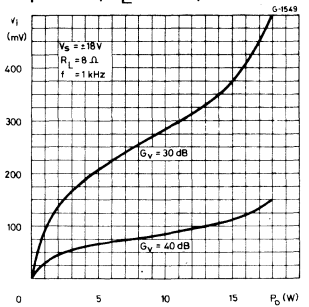


Fig. 10 - Open loop frequency response with different values of the rolloff capacitor C4

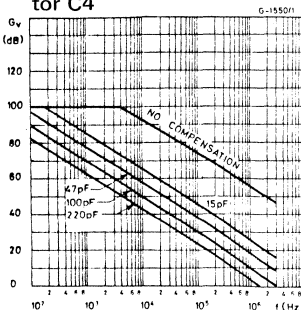


Fig. 11 - Value of C4 vs. voltage gain for different bandwidths

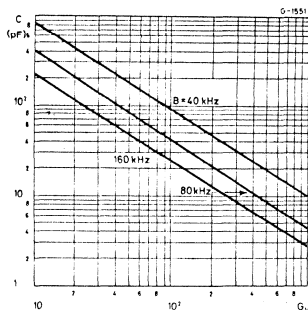


Fig. 12 - Quiescent current vs. supply voltage

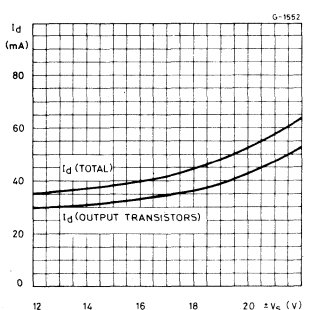


Fig. 13 - Supply voltage rejection vs. voltage gain

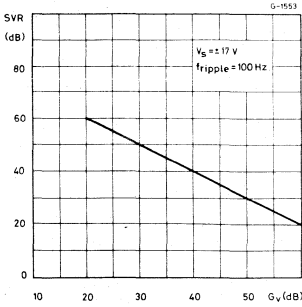


Fig. 14 - Power dissipation and efficiency vs. output power

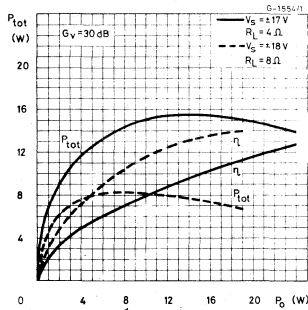
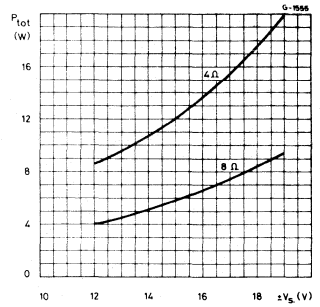
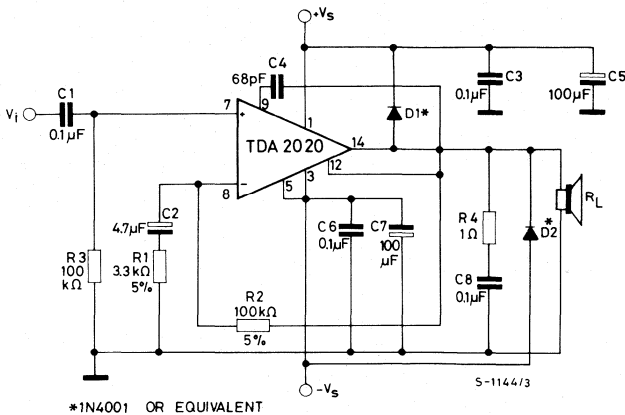


Fig. 15 - Maximum power dissipation vs. supply voltage (sine wave operation)



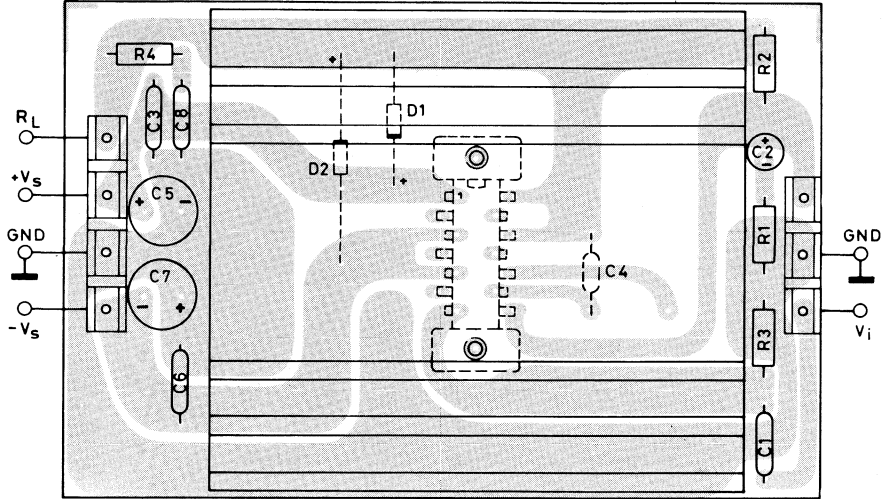
APPLICATION INFORMATION

Fig. 16 - Application circuit with split power supply



TDA 2020

Fig. 17 – P.C. Board and component layout for the circuit of fig. 16 (1:1 scale)



CS-0074

Fig. 18 – 15 W Hi-Fi stereo amplifier with preamplifier-equalizer for magnetic pick-ups

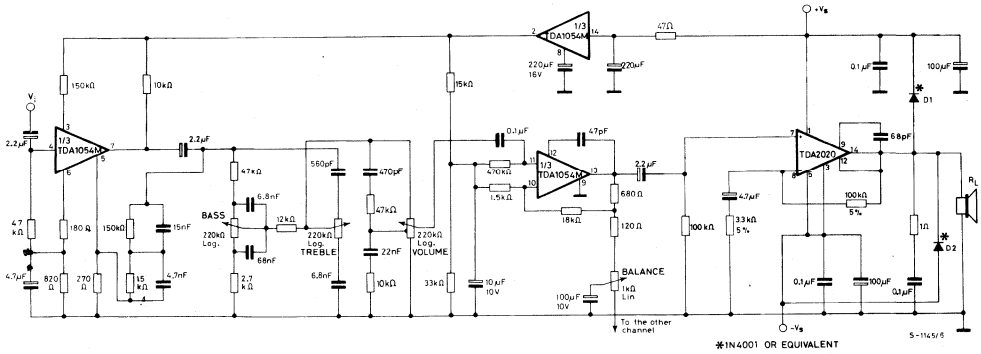


Fig. 19 – Stereo amplifier with split power supply

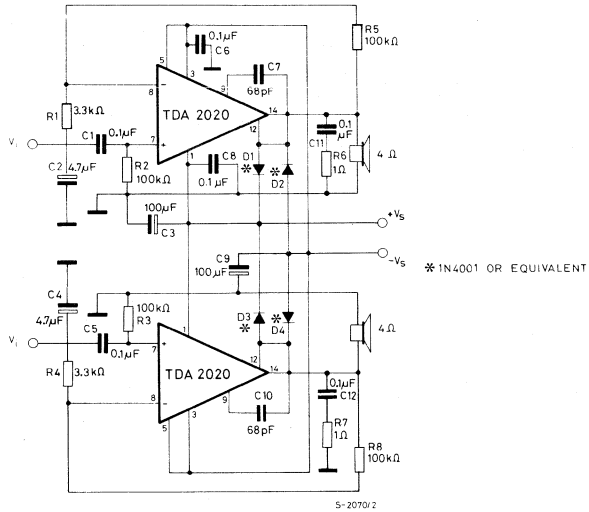
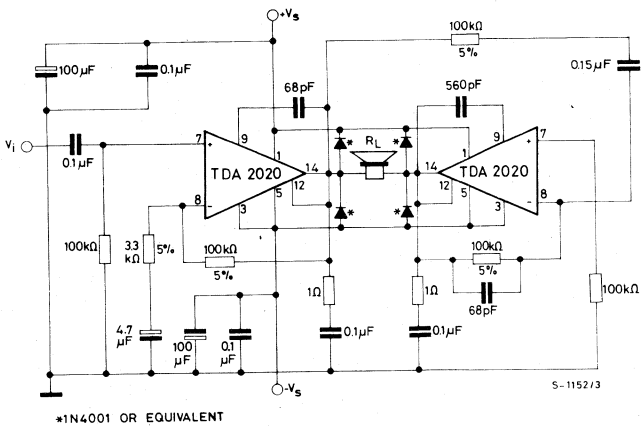


Fig. 20 – 30W bridge amplifier configuration with split power supply ($R_L = 8 \Omega$ $d \leq 1\%$; $V_s = \pm 17V$)



TDA 2020

SHORT CIRCUIT PROTECTION

The most important innovation in the TDA 2020 is an original circuit which limits the current of the output transistors. Fig. 21 shows that the maximum output current is a function of the collector-emitter voltage; hence the output transistors work within their safe operating area (fig. 22). This function can therefore be considered as being peak power limiting rather than simple current limiting. The TDA 2020 is thus protected against temporary overloads or short circuit. Should the short circuit exist for a longer time, the thermal shut-down comes into action and keeps the junction temperature within safe limits.

Fig. 21 - Maximum output current vs. voltage (V_{CE}) across each output transistor

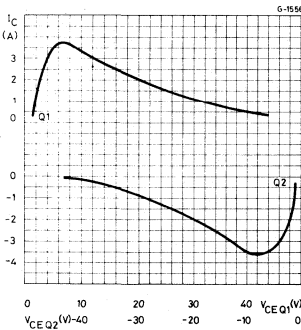
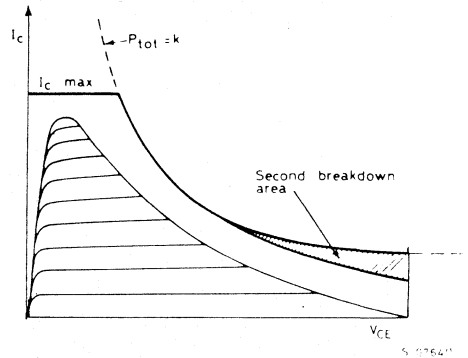


Fig. 22 - Safe operating area and collector characteristics of the protected power transistor



THERMAL SHUT-DOWN

The presence of a thermal limiting circuit offers the following advantages:

- 1) an overload on the output (even if it is permanent), or an above-limit ambient temperature can be easily supported since the T_j cannot be higher than 150°C
- 2) the heatsink can have a smaller factor of safety compared with that of a conventional circuit. There is no possibility of device damage due to high junction temperature.

If, for any reason, the junction temperature increases up to 150°C , the thermal shut-down simply reduces the power dissipation and the current consumption.

Fig. 23 - Output power and drain current vs. case temperature ($R_L = 8 \Omega$)

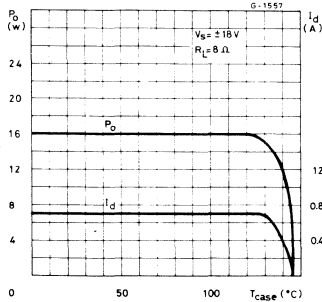
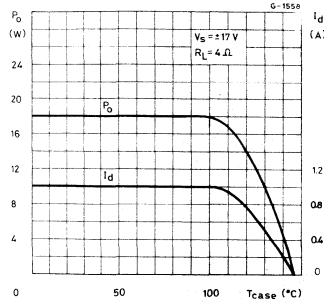


Fig. 24 - Output power and drain current vs. case temperature ($R_L = 4 \Omega$)



MOUNTING INSTRUCTIONS

The power dissipated in the circuit must be removed by adding an external heatsink as shown in figs. 25 and 26.

The system for attaching the heatsink is very simple: it uses a plastic spacer which is supplied with the device.

Thermal contact between the copper slug (of the package) and the heatsink is guaranteed by the pressure which the screws exert via the spacer and the printed circuit board; this is due to the particular shape of the spacer.

Note: the most negative supply voltage is connected to the copper slug, hence to the heatsink (because it is in contact with the slug).

Fig. 25 - Mounting system of TDA 2020

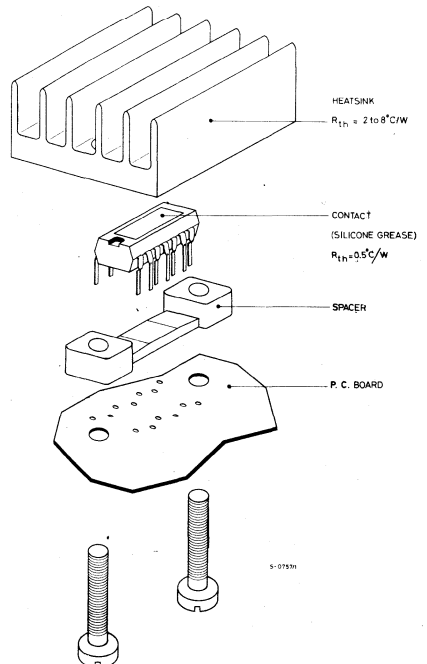
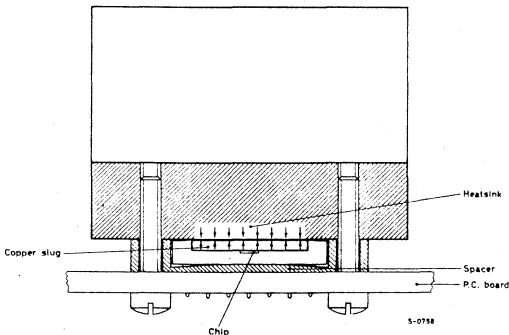


Fig. 26 - Cross-section of mounting system

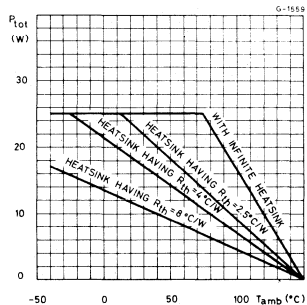


TDA 2020

MOUNTING INSTRUCTION (continued)

The maximum allowable power dissipation depends upon the size of the external heatsink (i.e. its thermal resistance); fig. 27 shows this dissipable power as a function of ambient temperature for different thermal resistance.

Fig. 27 - Maximum allowable power dissipation vs. ambient temperature



For a more detailed description of the TDA 2020 and related performance refer to SGS-ATES Application Note. n. 130.

LINEAR INTEGRATED CIRCUIT

Hi-Fi AUDIO DRIVER AMPLIFIER WITH SHORT CIRCUIT PROTECTION AND THERMAL SHUT-DOWN

- HIGH SUPPLY VOLTAGE: $\pm 25V$
- HIGH SUPPLY REJECTION: 80 dB
- PROGRAMMABLE SOA PROTECTION
- LOW DISTORTION (0.05% TYP.)
- LOW INPUT NOISE VOLTAGE ($4 \mu V$ TYP.)

The TDA 2020D is a monolithic integrated **operational amplifier** in a 14 lead quad in-line plastic package, intended for driving external power transistors in Hi-Fi amplifier (30 to 100W). This device incorporates an original (and patented) short circuit protection system, comprising an arrangement for automatically limiting the dissipated power so as to keep the working point of the external transistors within their safe operating area. A thermal shut-down system is also included. This thermal shut-down can also protect the external power transistors.

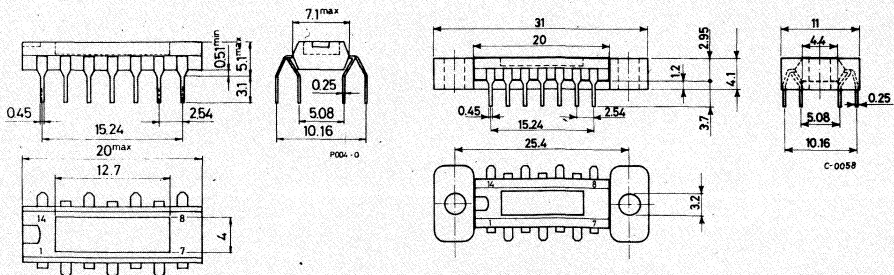
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	± 25	V
V_i	Input voltage	V_s	
V_i	Differential input voltage	± 15	V
I_o	Output peak current	1	A
P_{tot}	Power dissipation at $T_{case} \leq 75^\circ C$	25	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ C$

ORDERING NUMBERS: TDA 2020D A82 dual in-line plastic package
 TDA 2020D A92 quad in-line plastic package
 TDA 2020D AC2 dual in-line plastic package with spacer
 TDA 2020D AD2 quad in-line plastic package with spacer

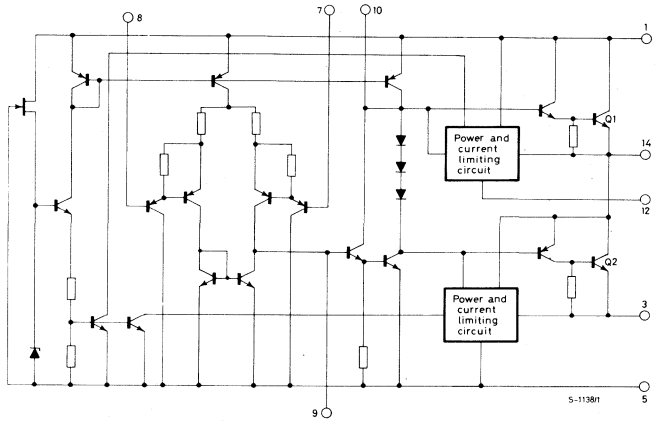
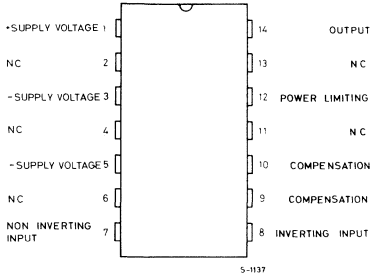
MECHANICAL DATA

Dimensions in mm



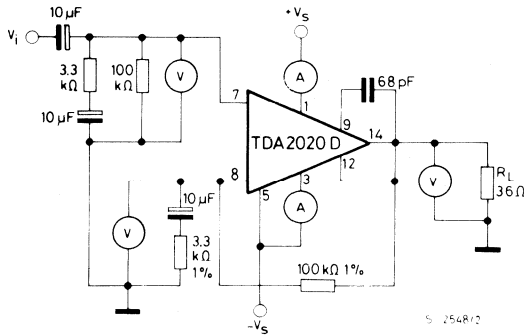
TDA 2020D

CONNECTION AND SCHEMATIC DIAGRAMS (top view)



The copper slug is electrically connected to pin 5 (substrate)

TEST CIRCUIT



THERMAL DATA

$R_{th j-case}$	Thermal resistance junction-case	max	3	$^{\circ}C/W$
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ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $V_s = \pm 20V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s	Supply voltage	± 5		± 25	V
I_d	Quiescent drain current	$V_s = \pm 25V$	40	80	mA
I_b	Input bias current		0.15		μA
V_{os}	Input offset voltage		5		mV
I_{os}	Input offset current		0.05		μA
V_{os}	Output offset voltage		10	100	mV
$V_{CE(sat)}$	Output saturation voltage	$I_o = 0.5A$	± 1.7	± 2	V
B	Frequency response (-3 dB)	$I_o = 0.5A$	10 to 160 000		Hz
d	Distortion	$G_v = 30\text{ dB}$ $f = 1\text{ kHz}$ $f = 40\text{ to }15\text{ 000 Hz}$	0.05 0.2	0.3	% %
	Intermodulation	DIN 45500	0.2		%
R_i	Input resistance (pin 7)		5		$M\Omega$
G_v	Voltage gain (open loop)	$f = 1\text{ kHz}$	100		dB
G_v	Voltage gain (closed loop)		29.5	30	30.5
e_N	Input noise voltage	B (-3 dB) = 10 to 20 000 Hz	4		μV
i_N	Input noise current		0.1		nA
SVR	Supply voltage rejection	$f_{ripple} = 100\text{ Hz}$ $G_v = 30\text{ dB}$	35	50	dB
I_d	Drain current	$P_o = 4.5W$ $P_o = 2W$	$R_L = 36\Omega$ $R_L = 36\Omega$	160 100	mA mA
T_{sd}	Thermal shut-down junction temperature		145		$^\circ C$
T_{sd}	Thermal shut-down case temperature	$P_{tot} = 5W$	135		$^\circ C$

TDA 2020D

Fig. 1 - Quiescent current vs. supply voltage

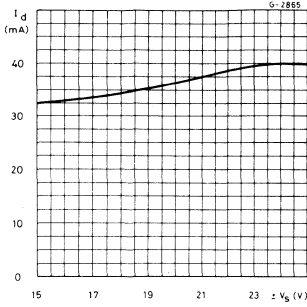


Fig. 2 - Output current vs. $V_{CE(sat)}$

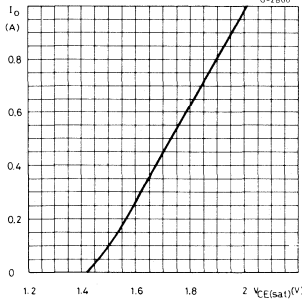


Fig. 3 - Power dissipation vs. supply voltage

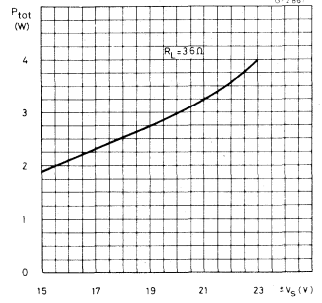


Fig. 4 - Open loop frequency response with different values of the rolloff capacitor

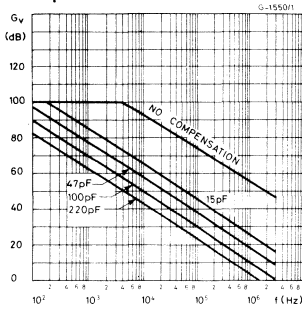


Fig. 5 - Value of rolloff capacitor vs. voltage gain for different bandwidths

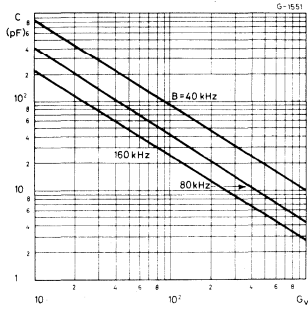


Fig. 6 - Supply voltage rejection vs. voltage gain

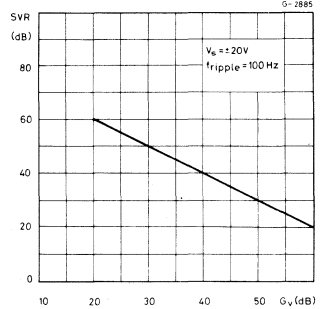


Fig. 7 - Transient response

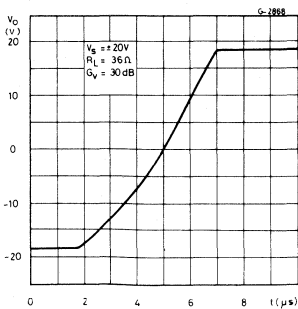
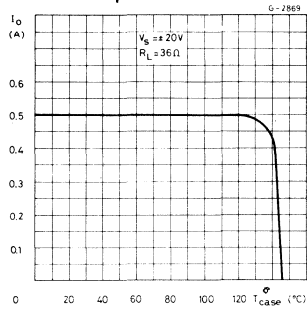
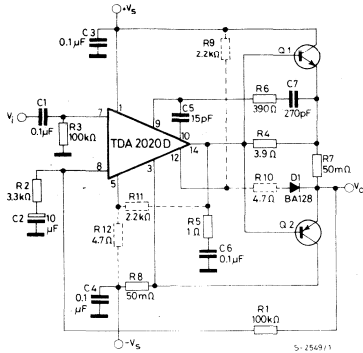


Fig. 8 - Output current vs. case temperature



APPLICATION INFORMATION

Fig. 9 - Application circuit for $P_o = 30$ to 50W



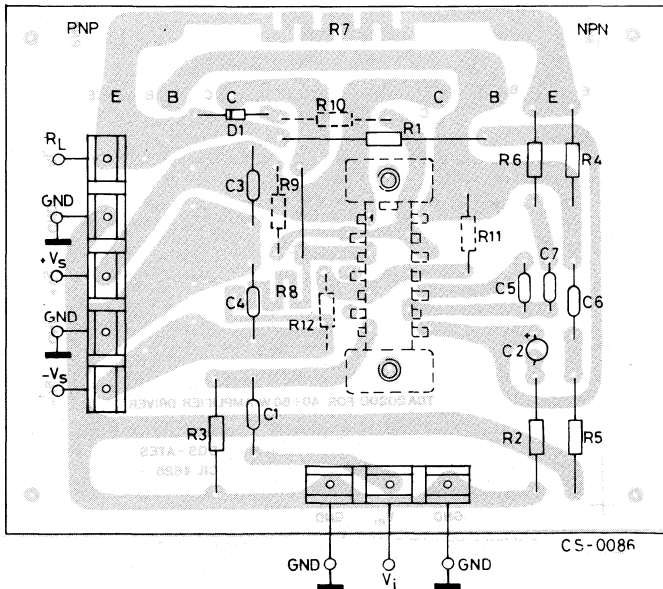
Note:

Resistors R9, R10, R11 and R12 are optional. Their purpose is to change the allowable operating area of the output transistors (see fig. 23).

The designer can choose different values according to working conditions (V_s , R_L) and to the SOA of the external transistors. When these resistors are not used the application circuit is modified as follows:

- a) R7, R8 are changed to 25 mΩ.
- b) R10, R12 are substituted by a short circuit.

Fig. 10 - P.C. board and component layout for the circuit of fig. 9 (1:1 scale)



P_o $R_L = 4\Omega$	30W	40W
$\pm V_s$	18V	20V
R9/R11	—	2.2 kΩ
R10/R12	4.7Ω	4.7Ω
Q1	BD707 or BDW21A	BD907 or BDW21A
Q2	BD708 or BDW22A	BD908 or BDW22A

Note:

If resistors R9, R10, R11 and R12 are not used, R7 and R8 must be 25 mΩ. The following table shows what length of wire (copper and constantan) is required to obtain a resistor of 25 mΩ for different values of ϕ .

ϕ (mm)	1	0.8	0.7	0.5	0.4	0.3
l (mm) copper	—	—	570	290	180	100
l (mm) constantan	40	25	20	10	6.5	—

TDA 2020D

Application suggestions

The recommended values of the components are those shown in application circuit of fig. 9, although different values can be used. The following table may help the amplifier designers.

Component	Recomm. value	Purpose	Larger than recommended value	Smaller than recommended value
C1	0.1 μ F	Elimination of DC current on volume control	Reduced lower cutoff frequency	Increased lower cutoff frequency
C2	10 μ F	To obtain DC gain equal to 1	Reduced lower cutoff frequency	Increased lower cutoff frequency
C3 and C4	0.1 μ F	Frequency stabilization		Danger of oscillations
C5	15 pF	Upper frequency cutoff	Reduced upper cutoff frequency	Increased upper cutoff frequency
C6	0.1 μ F	Frequency stabilization		Danger of oscillation
C7	270 pF	Compensation		Danger of oscillations
R1	100 k Ω	Closed loop gain determination	Larger closed loop gain	Smaller closed loop gain
R2	3.3 k Ω	Closed loop gain determination	Smaller closed loop gain	Larger closed loop gain
R3	R1	Input bias	Output DC offset variation	Output DC offset variation
R4	3.9 Ω	External power transistor driving	Danger of distortion	Increased load for the driver
R5	1 Ω	Frequency stabilization	Danger of oscillations	Danger of oscillations
R6	390 Ω	Compensation		
R7 and R8	50 m Ω	Current protection sensing	Reduced maximum output current value	Increased maximum output current value
R9, R10, R11, R12	see Fig. 23			
Q1 - Q2	BD 707 - BD 708 or BD 907 - BD 908 or BDW 21A - BDW 22A			
D1	BA 128	Short circuit prot.		

Fig. 11 – Output power vs. supply voltage

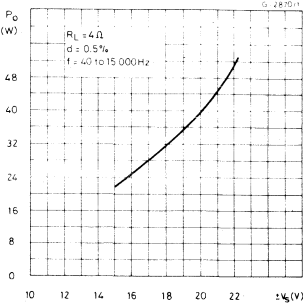


Fig. 12 – Output power vs. supply voltage

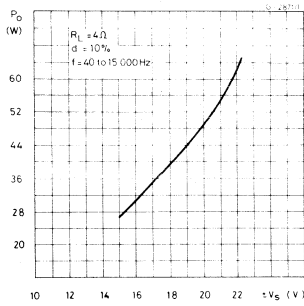


Fig. 13 – Distortion vs. output power

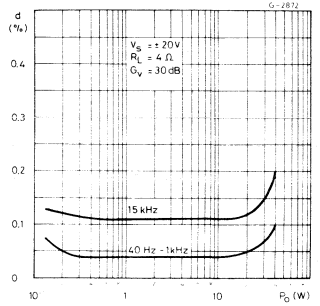


Fig. 14 – Distortion vs. output power

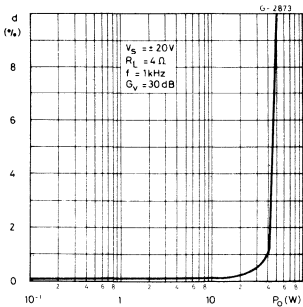


Fig. 15 – Distortion vs. frequency

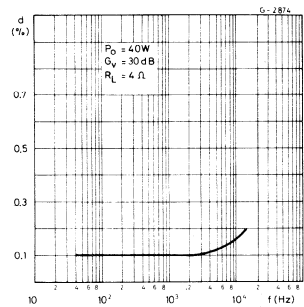


Fig. 16 – Input sensitivity vs. output power

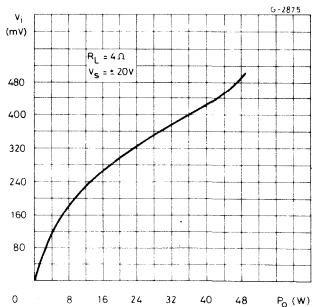


Fig. 17 – Maximum power dissipation vs. supply voltage (sine wave operation)

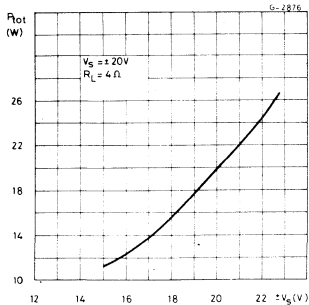
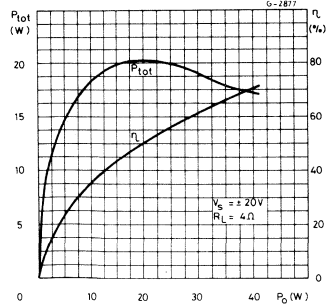
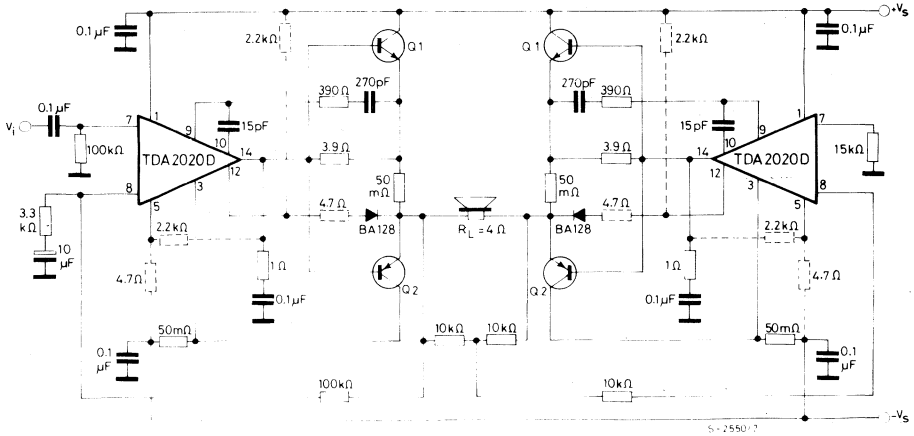


Fig. 18 – Power dissipation and efficiency vs. output power



TDA 2020D

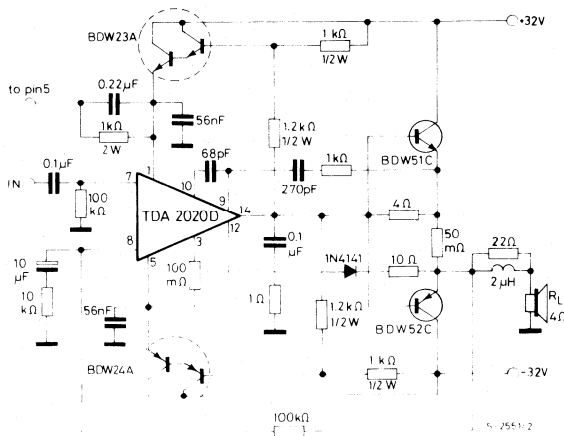
Fig. 19 - 60W to 100W bridge configuration application circuit



Note: With a bridge configuration the output power is increased while the other performances are the same as that of the application in fig. 9. The table shows the output power that can be obtained using different power transistor pairs.

- | | | |
|---|---|---|
| A | { | Q1 = BDW21A |
| | | Q2 = BDW22A; $V_s = \pm 15V$; $R_L = 4\Omega \cdot 60W$ |
| B | { | Q1 = BD707 |
| | | Q2 = BD708; $V_s = \pm 20V$; $R_L = 8\Omega \cdot 80W$ |
| C | { | Q1 = BDW51A |
| | | Q2 = BDW52A; $V_s = \pm 18V$; $R_L = 4\Omega \cdot 100W$ |

Fig. 20 - 80W Hi-Fi amplifier



For this application the maximum value of V_s in no-load condition is $\pm 45V$.

Application suggestions for circuit in fig. 20

Using the two circuits shown in fig. 21 and fig. 22 it is possible to use a transformer with a large spread of output voltage between load and no-load condition.

The voltage on pins 1 and 5 follows V_o according to the equations:

$$V_1 = V_o + (V_s - V_o) \cdot \frac{R_2}{R_1 + R_2} - 2 V_{BE}$$

$$V_5 = V_o - (V_s + V_o) \cdot \frac{R_2}{R_1 + R_2} + 2 V_{BE}$$

while the voltage between pins 1 and 5 is a constant. In fact:

$$V_{1-5} = V_1 - V_5 = V_s \cdot \frac{2 R_2}{R_1 + R_2} - 4 V_{BE}$$

V_{1-5} must not exceed 50V and then the maximum value of V_s in no-load condition will be:

$$V_{s \max} = (50 + 4 V_{BE}) \cdot \frac{R_1 + R_2}{2 R_2}$$

The minimum value of V_s depends on the output power requested and will be:

$$V_{s(\min)} = V_L + V_{CE(\text{sat})} \text{ with } V_L = \sqrt{2 P_o R_L}$$

Resistance R_2 must be greater than R_1 to guarantee a positive voltage on pin 1 and a negative voltage on pin 5 for correct working of TDA 2020D.

Note 1 — Between pins 1 and 5 a ceramic capacitor must be inserted to guarantee good stability.

Note 2 — It is possible to insert an electrolytic capacitor (10 μF) between pin 1 and GND and between pin 5 and GND, but in this case the maximum output voltage must be $V_{\text{peak}} = 23\text{V}$.

With the circuit in fig. 22 the voltage at pins 1 and 5 is kept constant by two zener diodes. In load conditions a current equal to $I_o = I/\beta$ flows in R ; the value of R is then given by $R = \frac{(V_{CE} - V_{BE})}{I} \beta$. In no-load condition, if ΔV is the increase in the supply voltage, the zener diodes dissipate a power depending on ΔV and β according to the equation:

$$P_z = V_z \cdot I_z = V_z \cdot \frac{\Delta V}{R} = V_z \cdot \frac{\Delta V \cdot I}{\beta (V_{CE} - V_{BE})}$$

Fig. 21

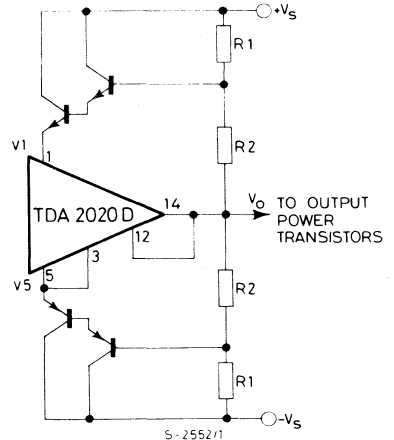
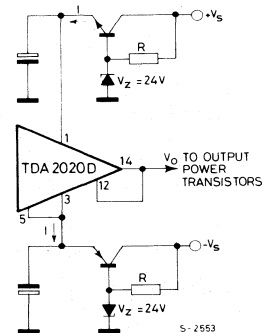


Fig. 22



SHORT CIRCUIT PROTECTION

The most important innovation in the TDA 2020D is an original circuit which limits the current of the output transistors. Fig. 23 shows that the maximum output current is a function of the collector-emitter voltage; hence the output transistors work within their safe operating area (fig. 24). This function can therefore be considered as being peak power limiting rather than simple current limiting. By choosing the appropriate values for R9, R10, R11, R12, (fig. 9) the maximum output current can be established as a function of the SOA of the output parameters being used.

Fig. 23 - Maximum output current vs. voltage [$V_{CE(sat)}$] across one output transistor, for different values of R10 (typical application circuit)

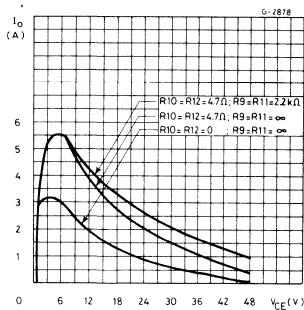
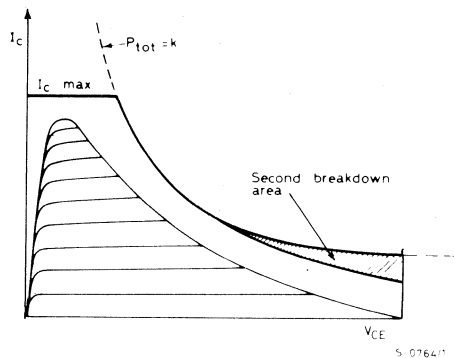


Fig. 24 - Safe operating area and collector characteristics of the protected power transistor



THERMAL SHUT-DOWN

The presence of a thermal limiting circuit offers the following advantages:

- 1) An overload on the output (even if it is permanent) or an above-limit ambient temperature can be easily withstood since the T_j cannot be higher than 150°C .
- 2) The heatsink can have a smaller safety factor than a conventional circuit. There is no possibility of device damage due to high junction temperature.

If, for any reason, the junction temperature increases up to 150°C , the thermal shut-down simply reduces the power dissipation and the current consumption. The thermal protection unit of the TDA 2020D will also provide thermal protection of the output transistors if they are mounted on the same heatsink as the I.C.

MOUNTING INSTRUCTIONS

Fig. 25 - Mounting system of TDA 2020D

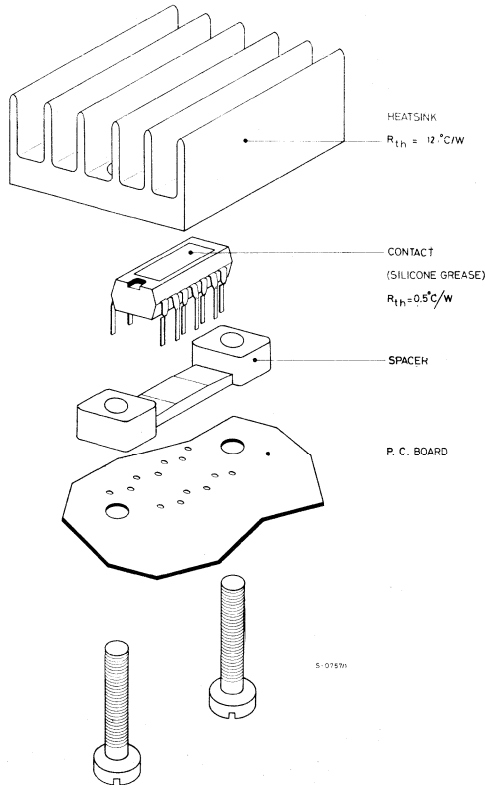
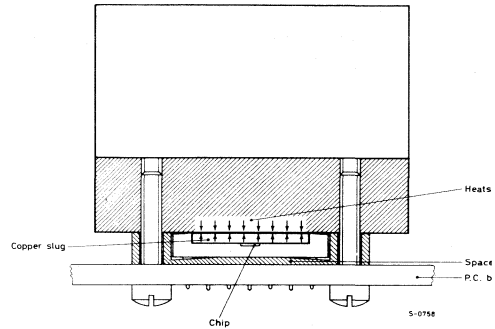


Fig. 26 - Cross-section of mounting system



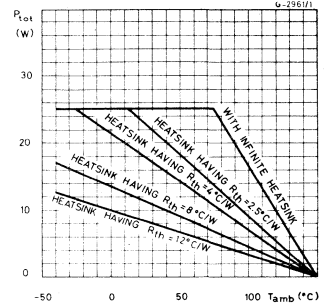
The power dissipated in the circuit must be removed by adding an external heatsink as shown in figs. 25 and 26.

The system for attaching the heatsink is very simple: it uses a plastic spacer which is supplied with the device.

Thermal contact between the copper slug (of the package) and the heatsink is guaranteed by the pressure which the screws exert via the spacer and the printed circuit board; this is due to the special shape of the spacer.

Note: The most negative supply voltage is connected to the copper slug, hence to the heatsink (because it is in contact with the slug).

Fig. 27 - Maximum allowable power dissipation vs. ambient temperature



TDA 2030

LINEAR INTEGRATED CIRCUIT

14W Hi-Fi AUDIO POWER AMPLIFIER WITH SHORT CIRCUIT PROTECTION AND THERMAL SHUT-DOWN

The TDA 2030 is a monolithic integrated circuit in Pentawatt[®] package, intended for use as a low frequency class AB amplifier. Typically it provides 14W output power ($d = 0.5\%$) at $\pm 14V/4\Omega$; at $\pm 14V$ the guaranteed output power is 12W on a 4Ω load and 8W on a 8Ω (DIN 45500). The TDA 2030 provides high output current and has very low harmonic and cross-over distortion. Further the device incorporates an original (and patented) short circuit protection system comprising an arrangement for automatically limiting the dissipated power so as to keep the working point of the output transistors within their safe operating area. A conventional thermal shut-down system is also included.

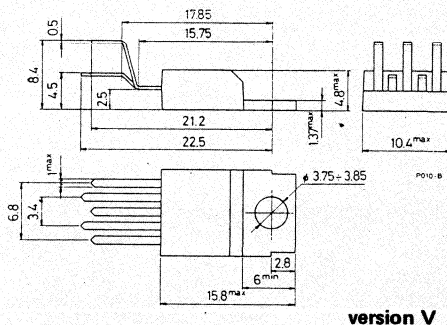
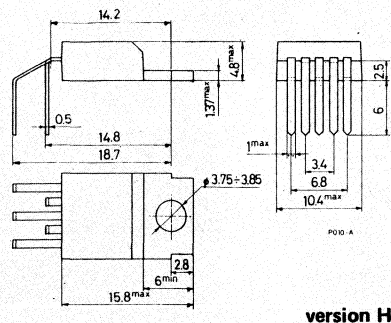
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	± 18	V
V_i	Input voltage	V_s	V
V_i	Differential input voltage	± 15	V
I_o	Output peak current (internally limited)	3.5	A
P_{tot}	Power dissipation at $T_{case} = 90^\circ C$	20	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ C$

ORDERING NUMBERS: TDA 2030 H; TDA 2030 V

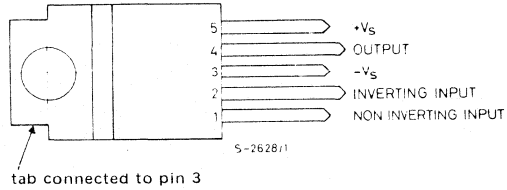
MECHANICAL DATA

Dimensions in mm

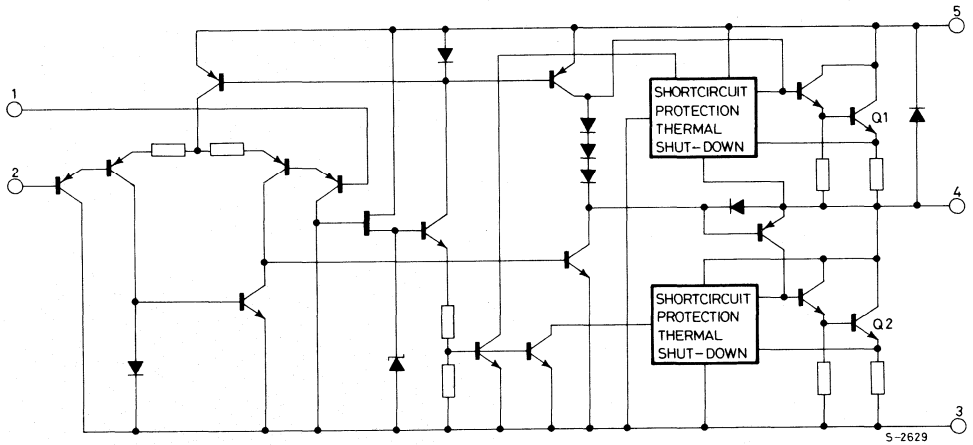


CONNECTION DIAGRAM

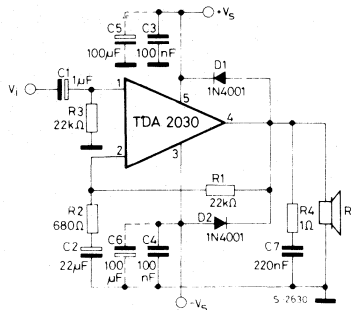
(top view)



SCHEMATIC DIAGRAM



TEST CIRCUIT



TDA 2030

THERMAL DATA

$R_{th\ j\text{-case}}$	Thermal resistance junction-case	max	3	$^{\circ}\text{C}/\text{W}$
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ELECTRICAL CHARACTERISTICS

(Refer to the test circuit; $V_s = \pm 14\text{V}$, $T_{amb} = 25^{\circ}\text{C}$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	
V_s	Supply voltage	± 6		± 18	V	
I_d	Quiescent drain current		40	60	mA	
I_b	Input bias current		0.2	2	μA	
V_{os}	Input offset voltage		± 2	± 20	mV	
I_{os}	Input offset current		± 20	± 200	nA	
V_{os}	Output offset voltage		± 2.5	± 22	mV	
P_o	Output power	$d = 0.5\%$ $f = 40$ to $15\ 000$ Hz $R_L = 4\ \Omega$ $R_L = 8\ \Omega$	$G_v = 30$ dB			
		$d = 10\%$ $f = 1$ kHz $R_L = 4\ \Omega$ $R_L = 8\ \Omega$	$G_v = 30$ dB			
d	Distortion	$P_o = 0.1$ to 12W $R_L = 4\ \Omega$ $f = 40$ to $15\ 000$ Hz	$G_v = 30$ dB			
		$P_o = 0.1$ to 8W $R_L = 8\ \Omega$ $f = 40$ to $15\ 000$ Hz	$G_v = 30$ dB			
V_i	Input sensitivity	$G_v = 30$ dB $P_o = 12\text{W}$ $P_o = 8\text{W}$	$f = 1$ kHz $R_L = 4\ \Omega$ $R_L = 8\ \Omega$			
					215 250	mV mV
B	Frequency response (-3 dB)	$G_v = 30$ dB $P_o = 12\text{W}$	$R_L = 4\ \Omega$			
				10 to 140 000	Hz	
R_i	Input resistance (pin 1)					
		0.5	5		M Ω	

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
G_V	Voltage gain (open loop)		90		dB
G_V	Voltage gain (closed loop)	$f = 1 \text{ kHz}$	30	30.5	dB
e_N	Input noise voltage	$B = 22 \text{ Hz to } 22 \text{ KHz}$	3	10	μV
i_N	Input noise current	$R_L = 4 \Omega$	80	200	pA
SVR	Supply voltage rejection	$R_L = 4 \Omega$ $G_V = 30 \text{ dB}$ $R_g = 22 \text{ k}\Omega$ $V_{\text{ripple}} = 0.5 \text{ V}_{\text{eff}}$ $f_{\text{ripple}} = 100 \text{ Hz}$	40	50	dB
I_d	Drain current	$P_O = 14 \text{ W}$ $R_L = 4 \Omega$ $P_O = 9 \text{ W}$ $R_L = 8 \Omega$	900 500		mA mA
T_{sd}	Thermal shut-down case temperature	$P_{\text{tot}} = 12 \text{ W}$	110		$^{\circ}\text{C}$

Fig. 1 - Output power vs. supply voltage

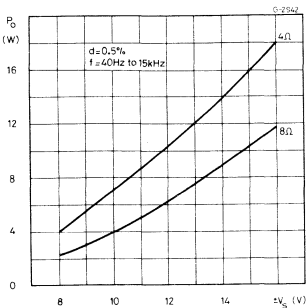


Fig. 2 - Output power vs. supply voltage

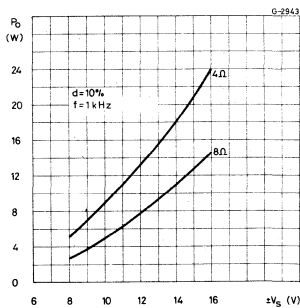


Fig. 3 - Distortion vs. output power

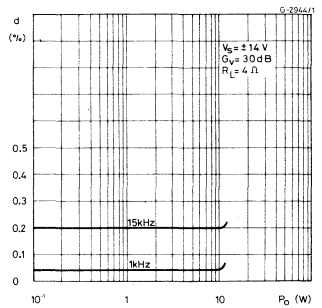


Fig. 4 - Distortion vs. output power

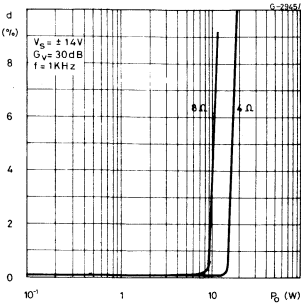


Fig. 5 - Distortion vs. output power

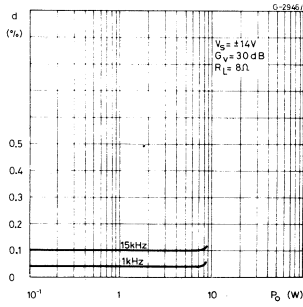


Fig. 6 - Distortion vs. frequency

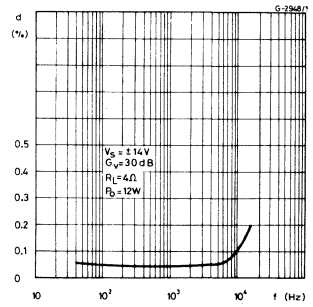


Fig. 7 - Distortion vs. frequency

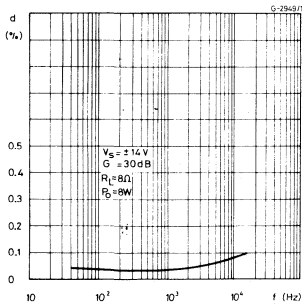


Fig. 8 - Sensitivity vs. output power

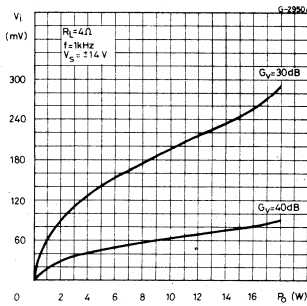


Fig. 9 - Sensitivity vs. output power

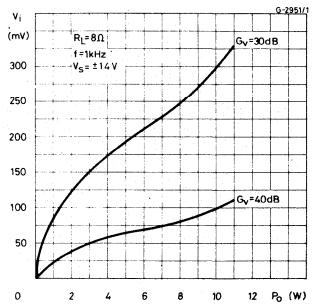


Fig. 10 - Frequency response with different values of the rolloff capacitor C8 (see fig. 16)

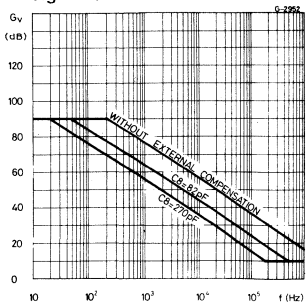


Fig. 11 - Value of C8 vs. voltage gain for different bandwidths (see fig. 16)

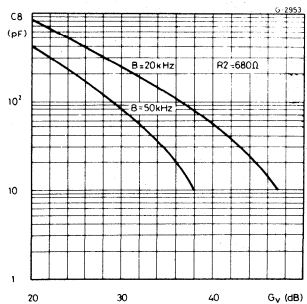


Fig. 12 - Quiescent current vs. supply voltage

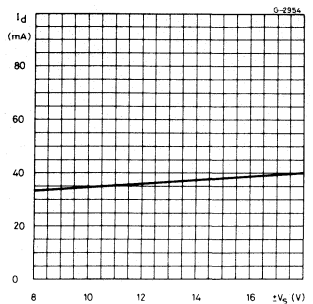


Fig. 13 - Supply voltage rejection vs. voltage gain

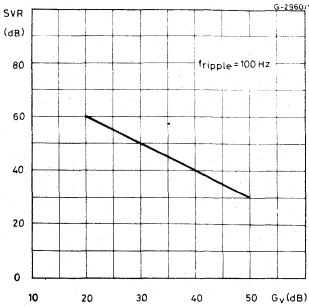


Fig. 14 - Power dissipation and efficiency vs. output power

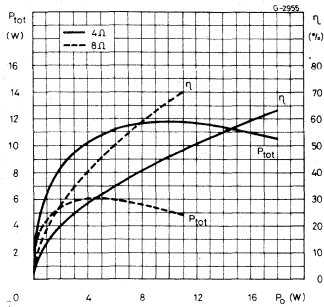
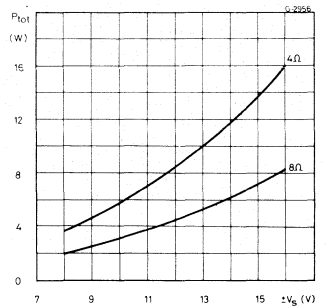


Fig. 15 - Maximum power dissipation vs. supply voltage (sine wave operation)



APPLICATION INFORMATION

Fig. 16 - Typical amplifier with split power supply

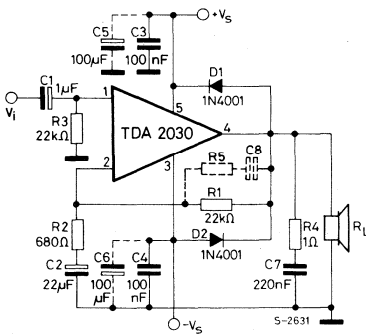
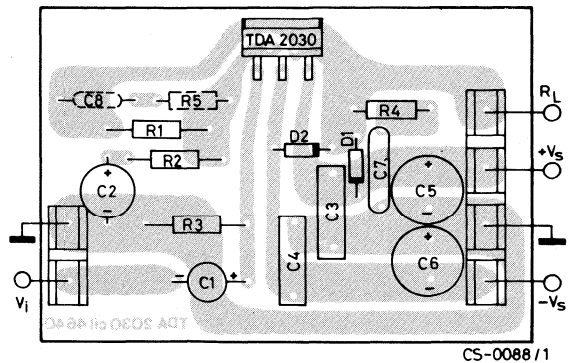


Fig. 17 - P.C. board and component layout for the circuit of fig. 16.



TDA 2030

APPLICATION INFORMATION (continued)

Fig. 18 - Typical amplifier with single power supply

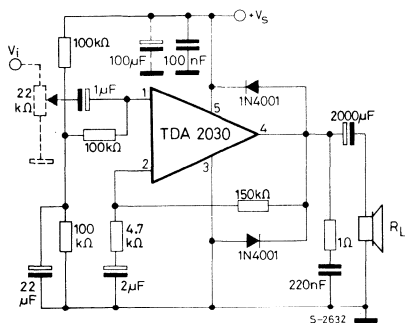


Fig. 19 - P.C. board and component layout for the circuit of fig. 18

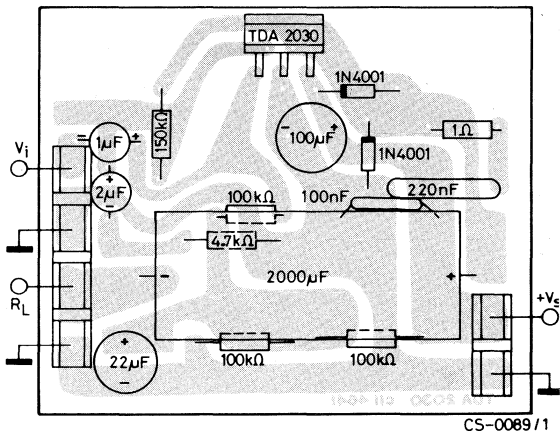
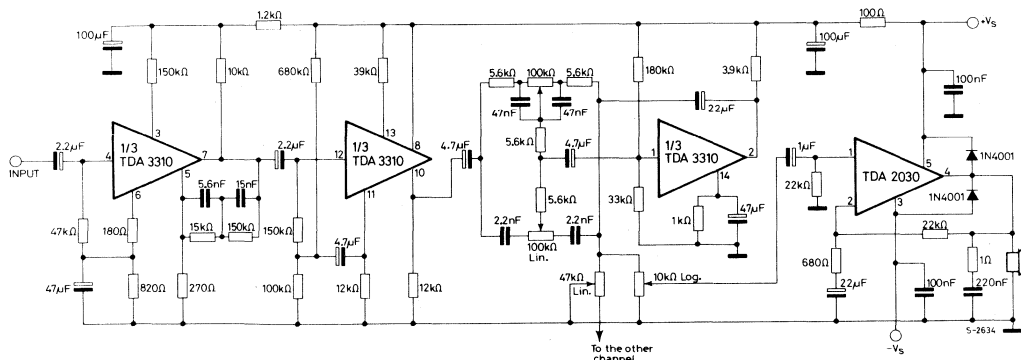


Fig. 20 - 14W Hi-Fi stereo amplifier with preamplifier equalizer for magnetic pick-ups



APPLICATION INFORMATION (continued)

Fig. 21 - Three way Hi-Fi active box.

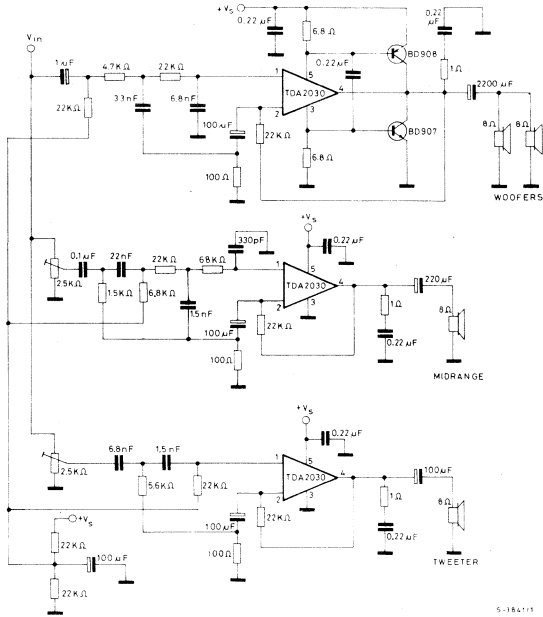
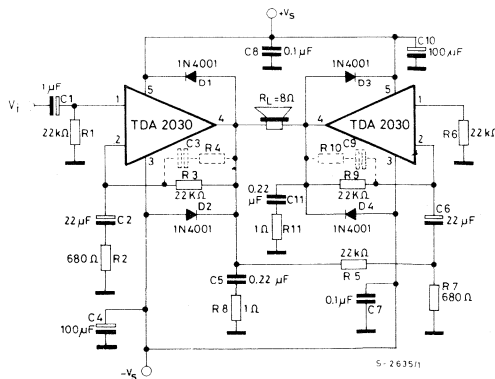


Fig. 22 - Bridge amplifier configuration with split power supply ($P_O = 28W$, $V_S = \pm 14V$)



TDA 2030

APPLICATION INFORMATION (continued)

Fig. 23 - P.C. board and component layout for the circuit in fig. 22 (1:1 scale)

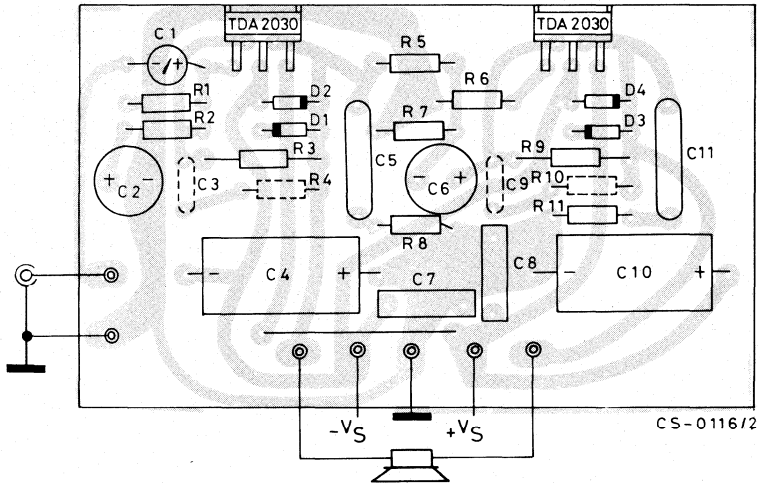
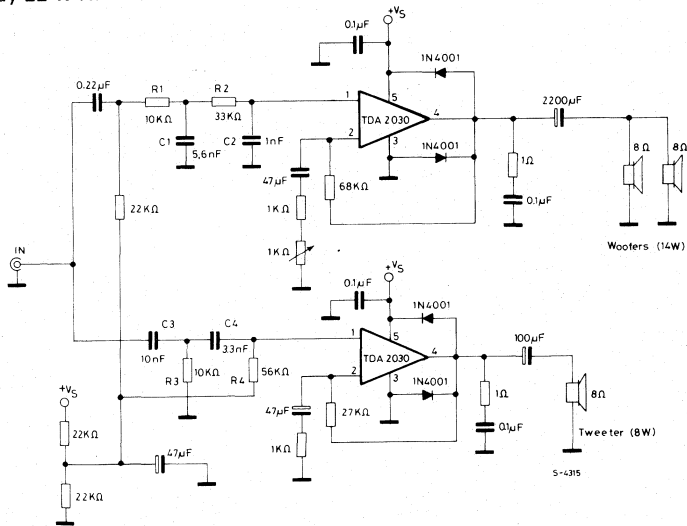


Fig. 24 - Two-way 22 W Hi-Fi active-box



PRACTICAL CONSIDERATIONS

Printed circuit board

The layout shown in fig. 16 should be adopted by the designers. If different layouts are used, the ground points of input 1 and input 2 must be well decoupled from the ground return of the output in which a high current flows.

Assembly suggestion

No electrical isolation is needed between the package and the heatsink with single supply voltage configuration.

Application suggestions

The recommended values of the components are those shown on application circuit of fig. 16. Different values can be used. The following table can help the designer.

Component	Recomm. value	Purpose	Larger than recommended value	Smaller than recommended value
R1	22 k Ω	Closed loop gain setting	Increase of gain	Decrease of gain
R2	680 Ω	Closed loop gain setting	Decrease of gain	Increase of gain
R3	22 k Ω	Non inverting input biasing	Increase of input impedance	Decrease of input impedance
R4	1 Ω	Frequency stability	Danger of oscillat. at high frequencies with induct. loads	
R5	$\approx 3 R2$	Upper frequency cutoff	Poor high frequencies attenuation	Danger of oscillation
C1	1 μF	Input DC decoupling		Increase of low frequencies cutoff
C2	22 μF	Inverting DC decoupling		Increase of low frequencies cutoff
C3,C4	0.1 μF	Supply voltage bypass		Danger of oscillation
C5,C6	100 μF	Supply voltage bypass		Danger of oscillation
C7	0.22 μF	Frequency stability		Danger of oscillat.
C8	$\approx \frac{1}{2\pi B R1}$	Upper frequency cutoff	Smaller bandwidth	Larger bandwidth
D1,D2	1N4001	To protect the device against output voltage spikes		

SHORT CIRCUIT PROTECTION

The TDA 2030 has an original circuit which limits the current of the output transistors. Fig. 25 shows that the maximum output current is a function of the collector emitter voltage; hence the output transistors work within their safe operating area (fig. 26). This function can therefore be considered as being peak power limiting rather than simple current limiting. The TDA 2030 is thus protected against temporary overloads or short circuit. Should the short circuit exist for a longer time, the thermal shut-down protection keeps the junction temperature within safe limits.

Fig. 25 - Maximum output current vs. voltage [V_{CEsat}] across each output transistor

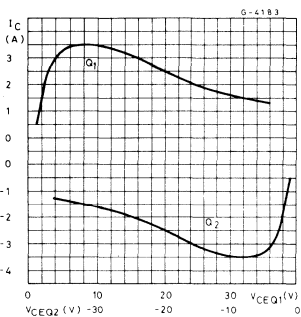
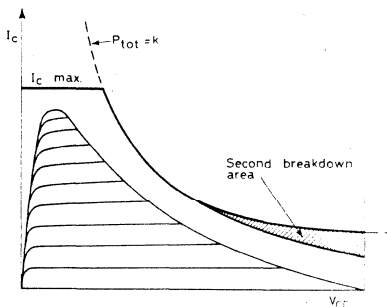


Fig. 26 - Safe operating area and collector characteristics of the protected power transistor



5-0764/1

THERMAL SHUT-DOWN

The presence of a thermal limiting circuit offers the following advantages:

- 1) An overload on the output (even if it is permanent), or an above limit ambient temperature can be easily supported since the T_j cannot be higher than 150°C .
- 2) The heatsink can have a smaller factor of safety compared with that of a conventional circuit. There is no possibility of device damage due to high junction temperature. If for any reason, the junction temperature increases up to 150°C , the thermal shut-down simply reduces the power dissipation and the current consumption.

The maximum allowable power dissipation depends upon the size of the external heatsink (i.e. its thermal resistance); fig. 29 shows this dissipable power as a function of ambient temperature for different thermal resistance.

Fig. 27 - Output power and drain current vs. case temperature ($R_L = 4\Omega$)

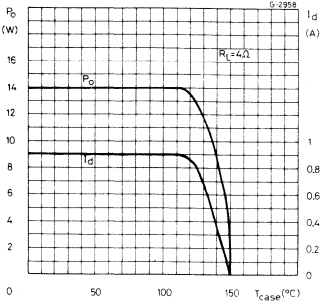


Fig. 28 - Output power and drain current vs. case temperature ($R_L = 8\Omega$)

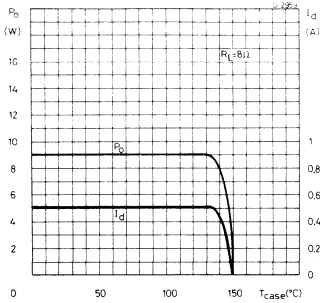


Fig. 29 - Maximum allowable power dissipation vs. ambient temperature

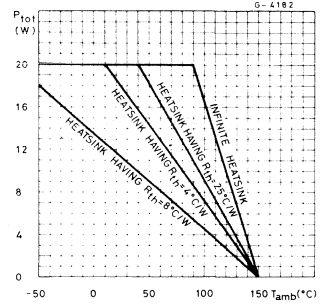
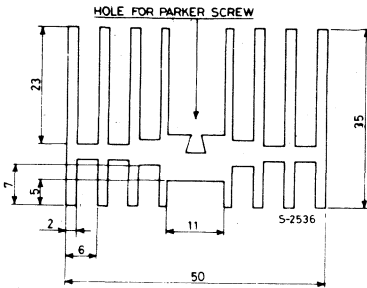


Fig. 30 - Example of heat-sink



Dimension : suggestion.

The following table shows the length that the heatsink in fig. 30 must have for several values of P_{tot} and R_{th} .

P_{tot} (W)	12	8	6
Length of heatsink (mm)	60	40	30
R_{th} of heatsink ($^{\circ}C/W$)	4.2	6.2	8.3

TDA 2054M

LINEAR INTEGRATED CIRCUIT

PREAMPLIFIER WITH ALC FOR MONO AND STEREO C_rO₂ CASSETTE RECORDERS

- EXCELLENT VERSATILITY IN USE (V_S from 4 to 20V)
- HIGH OPEN LOOP GAIN
- LOW DISTORTION
- LOW NOISE
- LARGE AUTOMATIC LEVEL CONTROL RANGE
- STEREO MATCHING BETTER THAN 3 dB

The TDA 2054M is a monolithic integrated circuit in a 16-lead dual in-line plastic package. The functions incorporated are:

- low noise preamplifier
- automatic level control system (ALC)
- high gain equalization amplifier

It is intended as preamplifier in tape and cassette recorders and players (C_rO₂), dictaphones, compressor and expander in telephonic equipments, Hi-Fi preamplifiers and in wire diffusion receivers; for stereo applications the ALC matching is better than 3 dB.

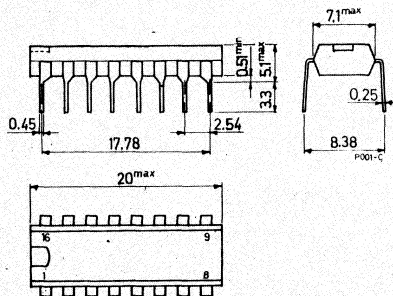
ABSOLUTE MAXIMUM RATINGS

V_S	Supply voltage	20	V
P_{tot}	Total power dissipation at $T_{amb} = 50^\circ\text{C}$	500	mW
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

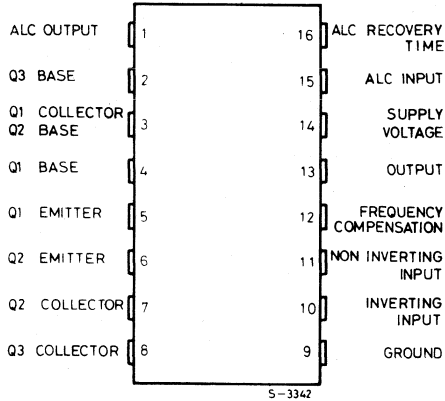
ORDERING NUMBERS: TDA 2054M mono applications
2 TDA 2054M stereo applications

MECHANICAL DATA

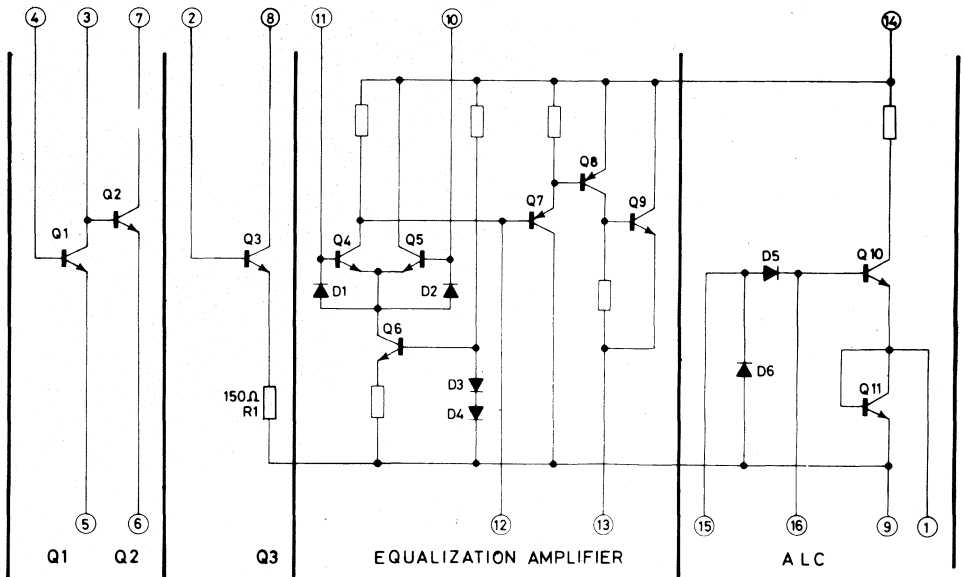
Dimensions in mm



CONNECTION DIAGRAM



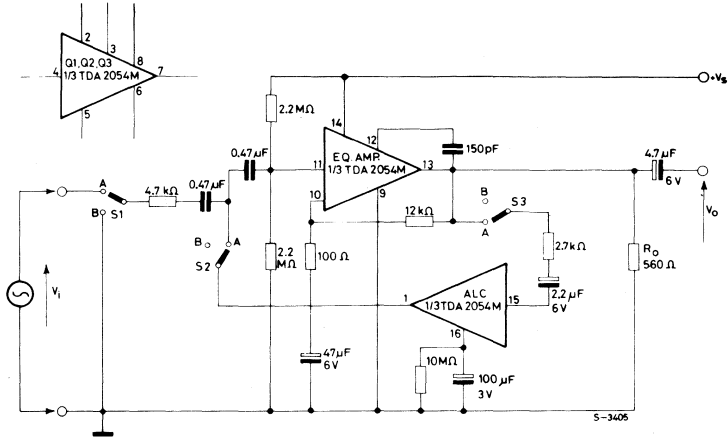
SCHEMATIC DIAGRAM



S-3404

TDA 2054M

TEST CIRCUIT



THERMAL DATA

$R_{th j-amb}$	Thermal resistance junction-ambient	max	200	$^{\circ}C/W$
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ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $T_{amb} = 25^{\circ}C$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	
V_s	Supply voltage	4		20	V	
I_d	Quiescent drain current	$V_s = 9V$ $S1 = S2 = S3 = \text{at B}$	10		mA	
h_{FE}	DC current gain (Q1, Q2, Q3)	$I_c = 0.1 \text{ mA}$ $V_{CE} = 5V$	300	500	—	
e_N	Input noise voltage (Q1, Q2, Q3)	$I_c = 0.1 \text{ mA}$ $V_{CE} = 5V$ $f = 1 \text{ KHz}$		2	$\frac{nV}{\sqrt{Hz}}$	
i_N	Input noise current (Q1, Q2, Q3)			0.5	$\frac{pA}{\sqrt{Hz}}$	
NF	Noise figure (Q1, Q2, Q3)	$I_c = 0.1 \text{ mA}$ $V_{CE} = 5V$ $R_g = 4.7 \text{ K}\Omega$ $B (-3 \text{ dB}) = 20 \text{ to } 10000 \text{ Hz}$		0.5	4	dB
G_v	Open loop voltage gain (for equalization amplifier)	$V_s = 9V$ $f = 1 \text{ KHz}$		60		dB
V_o	Output voltage with A.L.C.	$V_s = 9V$ $V_i = 100 \text{ mV}$ $f = 1 \text{ KHz}$ $S1 = S2 = S3 \text{ at A}$		0.6		V
e_N	Equivalent input noise voltage (for equalization amplifier pin 11)	$V_s = 9V$ $G_v = 40 \text{ dB}$ $S1 \text{ at B}$ $B (-3 \text{ dB}) = 20 \text{ to } 20000 \text{ Hz}$		1.3		μV
R_1	Q3 emitter resistance		105	150	195	Ω

TDA 2054M

Fig. 1 - Equivalent input spot voltage and noise current vs. bias current (transistors Q1, Q2, Q3)

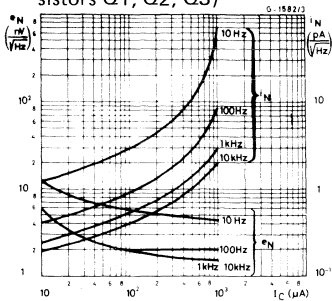


Fig. 2 - Equivalent input noise current vs. frequency (transistors Q1, Q2, Q3)

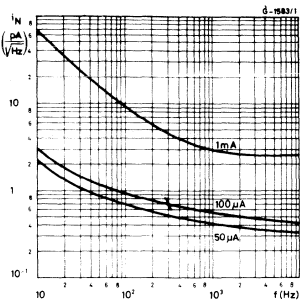


Fig. 3 - Equivalent input noise voltage vs. frequency (transistors Q1, Q2, Q3)

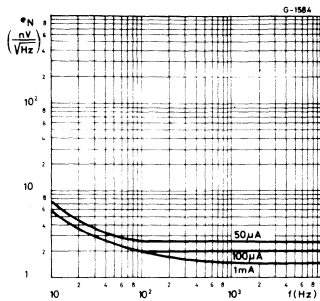


Fig. 4 - Noise figure vs. bias current (transistors Q1, Q2, Q3)

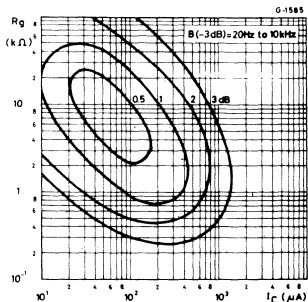


Fig. 5 - Optimum source resistance and minimum NF vs. bias current (transistors Q1, Q2, Q3)

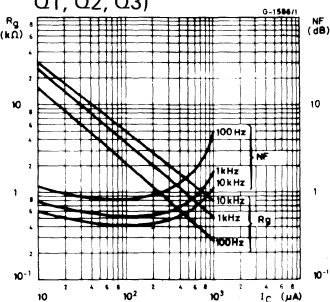


Fig. 6 - Current gain vs. collector current (transistors Q1, Q2, Q3)

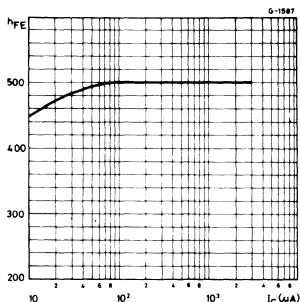


Fig. 7 - Open loop gain vs. frequency (equalization amplifier)

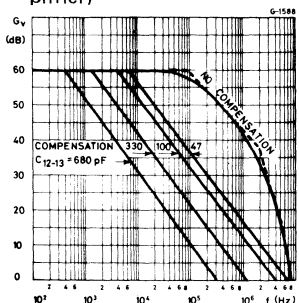


Fig. 8 - Open loop phase response vs. frequency (equalization amplifier)

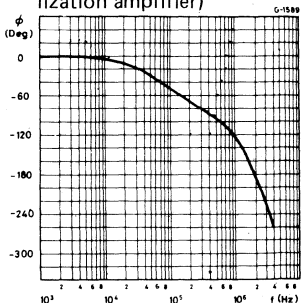
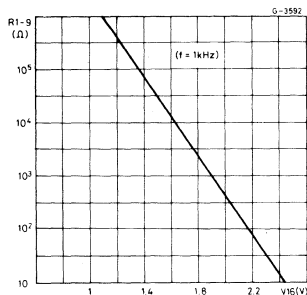


Fig. 9 - Dynamic resistance R1-9 vs. ALC voltage V16



TDA 2054M

APPLICATION INFORMATION

Fig. 9 - Application circuit for C₇O₂ cassette player and recorder

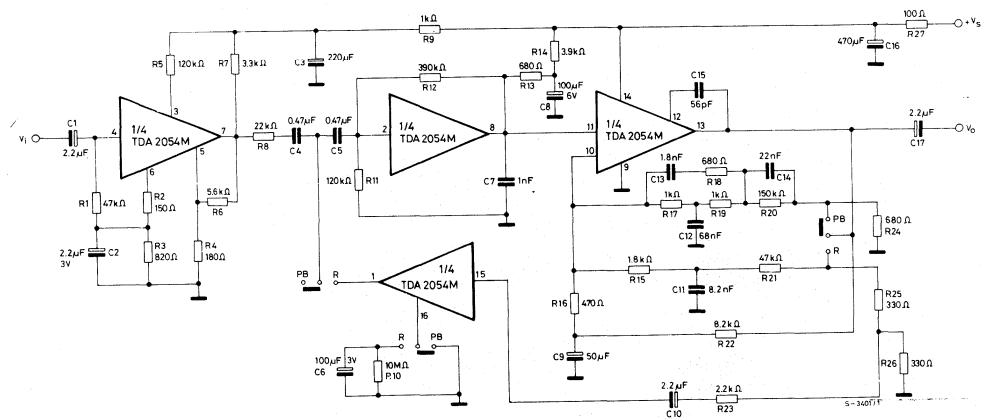
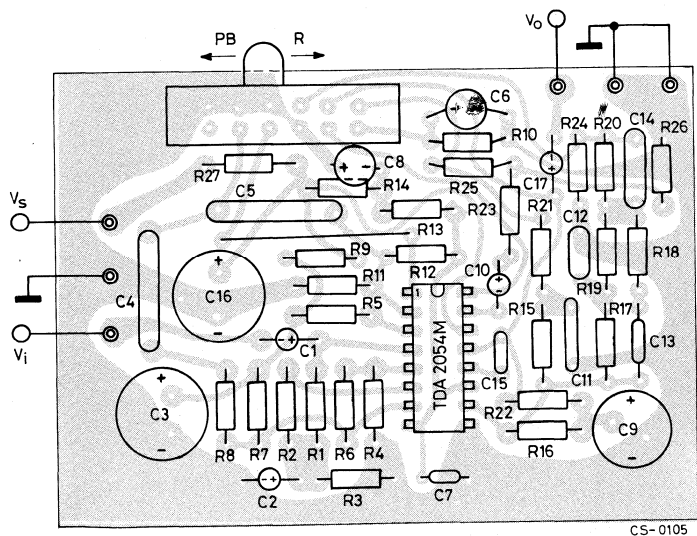


Fig. 10 - P.C. board and component layout for the circuit of Fig. 9 (1:1 scale)



CS-0105

TYPICAL PERFORMANCE OF CIRCUIT IN FIG. 9 ($T_{amb} = 25^{\circ}\text{C}$, $V_s = 9\text{V}$)

Parameter		Test conditions	Min.	Typ.	Max.	Unit
PLAYBACK						
G_v	Voltage gain (open loop)	$f = 20$ to 20000 Hz		134		dB
G_v	Voltage gain (closed loop)	$f = 1$ KHz		60		dB
Z_i	Input impedance	$f = 100$ Hz		10		$\text{K}\Omega$
		$f = 1$ KHz		41		$\text{K}\Omega$
		$f = 10$ KHz		43		$\text{K}\Omega$
Z_o	Output impedance	$f = 1$ KHz		12	35	Ω
B	Frequency response			see fig. 11		
d	Distortion	$V_o = 1\text{V}$ $f = 1$ KHz		0.2		%
	Output background noise	$Z_g = 300\Omega + 120$ mH (DIN 45405)		1.5		mV
***	Output weighted background noise			1		mV
$\frac{S+N}{N}$	Signal to noise ratio	$V_o = 1.5\text{V}$ $Z_g = 300\Omega + 120$ mH		60		dB
t_{on}^*	Switch-on time	$V_o = 1\text{V}$		500		ms

RECORDING

G_v	Voltage gain (open loop)	$f = 20$ to 20000 Hz		134		dB
G_v	Voltage gain (closed loop)	$f = 1$ KHz		72		dB
B	Frequency response			see fig. 13		
d	Distortion with ALC	$V_o = 1\text{V}$ $f = 10$ KHz		0.5		%
ALC	Automatic level control range (for 3 dB of output voltage variation)	$V_i \leq 40$ mV $f = 10$ KHz		54		dB
V_o	Output voltage before clipping without ALC	$f = 1$ KHz		3		V
V_o	Output voltage with ALC	$V_i = 30$ mV $f = 1$ KHz		1.1		V
t_l^*	Limiting time (see fig. 17)	$\Delta V_i = +40$ dB $f = 1$ KHz		75		ms
t_{set}^*	Level setting time (see fig. 17)			300		ms
t_{rec}^*	Recovery time (see fig. 17)	$\Delta V_i = -40$ dB $f = 1$ KHz		150		sec.
t_{on}^*	Switch-on-time	$V_o = 1\text{V}$		500		ms
$\frac{S+N}{N}^{***}$	Signal to noise ratio with ALC	$V_o = 1\text{V}$ $R_g = 470\Omega$		64		dB

* This value depends on external network.

** When the DIN 45511 norm for frequency response is not mandatory the equalization peak at 15 KHz can be avoided - so halving the output noise.

*** Weighted noise measurement (DIN 45405).

TDA 2054M

Fig. 11 - Frequency response for the circuit in fig.9 (playback)

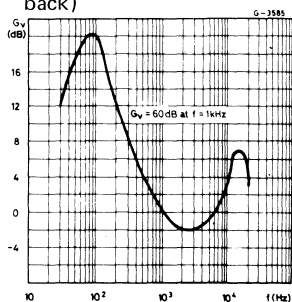


Fig. 12 - Distortion vs. frequency for the circuit in fig. 9 (playback)

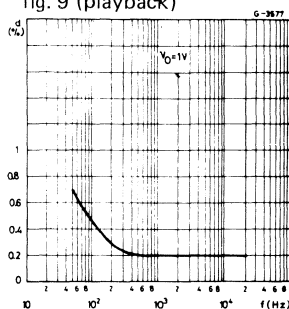


Fig. 13 - Frequency response for the circuit in fig. 9 (recording)

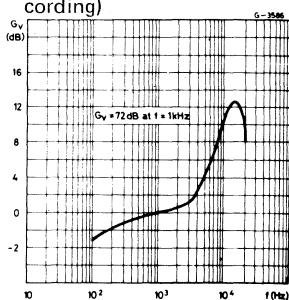


Fig. 14 - Output voltage variation and distortion with ALC vs. input voltage for the circuit in fig. 9 (recording)

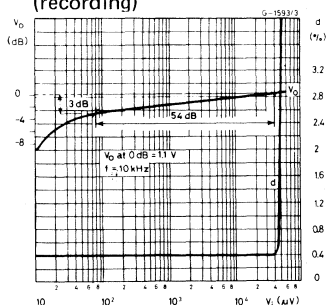


Fig. 15 - Distortion vs. frequency with ALC for the circuit in fig. 9 (recording)

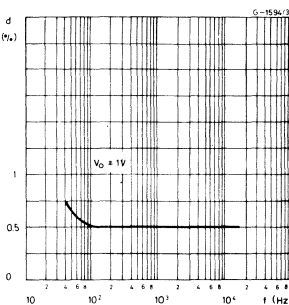


Fig. 16 - Limiting and level setting time vs. input signal variation

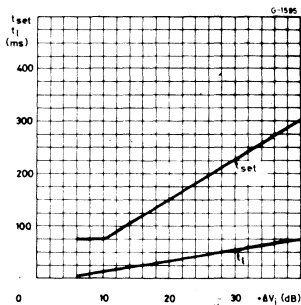
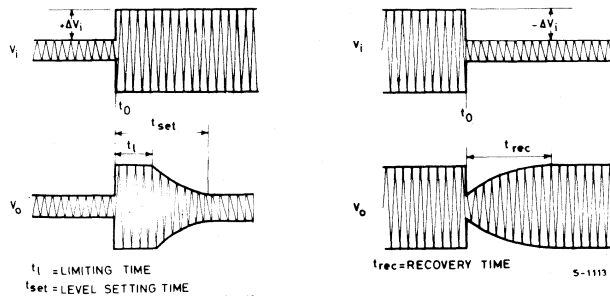


Fig. 17 - Limiting, level setting, recovery time



LINEAR INTEGRATED CIRCUIT

PAL SUBCARRIER REFERENCE OSCILLATOR FOR COLOUR TV

The TDA 2140 is a monolithic integrated circuit for regenerating and processing the subcarrier reference signals in the decoder circuit of PAL colour TV receivers. It is encapsulated in a 16-lead dual in-line plastic package and its main features are:

- High stability of the subcarrier oscillator with supply voltage and temperature variations.
- High noise immunity in ACC and APC circuits obtained by means of detectors activated only during key pulse
- High noise immunity in identification circuit
- Integrated 90° phase shifter
- No adjustments of ACC (Automatic Color Control) needed
- Hysteresis in color killer circuit
- Internal circuit, driven by flyback pulse, generated a composite blanking and burst key pulse
- When the antenna signal decreases, the saturation of the chroma signal is automatically reduced before colour killer action.
- Colour killer activated if the antenna signal is too low, if the oscillator is not locked, if the burst is absent or if PAL identification is wrong.

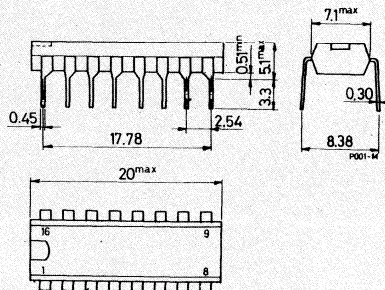
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage (pin 2)	15	V
V_{15}	Voltage at pin 15	{ +12 -50	V
P_{tot}	Total power dissipation at $T_{amb} \leq 70^\circ\text{C}$	800	mW
T_{stg}	Storage temperature	-55 to 150	$^\circ\text{C}$
T_{op}	Operating temperature	0 to 70	$^\circ\text{C}$

ORDERING NUMBER: TDA 2140

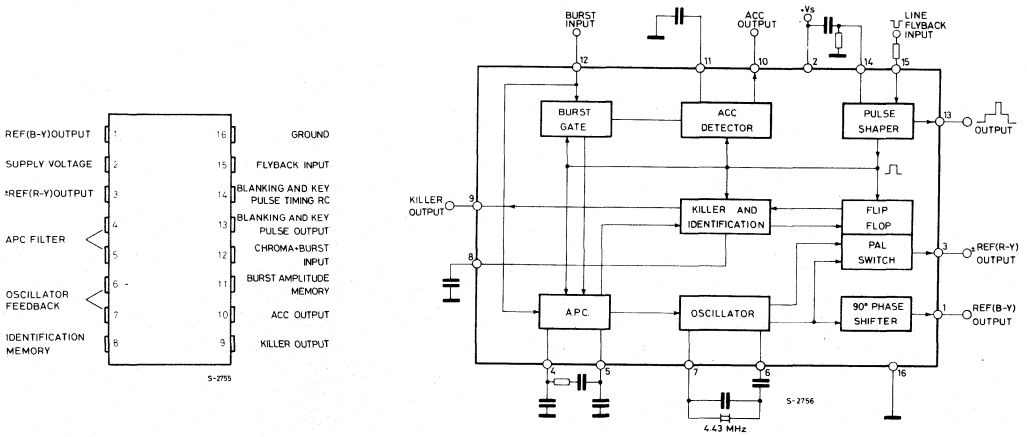
MECHANICAL DATA

Dimensions in mm

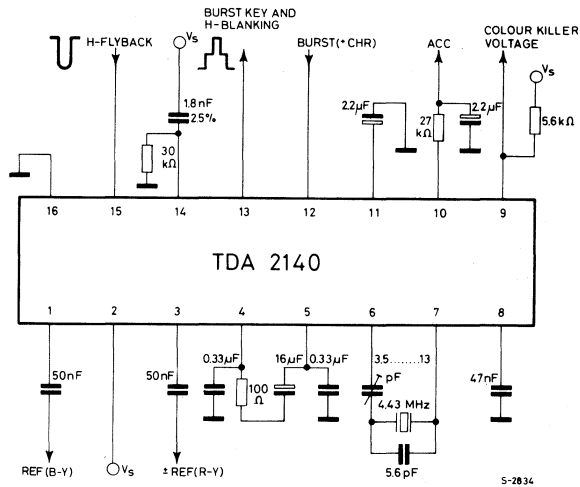


TDA 2140

CONNECTION AND BLOCK DIAGRAMS (top view)



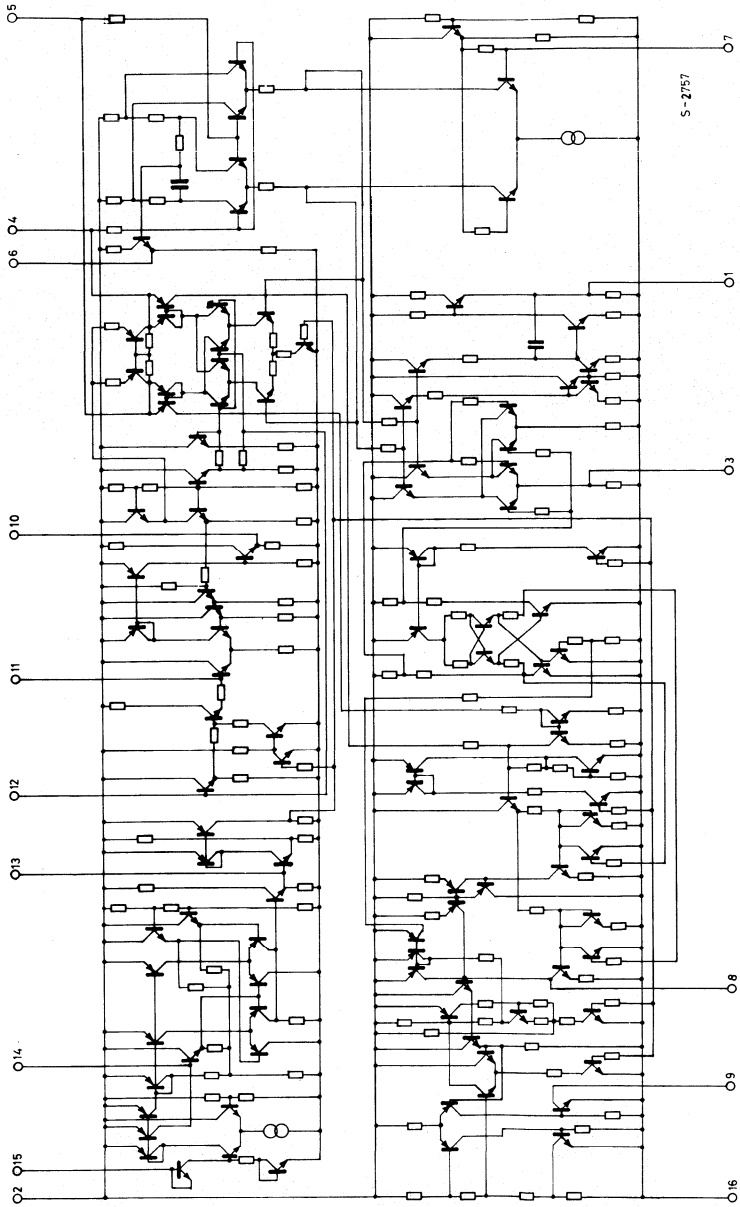
TEST CIRCUIT



THERMAL DATA

$R_{th j-amb}$	Thermal resistance junction-ambient	max	100	°C/W
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SCHEMATIC DIAGRAM



TDA 2140

ELECTRICAL CHARACTERISTICS

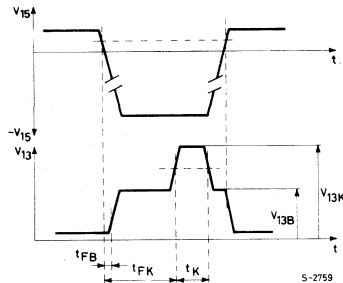
(Refer to the test circuit; $V_s = 12V$, $f_o = 4.43\text{ MHz}$, $T_{amb} = 25^\circ\text{C}$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s	Supply voltage (pin 2)	10.8		13.2	V
I_s	Supply current (pin 2)		45	64	mA
V_1	Ref. (B-Y) peak to peak output voltage		0.9		V
R_1	Ref. (B-Y) output resistance		100		Ω
V_3	\pm Ref. (R-Y) peak to peak output voltage		0.9		V
R_3	\pm Ref. (R-Y) output resistance		100		Ω
V_9	Colour killer output	Correct phase of PAL flip-flop	11.4		V
		Incorrect phase of PAL flip-flop		0.5	V
V_{10}	ACC output voltage (note 1)	$V_{12} = 0.9 V_{pp}$	1		V
V_{12}	Burst peak to peak input voltage (note 1)		0.9		V
V_{13K}	Key pulse peak output voltage (note 2)		5		V
V_{13B}	Blanking pulse peak output voltage (note 2)	2.1	2.5		V
R_{13}	Output resistance		100		Ω
t_K	Key pulse duration (note 2)	$V_{13} = 3V$		3.5	μs
t_{FK}	Phase relation between leading edges of flyback and key pulses (note 2)	$V_{13} = 3V$ $V_{15} = 1V$	6.5	6.8	μs
t_{FB}	Delay between flyback and blanking pulses (note 2)	$V_{13} = 1V$ $V_{15} = 1V$		0.4	μs
V_{15}	Input voltage of composite blanking and key pulse generator (flyback pulse) (note 2)	$V_{13} \leq 0.2V$	2.5	7.5	V
		$V_{13} \geq 1V$	-50	+1	V

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	
R_{15}	Line flyback pulse input resistance	$V_{15} = 2.5V$		1	$k\Omega$	
φ	Phase angle between Ref (B-Y) and Ref (R-Y) output signals		85	90	95	$^{\circ}$
Δf	Pull-in range	$V_{12} = 0.9 V_{pp}$		+300 -400	Hz	
$\frac{\Delta\varphi}{\Delta f}$	Static phase shift	$\Delta f = \pm 400$ Hz		10	$^{\circ}/kHz$	
$\frac{\Delta f}{\Delta T_{amb}}$	Oscillator frequency thermal drift	$T_{amb} = 20$ to $60^{\circ}C$		1	$Hz/^{\circ}C$	
$\frac{\Delta f}{\Delta V_s}$	Oscillator frequency voltage drift	$V_s = 10.8$ to $13.2V$		10	Hz/V	

- Notes:**
- 1 - Measured in closed loop configuration with TDA 2151 chroma amplifier.
 - 2 - Composite blanking and key pulse waveform.



APPLICATION INFORMATION

Pin 1 - Ref. (B-Y) output

The Ref. (B-Y) signal is obtained from the oscillator waveform by means of an operational amplifier with capacitive feedback, which guarantees a 90° phase shift with $\pm 5^{\circ}$ accuracy. Pin 1 has low output impedance and shows a triangular waveform.

Pin 2 - Positive supply

The operating supply voltage of the device ranges from 10.8V to 13.2V.

Pin 3 - \pm Ref. (R-Y) output

The phase of this signal is changed line by line from 0° to 180° by means of the PAL flip-flop, which is driven by the key pulses and is reset by the identification circuit. Pin 3 has low output impedance and shows a square waveform.

TDA 2140

APPLICATION INFORMATION (continued)

Pin 4 - Automatic phase control circuit

The APC circuit, which generates the voltage to control the oscillator by comparing the burst and oscillator waveforms, is activated only during the key pulse time. Therefore high noise immunity of the oscillator phase control is achieved. The filter network connected to pins 4 and 5 determines the bandwidth of the APC loop.

Pin 5 - (see pin 4)

Pin 6 - Oscillator

The tuning network of the oscillator is connected to pins 6 and 7. The free running frequency of the oscillator is calibrated by means of the variable capacitor connected in series to the quartz. The pull-in range is typically +300 Hz -400 Hz; its slight asymmetry is due to the characteristics of the circuit which controls the oscillator. The pull-in range can be enlarged by reducing the value of the capacitor connected in parallel to the quartz, but it should never fall below 3.3 pF.

Pin 7 - (see pin 6)

Pin 8 - Identification circuit

The capacitor connected between pin 8 and ground memorizes the identification circuit status. The identification circuit performance is influenced by the value of this capacitor and suitable ground layout must be provided. To reduce the identification sensitivity, a 6.8 M Ω resistor can be connected in parallel to the capacitor.

Pin 9 - Colour killer

Pin 9 is the output of the colour killer which is controlled by the identification circuit. Colour killing occurs if the antenna signal is too low, if the oscillator is not locked, if the burst is absent or if PAL identification is wrong. Colour killer activation and deactivation occur with different delays and with a hysteresis which eliminates the possibility of system oscillation.

Pin 10 - ACC detector

Pin 10 is the output of the ACC voltage to control the gain of the TDA 2150 chroma amplifier. At pin 11 the capacitor of the burst peak detector is connected to avoid annoying effects on the picture due to colours being affected by a very noisy signal. The ACC detector gradually desaturates the picture before the killer switches off the colours, in the event of low antenna signal levels.

Pin 11 - (see pin 10)

Pin 12 - Burst input circuit

Pin 12 is the input of the burst signal which is picked up together with the chrominance signal and has to be separated from the remainder of the line. This is done by the burst gate controlled by the key pulse. If the burst is coupled to the TDA 2140 via a band pass filter, the relative phase between sub-carriers and chrominance signal can be calibrated so that correct picture colours are obtained even with broadcasts which do not correspond perfectly to the PAL standard.

Pin 13 - Composite blanking and key pulse generator (sandcastle pulse)

The low impedance sandcastle pulse available at pin 13 of the IC is obtained from the flyback pulse applied at pin 15. The flyback pulse must be negative and have a maximum amplitude of 55 V_{pp}. The precision of the sandcastle timing is determined by the tolerances of the RC network connected to pin 14 of the IC; to avoid calibration, the maximum tolerances allowed are $\pm 2\%$ for the resistance and $\pm 2.5\%$ for the capacitance. When the composite blanking and key pulse are available from any other circuit, e.g. from jungle IC, the sandcastle generator of the TDA 2140 can not be used. In this case, the sandcastle pulse is sent to pin 13 of the TDA 2140, pin 14 is brought directly to V_s and pin 15 is brought to V_s via a 5.6 k Ω resistor. The internal circuit picks up the key pulse required to operate the IC.

Pin 14 - (see pin 13); Pin 15--(see pin 13); Pin 16 - Ground

LINEAR INTEGRATED CIRCUIT

LUMINANCE AND CHROMINANCE AMPLIFIER FOR COLOUR TV

The TDA 2151 is a monolithic integrated circuit for CTV receivers that amplifies and controls the luminance and chrominance signals. It is encapsulated in a 16-lead dual in-line plastic package and its main features are:

- No pre-adjustments are needed for DC controls of contrast, brightness and saturation
- Tracked DC contrast control in chrominance and luminance channels
- Beam current limiter acting on contrast and brightness controls
- Programmable contrast reduction at beam current limiter action
- Independent video signal output for driving the sync. separator; this is for VCR playback operation
- Black level of the video output signal thermally compensated
- Generation of a luminance service signal to adjust the CRT cathode bias.

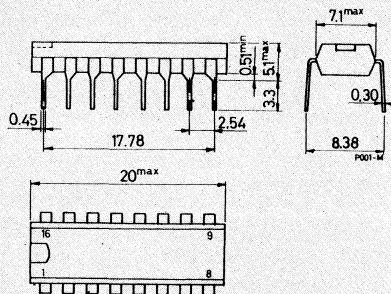
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage (pin 11)	15	V
V_1, V_8	Voltages at pin 1 and pin 8	V_s	
P_{tot}	Power dissipation at $T_{amb} \leq 70^\circ\text{C}$	800	mW
T_{stg}	Storage temperature	-55 to 150	$^\circ\text{C}$
T_{op}	Operating temperature	0 to 70	$^\circ\text{C}$

ORDERING NUMBER: TDA 2151

MECHANICAL DATA

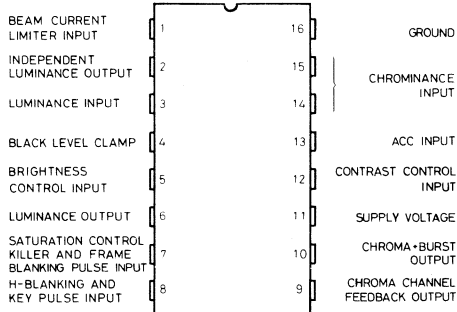
Dimensions in mm



TDA 2151

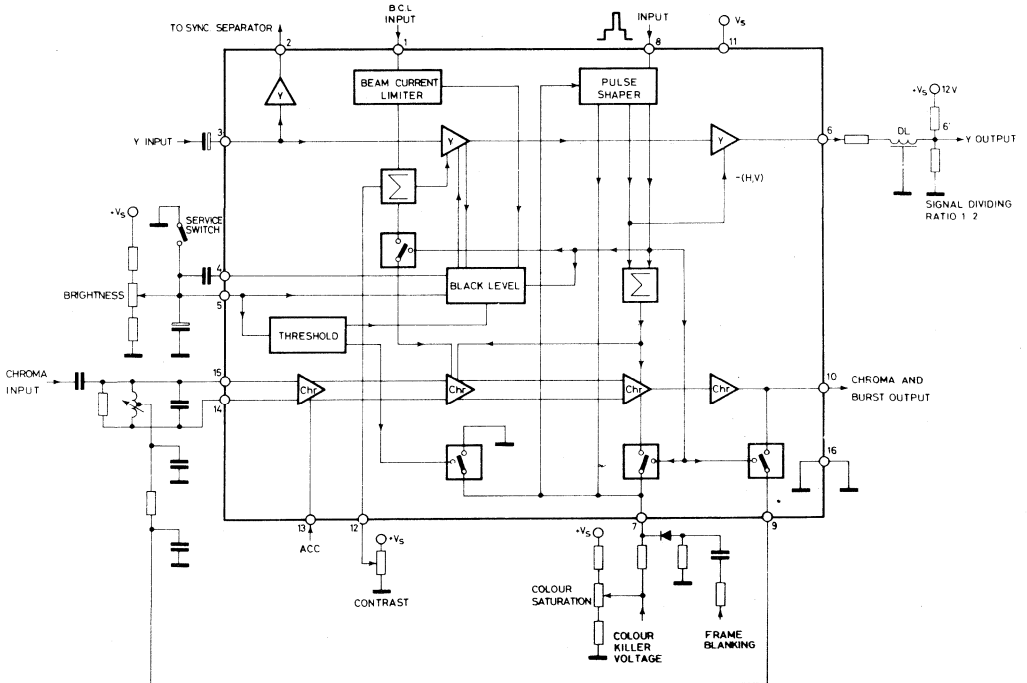
CONNECTION DIAGRAM

(top view)



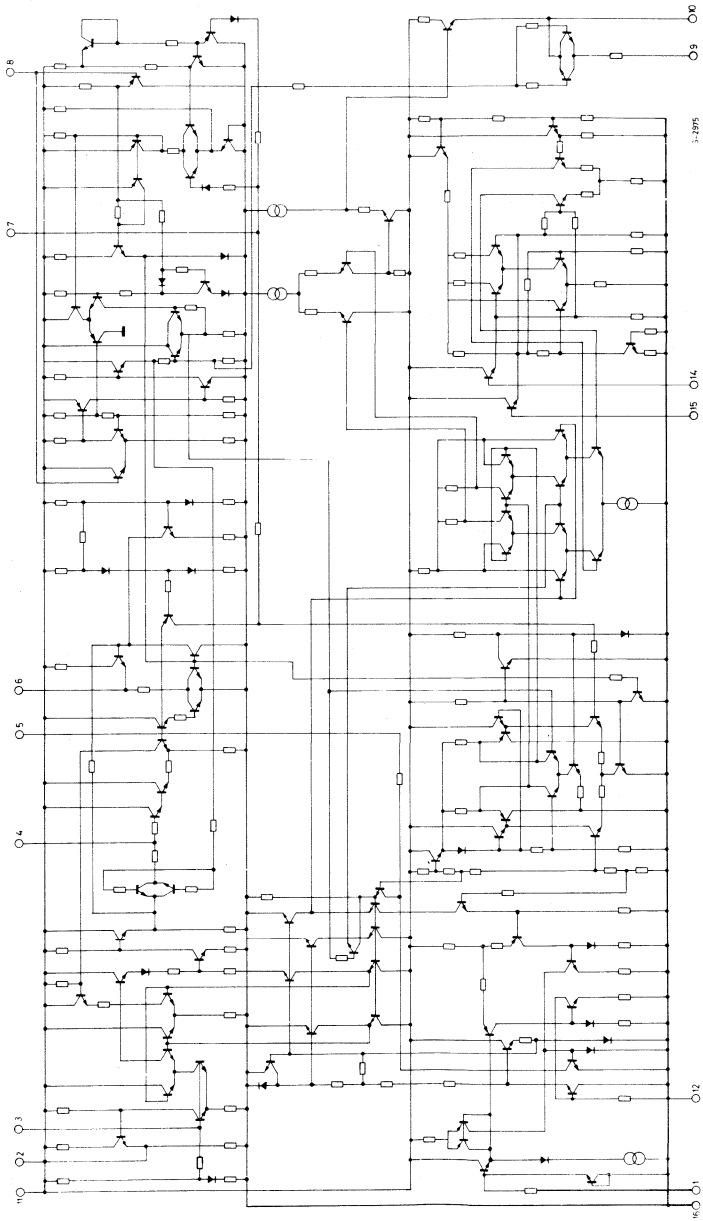
5-2762

BLOCK DIAGRAM



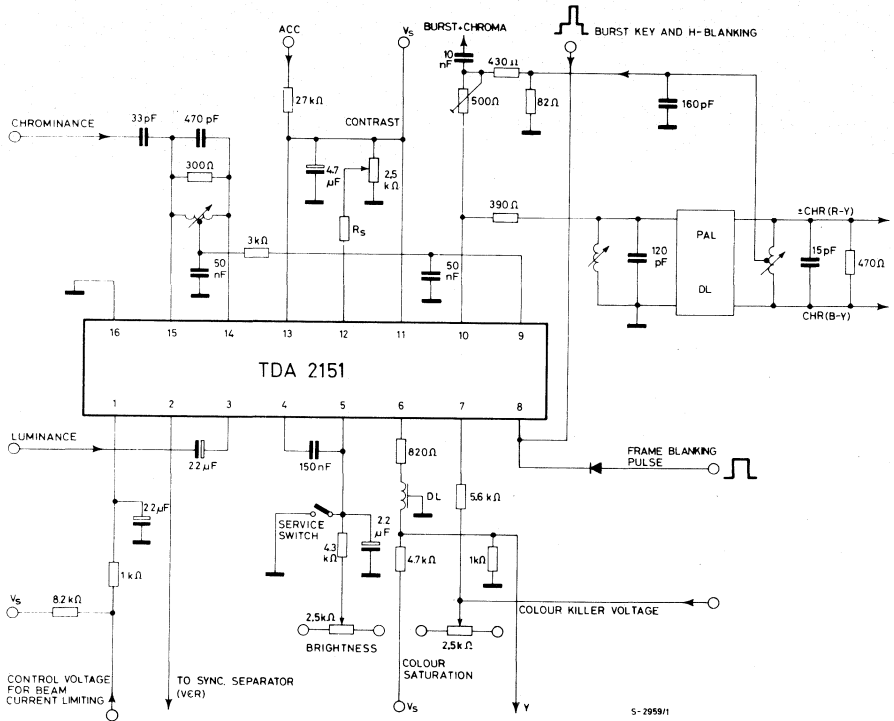
5-2260

SCHEMATIC DIAGRAM



TDA 2151

TEST CIRCUIT



THERMAL DATA

R _{th j-amb}	Thermal resistance junction-ambient	max	100	°C/W
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ELECTRICAL CHARACTERISTICS

(Refer to the test circuit, $V_s = 12V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s	Supply voltage (pin 11)	10.8		13.2	V
I_s	Supply current (pin 11)		45	56	mA

CHROMINANCE SECTION

V_i	Peak to peak input signal (between pin 14 and pin 15)	$f = 4.4 \text{ MHz}$			80	mV
V_o	Peak to peak chroma output signal (pin 10)	$f = 4.4 \text{ MHz}$ $K \leq 5\%$		3		V
V_o	Max. peak to peak chroma output signal (pin 10)	$f = 4.4 \text{ MHz}$		3.8		V
ΔG_{chr}	ACC range	$\Delta V_{10} \leq 1 \text{ dB}$	26			dB
ΔG_{chr}	Saturation control range	$V_{12} = 12V$ $\Delta V_7 = 2.1 \text{ to } 6.5V$		40		dB
$\frac{V_i}{V_o}$	Chroma signal attenuation during killer action	$V_{12} = 12V$	8			dB
$\frac{G_{chr}}{G_{burst}}$	Ratio of chroma voltage gain to burst voltage gain	$V_{12} = 12V$ $V_7 = 6.5V$	0.94	1	1.06	—
		$V_{12} = 12V$ $V_7 = 4.3V$	0.47	0.5	0.53	—
$\frac{\Delta G_y}{\Delta G_{chr}}$	Tracking ratio of luminance and chroma channels contrast control	$\Delta V_{12} = 0 \text{ to } 12V$		1	1.5	dB

LUMINANCE SECTION

V_i	Peak to peak input signal (pin 3)	100% white bar		1		V
R_i	Input resistance (between pin 3 and pin 16)			12		k Ω
C_i	Input capacitance (between pin 3 and pin 16)				8	pF
V_2	Independent luminance output signal (peak to peak)	$V_i = 1 \text{ Vpp}$		3.7		V
R_2	Independent luminance output resistance			100		Ω
V_5	Brightness DC control voltage			2 to 5.5		V

TDA 2151

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	
V_o	Luminance output signal at pin 6 (black to white)	$V_{12} = 12V$ $V_i = 1 V_{pp}$	2	2,2	2.4	V
		$V_{12} = 0V$ $V_i = 1 V_{pp}$	0.4		0.48	V
V_o	Black level of the luminance output signal (pin 6)	$V_5 = 4.7V$		3.6		V
V_o	Luminance service peak to peak output signal (pin 6)	$V_5 = 0V$		240		mV
V_8	Frame blanking pulse		1.4			V
I_7	Frame blanking pulse input current	Positive pulse	1			mA
		Negative pulse			-1	mA
$\frac{\Delta V_o}{\Delta V_5}$	Ratio of output blank level change to brightness control DC voltage change			0.5		—
ΔG_y	Contrast control range	$V_{12} = 0$ to $12V$		13		dB

BEAM CURRENT LIMITER CHARACTERISTICS

Fig. 1 - Y output signal (black to white) and its reduction due to beam current limiter action vs. contrast control voltage

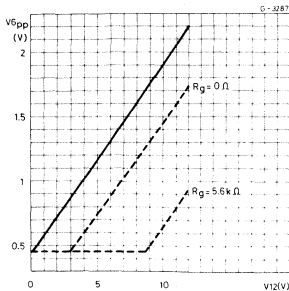


Fig. 2 - Normalized Y amplif. gain vs. b.c.l. control voltage

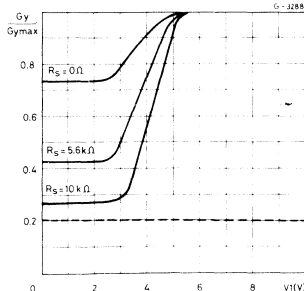
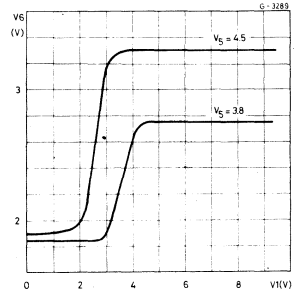


Fig. 3 - Y output black level vs. b.c.l. control voltage



APPLICATION INFORMATION

Pin 1 - Beam current limiter input

The beam current limiter is controlled through pin 1 by a DC voltage which is proportional to the average CRT beam current. When the beam current increases, the voltage applied at pin 1 decreases and causes first a reduction in contrast and then a reduction in brightness. The amount of the contrast reduction is programmable by means of the resistance R_s connected in series to pin 12. The characteristics of b.c.l. are shown in figures 1, 2, 3 and 4. By varying the values of the integrator circuit components on the EHT transformer, both the intervention point and the limitation slope can be adjusted to suit the various types of CRTs.

Pin 2 - VCR Output

The luminance signal, with typical amplitude of 3.5 Vpp, is available at pin 2 of the IC. This signal has positive sync. suitable for driving the sync. separator if external video sources such as VCRs or video disc players are to be used.

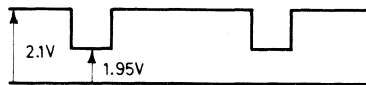
Pin 3 - Y input

The luminance signal, of amplitude 1 Vpp, is capacitively coupled to pin 3 of the IC which shows high input impedance. The luminance signal is separated from the chrominance signal by means of a 4.43 MHz trap. The design of this trap is very important. In fact the 4.43 MHz leakage at the decoder RGB outputs is largely due to the leakage which passes through the luminance channel.

Pins 4 and 5 - Black level clamp and brightness control

The clamp locking pulse is supplied by the pulse shaper circuit which receives the composite blanking and key pulse (sandcastle) from pin 8. The clamp circuit compares the brightness control setting. When pin 5 is connected to ground, a service signal suitable for alignment of CRT cutoffs is available at the luminance output.

The service signal on the voltage divider after the delay line is:



S - 2835

Pin 6 - Y output

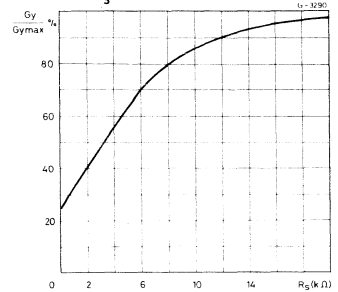
With contrast control at maximum, a luminance signal, with typical amplitude from white to black of 2.2V, is present at pin 6. The black level of this signal is determined by the brightness control voltage. To allow the luminance delay line to be adapted easily, output Y of the TDA 2151 has low impedance. Before the output, the luminance signal is cutoff during line and frame flyback by the horizontal and vertical blanking pulses.

Pin 7 - Saturation control

The gain of the chroma amplifier is set by means of the colour saturation control connected to pin 7 of the IC. The control range is between 2.1V and 6.5V, causing a chrominance channel gain variation of 60 dB. The colour killer, which is activated in the TDA 2140, also acts on pin 7 and guarantees 8 dB as minimum attenuation of the chroma signal.

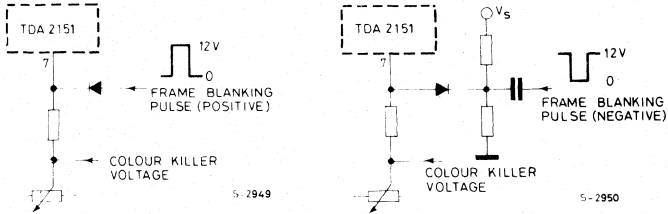
Pin 7 also receives frame blanking pulses. Using the application circuits shown on the next page, positive or negative blanking pulses can be applied to the IC.

Fig. 4 - Reduction of the contrast due to b.c.l. action vs. R_s .



TDA 2151

APPLICATION INFORMATION (continued)



Pin 8 - H and V blanking and key pulses input

The H and V blanking and key pulses are separated by means of internally fixed thresholds whose levels are 1.2V, 1.4V and 4V respectively. A suitable composite blanking and key pulse is generated by the TDA 2140 but any other source can be used if correct amplitude and phase of blanking and key pulses are provided. The input impedance at pin 8 is 50 k Ω .

Pin 9 - (see pins 14 and 15)

Pin 10 - Chroma output

Pin 10 is the low impedance chrominance output. In order to prevent the colour burst signal from being influenced by contrast and saturation controls, the second and third stages of the amplification chain are at maximum gain during the burst period. It is important to note that the signal, to which the TDA 2140 refers for generating the ACC control voltage, is picked up after the PAL delay line so that the attenuation spread of the delay line is compensated. This in addition to the low gain spread in the chrominance amplification chain, eliminates presetting of the saturation control. With saturation and contrast controls at maximum, the relationship between chrominance and burst signals at pin 10 corresponds to that at the input; this relationship, referred to the brightness output signal, gives an oversaturation of 6 dB.

Pin 11 - Positive supply

The operating supply voltage of the device ranges from 10.8V to 13.2V.

Pin 12 - Contrast control

The contrast control is connected to pin 12. A special circuit gives a linear gain characteristic to the contrast control voltage; gain variation is 14 dB over the 0 to 12V DC control voltage range. The contrast control acts in the same way on the luminance channel and on the chrominance channel. Excellent tracking is thus obtained between luminance channel amplification and chrominance channel amplification throughout the range of contrast adjustment.

Pin 13 - ACC input

Pin 13 is the high impedance input for controlling the gain of the chroma amplifier. It has to be connected to pin 10 of the TDA 2140 through a low pass filter whose purpose is to reduce the ripple on the ACC control voltage.

Pins 14 and 15 - Chroma input

The chroma signal is carried symmetrically by pins 14 and 15 to the high impedance input of a 4 stage amplification chain. The gain of the first stage is regulated by the ACC voltage generated in the TDA 2140. The balanced chrominance signal which leaves the bandpass filter is applied between pins 14 and 15. The maximum signal handling capability of the input circuit is 80 mVpp. Due to the high gain of the chrominance amplifiers, attenuation of the Y signal must be good and both the group delay and the overall delay introduced by the filter must be minimal. DC feedback is used between the last stage (pin 9) and the input to stabilize DC operation of the amplification chain.

Pin 16 - Ground

LINEAR INTEGRATED CIRCUIT

SYNCHRONOUS DEMODULATOR AND RGB MATRIX FOR COLOUR TV WITH ON SCREEN DISPLAY FACILITY

The TDA 2161 is a monolithic integrated circuit for demodulating and matrixing chroma signals. It is used for RGB cathode driving of colour pictures tubes and is directly coupled to the video output stages. The TDA 2161 is encapsulated in a 16-lead dual in-line plastic package and its main features are:

- High stability of DC output voltages ensured by applying heavy feedback from the output stages
- Large bandwidth
- Tight thermal coupling between the three channels
- Low subcarrier leakage due to integrated active filters
- Large black level adjustment range
- Large dynamic swing of the output signals
- High electrical stability of RGB amplifiers assured by internal frequency compensations
- Box blanking for characters display on screen.

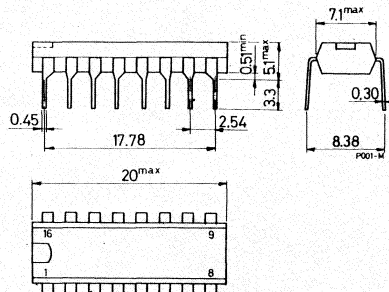
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage (pin 9)	15	V
V_{12}	Voltage at pin 12	V_s	
P_{tot}	Total power dissipation at $T_{amb} \leq 70^\circ\text{C}$	800	mW
T_{stg}	Storage temperature	-55 to 150	$^\circ\text{C}$
T_{op}	Operating temperature	0 to 70	$^\circ\text{C}$

ORDERING NUMBER: TDA 2161

MECHANICAL DATA

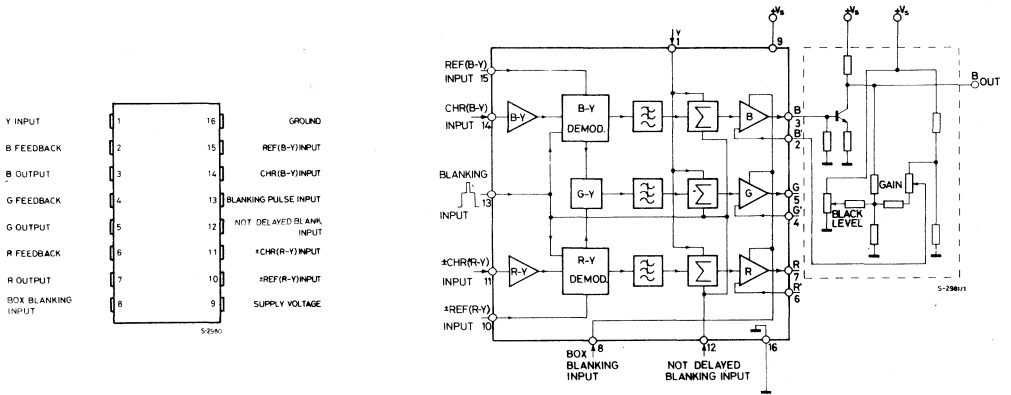
Dimensions in mm



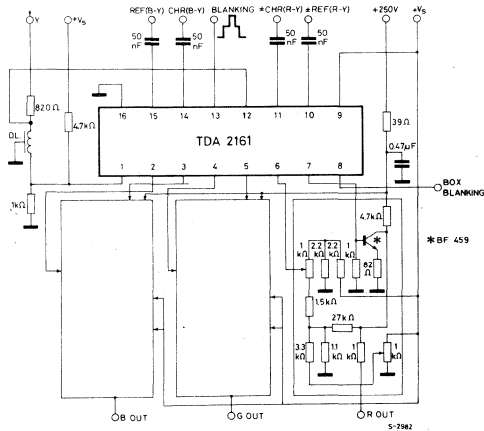
TDA 2161

CONNECTION AND BLOCK DIAGRAMS

(top view)



TEST CIRCUIT

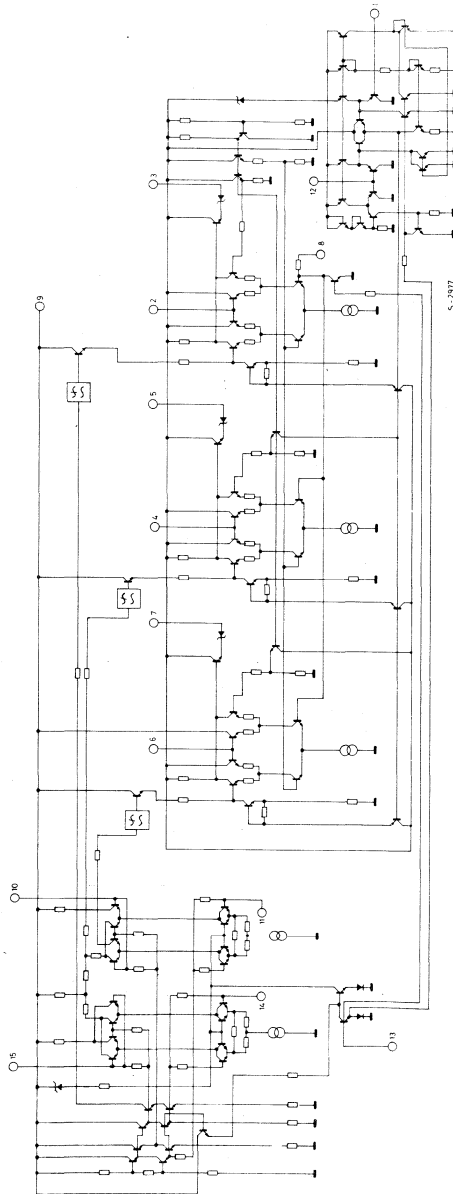


THERMAL DATA

$R_{th j-amb}$ Thermal resistance junction-ambient

max 100 °C/W

SCHEMATIC DIAGRAM



TDA 2161

ELECTRICAL CHARACTERISTICS

(Refer to the test circuit, $V_s = 12V$, $T_{amb} = 25^\circ C$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	
V_s	Supply voltage (pin 9)	10.8		13.2	V	
I_s	Supply current (pin 9)		35	46	mA	
V_1	Peak to peak luminance input signal	CRT cathodes signal = 100 Vpp		1	V	
V_1	Black level voltage of luminance input signal		2.2		V	
R_1	Luminance input resistance		50		k Ω	
G_V	Gain of luminance channels (including video output stages)	$f = 0.5 \text{ MHz}$ $V_i = 1 \text{ Vpp}$	100		—	
B_V	Frequency response of luminance channels (-3 dB)	$V_i = 200 \text{ mVpp}$	6		MHz	
V_8	Box blanking input pulse	2.5		5	V	
V_{11}	Chr. (R-Y) peak to peak input signal for max. output	$f = 4.4 \text{ MHz}$ Output signals linearity factor: $m = 0.7$	470		mV	
V_{14}	Chr. (B-Y) peak to peak input signal for max. output		350		mV	
R_{11}	Chr. (R-Y) input resistance	$f = 4.4 \text{ MHz}$	1		k Ω	
C_{11}	Chr. (R-Y) input capacitance			5	pF	
R_{14}	Chr. (B-Y) input resistance		1		k Ω	
C_{14}	Chr. (B-Y) input capacitance			5	pF	
V_{10}	\pm Ref. (R-Y) peak to peak input signal		0.8		V	
R_{10}	\pm Ref. (R-Y) input resistance		2		k Ω	
V_{15}	Ref. (B-Y) input signal		0.8		V	
R_{15}	Ref. (B-Y) input resistance		2		k Ω	
G_{R-Y}	Gain of (R-Y) demodulator (note)		$f = 4.4 \text{ MHz}$ $V_i = 50\text{mVpp}$	3.3		—

ELECTRICAL CHARACTERISTICS (continued)

Parameter		Test conditions	Min.	Typ.	Max.	Unit
G_{B-Y} G_{R-Y}	(B-Y) demodulator gain to (R-Y) demodulator gain ratio	$f = 4.4 \text{ MHz}$ $V_i = 50 \text{ mVpp}$ $V_{14} = 50 \text{ mVpp}$ $V_{10} = V_{15} = 700 \text{ mVpp}$		1.78		—
V_{G-Y} V_{R-Y}	(G-Y) to (R-Y) matrix ratio	$f = 4.4 \text{ MHz}$ $V_{11} = 50 \text{ mVpp}$ $V_{10} = 700 \text{ mVpp}$		-0.51		—
V_{G-Y} V_{B-Y}	(G-Y) to (B-Y) matrix ratio	$f = 4.4 \text{ MHz}$ $V_{14} = 50 \text{ mVpp}$ $V_{15} = 700 \text{ mVpp}$		-0.19		—
B_{Chr}	Frequency response of colour difference channels (-3 dB)	$V_{11} = 0.1 \text{ Vpp}$ $V_{14} = 0.1 \text{ Vpp}$ $V_{10} = V_{15} = 700 \text{ mVpp}$	1	1.2		MHz
V_3	B output voltage swing	$m \geq 0.7$		3		V
V_5	G output voltage swing			3		V
V_7	R output voltage swing			3		V
V_{13}	Blanking input voltage		1			V
I_{13}	Blanking input current		10			μA
ΔV_o	DC differential voltage between RGB outputs (at c.r.t. cathodes)	$V_1 = V_{12}$			5	V
	Residual carrier at the CRT cathodes				2	Vpp

APPLICATION INFORMATION

Pin 1 - Luminance input

The luminance signal enters at pin 1 with a typical black to white amplitude of 1V and a black level of 2.2V. The typical input impedance is $50 \text{ k}\Omega/5 \text{ pF}$.

Pin 2 - Blue channel feedback

The DC working points and gains of the output stages and the IC amplifier stages are stabilized by the feedback circuits. The gain and black level of the RGB output stages are adjusted to have the black and white setting points on the picture tube, by means of the potentiometers in the feedback paths.

TDA 2161

APPLICATION INFORMATION (continued)

Pin 3 – Blue signal output

The low output impedance and the dynamic swing of the B signal output allows direct driving of the video output stage.

Pin 4 – Green channel feedback (see pin 2)

Pin 5 – Green signal output (see pin 3)

Pin 6 – Red channel feedback (see pin 2)

Pin 7 – Red signal output (see pin 3)

Pin 8 – Box blanking input

Positive going pulses are required. The high impedance input is TTL compatible.

Pin 9 – Positive supply

The operating supply voltage of the device ranges from 10.8 to 13.2V.

Pin 10 – \pm (R-Y) reference input

A DC blocking capacitor is required to avoid DC unbalance of the demodulator. A minimum peak to peak signal of 0.5V is required to ensure good demodulator performance.

Pin 11 – \pm (R-Y) chroma signal input

The (B-Y) and (R-Y) demodulators have different amplification gain to compensate for the different attenuation of the chrominance signal components. This results in a gain of 3.3 for the (R-Y) detector while the relationship between the gain of the (B-Y) detector and that of the (R-Y) detector is 1.78. The gain is calculated on the peak-to-peak values at the input and output of the demodulator, using standard colour bars as a test signal. To obtain maximum output, the chrominance input signals must have a typical value of 350 mVpp for (B-Y) and 370 mVpp for (R-Y). In addition to the chrominance signal components, the burst also arrives at the demodulators. If demodulated, the burst would alter the blanking level on the video output stages. The demodulators must therefore be shut off during flyback and this is done by the sandcastle pulse applied at pin 13 of the IC. The (G-Y) component is obtained from the outputs of the two demodulators by means of the passive matrix according to the equation. $(G-Y) = -0.51 (R-Y) - 0.19 (B-Y)$.

Pin 12 – Not delayed blanking input

The not delayed blanking pulse, available before the luminance delay line, is combined internally with the blanking pulse applied at pin 13.

Pin 13 – Blanking input

The demodulators are blanked by applying at pin 13 a positive pulse which must exceed the internal threshold of 1.5V. The input impedance is 5 k Ω .

Pin 14 – (B-Y) chroma signal input (see pin 11)

Pin 15 – (B-Y) reference input (see pin 10)

Pin 16 – Ground

TDA 2190

LINEAR INTEGRATED CIRCUIT

COMPLETE TV SOUND CHANNEL WITH V.C.R. AND C.C.C.

The TDA 2190 is a monolithic integrated circuit in 16-lead dual in-line power dip. It performs the following functions:

- IF limiter-amplifier and low-pass filter.
- FM detector.
- DC volume control.
- AF preamplifier and AF power amplifier with thermal shut-down protection and choice of class B or C.C.C. operation mode
- VCR facility with common pin for input and output (playback and recording).
- VCR input and FM Detector DC switching for recording and playback.

The main features of TDA 2190 are:

- Suitable for all TV standards with FM modulation.
- Class B or constant current consumption (C.C.C.) operation mode.
- Video cassette recorder (VCR) facility according to DIN norms.
- DC or AC volume control.
- Physiological volume and tone controls (AC volume control mode).
- LC or ceramic filters can be used for input and detector networks.
- High output power (10W) easily achieved by very simple external stage.

Performance

- Very low spread of DC volume control.
- DC volume control thermally compensated.
- Very low current ripple in C.C.C. operation mode.
- 4W output power.
- No radiation problem

Safety

- Thermal protection of AF output stage.
- Short-circuit protection of VCR input-output pin.

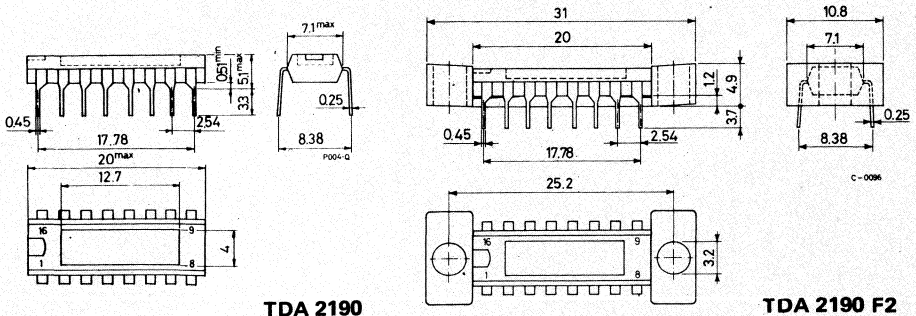
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage (pins 14 and 15)	28	V
V_i	Input peak voltage (pin 10)	1	V
V_3	Voltage at pin 3	V_s	V
I_o	Output peak current (non repetitive)	2	A
I_o	Output peak current (repetitive)	1.5	A
P_{tot}	Power dissipation at $T_{case} = 75^\circ\text{C}$	15	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBERS: TDA 2190
TDA 2190 F2

MECHANICAL DATA

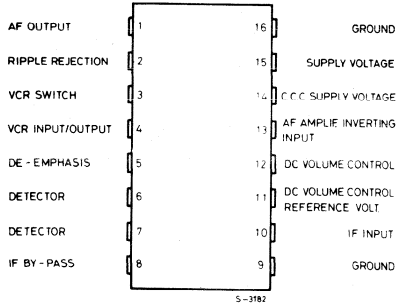
Dimensions in mm



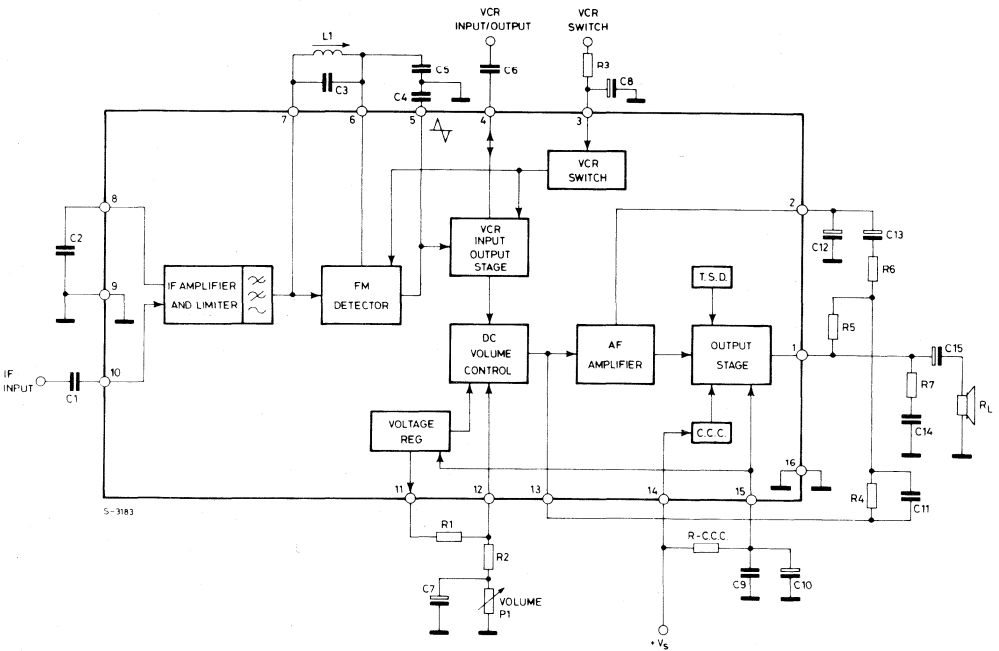
TDA 2190

TDA 2190 F2

CONNECTION DIAGRAM



BLOCK DIAGRAM



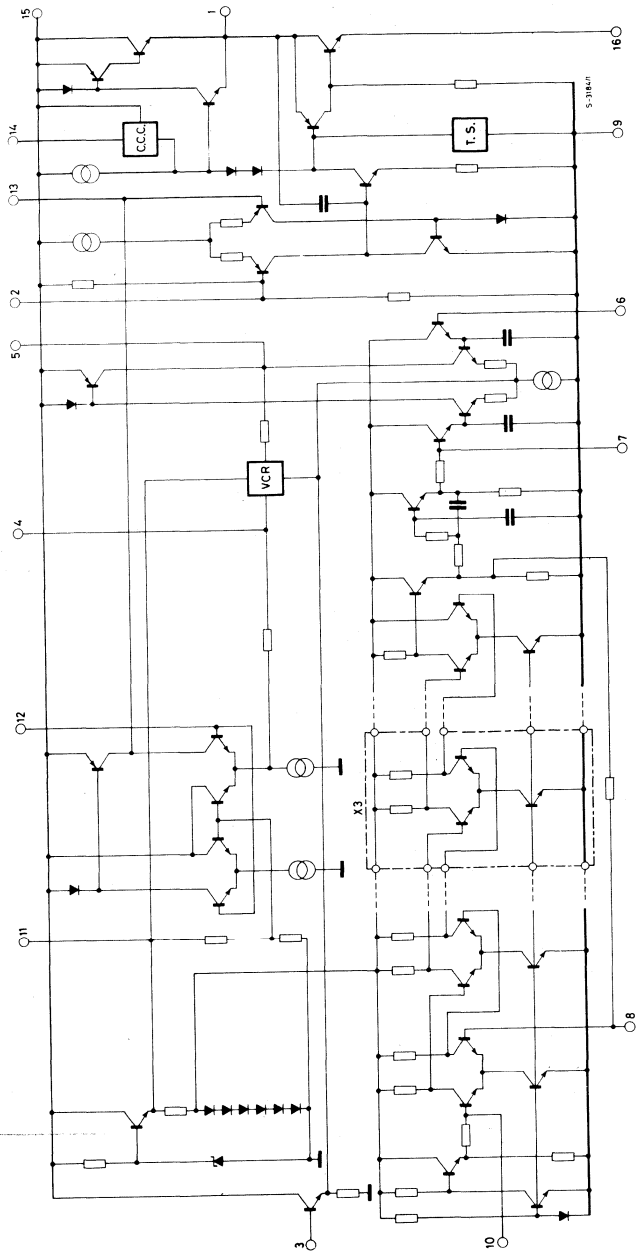
THERMAL DATA

$R_{th j-case}$ Thermal resistance junction-case

max. 5 °C/W

TDA 2190

SCHEMATIC DIAGRAM



TDA 2190

ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $V_s = 24V$, $f_o = 5.5\text{MHz}$, $f_m = 1\text{KHz}$, class B, $T_{amb} = 25^\circ\text{C}$, unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
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DC CHARACTERISTICS

V_s	Supply voltage (pins 14 and 15)		11		28	V
V_o	Quiescent output voltage (pin 1)	$V_s = 24V$ $P_1 = 0$	11	12	13	V
		$V_s = 12V$ $P_1 = 0$	5.1	6	6.9	
V_4	Pin 4 DC voltage	Playback and recording	5	6	7	V
V_{11}	DC volume control reference voltage	$P_1 = 0$ to $5\text{K}\Omega$	4	4.7	5.5	V
V_{14-15}	C.C.C. reference voltage (between pins 14 and 15)		0.9	1.1	1.3	V
I_d	Quiescent drain current	$V_s = 24V$ $P_1 = 0$	25	45	65	mA
		$V_s = 12V$ $P_1 = 0$	20	35	50	

IF AMPLIFIER AND DETECTOR

V_i (threshold)	Input limiting voltage at pin 10	$P_1 = 0$	$\Delta f = \pm 25\text{KHz}$		40	100	μV
V_5	Recovered audio voltage	$V_i \geq 1\text{mV}$ $P_1 = 0$	$\Delta f = \pm 25\text{KHz}$	240	400	480	mV
AMR	Amplitude modulation rejection	$V_i = 1\text{mV}$ $m = 0.3$	$\Delta f = \pm 50\text{KHz}$		62		dB
R_i	Input resistance (pin 10)	$V_i = 1\text{mV}$			10		$\text{K}\Omega$
C_i	Input capacitance (pin 10)	$V_i = 1\text{mV}$			5		pF

DC VOLUME CONTROL

A	Volume attenuation (resistance control)	$P_1 = 0\Omega$ $P_1 = 2.3\text{K}\Omega$ $P_1 = 5\text{K}\Omega$		80 22	90 30 0	38 3	dB dB dB
V_C	Control voltage	A = 90 dB A = 30 dB A = 0 dB			0 1.5 3		V V V
$\frac{\Delta A}{\Delta T_{tab}}$	Volume attenuation thermal drift (resistance control)	$T_{tab} = 25$ to 85°C $P_1 = 2.3\text{K}\Omega$			-0.05		$\frac{\text{dB}}{^\circ\text{C}}$

AUDIO FREQUENCY AMPLIFIER

P_o	Output power in class B mode	$d = 10\%$					
		$V_s = 24V$	$R_L = 16\Omega$		4.1		W
		$V_s = 12V$	$R_L = 8\Omega$		1.5		W
		$d = 2\%$					
		$V_s = 24V$	$R_L = 16\Omega$		3		W
		$V_s = 12V$	$R_L = 8\Omega$		1.2		W

TDA 2190

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
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AUDIO FREQUENCY AMPLIFIER (continued)

P_o	Output power in C.C.C. mode	$d = 10\%$ $V_s = 24V$ $V_s = 12V$	$R_L = 16\Omega$ $R_L = 8\Omega$		3.5 1.2	W W
B	Frequency response of audio amplifier (-3 dB)	$P_o = 1W$	$R_L = 16\Omega$		50 ÷ 10000	Hz
SVR	Supply voltage rejection ratio	$P_1 = 0$ $R_L = 16\Omega$	$V_i = 1 mV$ $f_{ripple} = 100 Hz$	$\Delta f = 0$	50	dB

V.C.R.

V_3	Input switching voltage for recording				2	V	
V_3	Input switching voltage for playback			8.5		V	
R_3	Input resistance	$V_3 = 1$ to 10V		50	100	K Ω	
V_{4i}	Input voltage (playback)	$V_3 \geq 8.5V$ $P_{out} = 1W$	$P_1 = 5 K\Omega$	45	90	180	mV
V_{4out}	Output voltage (recording)	$V_3 \leq 2V$ $P_1 = 0$	$V_i = 1 mV$ $\Delta f = \pm 25 KHz$	240	400	480	mV
R_{4i}	Input resistance (playback)	$V_3 \geq 8.5V$		10	13		K Ω
R_{4out}	Output resistance (recording)	$V_3 \leq 2V$			140		Ω
d	Total harmonic distortion of pin 4 output signal	$P_1 = 0$ $\Delta f = \pm 25 KHz$	$V_i = 1 mV$ $V_3 \leq 2V$		0.5		%
SVR	Supply voltage rejection at output pin 4	$P_1 = 0$ $\Delta f = 0$	$V_3 \leq 2V$ $f_{ripple} = 100 Hz$	$V_i \geq 1 mV$	50		dB
$\frac{S+N}{N}$	Signal and noise to noise ratio (pin 4)	$V_3 \leq 2V$ $\Delta f = \pm 50 KHz$	$V_i \geq 1 mV$	50	67		dB

OVERALL CIRCUIT

$\frac{S+N}{N}$	Signal and noise to noise ratio	$V_i \geq 1 mV$ $\Delta f = \pm 50 KHz$	$V_o = 4V$	50	67		dB
d	Distortion	$P_o = 50 mW$ $V_s = 24V$ $V_s = 12V$	$\Delta f = \pm 25 KHz$ $R_L = 16\Omega$ $R_L = 8\Omega$		0.5 0.5		% %

TEST CIRCUIT

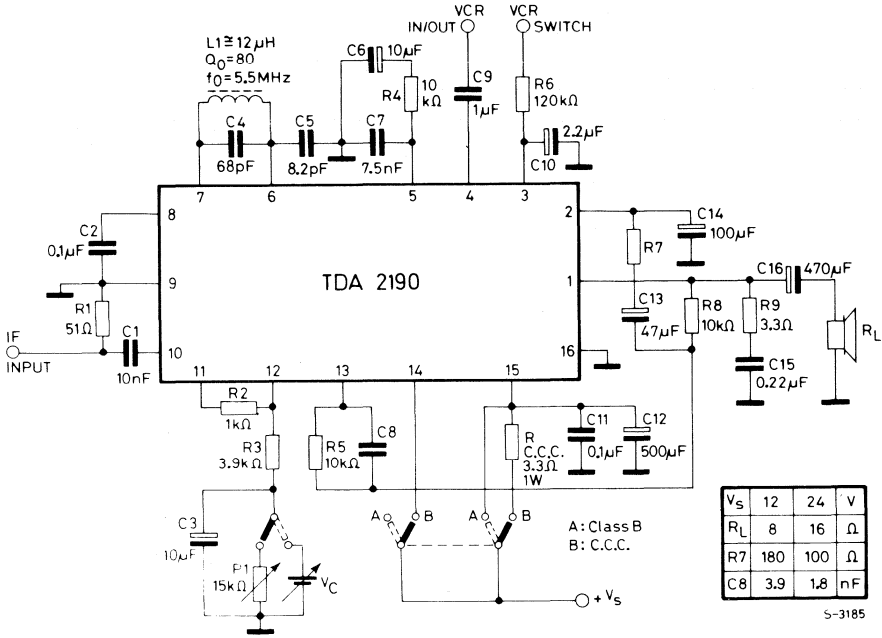


Fig. 1 - Relative audio output and signal to noise ratio vs. input signal

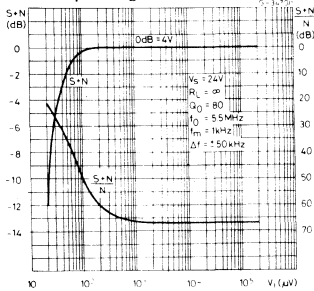


Fig. 2 - AM rejection vs. input signal

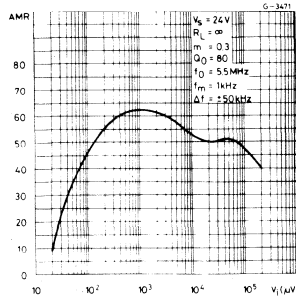
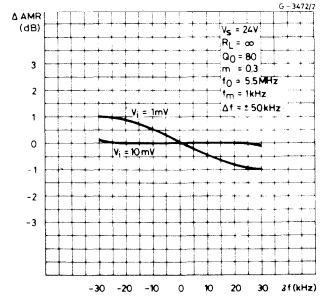


Fig. 3 - Δ AM rejection vs. tuning frequency change



TDA 2190

Fig. 4 - Detected audio voltage (pin 5) vs. unloaded Q-factor of the detector coil

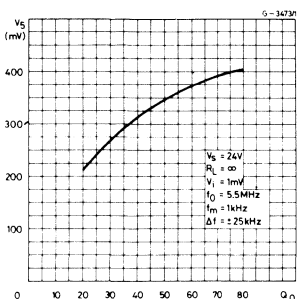


Fig. 5 - Distortion of the detected signal (pin 5) vs. unloaded Q-factor of the detector coil

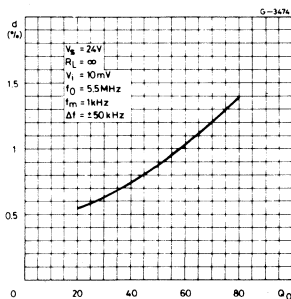


Fig. 6 - Output voltage attenuation vs. DC volume control resistance (P1) and vs. DC volume control voltage (V_C)

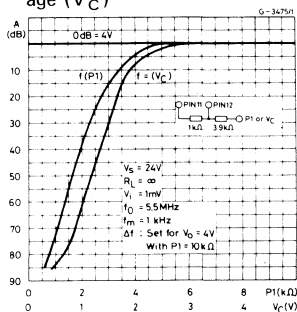


Fig. 7 - Distortion vs. frequency deviation

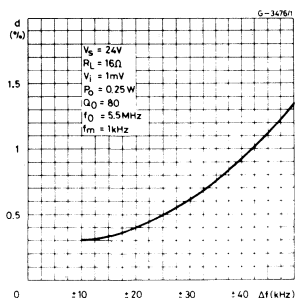


Fig. 8 - Distortion vs. tuning frequency change

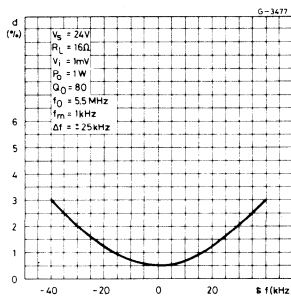


Fig. 9 - Switch-off attenuation of the VCR at pin 4 vs. switch-off voltage at pin3

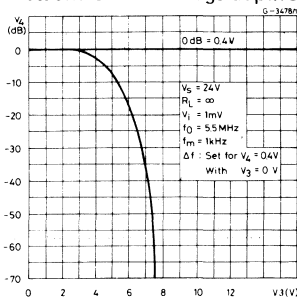


Fig. 10 - Overall frequency response

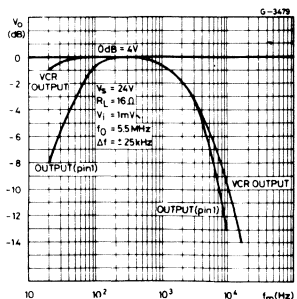


Fig. 11 - Audio amplifier frequency response

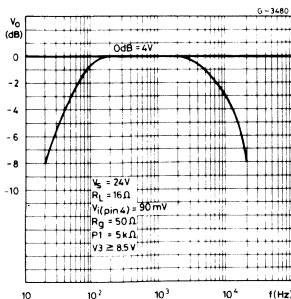


Fig. 12 - Distortion vs. output power ($V_5 = 24V$ and $R_L = 16\Omega$)

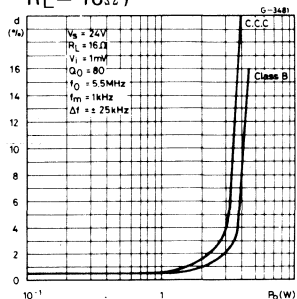


Fig. 13 - Distortion vs. output power ($V_S = 12V$ and $R_L = 8\Omega$)

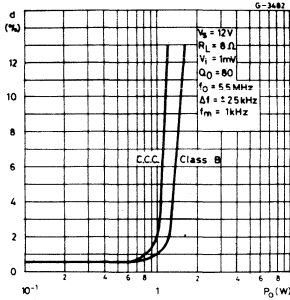


Fig. 14 - Output power vs. supply voltage (class B mode)

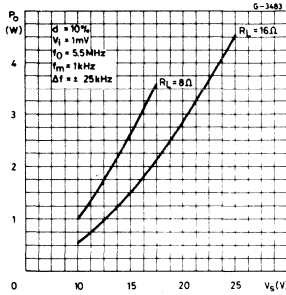


Fig. 15 - Maximum power dissipation vs. supply voltage (sine wave operation; class B mode)

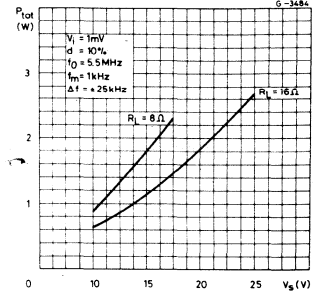


Fig. 16 - Power dissipation and efficiency vs. output power (class B mode)

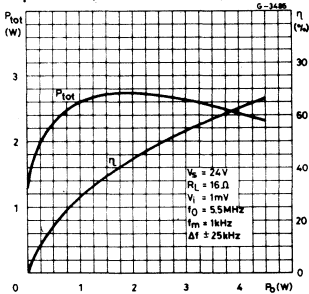


Fig. 17 - Output power vs. supply voltage (C.C.C. mode)

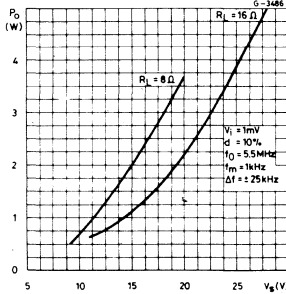


Fig. 18 - Power dissipation and efficiency vs. output power (C.C.C. mode)

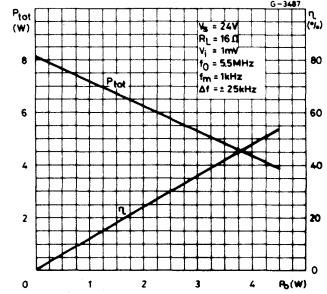


Fig. 19 - Current ripple vs. R-CCC value (C.C.C. mode only)

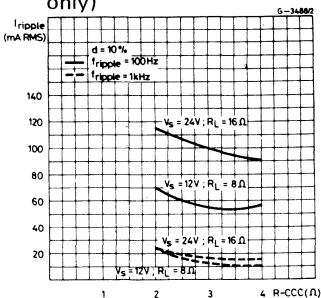


Fig. 20 - Current ripple vs. signal frequency (C.C.C. mode only)

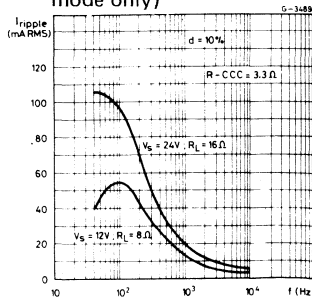
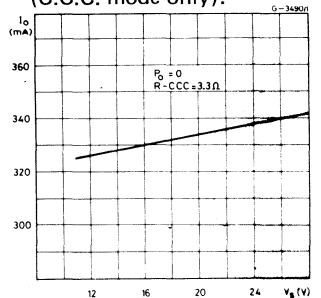


Fig. 21 - Quiescent drain current vs. supply voltage (C.C.C. mode only)



TDA 2190

Fig. 22 – Quiescent output voltage (pin 1) vs. supply voltage

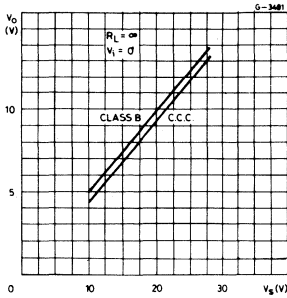


Fig. 23 – Supply voltage ripple rejection vs. volume control attenuation

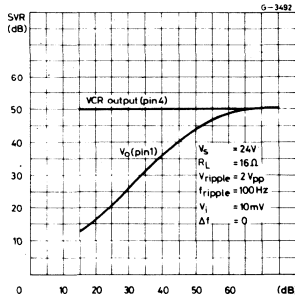
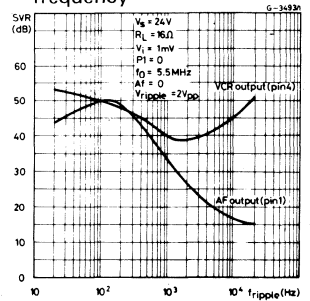


Fig. 24 – Supply voltage ripple rejection at the AF and VCR outputs vs. ripple frequency



APPLICATION INFORMATION (Refer to the block diagram)

IF amplifier and limiter

The IF sound signal is amplified and limited by a chain of 6 differential stages. To avoid the possibility of radiation problems an active low pass filter has been integrated to eliminate the high frequency harmonics from the signal sent to the detector.

Pin 10 is the non inverting input of the amplifier-limiter and it is used as input of the IF sound signal coming from the input network which can employ either LC or ceramic filters. The typical input impedance of pin 10 is $10 K\Omega$, $5 pF$ at $f_0 = 5.5 MHz$.

Pin 8 is the inverting input, of the amplifier-limiter. The DC negative feedback of the amplifier is applied internally to this pin which must therefore be decoupled by means of a by pass capacitor toward ground.

FM detector

Signal detection is obtained by means of a peak differential detector which enables radiation problems to be minimized.

Pin 7 is the first input of the peak differential detector and it is the output of the low pass filter. The typical output impedance is $2.7 K\Omega$.

Pin 6 is the second input of the peak differential detector. This pin must be supplied with the same DC voltage as the other input (pin 7) and this is done by coil L1. External components L1 C3 and C5 transform the frequency variations into amplitude variations useful to drive the detector. Network L1 C3 C5 has two resonance frequencies:

$$f_1 \text{ series resonance for } X_{C5} = \frac{X_{L1} \cdot X_{C3}}{X_{C3} + X_{L1}}$$

$$f_2 \text{ parallel resonance for } X_{L1} = X_{C3}$$

APPLICATION INFORMATION (continued)

Coil L₁ must be tuned at frequency $f_o = \text{IF sound}$, equidistant from frequencies f_1 and f_2 to which the peaks of the "S" response of the detector correspond. The separation between the peaks is defined by

$$\text{the ratio } \frac{f_2^2}{f_1^2} = 1 + \frac{C5}{C3}.$$

Network L1 C3 C5 can obviously be substituted by a ceramic filter.

Pin 5 is the output of the FM detector. Its output impedance of 20 K Ω , in combination with capacitor C4 connected between pin 5 and ground, defines the time constant of the deemphasis. The detector "S" curve is visible at pin 5. Improved AMR performance can be obtained by connecting a 10 K Ω 10 μ F RC series network between pin 5 and ground.

VCR

This function, required by receivers capable of recording complete TV signals, is made in accordance with DIN Norms. A single pin (pin 4) acts both as output of the signal to be recorded and as input of the signal to be played back. The function of this pin is changed by means of a control, applied to pin 3, consisting of two different levels of DC voltage. The operating conditions of pins 3 and 4 are:

Mode	VCR Switch pin 3	Function of pin 4	Impedance of pin 4	Signal at pin 4
Recording	$V_3 \leq 2V$	Output	$R4 = 140\Omega$	$V_4 = 400 \text{ mV}$
Playback	$V_3 \geq 8.5V$	Input	$R4 = 13 \text{ K}\Omega$	$V_4 = 90 \text{ mV}$

In the recording state the output signal at pin 4 is independent of the volume control, while during playback the signal applied at pin 4 is regulated by the volume control before being sent to the audio amplifier.

Pin 3, input of the VCR switch, has an impedance greater than 50K Ω for any value of input voltage. Control pulses at pin 3 with very sharp edges cause temporary unbalancing of the circuit and produce audible signals. This effect is eliminated by means of R3 C8 which slows down the control edges. In the playback state the IF sound signal coming from the detector is automatically blocked by the VCR switch.

Pin 4, input-output of the audio signal, has a DC typical voltage of 6V. C6 must therefore be used to decouple it from the VCR.

The output signal of pin 4 can be used to perform the AC volume control (fig. 31). The potentiometer must be connected between pin 4 and ground and the slider must be connected to pin 13 after DC decoupling.

DC volume control

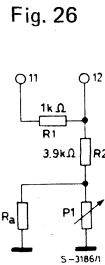
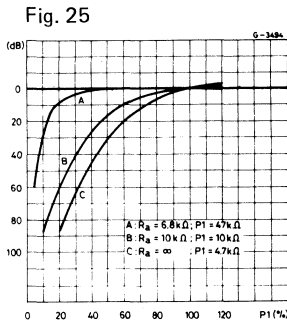
The audio signal coming from the FM detector or from the VCR is adjusted in amplitude by means of a DC controlled active attenuator. The attenuation can be changed either by means of a potentiometer or by means of a DC voltage.

Pin 11 supplies the reference voltage for the volume control.

This voltage is between 4V and 5.5V and has a thermal coeff. of +0.25%/°C. The maximum current which can be supplied by pin 11 is 10 mA.

APPLICATION INFORMATION (continued)

Pin 12 is the input of the DC volume control. To minimize the attenuation spreads, the volume control network R1, R2, P1 is supplied by the reference voltage of pin 11. The attenuation of the signal is inversely proportional to the voltage applied at pin 12; therefore maximum attenuation is for $V_{12} = 0$ or for $P1 = 0$. Capacitor C7, connected in parallel to the volume potentiometer, eliminates any signals or spikes picked up by the connection wires of the potentiometer. The volume control characteristic depends on the configuration and on the values of the components of the network connected to pins 11 and 12. The suggested values are: $R1 = 1\text{ K}\Omega$ $R2 = 3.9\text{ K}\Omega$ and $P1 = 5\text{ K}\Omega$ with linear variation; with this network a linear variation of the output power is obtained. Different slopes of the volume control and relative networks are shown in figs. 25 and 26.



The volume can also be controlled by means of a DC voltage applied between resistor R2 and ground instead of potentiometer P1. Using this configuration, volume variation can be obtained by means of remote control as shown in fig. 36.

AF amplifier

The AF amplifier consists of an operational amplifier with thermally protected (thermal shut down) output stage. By using a simple external variant the power stage can be made to operate in class B or in constant current consumption.

Pin 1 is the output of the power amplifier. The network which defines the gain and the band of the audio amplifier is connected between pins 1, 2 and 13.

The input voltage of the amplifier is $I \cdot R4$, where I is the signal output current of the DC volume control block. The closed loop gain of the amplifier is given by $G_v = R5/R6$;

Therefore the output voltage is given by

$$V_o = I \cdot R4 \cdot \frac{R5}{R6}$$

Changing the values of these resistors, different output voltage (i.e. different closed loop gain) can be obtained.

When impedances, rather than pure resistors, are used, the closed loop gain is changed with frequency. In particular at high frequencies the gain is reduced by capacitor C11 and at low frequencies it is reduced by capacitor C13.

The Boucherot cell R7 C14 guarantees the stability of the circuit in all the operating conditions.

Pin 2, the non inverting input of the audio amplifier, is connected to an integrated voltage divider which fixes its DC voltage at $V_s/2$.

APPLICATION INFORMATION (continued)

Since the voltage of pin 2 is the reference of the input differential stage of the audio amplifier, both the voltage of pin 13 and the voltage of pin 1 are equal to $V_s/2$. Capacitor C12, connected between pin 2 and ground, has the dual function of eliminating the audio signals from pin 2 and providing the supply voltage ripple rejection.

Pin 13 is the inverting input of the audio preamplifier; the output of the DC volume control is also connected to this pin.

Supply

The device can operate either in class B or in C.C.C. mode. In class B the supply current is highly variable and depends on the power supplied to the load. The supply must therefore be well filtered to prevent modulation effects on the supply itself which may influence other circuits in the TV. In C.C.C. mode supply current is constant and the supply system can therefore be simplified; for example the sound channel can be supplied directly by the line transformer without problems of modulation of the picture size.

Pin 15 is the main supply of the device; when it is connected directly to the power supply and pin 14 is left open, the circuit operates in class B.

Pin 14 is the supply point for C.C.C. The reference system, connected between pin 14 and pin 15, determines a constant voltage of 1.1V between the two pins. To make the device operate in C.C.C. mode, pin 14 must be connected to the supply and a resistor R-CCC must be connected between pin 14 and pin 15; the value of this resistor defines the quiescent current $I_{CCC} = 1.1V/R-CCC$.

Pin 9 is the main ground of the circuit.

Pin 16 is the ground of the power output stage only.

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APPLICATION INFORMATION (continued)

Fig. 27 - Typical application circuit (class B mode)

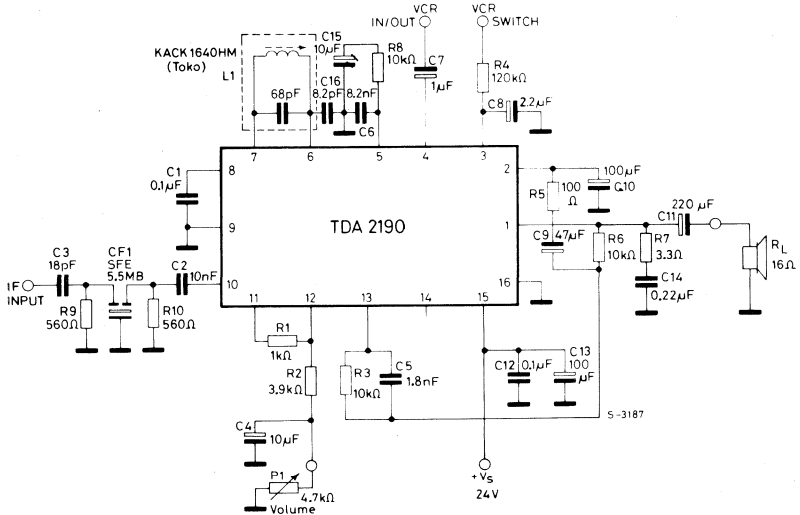
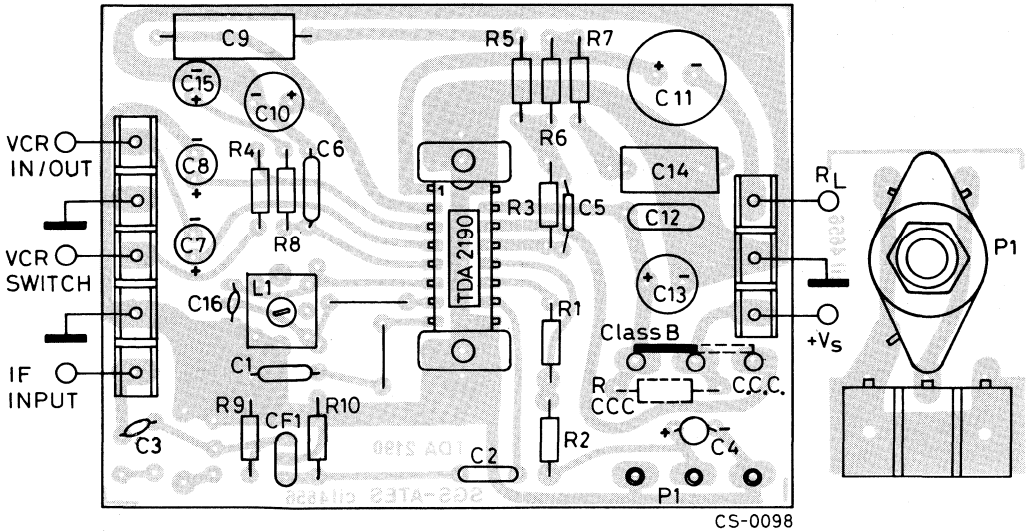


Fig. 28 - P.C. board and component layout of the circuit shown in fig. 27 (1:1 scale)



APPLICATION INFORMATION (continued)

Fig. 29 - Application using a ceramic discriminator and an LC network at the IF input (C.C.C. mode)

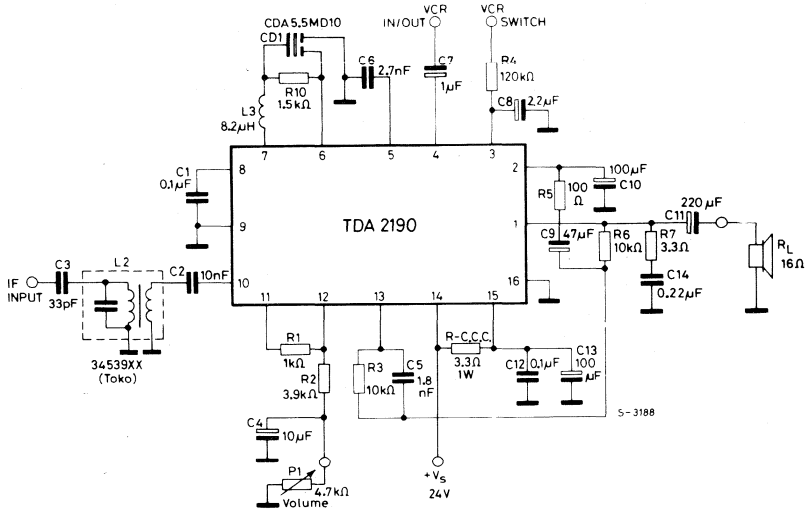
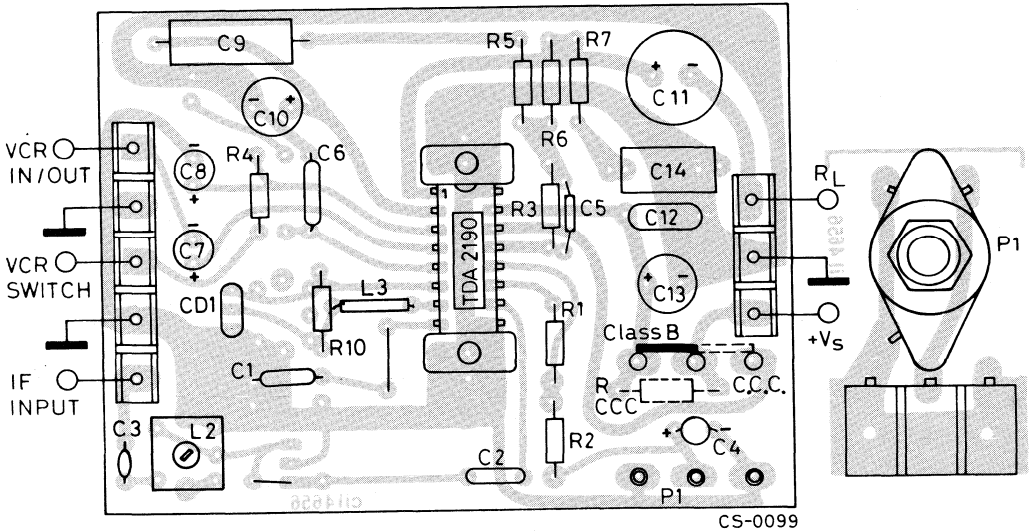


Fig. 30 - P.C. board and component layout of the circuit shown in fig. 29. (1:1 scale)



APPLICATION INFORMATION (continued)

Fig. 33 – Application circuit with physiological volume control

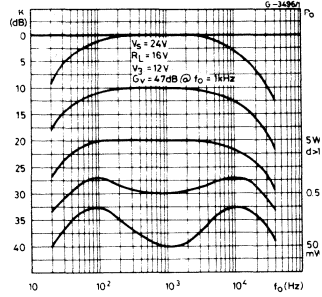
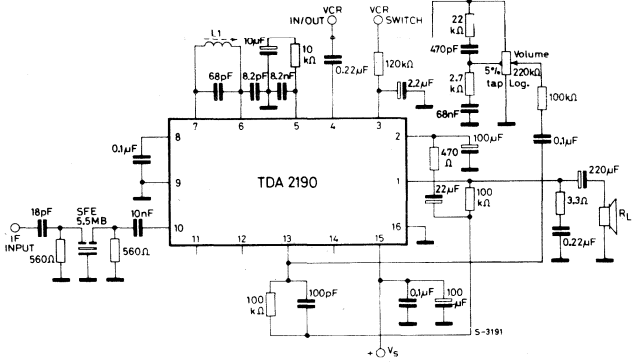
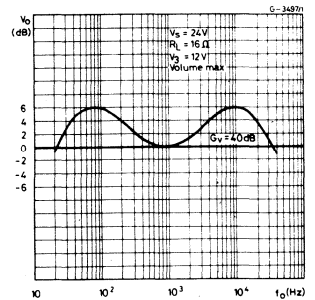
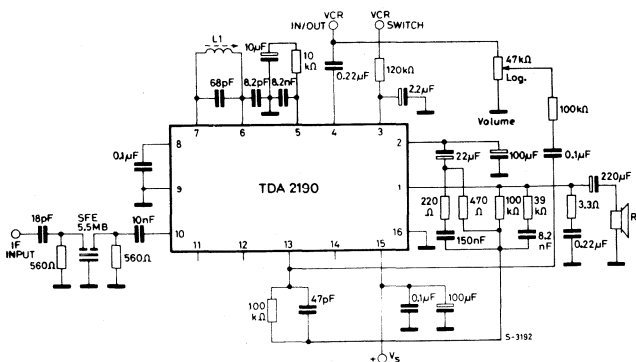


Fig. 34 – Application circuit with fixed bass and treble boost



MOUNTING INSTRUCTIONS

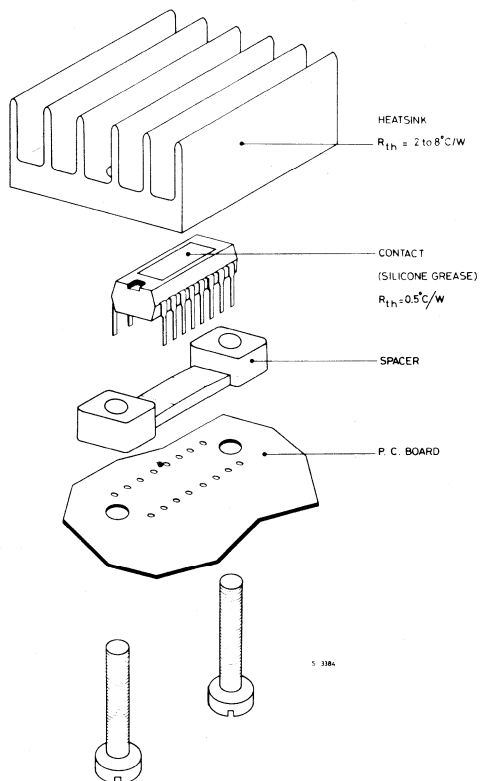
The power dissipated in the circuit must be removed by adding an external heatsink as shown in figs. 37 and 38.

The system for attaching the heatsink is very simple: it uses a plastic spacer which is supplied with the device on request (TDA 2190 F2).

Thermal contact between the copper slug (of the package) and the heatsink is guaranteed by the pressure which the screws exert via the spacer and the printed circuit board; this is due to the particular shape of the spacer.

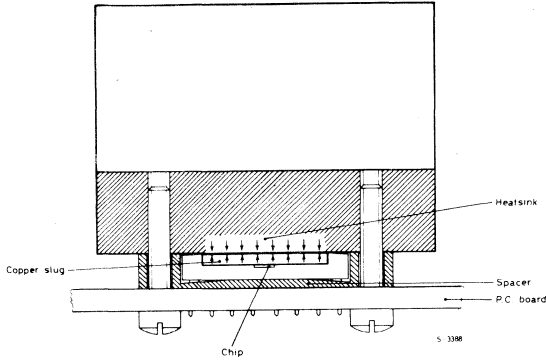
Note : The most negative supply voltage is connected to the copper slug, hence to the heatsink (because it is in contact with the slug).

Fig. 37 - Mounting system



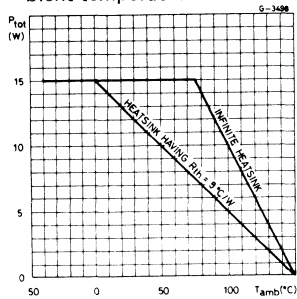
MOUNTING INSTRUCTIONS (continued)

Fig. 38 – Cross-section of mounting system



The maximum allowable power dissipation depends upon the size of the external heatsink (i.e. its thermal resistance): fig. 39 shows this dissipable power as a function of ambient temperature for a heatsink having $5^{\circ}\text{C}/\text{W}$.

Fig. 39 – Maximum allowable power dissipation vs. ambient temperature



LINEAR INTEGRATED CIRCUIT

Hi-Fi DUAL PREAMPLIFIER

The TDA2310 is a dual high quality **class A** preamplifier intended for extremely low distortion application in Hi-Fi systems.

The TDA2310 is a monolithic integrated circuit in a 14-lead dual-in-line plastic package and its main features are:

- Very high dynamic range
- Very low distortion
- High open loop bandwidth
- Very low noise
- No pop-noise
- High slew-rate: $14\text{V}/\mu\text{s}$ ($G_v = 30\text{ dB}$) - $50\text{V}/\mu\text{s}$ ($G_v = 50\text{ dB}$)
- Large output voltage swing
- Single or split supply operation
- Output short circuit protection

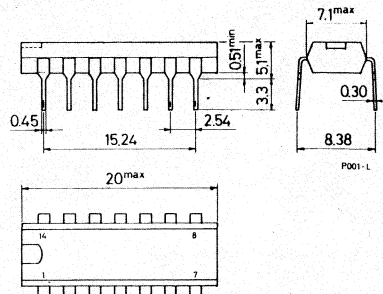
ABSOLUTE MAXIMUM RATINGS

V_s	DC supply voltage	± 22	V
V_s	Operating supply voltage	± 20	V
V_{cm}	Common mode input voltage	± 15	V
V_i	Differential input voltage	± 5	V
P_{tot}	Total power dissipation at $T_{amb} < 70^\circ\text{C}$	800	mW
T_j, T_{stg}	Junction and storage temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBER: TDA2310

MECHANICAL DATA

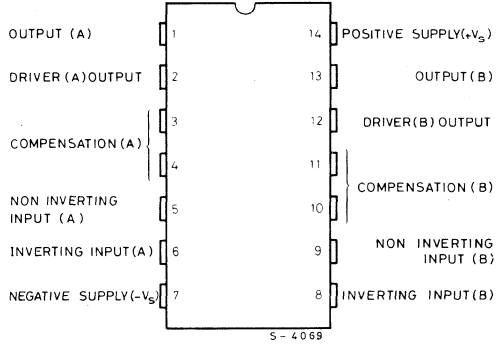
Dimensions in mm.



TDA 2310

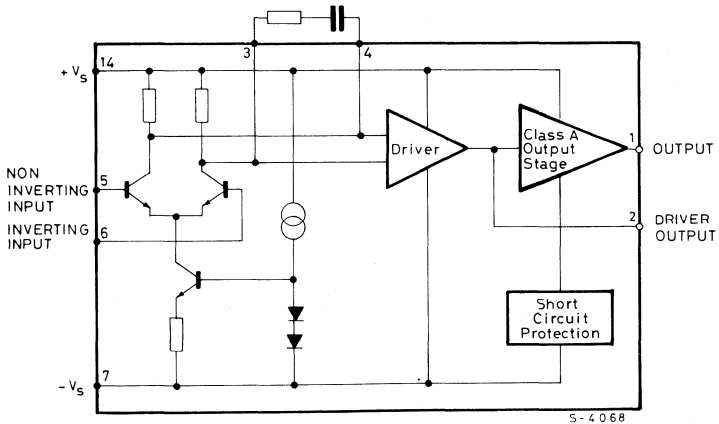
CONNECTION DIAGRAM

(top view)



BLOCK DIAGRAM

(one section)



THERMAL DATA

$R_{thj-amb}$	Thermal resistance junction-ambient	max.	100 °C/W
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Fig. 1 - Gain and distortion test

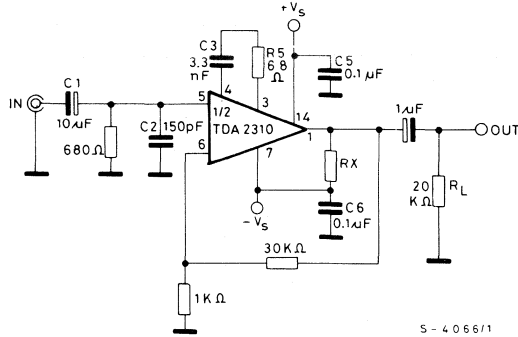
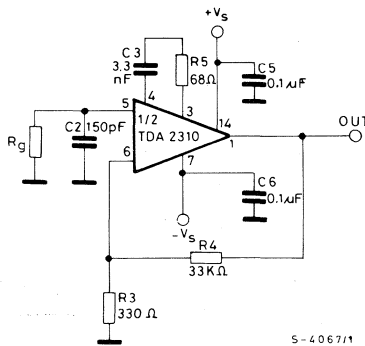


Fig. 2 - Noise test



ELECTRICAL CHARACTERISTICS (Refer to the Test circuit of fig. 1, $T_{amb} = 25^{\circ}\text{C}$, $V_s = \pm 15\text{V}$, $G_v = 30\text{dB}$, $R_L = 20\text{K}\Omega$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s	Supply voltage	± 5		± 20	V
I_s	Supply current		10	15	mA
I_b	Input bias current		0.2	1	μA
I_{os}	Input offset current		50	300	nA
V_{os}	Input offset voltage		1	3	mV

TDA 2310

ELECTRICAL CHARACTERISTICS (continued)

Parameter		Test conditions		Min.	Typ.	Max.	Unit
G _V	Voltage gain (open loop)	f = 1KHz	No compensation		85		dB
		f = 20KHz			85		dB
ΔG _V	Voltage gain spread (closed loop)	f = 1KHz			±0.2		dB
		f = 100KHz			±0.5		dB
R _i	Input resistance	f = 1KHz			5		MΩ
R _o	Output resistance				10		Ω
V _{pp}	Output voltage swing (peak to peak)	d = 1%	f = 1KHz		24		V
			f = 100KHz		22		V
V _o	Output voltage (rms)	R _x = 8.2KΩ	f = 1KHz	6	8		V
			f = 20KHz	6	8		V
BW	Power bandwidth	V _o = 20 V _{pp} , R _x = 8.2 KΩ			160		KHz
SR	Slew rate	G _V = 30dB			14		V/μs
		G _V = 50dB (C ₃ = 330pF, R ₅ = 470Ω)			50		
d	Total harmonic distortion	V _o = 3V	f = 1KHz		0.035		%
			f = 20 KHz		0.035		%
d ₂	Second order CCIF intermodulation distortion	V _{o1} = 1V V _{o2} = 1V	f ₂ - f ₁ = 1 KHz		0.01	0.1	%
d ₃	Third order CCIF intermodulation distortion	f ₁ = 14KHz f ₂ = 15KHz	2f ₁ - f ₂ = 13 KHz		0.03	0.1	%
e _N	* Total input noise	R _g = 600Ω R _g = 3.3KΩ ^(°)			0.6 1.0	0.8	μV
		R _g = 600Ω R _g = 3.3KΩ ^(°°)			0.75 1.2		μV
S/N	* Signal to noise ratio	V _o = 500mV	R _g = 3.3K R _g = 600 ^(°) R _g = 0		74 78 80		dB
			R _g = 3.3K R _g = 600 ^(°°) R _g = 0		72 76 78		dB
C _s	Channel separation	f = 20KHz R _g = 600Ω			100		dB
CMR	Common mode rejection	R _g = 600Ω			95		dB
SVR	Supply voltage rejection	R _g = 600Ω			85		dB
I _{sh}	Output short circuit current				15		mA

(*) Test circuit of fig. 2 (G_V = 40 dB)

(°) BW = curve A

(°°) BW = 22Hz to 22KHz

Fig. 3 - Harmonic distortion vs. output level.

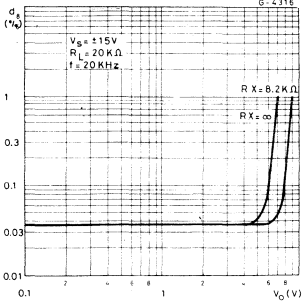


Fig. 4 - Harmonic distortion vs. frequency.

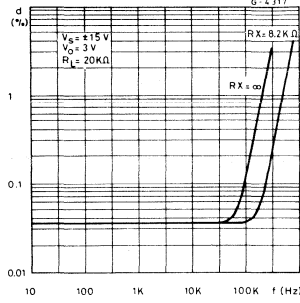


Fig. 5 - Output voltage swing vs. frequency.

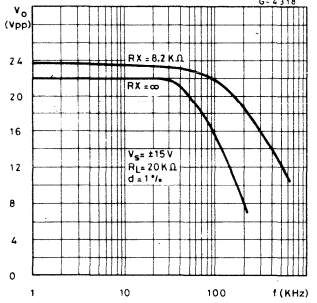


Fig. 6 - Output voltage swing vs. load resistance.

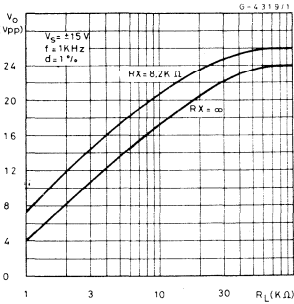


Fig. 7 - Total input noise vs. source resistance.

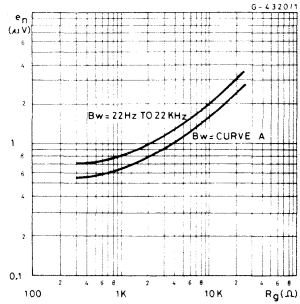


Fig. 8 - Noise density vs. frequency.

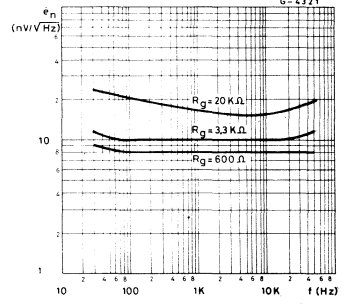


Fig. 9 - Open loop frequency response.

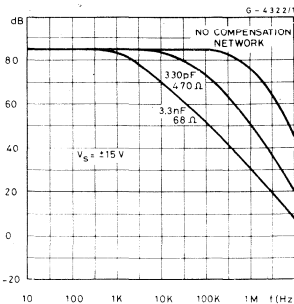


Fig. 10 - Closed loop gain vs. frequency.

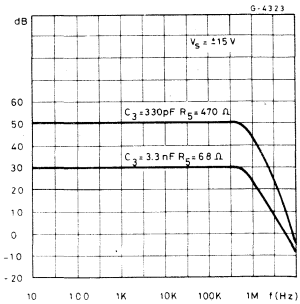
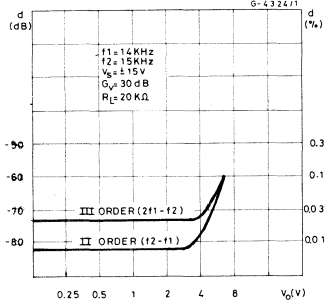


Fig. 11 - Two tone CCIF intermod. distortion.



TDA 2310

APPLICATION INFORMATION

Fig. 12 - Very low dynamic distortion stereo RIAA preamplifier.

$V_s = \pm 15V$

RIAA frequency response (20Hz to 20KHz) = ± 0.5 dB

Harmonic distortion = 0.02% ($f = 20KHz$)

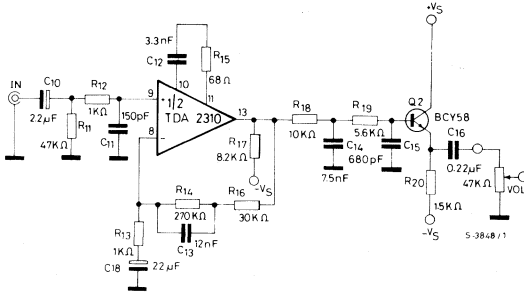
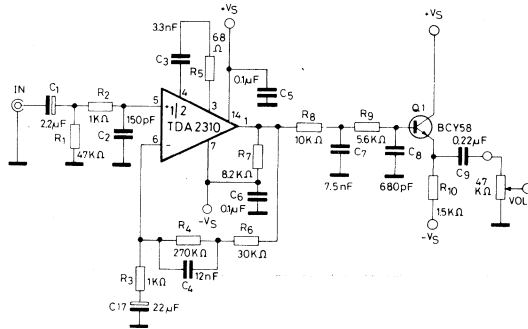


Fig. 13 - RIAA preamplifier response.

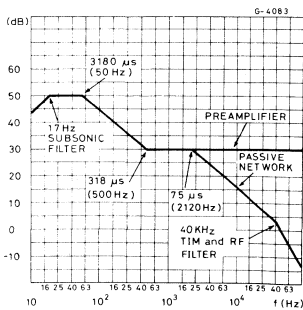


Fig. 14 - Two tone intermodulation distortion vs. input level.

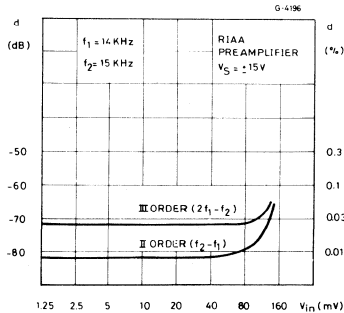
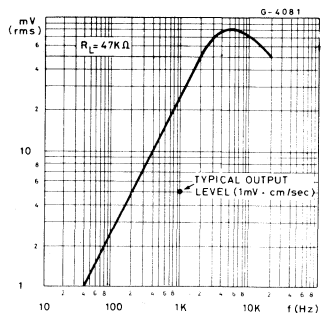
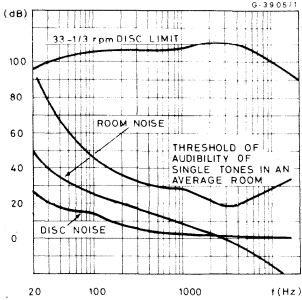


Fig. 15 - Maximum output level of high quality magnetic cartridge vs. frequency.



APPLICATION INFORMATION (continued)

Fig. 16 - Dynamic range of disc music.

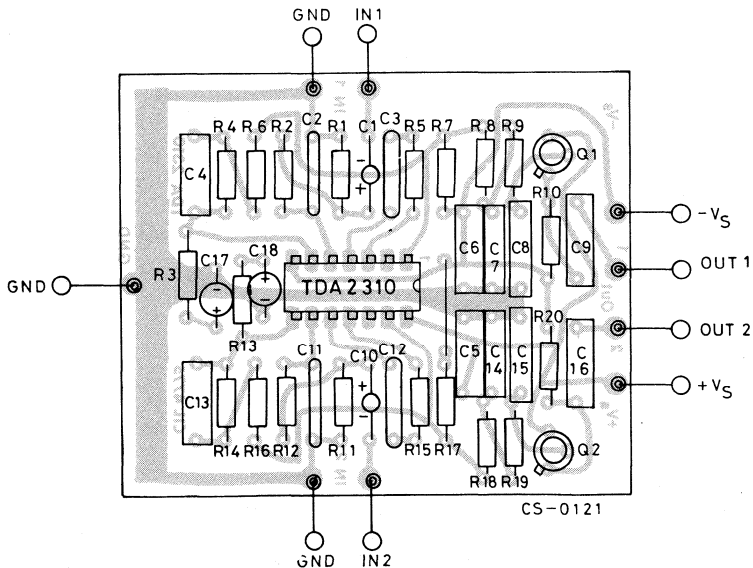


As shown in fig. 15 the maximum expected output level of an high quality magnetic cartridge playing modern discs is lower than 80mV rms.

The dynamic range needed is about 70dB (fig. 16).

The TDA2310 is perfectly suited to RIAA preamplifier applications due to the ~100 dB dynamic range (150mV input 0.1% distortion to 1 μ V noise).

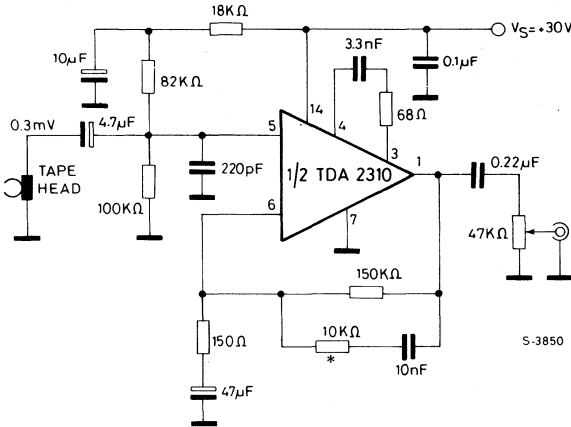
Fig. 17 - PC board and components layout of RIAA preamplifier (1:1 scale)



TDA 2310

APPLICATION INFORMATION (continued)

Fig. 18 - Hi-Fi tape preamplifier (EQ. = 70 μ s).



* 18K Ω for EQ = 120 μ s.

Fig. 19 - Frequency response of graphic equalizer of fig.20

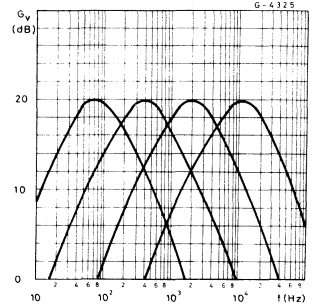
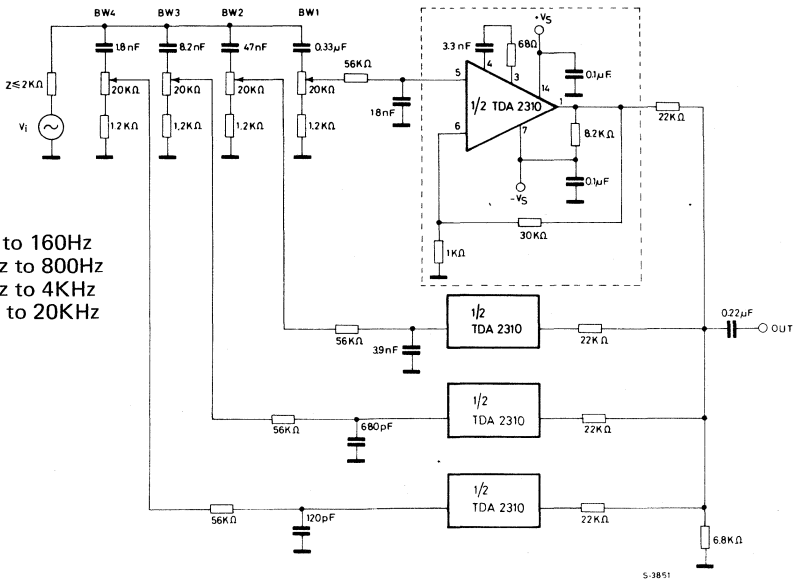


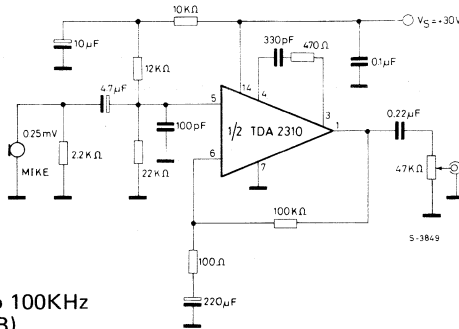
Fig. 20 - Four band graphic equalizer



BW1 = 30Hz to 160Hz
 BW2 = 160Hz to 800Hz
 BW3 = 800Hz to 4KHz
 BW4 = 4KHz to 20KHz

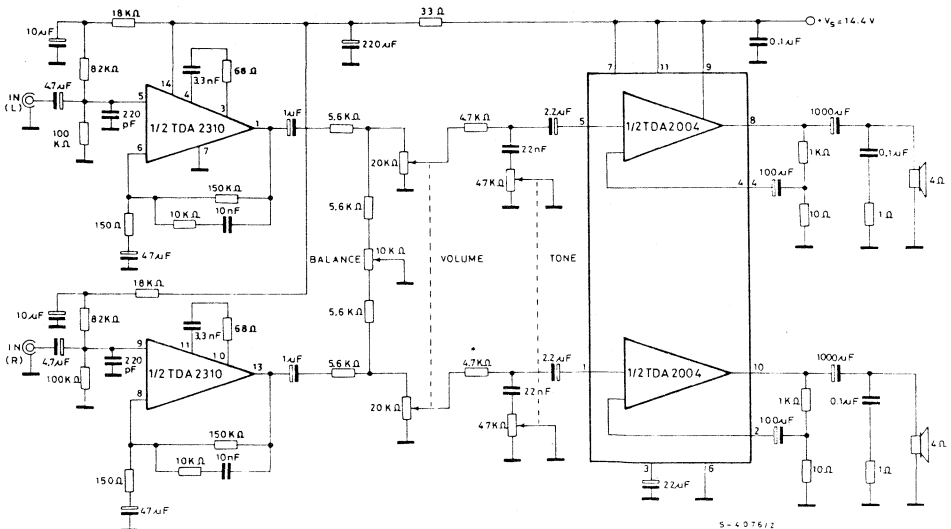
APPLICATION INFORMATION (continued)

Fig. 21 - High slew-rate microphone preamplifier.



$G_v = 60\text{dB}$
 $B = 15\text{Hz to } 100\text{kHz}$
 $(\pm 0.5\text{dB})$
 $SR = 50\text{V}/\mu\text{s}$
 $V_o = 5\text{V} (d = 0.05\%, f = 20\text{kHz})$

Fig. 22 - High quality, 10 + 10W car radio tape player



TDA 2310

APPLICATION INFORMATION (continued)

The table shows the suggested compensation networks depending on the slew-rate and gain required in the application.

Slew-Rate (V/ μ s)	G_V min. (dB)	Compensation Network	Note
50	50	<p>S-4071</p>	$R = 470\Omega$ $C = 330\text{pF}$ High gain Applications
14	30	<p>S-4071</p>	$R = 68\Omega$ $C = 3.3\text{nF}$ RIAA Preamplifier
14	10	<p>S-4072/1</p>	Inverting Configuration $R_1 = 56\text{K}\Omega$ $R_2 = 180\text{K}\Omega$ $R_3 = 680\Omega$ $C_1 = 10\text{nF}$
	0	$R = 68\Omega$ $C = 3.3\text{nF}$	
5	20	<p>S-4071</p>	$R = 33\Omega$ $C = 10\text{nF}$ Low Slew-Rate Applications
2	6	<p>S-4071</p>	$R = 10\Omega$ $C = 47\text{nF}$

TDA 3190

LINEAR INTEGRATED CIRCUIT

COMPLETE TV SOUND CHANNEL

The TDA3190 is a monolithic integrated circuit in a 16-lead dual in-line plastic package. It performs all the functions needed for the TV sound channel:

- IF limiter-amplifier
- DC volume control
- Active low-pass filter
- AF preamplifier
- FM detector
- AF output stage

The TDA 3190 can give an output power of 4.2W ($d = 10\%$) into a 16Ω load at $V_s = 24V$, or 1.5W ($d = 10\%$) into an 8Ω load at $V_s = 12V$. This performance, together with the FM-IF section characteristics of high sensitivity, high AM rejection and low distortion, enables the device to be used in almost every type of television receivers.

The device has no irradiation problems, hence no external screening is needed.

The TDA 3190 is a pin to pin replacement of TDA 1190Z.

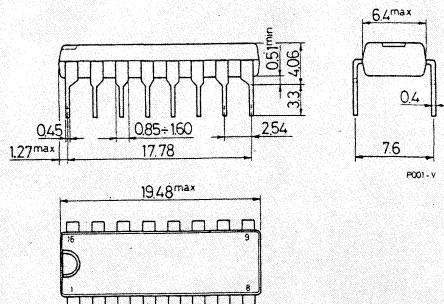
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage (pin 10)	28	V
V_i	Input signal voltage (pin 1)	1	V
I_o	Output peak current (non-repetitive)	2	A
$I_{o,r}$	Output peak current (repetitive)	1.5	A
P_{tot}	Power dissipation: at $T_{pins} = 90^\circ C$	4.3	W
	at $T_{amb} = 70^\circ C$ (free air)	1	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ C$

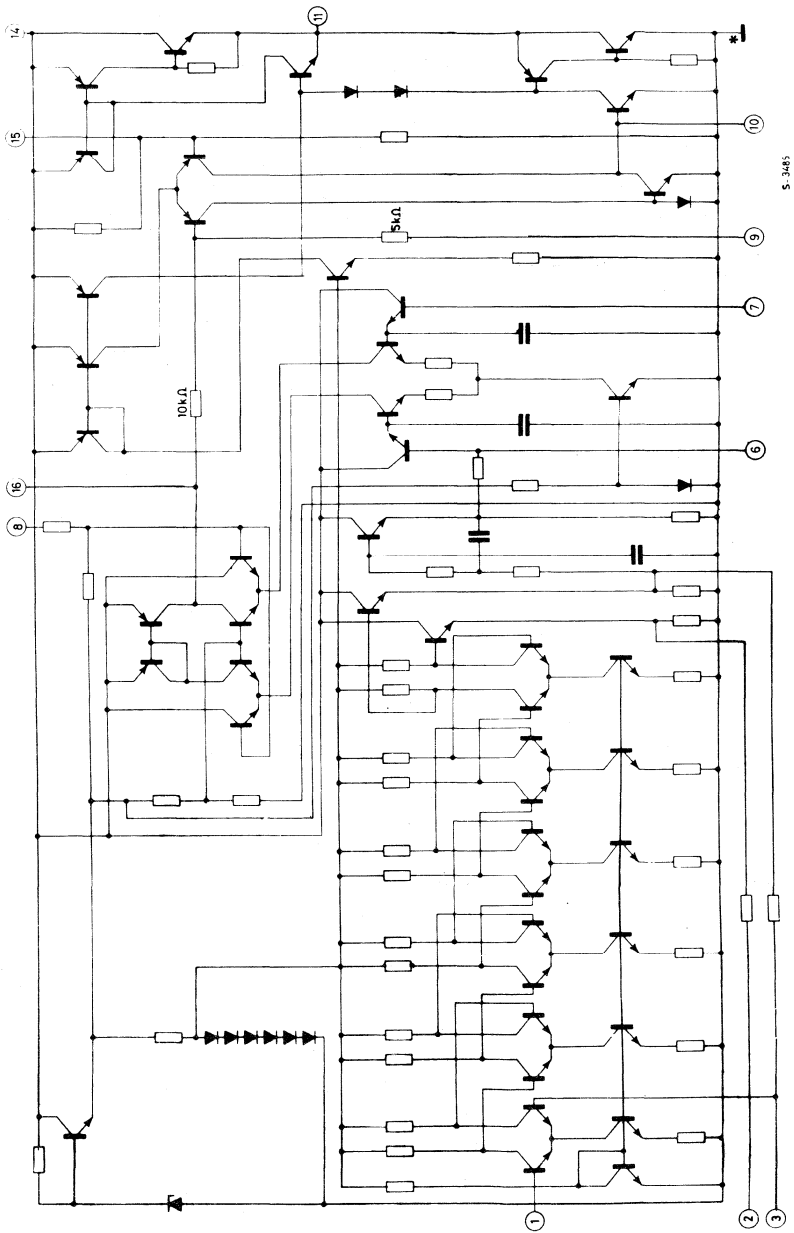
ORDERING NUMBERS: TDA 3190

MECHANICAL DATA

Dimensions in mm



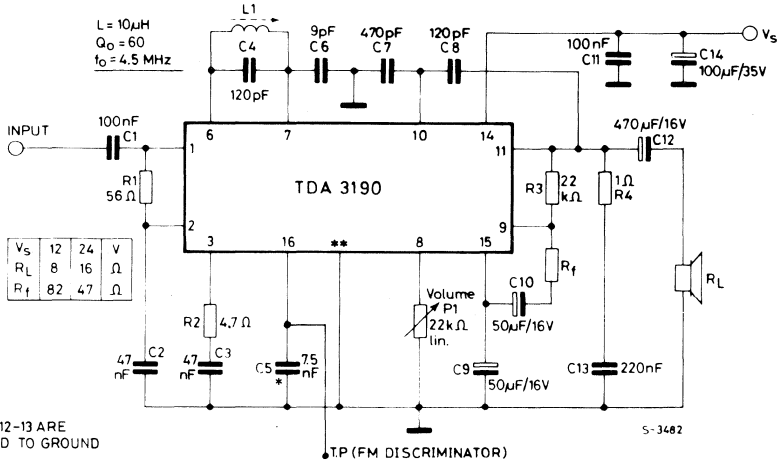
SCHEMATIC DIAGRAM



*PINS 4-5-12-13 ARE CONNECTED TO GROUND

TDA 3190

TEST CIRCUIT



THERMAL DATA

$R_{th\ j-pins}$	Thermal resistance junction-pins	max	14	$^{\circ}\text{C/W}$
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	80*	$^{\circ}\text{C/W}$

* Obtained with the GND pins soldered to printed circuit with minimized copper area.

ELECTRICAL CHARACTERISTICS (Refer to the test circuit, $V_s = 24\text{V}$, $T_{amb} = 25^{\circ}\text{C}$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	
V_s	Supply voltage (pin 14)	9		28	V	
V_o	Quiescent output voltage (pin 11)	$V_s = 24\text{V}$ $V_s = 12\text{V}$	11 5.1	12 6	13 6.9	V V
I_d	Quiescent drain current	$P_1 = 22\text{K}\Omega$ $V_s = 24\text{V}$ $V_s = 12\text{V}$	11	22 19	45 40	mA mA
P_o	Output power	$d = 10\%$ $f_m = 400\text{ Hz}$ $f_o = 4.5\text{ MHz}$ $\Delta f = \pm 25\text{ KHz}$ $V_s = 24\text{V}$ $R_L = 16\Omega$ $V_s = 12\text{V}$ $R_L = 8\Omega$		4.2 1.5		W W
		$d = 2\%$ $f_m = 400\text{ Hz}$ $f_o = 4.5\text{ MHz}$ $\Delta f = \pm 25\text{ KHz}$ $V_s = 24\text{V}$ $R_L = 16\Omega$ $V_s = 12\text{V}$ $R_L = 8\Omega$		3.5 1.4		W W

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_i Input limiting voltage (-3 dB) at pin 1	$f_o = 4.5 \text{ MHz}$ $\Delta f = \pm 7.5 \text{ KHz}$ $f_m = 400 \text{ Hz}$ $P_1 = 0$		40	100	μV
d Distortion	$P_o = 50 \text{ mW}$ $f_m = 400 \text{ Hz}$ $f_o = 4.5 \text{ MHz}$ $\Delta f = \pm 7.5 \text{ KHz}$ $V_s = 24\text{V}$ $R_L = 16\Omega$ $V_s = 12\text{V}$ $R_L = 8\Omega$		0.75 1		% %
B Frequency response of audio amplifier (-3 dB)	$R_L = 16\Omega$ $C_8 = 120 \text{ pF}$ $C_7 = 470 \text{ pF}$ $P_1 = 22 \text{ K}\Omega$ $R_f = 82\Omega$ $R_f = 47\Omega$		70 to 12000 70 to 7000		Hz Hz
V_o Recovered audio voltage (pin 16)	$V_i \geq 1 \text{ mV}$ $f_o = 4.5 \text{ MHz}$ $f_m = 400 \text{ Hz}$ $\Delta f = \pm 7.5 \text{ KHz}$ $P_1 = 0$		120		mV
AMR Amplitude modulation rejection	$V_i \geq 1 \text{ mV}$ $f_o = 4.5 \text{ MHz}$ $f_m = 400 \text{ Hz}$ $\Delta f = \pm 25 \text{ KHz}$ $m = 0.3$		55		dB
$\frac{S+N}{N}$ Signal to noise ratio	$V_i \geq 1 \text{ mV}$ $V_o = 4\text{V}$ $f_o = 4.5 \text{ MHz}$ $f_m = 400 \text{ Hz}$ $\Delta f = \pm 25 \text{ KHz}$	50	65		dB
R_3 External feedback resistance (between pins 9 and 11)				25	$\text{K}\Omega$
R_i Input resistance (pin 1)	$V_i = 1 \text{ mV}$		30		$\text{K}\Omega$
C_i Input capacitance (pin 1)	$f_o = 4.5 \text{ MHz}$		5		pF
SVR Supply voltage rejection	$R_L = 16\Omega$ $f_{\text{ripple}} = 120 \text{ Hz}$ $P_1 = 22 \text{ K}\Omega$		46		dB
A_V DC volume control attenuation	$P_1 = 12 \text{ K}\Omega$		90		dB

TDA 3190

Fig. 1 - Relative audio output voltage and output noise vs. input signal.

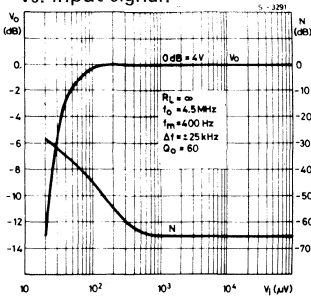


Fig. 2 - Output voltage attenuation vs. DC volume control resistance.

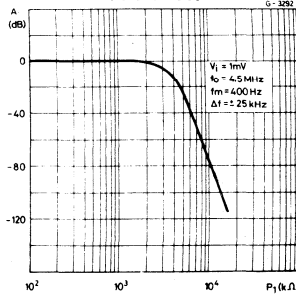


Fig. 3 - Amplitude modulation rejection vs. input signal.

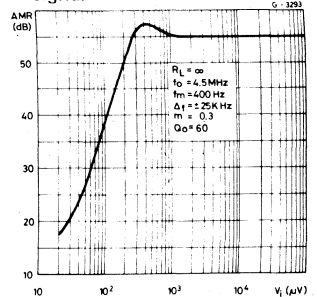


Fig. 4 - ΔAMR vs. tuning frequency change.

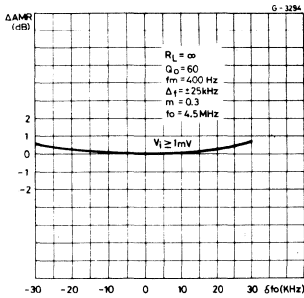


Fig. 5 - Recovered audio voltage vs. unloaded Q factor of the detector coil.

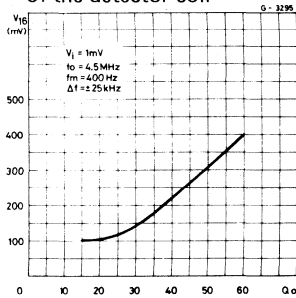


Fig. 6 - Distortion vs. output power.

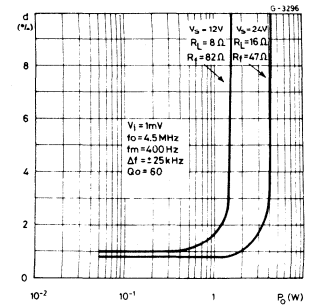


Fig. 7 - Distortion vs. frequency deviation.

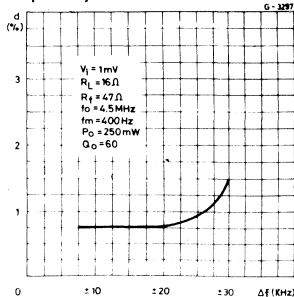


Fig. 8 - Distortion vs. tuning frequency change.

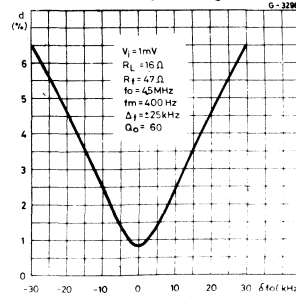


Fig. 9 - Audio amplifier frequency response.

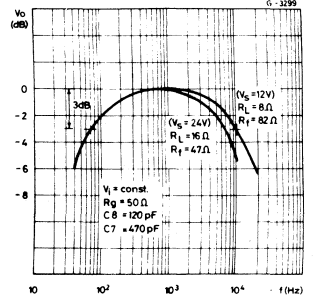


Fig. 10 - Supply voltage ripple rejection vs. ripple frequency

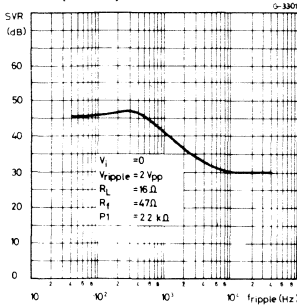


Fig. 11 - Supply voltage ripple rejection vs. volume control attenuation

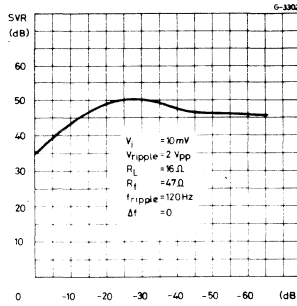


Fig. 12 - Output power vs. supply voltage

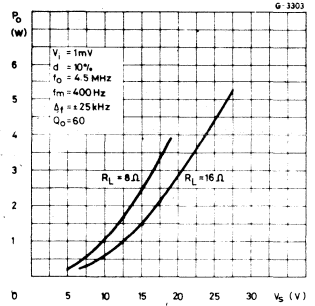


Fig. 13 - Maximum power dissipation vs. supply voltage (sine wave operation)

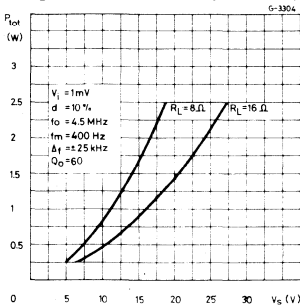


Fig. 14 - Power dissipation and efficiency vs. output power

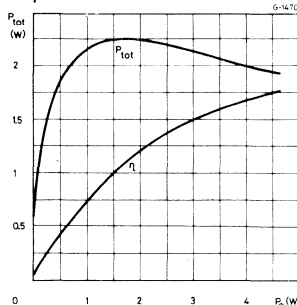
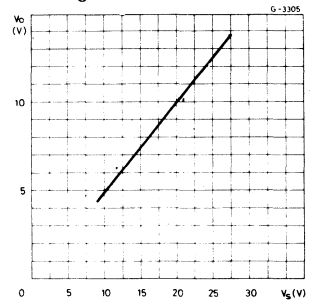


Fig. 15 - Quiescent output voltage (pin 11) vs. supply voltage



APPLICATION INFORMATION

The electrical characteristics of the TDA 3190 remain almost constant over the frequency range 4.5 to 6 MHz, therefore it can be used in all television standards (FM mod.). The TDA 3190 has a high input impedance, so it can function with a ceramic filter or with a tuned circuit that provide the necessary input selectivity.

The value of the resistors connected to pin 9, determine the AC gain of the audio frequency amplifier. This enables the desired gain to be selected in relation to the frequency deviation at which the output stage of the AF amplifier, must enter into clipping.

Capacitor C8, connected between pins 10 and 11, determines the upper cutoff frequency of the audio bandwidth. To increase the bandwidth the values of C8 and C7 must be reduced, keeping the ratio C7/C8 as shown in the table of fig. 16.

The capacitor connected between pin 16 and ground, together with the internal resistor of 10 K Ω forms the de-emphasis network. The Boucherot cell eliminates the high frequency oscillations caused by the inductive load and the wires connecting the loudspeaker.

TDA 3190

APPLICATION INFORMATION (continued)

Fig. 16 - Typical application circuit

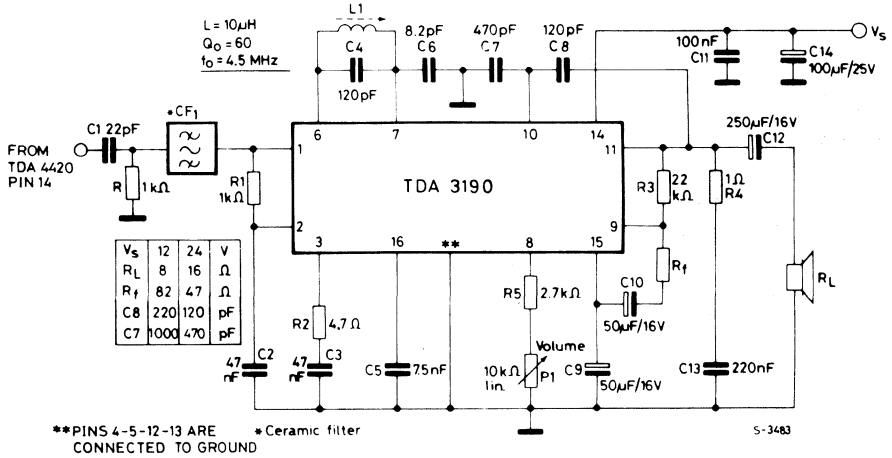
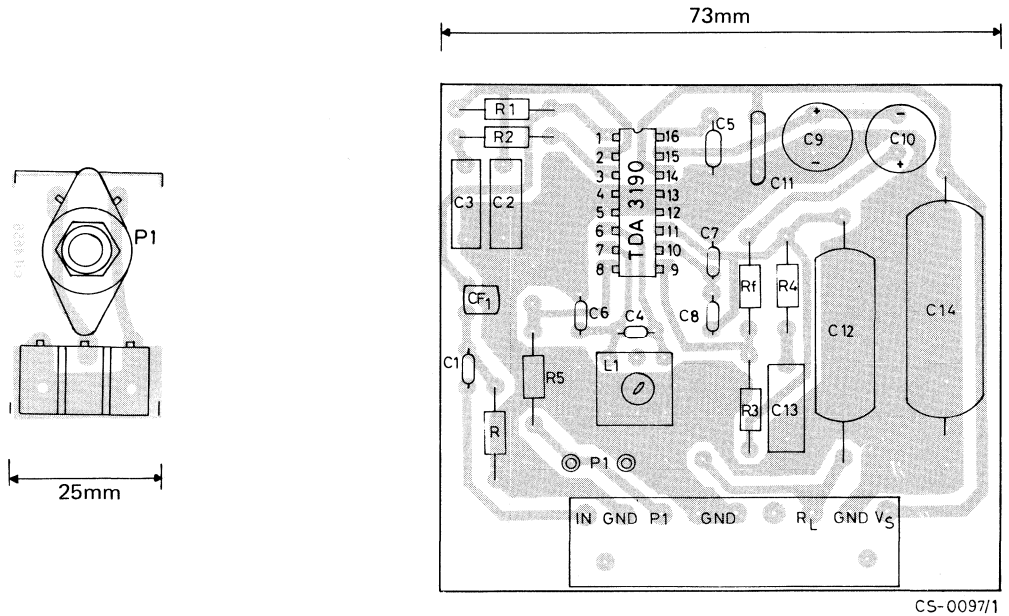


Fig. 17 - P.C. board and component layout of the circuit shown in Fig. 16 (1:1 scale)



MOUNTING INSTRUCTIONS

The $R_{th\ j-amb}$ of the TDA 3190 can be reduced by soldering the GND pins to a suitable copper area of the printed circuit board (Fig. 18) or to an external heatsink (Fig. 19).

The diagram of figure 20 shows the maximum dissippable power P_{tot} and the $R_{th\ j-amb}$ as a function of the side "ℓ" of two equal square copper areas having a thickness of 35μ (1.4 mils).

During soldering the pins temperature must not exceed 260°C and the soldering time must not be longer than 12 seconds.

The external heatsink or printed circuit copper area must be connected to electrical ground.

Fig. 18 - Example of P.C. board copper area which is used as heatsink.

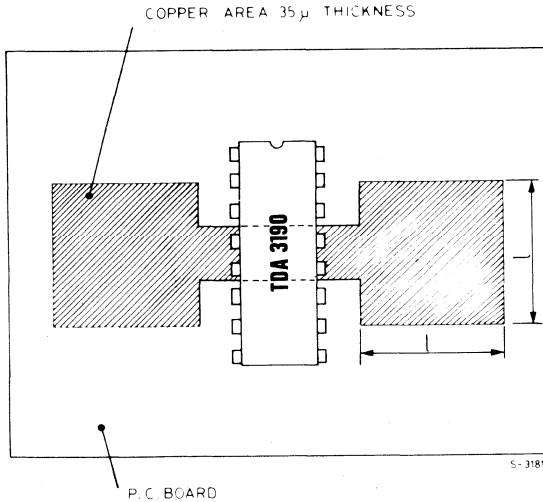


Fig. 19 - External heatsink mounting example

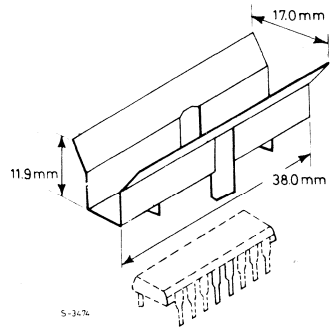


Fig. 20 - Maximum dissippable power and junction to ambient thermal resistance vs. side "ℓ"

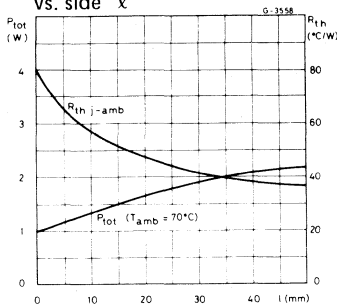
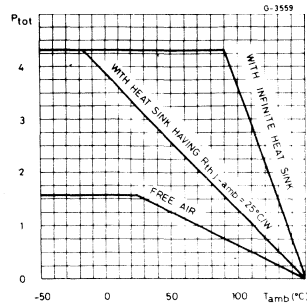


Fig. 21 - Maximum allowable power dissipation vs. ambient temperature



TDA 3310

LINEAR INTEGRATED CIRCUIT

LOW NOISE NPN TRANSISTOR ARRAY

The TDA 3310 is an assembly of 5 NPN transistors in 14-lead dual in-line plastic package. The transistors of TDA 3310 are designed for **low noise and high h_{FE}** . Applications are:

- Hi-Fi preamplifiers
- Infrared receivers for TV remote control
- Dictaphones
- C.B. system applications
- Professional audio systems and active filters.

The collector of each transistor of the TDA 3310 is isolated from the substrate by an integrated diode.

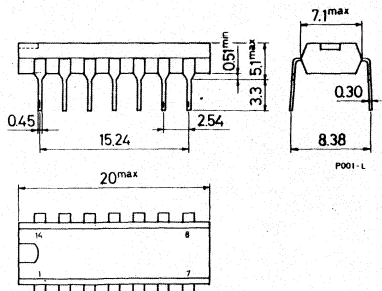
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	20	V
I_C	Collector current (each transistor)	50	mA
P_{tot}	Total power dissipation at $T_{amb} = 50^\circ\text{C}$	500	mW
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

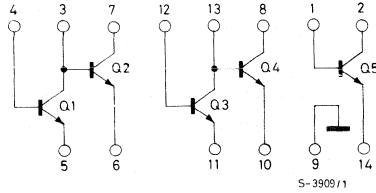
ORDERING NUMBER: TDA 3310

MECHANICAL DATA

Dimensions in mm



SCHEMATIC DIAGRAM



ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^{\circ}\text{C}$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s Supply voltage				20	V
h_{FE} DC current gain	$V_{CE} = 5\text{V}$ $I_C = 100\ \mu\text{A}$	300	500		—
NF Noise figure	$V_{CE} = 5\text{V}$ $I_C = 100\ \mu\text{A}$ $R_g = 2\ \text{k}\Omega$ $R_g = 10\ \text{k}\Omega$		1 0.5	4	dB dB
$V_{CE(sat)}$ Collector-emitter saturation voltage	$I_C = 10\ \text{mA}$ $I_B = 1\ \text{mA}$		0.3		V
I_{CEO} Collector cutoff current	$V_{CE} = 10\text{V}$		0.1	0.5	μA

Fig. 1 - Equivalent input spot noise voltage and current vs. collector current

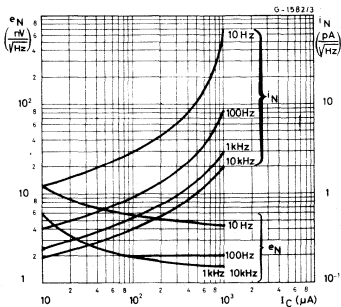


Fig. 2 - Equivalent input noise current vs. frequency

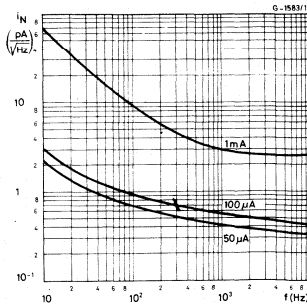
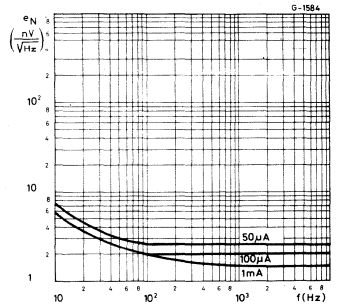


Fig. 3 - Equivalent input noise voltage vs. frequency



TDA 3310

Fig. 4 - Noise figure

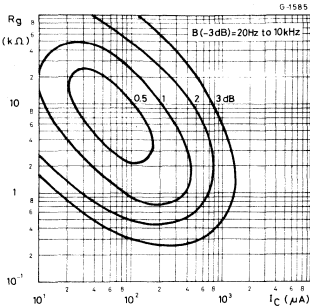


Fig. 5 - Optimum source resistance and NF vs. collector current

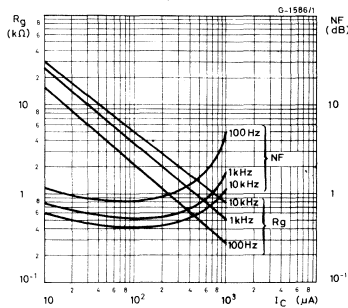
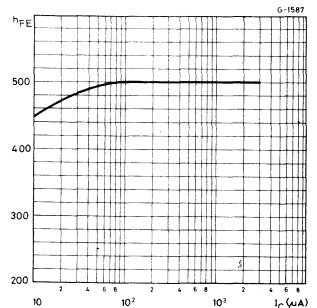
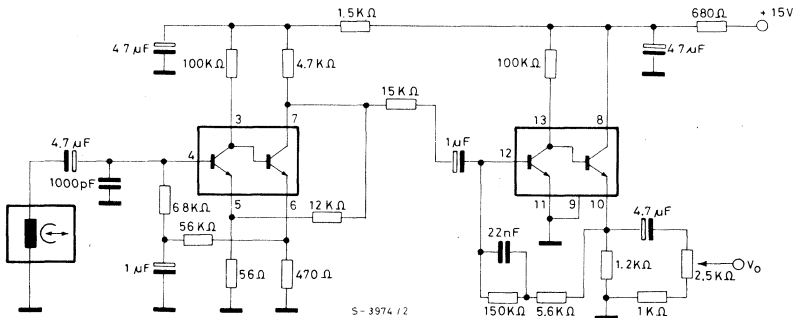


Fig. 6 - Current gain vs. collector current



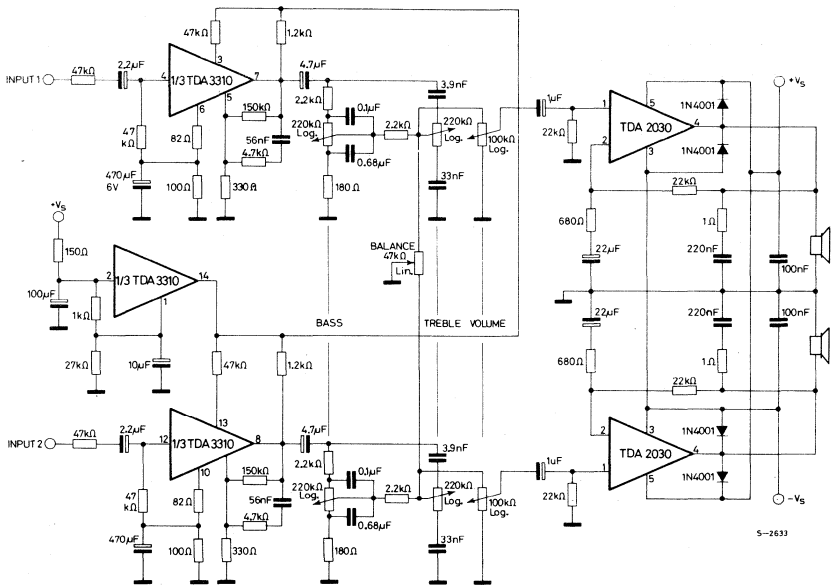
TYPICAL APPLICATIONS

Fig. 7 - Tape preamplifier



TDA 3310

Fig. 8 - 15 + 15 W high quality stereo amplifier with preamplifier equalizer for ceramic pick-ups.



TDA 3410

LINEAR INTEGRATED CIRCUIT

LOW NOISE DUAL PREAMPLIFIER WITH AUTOREVERSE

The TDA 3410 is a dual preamplifier with tape autoreverse facility for the amplification of low level signals in applications requiring very low noise performance, as stereo cassette players. Each channel consists of two independent amplifiers. The first has a fixed gain of 30 dB while the second one is an operational amplifier optimized for high quality audio application.

The TDA 3410 is a monolithic integrated circuit in a 16-lead dual in-line plastic package and its main features are:

- Very low noise
- High gain
- Low distortion
- Single supply operation
- Wide supply range
- SVR = 120 dB
- Large output voltage swing
- Tape autoreverse facility
- Short circuit protection

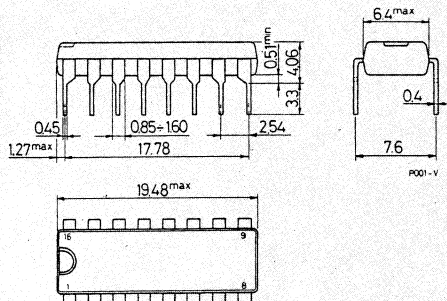
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	36	V
P_{tot}	Total power dissipation at $T_{amb} = 60^\circ\text{C}$	600	mW
T_j, T_{stg}	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

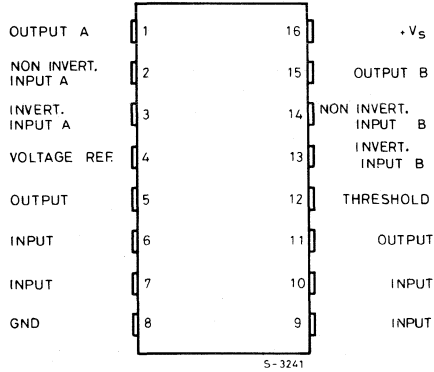
ORDERING NUMBER: TDA 3410

MECHANICAL DATA

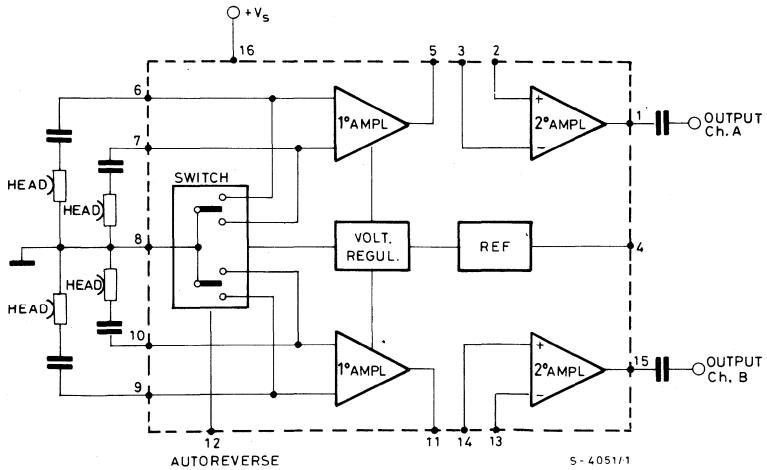
Dimensions in mm



CONNECTION DIAGRAM (top view)



BLOCK DIAGRAM



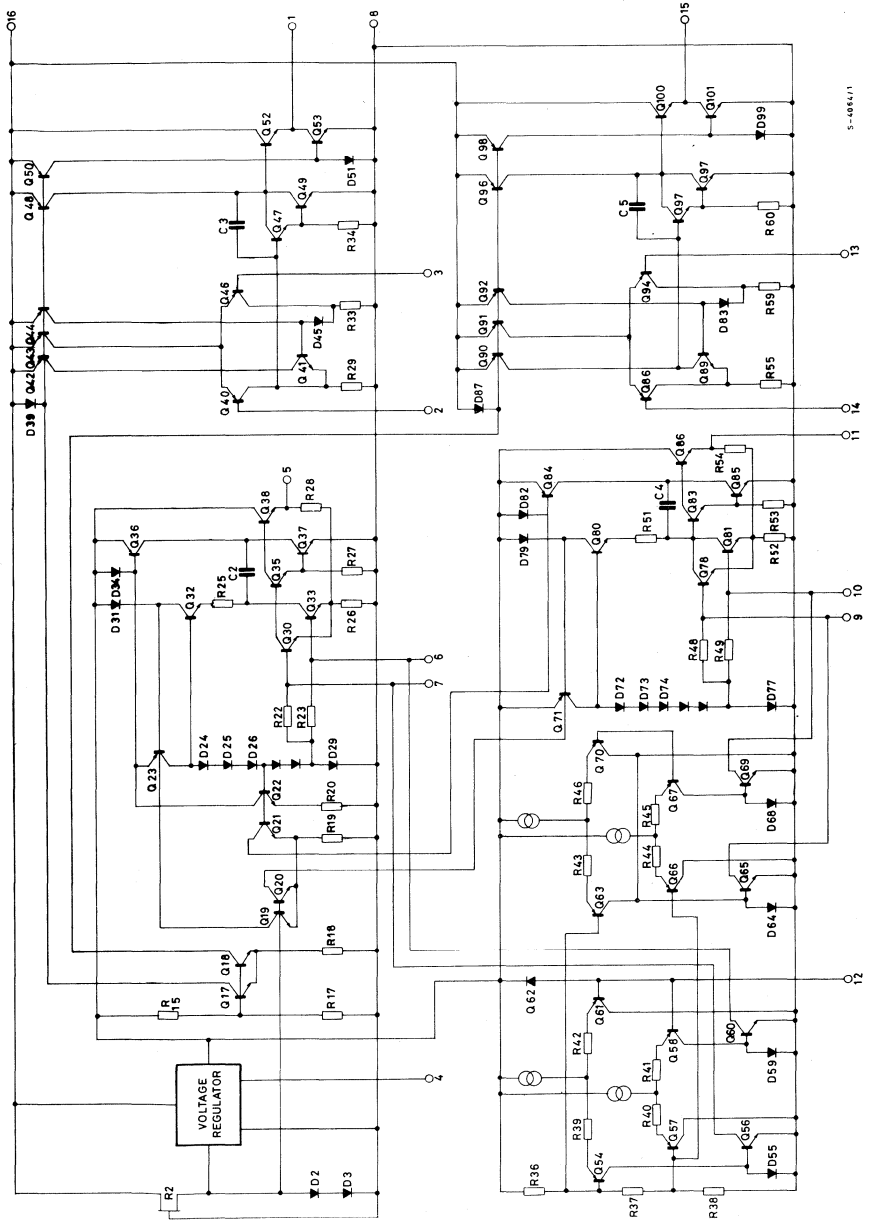
THERMAL DATA

$R_{th\ j-amb}$ Thermal resistance junction-ambient

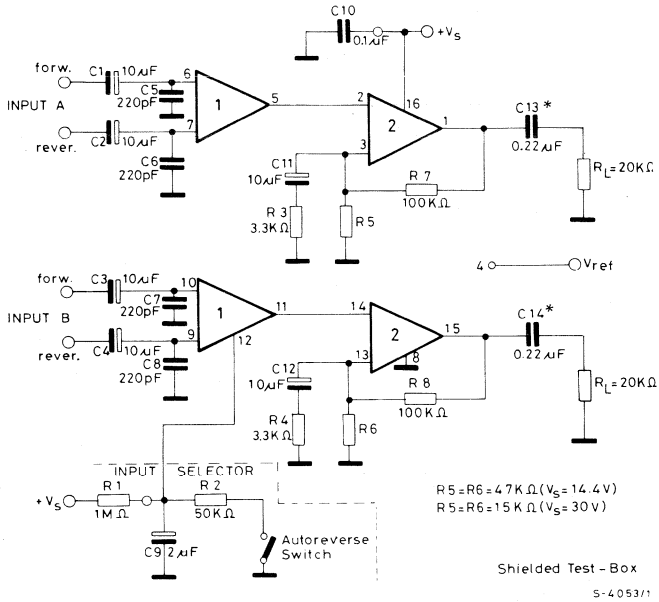
max 150 °C/W

TDA 3410

SCHEMATIC DIAGRAM



TEST CIRCUIT (Flat Gain - $G_v = 60$ dB)



* Mylar or polycarbonate capacitors.

ELECTRICAL CHARACTERISTICS ($T_{amb} = 25^\circ C$, $V_s = 14.4V$, $G_v = 60$ dB, refer to the test circuit, unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
I_s	Supply current	$V_s = 8V$ to $30V$			mA
I_o	Output current (pins 1-15)	Source	10		mA
		Sink	1		mA
G_v	Closed loop gain	$f = 20$ Hz to 20 KHz		60	dB
R_i	Input resistance	$f = 1$ KHz		50	$K\Omega$
R_o	Output resistance (pins 1-15)	$f = 1$ KHz		50	Ω
THD	Total harmonic distortion	$V_o = 300$ mV $f = 1$ KHz		0.05	%
		$f = 10$ KHz		0.05	%

TDA 3410

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_o Output voltage swing (pins 1-15)	Peak to Peak $V_s = 14.4V$ $V_s = 30V$		12 28		.V V
V_o Output voltage (pins 1-15)	$d = 0.5\%$ $V_s = 14.4V$ $f = 1 \text{ KHz}$ $V_s = 30V$.4 8		V_{rms} V_{rms}
e_n Total input noise ($^\circ$)	$R_g = 50\Omega$ $R_g = 600\Omega$ $R_g = 5K\Omega$		0.25 0.4 1.3	0.6	μV μV μV
S/N Signal to noise ratio ($^\circ$)	$V_{in} = 0.3 \text{ mV}$ $R_g = 600\Omega$ $V_{in} = 1 \text{ mV}$ $R_g = 0$		57 73		dB dB
CS Channel separation	$f = 1 \text{ KHz}$		60		dB
CT($^{\circ\circ}$) Cross-talk (differential input)	$f = 1 \text{ KHz}$		80		dB
SVR Supply voltage rejection ($^{\circ\circ}$)	$f = 1 \text{ KHz}$ $R_g = 600\Omega$		120		dB
SVR ($^{\circ\circ}$) Of reference voltage (Pin 4)	$f = 1 \text{ KHz}$ $R_g = 600\Omega$		100		dB
V_{ref} Reference voltage (pin 4)			55		mV
R_{ref} Ref. voltage output resistance (pin 4)			100		Ω
$\frac{\Delta V_{ref}}{\Delta T}$ Voltage temperature coefficient			10		$\mu V/^\circ C$

($^\circ$) The weighting filter used for the noise measurement has a curve A frequency response.

($^{\circ\circ}$) Referred to the input.

($^{\circ\circ\circ}$) Between a disabled input and an input ON.

ELECTRICAL CHARACTERISTICS (Refer test circuit, $V_s = 30V$)

AMPLIFIER N° 1

Parameter	Test conditions	Min.	Typ.	Max.	Unit
G_v Gain (pins 6 to 5)		29	30	30.5	dB
d Distortion	$V_o = 300 \text{ mV}$ $f = 1 \text{ KHz}$ $f = 10 \text{ KHz}$		0.05 0.05		%
e_n Total input noise (°)	$R_g = 600\Omega$		0.4		μV
Z_o Output impedance (pin 5)	$f = 1 \text{ KHz}$		100		Ω
I_o Output current (pin 5)			1		mA
V_5 DC output voltage (pin 5)	$V_s = 10V$	1.3	2	2.7	V

AMPLIFIER N° 2

G_v Open loop voltage gain (pins 2 to 1)			100		dB
I_B Input bias current			0.2		μA
V_{os} Input offset voltage			2		mV
I_{os} Input offset current			0.05		μA
BW Small signal bandwidth	$G_v = 30 \text{ dB}$		150		KHz
e_n Total input noise (°)	$R_g = 600\Omega$		2		μV
R_i Input impedance	$f = 1 \text{ KHz}$ (open loop)	150	500		K Ω

AUTOREVERSE

P_{in}	$V_{12} < 2V$	$V_{12} > 4.5V$
6 – 10	OFF	ON
7 – 9	ON	OFF

(°) The weighting filter used for the noise measurement has a curve A frequency response.

TDA 3410

Fig. 1 - Total input noise vs. source resistance (curve A)

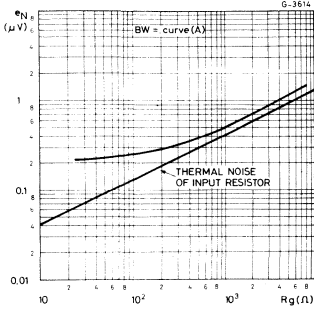


Fig. 2 - Total input noise vs. source resistance (BW= 22 Hz to 22 KHz)

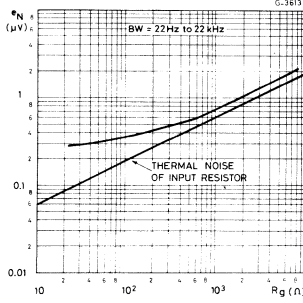


Fig. 3 - Total harmonic distortion vs. output voltage

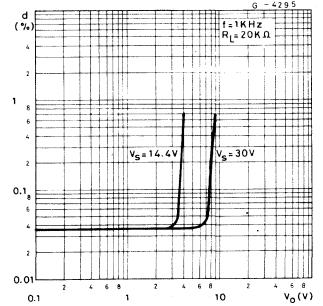


Fig. 4 - Very low noise stereo preamplifier for cassette players

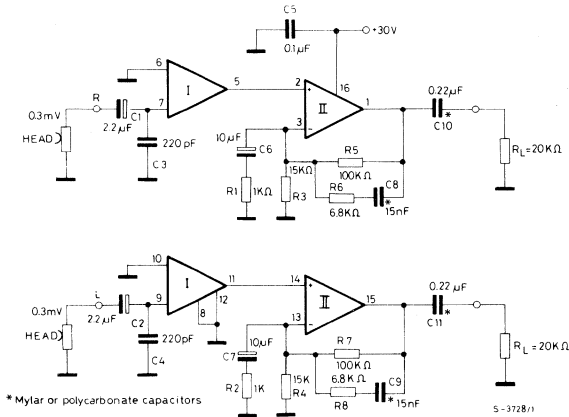
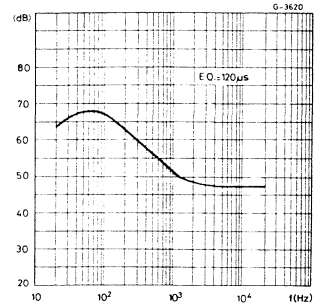


Fig. 5 - Frequency response



TDA 3410

Fig. 6 - Very low noise stereo preamplifier for car cassette players (with Gap Loss Correction and autoreverse function)

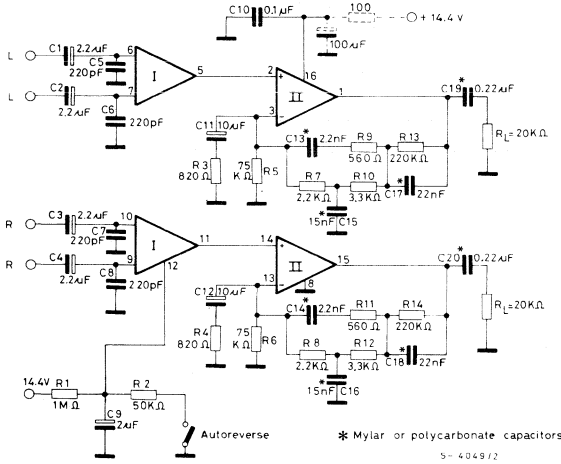


Fig. 7 - Frequency response

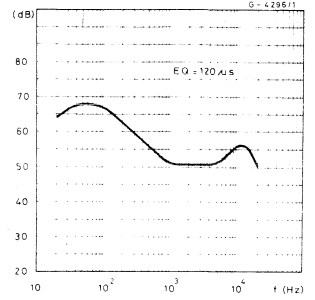
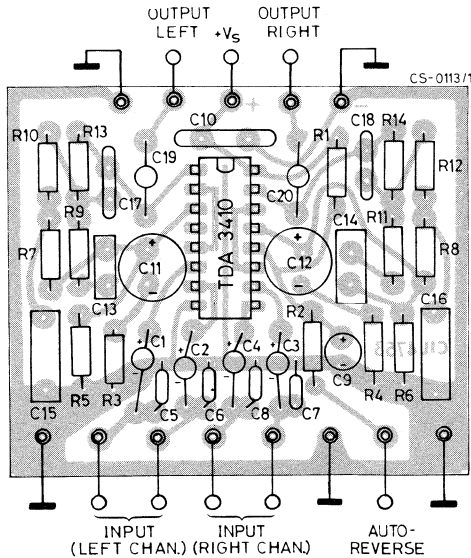


Fig. 8 - P.C. board and component lay-out (1:1 scale) for the circuit of fig. 6



TDA 3410

Fig. 9 - Stereo preamplifier for car cassette players, with low value capacitors (Autoreverse function)

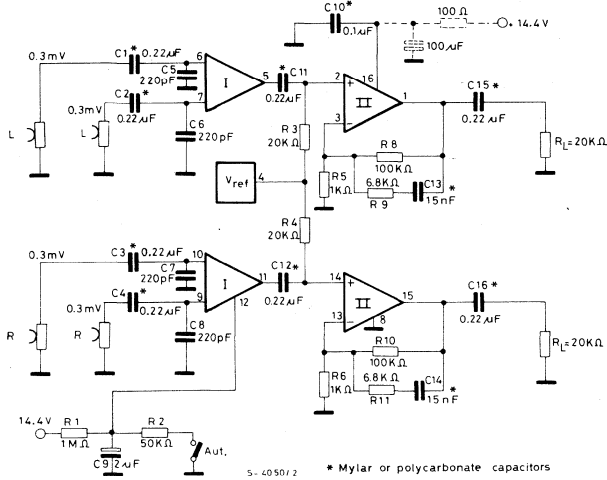


Fig. 10 - Frequency response

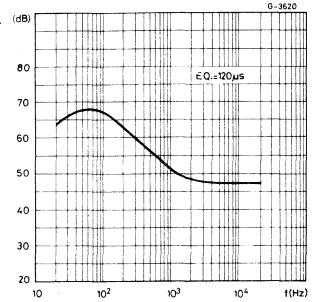
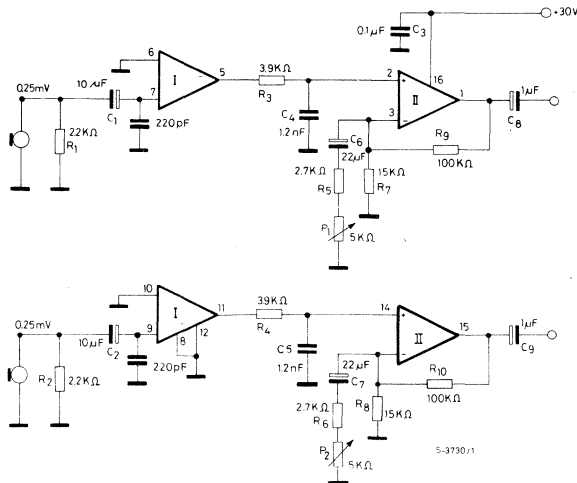


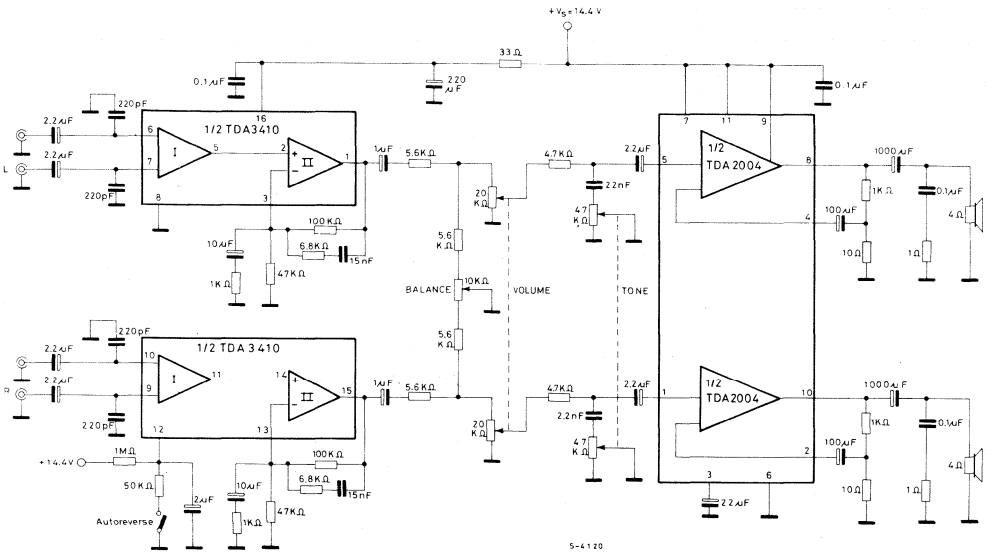
Fig. 11 - Dual channel microphone preamplifier



TDA 3410

APPLICATION INFORMATION

Fig. 12 - Complete stereo tape players (10 + 10W)



TDA 4420

LINEAR INTEGRATED CIRCUIT

PRELIMINARY DATA

VISION IF SYSTEM WITH AFC

- HIGH GAIN-HIGH STABILITY
- VERY LOW INTERMODULATION PRODUCTS
- MINIMUM DIFFERENTIAL ERROR
- CONSTANT INPUT IMPEDANCE INDEPENDENT OF AGC
- FAST AGC GATING-ACTION, LARGELY INDEPENDENT OF PULSE SHAPE AND AMPLITUDE
- ADJUSTABLE WHITE LEVEL
- LARGE AFC OUTPUT CURRENT SWING (PUSH-PULL OUTPUT)
- SWITCHABLE AFC

The TDA4420 is a monolithic integrated circuit in 18 lead dual in-line plastic package. The functions incorporated are:

- gain controlled vision IF amplifier
- video demodulator controlled by picture carrier
- AGC detector with gating facility
- AGC amplifier for tuner drive with variable delay
- phase comparator for AFC current generation
- electronic AFC switch, controlled by a DC threshold detector
- thermally compensated push-pull AFC output stage.

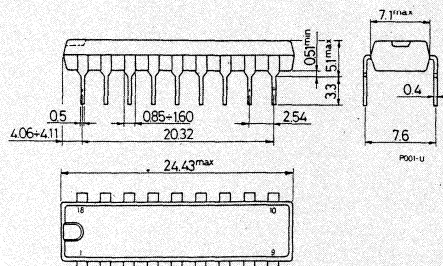
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage (pin 15)	15	V
V_5	Voltage at pin 5	15	V
I_{13}, I_{14}	Video DC output current	5	mA
P_{tot}	Total power dissipation at $T_{amb} \leq 70^\circ\text{C}$	1	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBER: TDA 4420

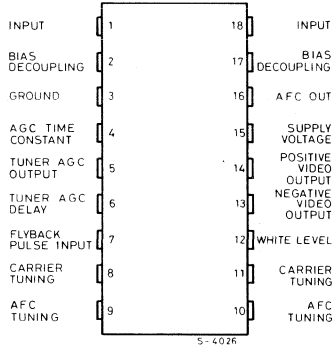
MECHANICAL DATA

Dimensions in mm

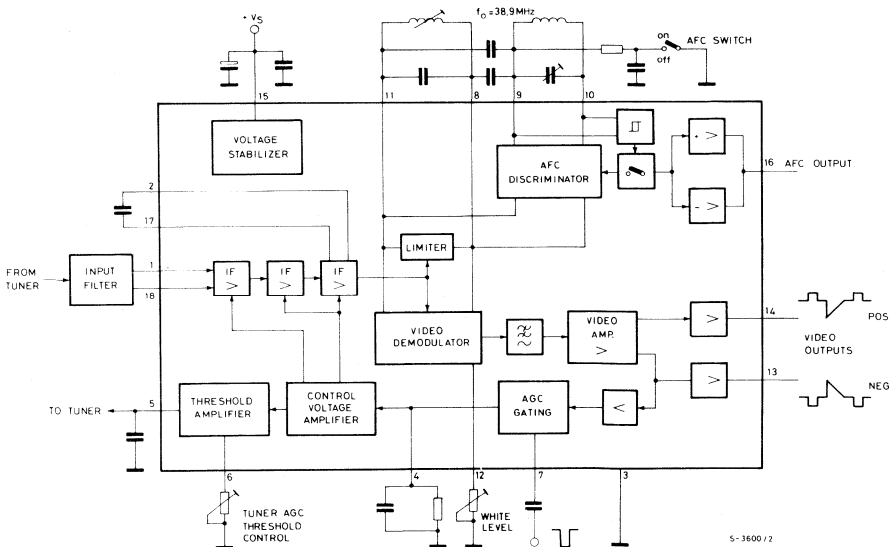


TDA 4420

CONNECTION DIAGRAM (top view)

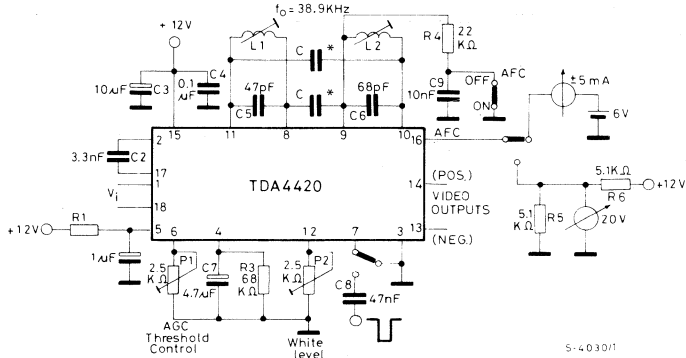


BLOCK DIAGRAM



TDA 4420

TEST CIRCUIT



Note: (*) C \cong 1.5 pF (pin and lead capacitance).

THERMAL DATA

$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	80	$^{\circ}\text{C}/\text{W}$
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ELECTRICAL CHARACTERISTICS (Refer to the test circuit; $V_s = 12\text{V}$, $f_o = 38.9\text{ MHz}$; $P_1 = 2.5\text{ K}\Omega$; pin 7 connected to GND; P_2 adjusted for $V_{13} = 3.3\text{Vpp}$; AFC off; $T_{amb} = 25^{\circ}\text{C}$ unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
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DC CHARACTERISTICS

V_s	Supply voltage range (pin 15)		10	12	15	V
I_s	Supply current (pin 15)			52		mA
V_{14}	Video output DC voltage	$V_{13} = 5.5\text{V}$ (1)		5.6		V
V_{13}	Video output DC voltage	pin 12 open (1)			4.5	V
		pin 12 grounded (1)	7			V
V_{13}	Peak black clamping level at negative video output		1.75	1.9	2.15	V
I_{13}	Output DC current (pin 13)	$V_s = 15\text{V}$ $V_{13} = 8\text{V}$		1.6		mA
I_9, I_{10}	DC control current for AFC off		150	300		μA

ELECTRICAL CHARACTERISTICS (continued)

Parameter		Test conditions	Min.	Typ.	Max.	Unit
AC CHARACTERISTICS						
I_5	Available tuner AGC current	(2)		10		mA
V_7	AGC gating pulse input peak voltage	f pulse = 15625 Hz (3)	-1.5	-3	-5	V
V_o	Peak to peak video output signal (pin 13)	$V_{13} = 5.5V$ (4), (5)		3.3		V
		$V_{13} = 6.4V$ (4), (5)		4.2		V
ΔV_i	AGC range	(6)	50	60		dB
B	Frequency response (-3 dB)	(4)	8	10		MHz
V_i	Input sensitivity	(7), (8)	100	150	200	μV
V_{13}, V_{14}	Video carrier and video carrier 2nd harmonic leakage at video output	$V_i = 30$ dB (4) $f_o = 38.9$ MHz $2 f_o = 77.8$ MHz			30 50	mV mV
V_{14}	Sound IF at positive video output (5.5 MHz)	(4), (9)	30			mV
d	Differential distortion of negative video output signal	$V_i = 30$ dB (standard staircase modulating signal)		3		%
d_{im}	Intermodulation product at video outputs (1.07 MHz)	(4), (10)		-50		dB
R_i	Input resistance between pins 1 and 18	(4)		1.4		K Ω
C_i	Input capacitance between pins 1 and 18			2		pF
V_{16}	AFC voltage range	(11)	1		$V_s - 1.5$	V
I_{16}	Maximum available AFC current	(12)			± 3	mA
$\frac{\Delta I_{16}}{\Delta f}$	AFC slope	(13)		± 0.01		$\frac{mA}{KHz}$

Notes:

- (1) V_{13} and V_{14} are simultaneously adjustable by means of the resistance connected between pin 12 and ground (P_2).
- (2) $\Delta V_i = +60$ dB (see note 7); $f_m = 100$ KHz; $m = 0.82$.
- (3) Input at pin 7 through C8.
- (4) The input voltage V_i can have any value within the AGC range.
- (5) P_2 adjusted for $V_{13} = 5.5V$ or $V_{13} = 6.4V$; $f_m = 100$ KHz; $m = 0.82$.
- (6) $\Delta V_o = 1$ dB; $f_m = 100$ KHz; $m = 0.82$.

TDA 4420

- (7) The measured amplitude is assumed as 0 dB reference level of V_i that is the rms value of the unmodulated video carrier (modulation down).
- (8) P_2 is adjusted in order to have $V_{13} = 3V_{pp}$ at $V_i = 4$ mV, then the sensitivity is obtained as the minimum input voltage that maintains this output level. $f_m = 100$ KHz; $m = 82\%$.
- (9) $f_o = 38.9$ MHz (video carrier); $f_a = 33.4$ MHz (sound carrier); the amplitude of the sound carrier is 30 dB below the amplitude of the video carrier.
- (10) V_i at $f_o = 38.9$ MHz (video carrier); $f_a = 33.4$ MHz, 6 dB below V_i (sound carrier); $f_b = 34.47$ MHz, 24 dB below V_i (Chroma subcarrier).
- (11) $V_i = 40$ dB; $R_5 = R_6 = 5.1$ K Ω ; AFC on; $f_o = 39.9$ MHz; $f_o = 37.9$ MHz.
- (12) $V_i = 40$ dB; $f_o = 39.2$ MHz; AFC on; $V_{16} = 6V$.
- (13) $V_i = 40$ dB; $f_o = 38.9$ MHz; $f_2 = 39.2$ MHz; AFC on; $V_{16} = 6V$.

Fig. 1 - Set-up for measurement of d_{im}

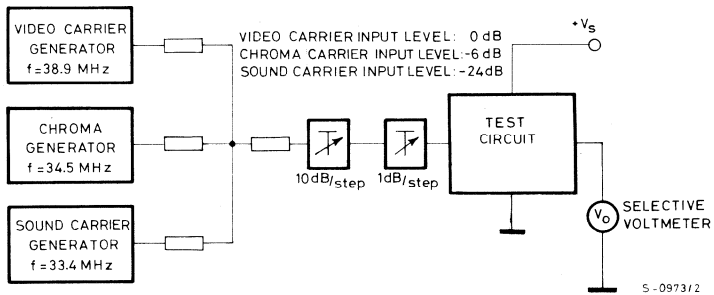
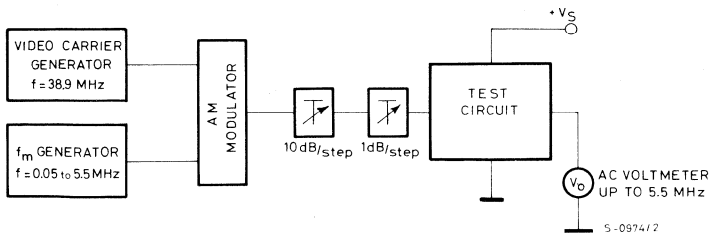
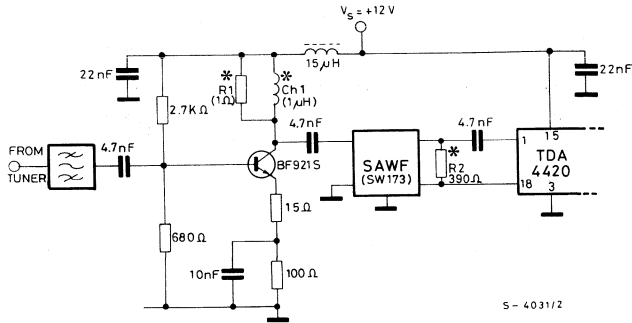


Fig. 2 - Set-up for measurement of ΔV_o



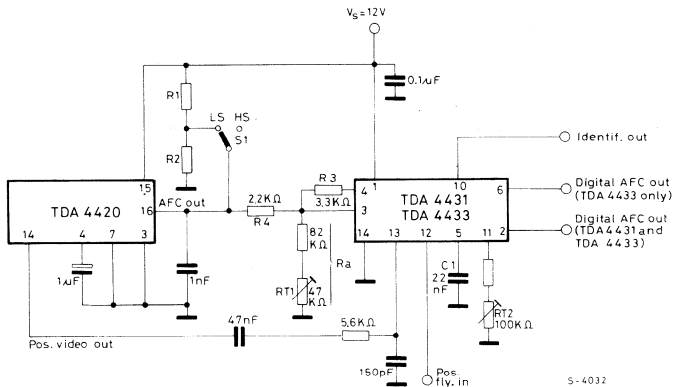
APPLICATION INFORMATION

Fig. 3 - Application circuit



* R_1 ; R_2 ; Ch_1 , depend from the SAWF characteristics

Fig. 4 - TV Signal identification circuit



TV signal identification circuit:

The suggested application circuit is shown in fig. 4.
The passive components are chosen as follows:

- R_1 and R_2 : these define the AFC response slope. For $R_1 = R_2 = 5.1 K\Omega$, the typical slope is 750/11 KHz/V (with AFC output unloaded).
- S_1 : switches between low slope (LS) and high slope (HS). The high slope is typically 88/11 KHz/V.

APPLICATION INFORMATION (continued)

R_3 and R_4 : the ratio $(R_3 + R_4)/R_3$ defines the digital AFC width (δf) calculated from the linear AFC width ($2\Delta f$). With $V_s = 12V$, the relation is:

$$\delta f = 0.036 (2\Delta f) \frac{R_3 + R_4}{R_3}$$

R_{T1} : by means of this trimmer it is possible to align the linear tuning with the digital one, at the same frequency. The typical relation is:

$$R_a = 33 R_3$$

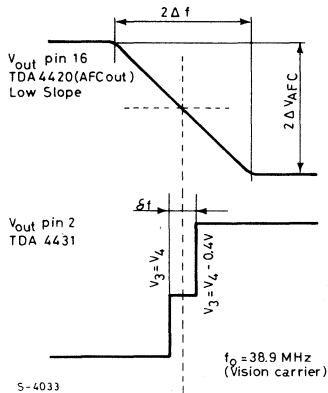
with $R_3 = 3.3 K\Omega$, R_a can be a fixed resistor of $110 K\Omega$.

R_{T2} : by means of this trimmer it is possible to choose the better sensitivity. It is possible to put a fixed resistor at pin 11 in the range of $68 K\Omega$ to $100 K\Omega$.

To make better sensitivity adjustment of trimmer R_{T2} , it is necessary to use only a weak signal at the antenna. The video information must be a black picture or a field of small white points on a black field. Furthermore, the action of the syncs separator must be as quick as possible.

In receivers with automatic program search, S1 should be in the HS position and then the components S1, R1 and R2 can be omitted completely.

Fig. 5 - Linear and digital AFC characteristics (TDA 4420 and TDA 4431)



LINEAR INTEGRATED CIRCUITS

TV SIGNAL IDENTIFICATION CIRCUIT AND AFC INTERFACE

The TDA4431 and the TDA4433 are monolithic integrated circuits in a 14 lead dual-in-line plastic package. They integrate the following functions:

- TV signal identifier – Sync. separator – Threshold detector – Digital Interface – Voltage regulator

They are intended for use in Electronic Program Memory tuning systems, the TDA4431 in conjunction with M193B1, while the TDA4433 with M293B1. The circuits features are:

- Identification of true TV stations only.
- Low impedance output of the identification signal.
- Digital control signal for automatic search and AFC operation.
- Thermal compensation of the voltage regulator.

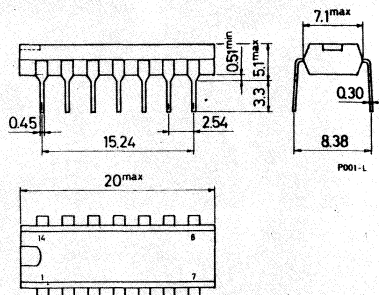
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage (pin 1)	16	V
V_3	Voltage at pin 3	16	V
V_{13}	Voltage at pin 13	-5 to +6	V
I_2	Pin 2 current (TDA4431)	± 1	mA
$I_6 ; I_2$	Pin 6 and pin 2 current (TDA4433)	1	mA
I_{10}	Pin 10 current	2	mA
I_{11}	Pin 11 current	2	mA
I_{12}	Pin 12 current	± 2	mA
P_{tot}	Total power dissipation at $T_{amb} \leq 70^\circ\text{C}$	800	mW
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBERS: TDA 4431
TDA 4433

MECHANICAL DATA

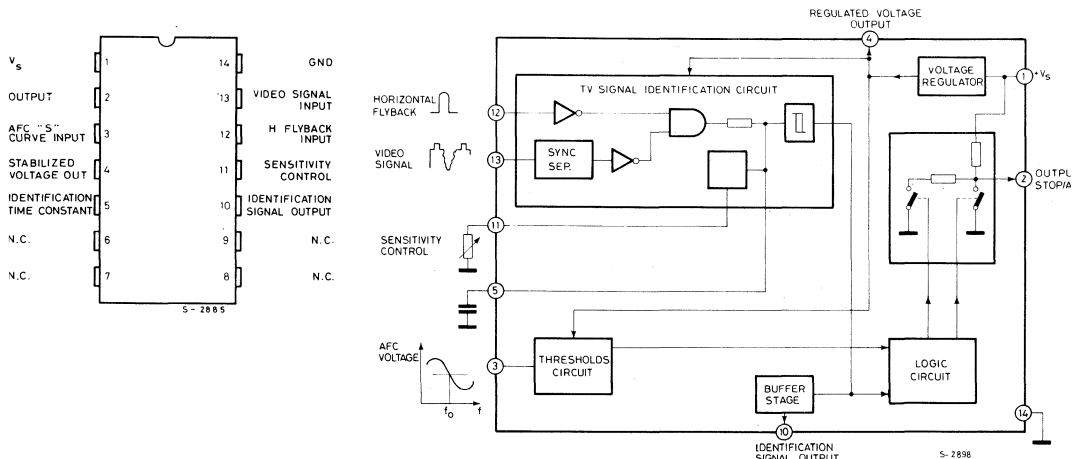
Dimension in mm



TDA 4431 TDA 4433

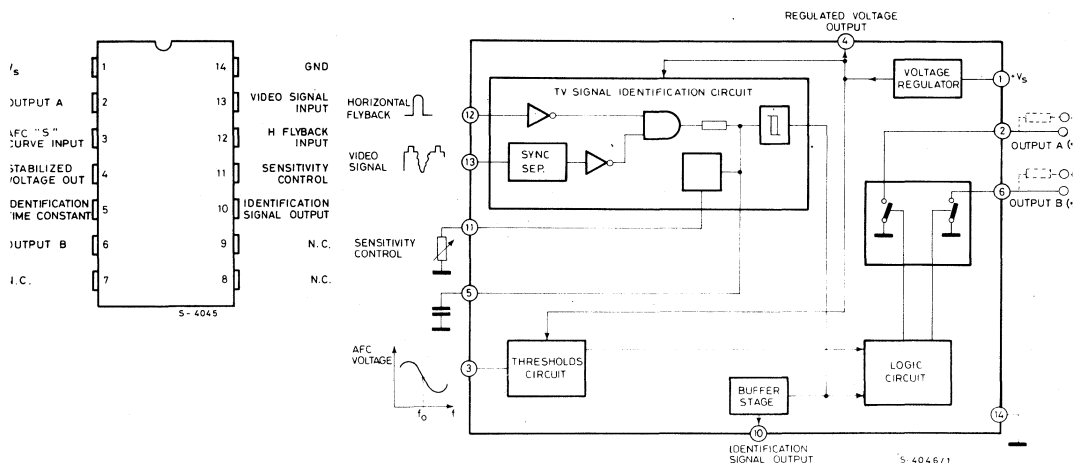
CONNECTION AND BLOCK DIAGRAM (TDA4431)

(Top view)



CONNECTION AND BLOCK DIAGRAM (TDA4433)

(Top view)



* Open collector outputs

TDA 4431 TDA 4433

ELECTRICAL CHARACTERISTICS (continued)

Parameter		Test conditions	Min.	Typ.	Max.	Unit
V ₆	Output voltage	f _{tuning} < f _o I ₆ = 1mA			0.8	V
		f _{tuning} = f _o I ₆ = 1mA			0.8	V
	(TDA4433)	f _{tuning} > f _o	V ₅ -0.5			V
I ₂	Output current (TDA4431)				± 25	μA
V ₃	Input voltage range		4		8	V
V _{3U}	Upper threshold voltage (see fig. 2)		V ₄ -25	V ₄	V ₄ +25	mV
V _{3L}	Lower threshold voltage (see fig. 2)		V ₄ -425	V ₄ -400	V ₄ -375	mV
R ₃	Input resistance	V ₃ = V ₄	1.4			MΩ
V ₄	Regulated voltage	I ₄ = 1mA		6.6		V
I ₄	Output current				1	mA
R ₄	Output differential resistance			60		Ω
$\frac{\Delta V_4}{\Delta T_s}$	Regulated voltage thermal drift				± 2	mV/°C
V ₁₀	Identification output voltage	no identification	I ₁₀ = 1mA	V ₅ -1.3		V
		identification			20	mV
R ₁₀	Output resistance			100		Ω
V ₁₂	Switch off threshold voltage				1	V
I ₁₂	Input flyback current		0.5		1.5	mA
R ₁₂	Input resistance	V ₁₂ = 3V		10		KΩ
t _{fly}	Flyback pulse duration		10		17	μsec.
t	Time delay between leading edges of flyback pulse and sync. pulse		0		3.5	μ sec.
V ₁₃	Video input signal (peak to peak)		2.5		4.5	V
V ₁₃	Sync. pulse amplitude (above black level)		0.52			V
R ₁₃	Input resistance				1.5	KΩ

Fig. 1 - Medium output voltage Vs. Supply voltage.

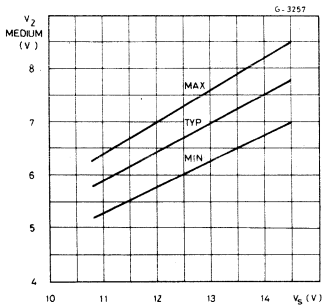
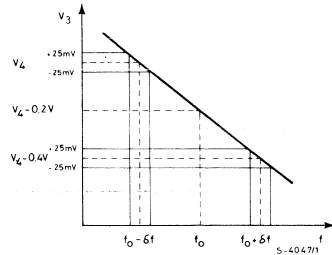


Fig. 2 - Digital AFC threshold voltage vs. frequency.



Input Voltage (V_3)	TDA4431	TDA4433	
	Output voltage (V_2)	Output voltage (V_2)	Output voltage (V_6)
$V_3 > V_4$	Low level	High level	Low level
$V_4 - 0.4V < V_3 < V_4$	Medium level	Low level	Low level
$V_3 < V_4 - 0.4V$	High level	Low level	High level

APPLICATION INFORMATION (refer to the block diagram)

TV signal identification circuit:

The circuit recognizes only TV signals by checking logically during one line the coincidence between the horizontal flyback pulse and the pulse detected by a sync. separator.

The signal identification is carried out by charging the capacitor connected to pin 5; when the capacitor voltage overcomes a fixed threshold voltage, a Schmitt trigger switches and enables the AFC control. If a TV signal is recognized, the capacitor is slightly charged every line and its voltage reaches the threshold after a number of line which is defined by the value of the capacitor itself. The sensitivity of the identification circuit, hence the number of lines required to charge the capacitor, can be adjusted by means of the resistor connected between pin 11 and ground.

When the identification has been made, a signal (level L) is available at pin 10.

TDA 4431

TDA 4433

Threshold circuit:

The circuit detects 3 ranges of AFC voltage and in combination with the TV signal identification circuit drives the electronic switches.

With a correct TV signal, the output levels corresponding to the 3 ranges are:

	TDA4431	TDA4433	
	(V ₂)	(V ₂)	(V ₆)
f _o - δf	L	H	L
f _o	M	L	L
f _o + δf	H	L	H

L = Low level
M = Medium level
H = High level

Note that the output levels are different for the two devices.

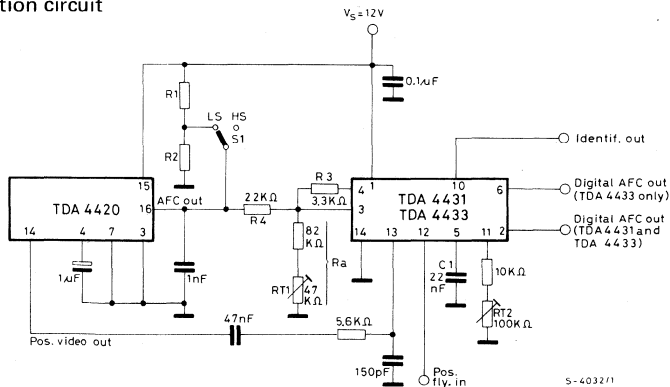
The TDA4431 provides three output levels: low (L), medium (M) and high (H). The output at pin 2 remains at medium level if no video signal is applied at the input or if a video signal is applied but is not identified as a true TV signal.

The TDA 4433 has two separate outputs which can have only two states, high (H) or low (L). The outputs at pin 2 and at pin 6 remain at a low level with no video signal input or with a video signal not identified as a true TV signal. Both pin 2 and pin 6 are open collector outputs and must be pulled-up to the positive supply voltage by external resistors.

Voltage Regulator

The circuit can deliver 1mA and it can be used as D/A converter reference to supply fine tuning voltage.

Fig. 3 - Application circuit



S-4032/1

The passive components should be chosen as follows:

R_1 and R_2 : these define the AFC response slope. For $R_1 = R_2 = 5.1\text{K}\Omega$, the typical slope is 750/11 KHz/V (with AFC output unloaded).

S_1 : switches between low slope (LS) and high slope (HS). The high slope is typically 88/11 KHz/V.

R_3 and R_4 : the ratio $(R_3 + R_4)/R_3$ defines the digital AFC width (δf) calculated from the linear AFC width ($2\Delta f$). With $V_s = 12\text{V}$, the relation is:

$$\delta f = 0.036 (2\Delta f) \frac{R_3 + R_4}{R_3}$$

R_{T1} : by means of this trimmer it is possible to align the linear tuning with the digital one, at the same frequency. The typical relation is:

$$R_a = 33 R_3$$

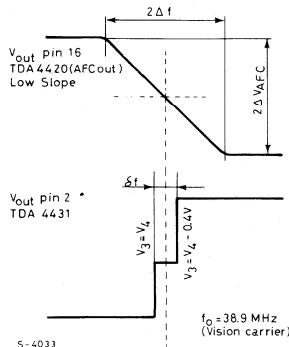
with $R_3 = 3.3\text{K}\Omega$, R_a can be a fixed resistor of $110\text{K}\Omega$.

R_{T2} : by means of this trimmer it is possible to choose the better sensitivity. It is possible to put a fixed resistor at pin 11 in the range of $68\text{K}\Omega$ to $100\text{K}\Omega$.

To make a better sensitivity adjustment of trimmer R_{T2} , it is necessary to use only a weak signal at the antenna. The video information must be a black picture or a field of small white points on a black field. Furthermore, the action of the syncs separator must be as quick as possible.

In receivers with automatic program search, S_1 should be in the HS position and then the components S_1 , R_1 and R_2 can be omitted completely.

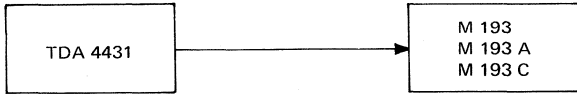
Fig. 4 — Linear and digital AFC



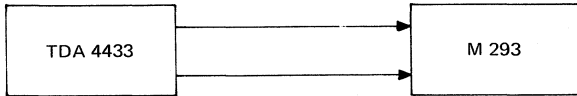
TDA 4431 TDA 4433

EPM SYSTEM CONFIGURATIONS

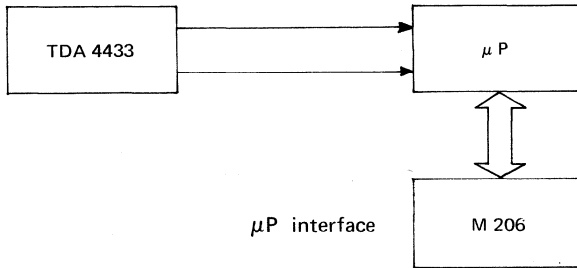
1) For 16 channels



2) For 32 channels



3) With microprocessor



LINEAR INTEGRATED CIRCUIT

MULTIFUNCTION SYSTEM FOR TAPE PLAYERS

The TDA 7270S is a multifunction monolithic integrated circuit in a 16-lead dual in-line plastic package specially designed for use in car radios cassette players, but suitable for all applications requiring tape playback.

It has the following functions:

- Motor speed regulator
- Automatic stop
- Manual stop
- Pause
- Cassette ejection
- Radio - Playback automatic switching.

The circuit incorporates also:

- Thermal protection
- Short circuit protection to ground (all the pins)

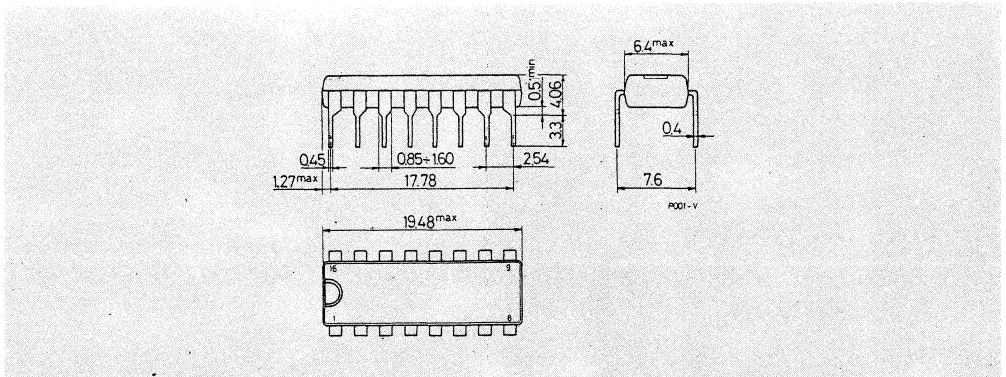
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	20	V
I_1	Sink peak current at pin 1	2	A
I_5	Sink peak current at pin 5	2	A
P_{tot}	Power dissipation at $T_{amb} \leq 80^\circ\text{C}$	1	W
$T_{stg}; T_j$	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

ORDERING NUMBER: TDA 7270 S

MECHANICAL DATA

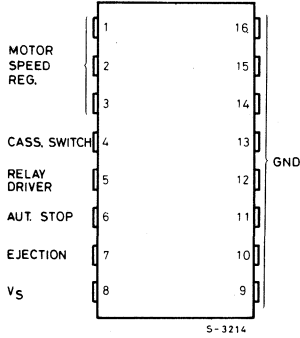
Dimensions in mm.



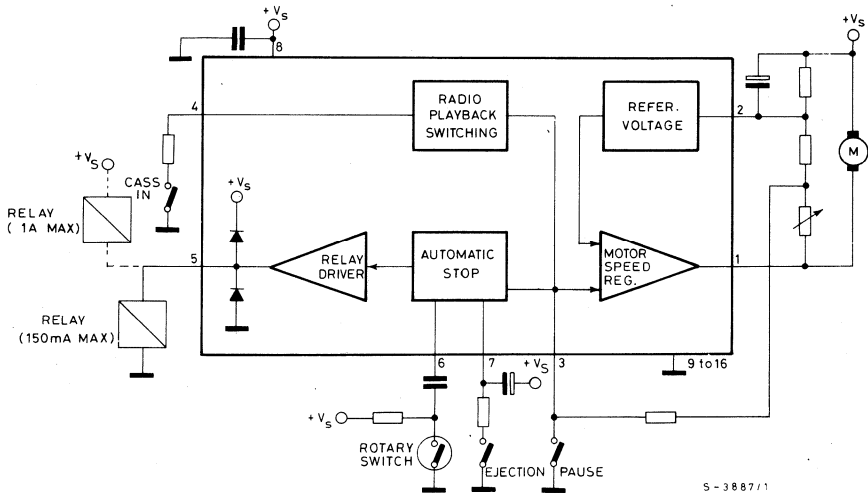
TDA 7270S

CONNECTION DIAGRAM

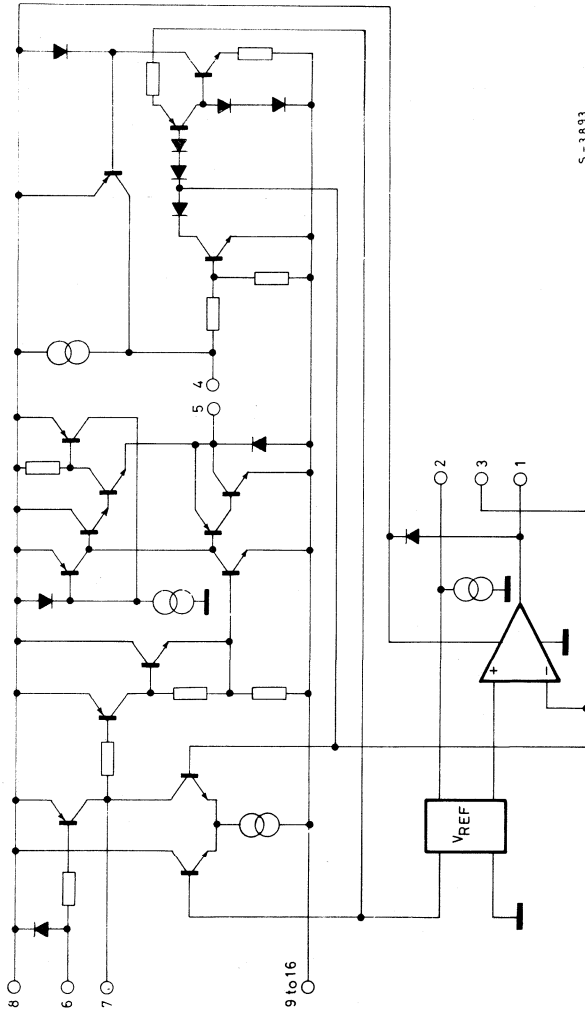
(top view)



BLOCK DIAGRAM



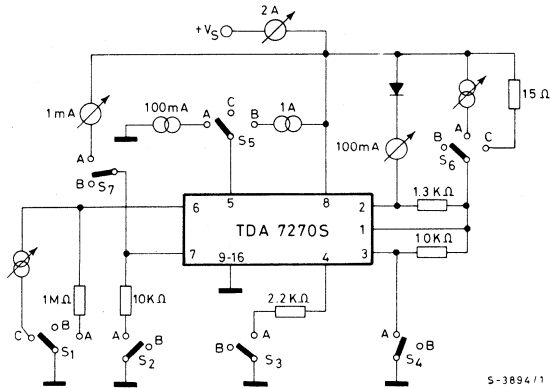
SCHEMATIC DIAGRAM



S-3893

TDA 7270S

TEST CIRCUIT



THERMAL DATA

$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	70	°C/W
$R_{th\ j-case}$	Thermal resistance junction-pins	max	15	°C/W

ELECTRICAL CHARACTERISTICS (Refer to the test circuit; $T_{amb} = 25^{\circ}\text{C}$; $V_s = 14\text{V}$; S_7 at B, unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s	Supply voltage	6		18	V
I_d	Quiescent drain current		5	10	mA
		Automatic stop- S_3 at B; S_4 at B			
			9	15	
I_5	Maximum output current for relay driving	150			mA
T_{sd}	Thermal shut-down case temperature	$P_{tot} = 1\text{W}$ $(\frac{\Delta V_{ref}}{V_{ref}} = -5\%)$	105	125	°C

ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
-----------	-----------------	------	------	------	------

MOTOR SPEED CONTROL

I_{MS}	Starting current (pin 1)		1			A
V_{ref}	Reference voltage (pin 2-3)	$I_M = 100 \text{ mA}$	1.15	1.25	1.35	V
$\frac{\Delta V_{ref}}{V_{ref}} / \Delta V_s$		$I_M = 100 \text{ mA}$ $V_s = 8 \text{ to } 18 \text{ V}$		0.1	0.4	%/V
$\frac{\Delta V_{ref}}{V_{ref}} / \Delta I_M$		$I_M = 50 \text{ to } 400 \text{ mA}$		0.01	0.03	%/mA
$\frac{\Delta V_{ref}}{V_{ref}} / \Delta T$		$I_M = 100 \text{ mA}$ $T_{amb} = -20 \text{ to } 70^\circ \text{C}$		0.01		%/°C
V_2	Operating voltage	$I_M = 100 \text{ mA}$ $\frac{\Delta V_{ref}}{V_{ref}} = -5\%$	2.4			V
K	Reflection coeff. (K= I_M/I_T see fig. 12)	$I_M = 100 \text{ mA}$	18	20	22	—
$\frac{\Delta K}{K} / \Delta V_s$		$I_M = 100 \text{ mA}$ $V_s = 8 \text{ V to } 18 \text{ V}$		0.3	1	%/V
$\frac{\Delta K}{K} / \Delta I_M$		$I_M = 50 \text{ to } 400 \text{ mA}$		0.005	0.02	%/mA
$\frac{\Delta K}{K} / \Delta T$		$I_M = 100 \text{ mA}$ $T_{amb} = -20 \text{ to } 70^\circ \text{C}$		0.01		%/°C

PAUSE

I_3	Current consumption	S_4 at A	1.4			mA
V_{8-1}		S_4 at A			0.2	V

EJECTION

I_7		S_2 in A	20			μA
V_{5-8}	Saturation voltage	$I_5 = 100 \text{ mA}$		2.1	3	V
V_5	Saturation voltage	$I_{5-8} = 1.5 \text{ A}$		2.2	3	V
V_4	(Pause condition)	S_1 at A S_3 at A S_4 at A	6			V
V_4	(Radio)	S_1 at A S_3 at B S_4 at B	6	9		V
V_4	(Tape)	S_1 at A S_3 at A S_4 at B			1.7	V
R_o	Output impedance at pin 4	S_3 at B		16	22	$\text{K}\Omega$

AUTOMATIC STOP

V_{8-1}	Saturation voltage	S_1 at B S_2 at B S_3 at B			1	μA
I_6	Minimum current to avoid stop	S_1 at C			1	μA
I_{7-8}	Load current for delay circuit	$I_6 = 0$ S_7 at A S_2 at B	10.5	15	19.5	μA

TDA 7270S

Fig. 1 - Reference voltage vs. supply voltage.

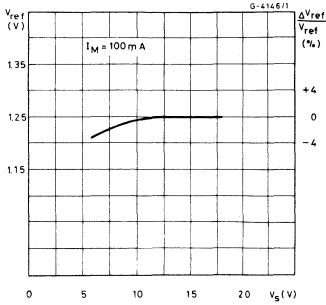


Fig. 2 - Reference voltage vs. motor current.

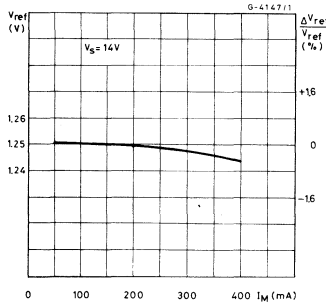


Fig. 3 - Reference voltage vs. ambient temperature.

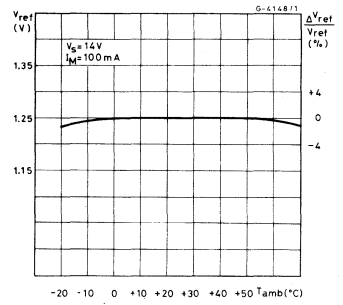


Fig. 4 - Saturation voltage (pins 5-8) vs. pin 5 current.

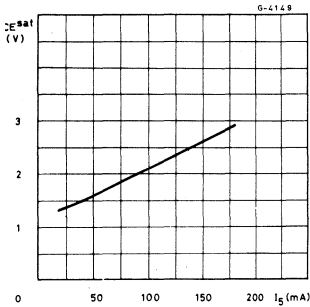


Fig. 5 - Reflection coefficient vs. supply voltage.

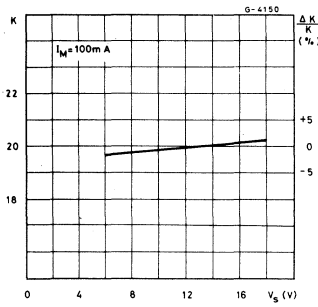


Fig. 6 - Reflection coefficient vs. motor current.

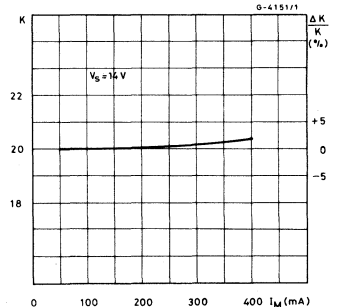


Fig. 7 - Reflection coefficient vs. ambient temperature.

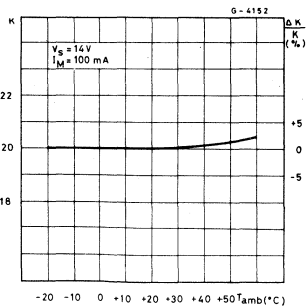
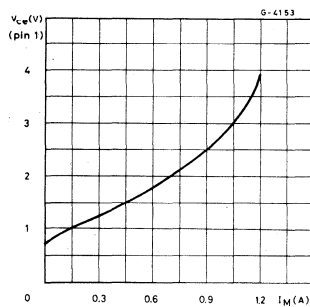


Fig. 8 - Pin 1 saturation voltage vs. motor current.



APPLICATION INFORMATION

The TDA 7270S incorporates four different functional blocks:

- 1) Motor speed control.
- 2) Autostop circuit.
- 3) Radio/Playback switching
- 4) Relay driver.

The **motor speed control** is a conventional circuit providing correction for the internal losses of the motor. Fig. 9 shows the external circuit.

The values of R_T , R_S and R_K determine the regulation characteristics and motor speed.

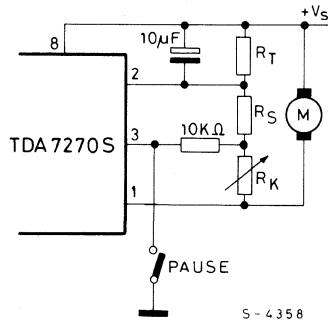
$$R_T = K \cdot R_M$$

where K = the IC regulator reflection coefficient and R_M = motor internal resistance.

The following condition must be always satisfied

$$R_S \leq 4 R_T$$

Fig. 9



The voltage applied across the motor is given by

$$V_{8-1} = V_{ref} \left[1 + \frac{R_T}{R_S} \left(1 + \frac{1}{K} \right) + \frac{R_K}{R_S} \right]$$

and this is proportional to R_K which therefore adjusts the speed.

The voltage between pin 2 and the supply must not fall below 0.3V and so

$$\left[V_{ref \min} \left(\frac{R_T}{R_S} \right) + I_{M \min} \left(\frac{R_T}{K_{max}} \right) \right] > 0.3V$$

The "pause" condition corresponds to $V_3 < 50$ mV; in this condition the motor will stop ($V_{1-8} < 0.2V$), the capacitor C_2 on the autostop circuit (see below) will no longer be charged and the pin 4 (cassette/radio switch output) will be pulled high.

TDA 7270S

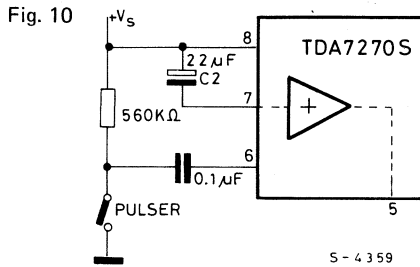
APPLICATION INFORMATION (continued)

The **autostop circuit** is shown in fig. 10.

In normal operation the capacitor C_2 ($22 \mu\text{F}$) is slowly charged by a constant current drawn by pin 7 of $15 \mu\text{A}$, and each time the pulser (a switch on the cassette take-up speed shaft) closes, C_2 is discharged. If the cassette stops, and the pulse stops, the voltage on pin 7 falls.

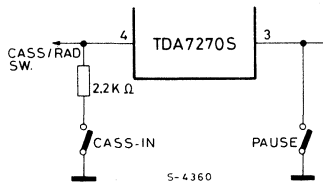
This switches the power amplifier state and pin 5 goes low. Pin 5 can be used for one of two purposes:

- 1) to drive a stop warning light connected from pin 5 supply V_S .
- 2) to actuate a solenoid wired either to ground (to release the cassette) or to supply (to eject the cassette).



The **pause and/or cassette/radio switching** shown in fig. 11 has an input/output on pin 4. If pin 4 is not used it should be grounded.

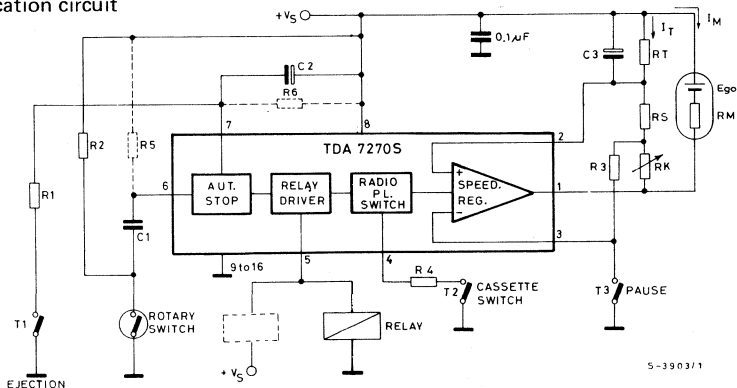
Fig. 11



This pin has the following logic.

Cass IN	Pause	Pin 4	Function
Open	Open	> 6V	motor off/radio on
Open	Close	> 6V	motor off/radio on
Close	Open	< 1.7V	motor on/cass. on
Close	Close	> 6V	pause/radio on

Fig. 12 - Application circuit



DESCRIPTION OF OPERATION (Refer to fig. 12)

When the cassette is introduced the switch T_2 closes, the motor start to turn and the rotary switch generates the pulses which keep the levels of pin 5 and pin 7 high. A relay between pin 5 and ground holds the cassette. If there are no pulses at pin 6 (because tape stopped) or if the ejection switch T_1 is closed, the voltages at pin 5 and pin 7 drop; the relay is thus de-energized and the cassette ejected; as soon as the cassette is ejected, the switch T_2 opens and the motor stops. The capacitor at pin 7 discharges allowing the system to start again when another cassette is inserted. In other types of mechanical systems the cassette is ejected by energizing a relay; in this case the relay must be connected between pin 5 and the supply; the sequence of operations is then the same as described above. If the pause switch T_3 is closed, the motor stops even though there are no pulses at pin 6, the voltage levels at pins 7 and 5 remain high so the cassette is not ejected and the motor is ready to start again as soon as the pause key is released. A voltage for driving the radio-tape switching is available at pin 4. This voltage level is high ($> 6V$) with stopped motor and is low ($< 1.7V$) with running motor.

APPLICATION SUGGESTION (See figure 12)

Component	Recommended value	Purpose	Larger than recommended value	Smaller than recommended value	Allowed range	
					Min.	Max.
R_1	10 K Ω	Limits current from pin 7	Delayed ejection. Possibility that ejection does not work	High driving current at pin 7	0	100K Ω
R_2	560 K Ω	By rotary switch it produces pulses which disable the automatic stop	Undesired operation of automatic switch	Possibility of audio interference spikes	100K Ω	2M Ω
R_3	10 K Ω	Limits the motor current during pause (T_3 closed)	Reference voltage variation	Higher motor current during pause (T_3 closed) with delayed stop of motor	1K Ω	47K Ω
R_4	2.2 K Ω	Fixes voltage of pin 4 during pause and playback	Voltage at pin 4 increases	Voltage at pin 4 decreases. Radio-Playback switching could not work	1.5K Ω	2.7K Ω
R_5	560 K Ω	Compensates for current loss between pin 6 and ground	Limited compensation	Necessity to increase C_1 and decrease R_2	100K Ω	∞
R_6	1 M Ω	Compensates for current loss between pin 7 and ground. Also reduces recovery time	Limited compensation	Possibility that automatic stop will not work	560K Ω	∞
R_T	$K \cdot R_M$ (typical values)	Compensates for voltage drops at motor terminals vs. ΔI_M	Danger of oscillations	Poor speed regulation versus ΔI_M	See note on next page	

TDA 7270S

APPLICATION SUGGESTION (continued)

Component	Recommended value	Purpose	Larger than recommended value	Smaller than recommended value	Allowed range	
					Min.	Max.
R_S	See Note (*)	Fixes the current value in R_T and R_K for $I_M=0$	Danger of saturation of non inverting input of regulator (pin 2). Considerable speed variation for small variation of R_K	Impossibility to obtain a low motor speed		$4 R_T$
R_K	See Note (*)	Fixes the requested V_{8-1}	Wide speed variation versus ΔR_K	Limited speed variation versus ΔR_K		
C_1	$0.1 \mu F$	DC isolation	Electrolytic capacitors cannot be used	Undesired automatic stop	$0.047 \mu F$	
C_2	$22 \mu F$	Integrates the pulses of the rotary switch	High recovery time	Low recovery time. Undesired automatic stop	$3.3 \mu F$	
C_3	$10 \mu F$	By pass	Wow and flutter problems	Instability at low temperature	$5 \mu F$	$22 \mu F$
Rotary switch frequency	20 Hz	Keeps automatic stop off	Possibility of audio interference spikes	Necessity to increase C_1 and C_2		

NOTE (*):

- $V_{8-1} = V_{ref} \left[1 + \frac{R_T}{R_S} \left(1 + \frac{1}{K} \right) + \frac{R_K}{R_S} \right]$ from which it can be seen that V_{8-1} varies linearly with R_K .
- The voltage between pin 2 and the supply must not fall below $0.5V$, so the following expression must be verified

$$\left[V_{ref \min} \left(\frac{R_T}{R_S} \right) + I_{M \min} \left(\frac{R_T}{K_{max}} \right) \right] > 0.3V$$
- During the pause, the voltage between pin 3 and ground must be lower than $1.3V$.

Fig. 13 - Speed variation vs. supply voltage

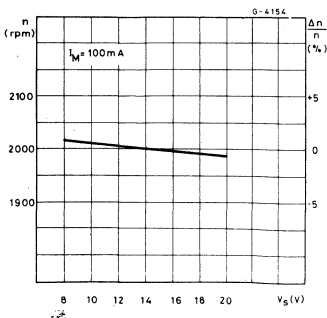


Fig. 14 - Speed variation vs. motor current

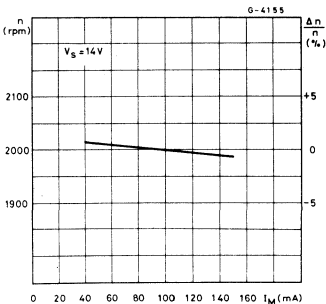
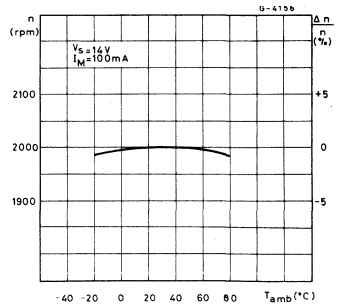


Fig. 15 - Speed variation vs. ambient temperature



APPLICATION SUGGESTION (continued)

Fig. 16 - Delay time of the relay driver
($C_2 = 2.2 \mu\text{F}$)

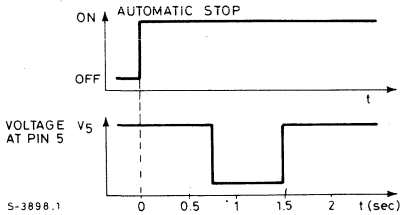
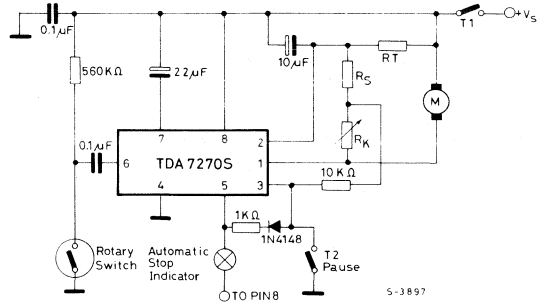


Fig. 17 - Low cost application circuit



The circuit shown in fig. 17 offers the following functions:

- 1) motor speed regulation
- 2) automatic stop
- 3) autostop warning light
- 4) pause.

The circuit incorporates an additional resistor/diode from pin 3 to pin 5. When the cassette stops, and the pulser no longer generates pulses, pin 5 falls to a low level and the stop indicator is on.

Pin 3 is pulled low through the $1 \text{ K}\Omega$ resistor and the diode, however pin 3 must not be pulled lower than 1.3 V since this would cause pin 5 to go high again. The current of about 1 mA out of pin 3 causes V_{3-5} to be about 1.5 V .

In this way the motor remains stopped and pin 5 remains low.

MOUNTING INSTRUCTIONS

Fig. 18 - Example of heatsink using PC board copper

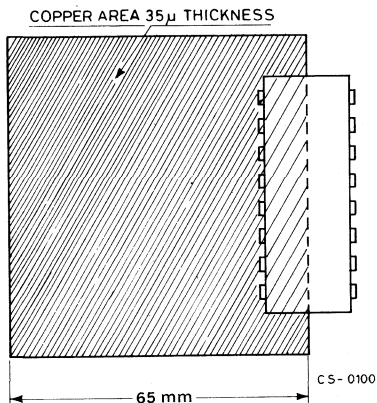
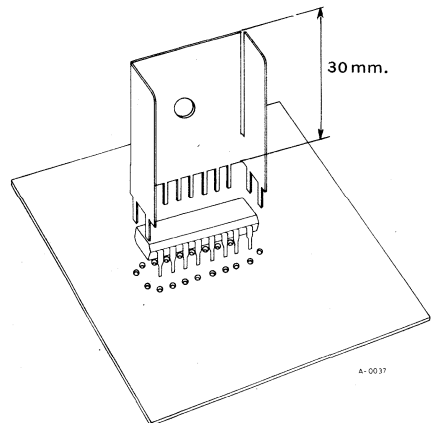


Fig. 19 - Example of external heatsink



Figures 18 and 19 show two ways to make the device dissipate. In both cases, $R_{th} = 35^\circ\text{C/W}$.

TDA 7770

LINEAR INTEGRATED CIRCUIT

MULTIFUNCTION SYSTEM FOR TAPE RECORDERS

The TDA 7770 is a monolithic integrated circuit in a 12 lead quad-in line plastic package. It is intended for use in recording and playback systems.

The functions incorporated are:

- Motor speed regulator
- Automatic stop with indicator lamp
- DC manual stop (pause)
- Biasing and erasing oscillator
- Automatic level control of oscillator signal
- DC record-playback switching.

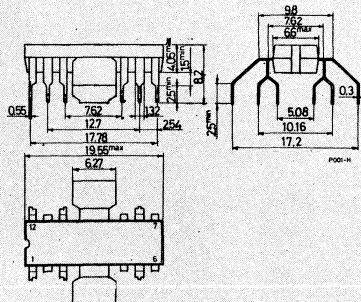
ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	20	V
P_{tot}	Total power dissipation at $T_{amb} < 80^\circ\text{C}$ at $T_{tab} < 90^\circ\text{C}$	1	W
T_{stg}, T_j	Storage and junction temperature	5	W
		-40 to 150	$^\circ\text{C}$

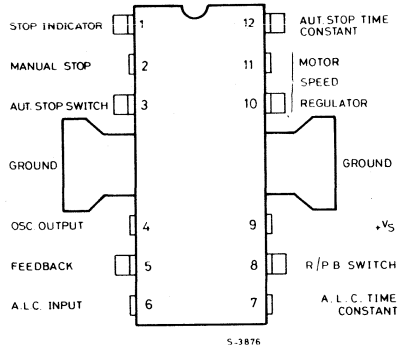
ORDERING NUMBER: TDA 7770

MECHANICAL DATA

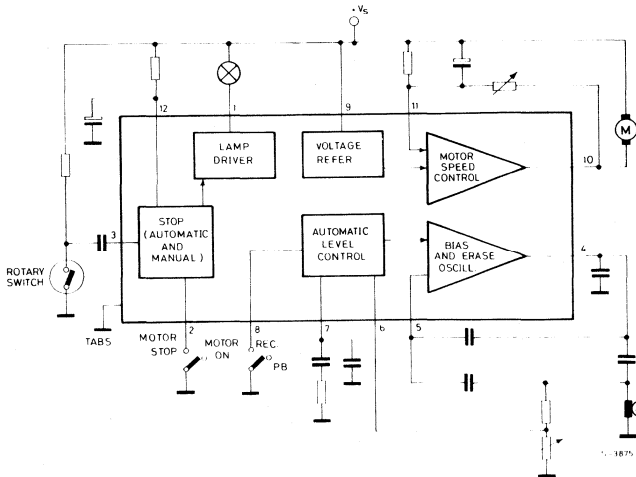
Dimensions in mm



CONNECTION DIAGRAM (top view)

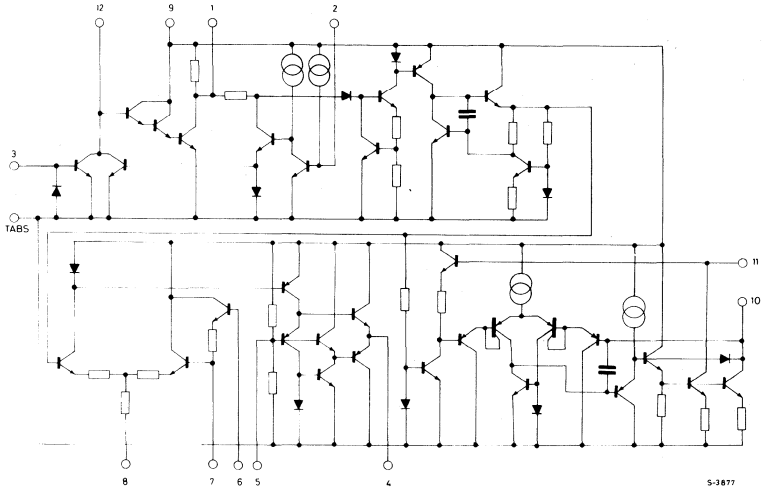


BLOCK DIAGRAM

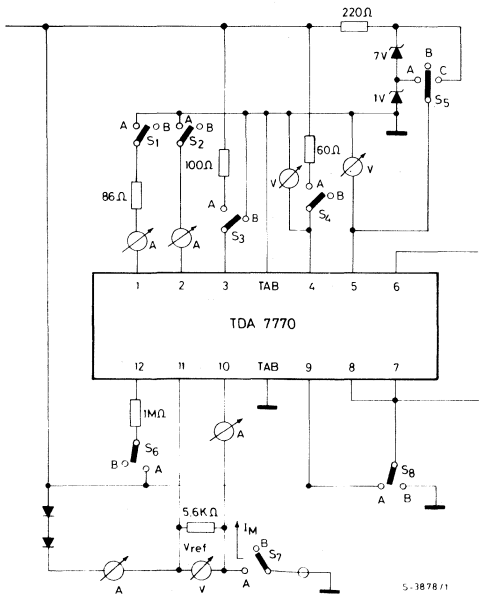


TDA 7770

SCHEMATIC DIAGRAM



TEST CIRCUIT



TEST		SWITCHES POSITION							
		S1	S2	S3	S4	S5	S6	S7	S8
GENERAL	I_d	/	/	/	/	/	/	B	B
M.S.C.*	$V_{ref}; I_{MS}$ K	/	/	/	/	/	/	A	/
B.E.O.**	V_{4L}	/	/	/	A	A	/	/	B
	V_{4H}	/	/	/	A	C	/	/	B
	V_{5-4}	/	/	/	A	C	/	/	B
MANUAL STOP	I_2	/	A	B	/	/	/	/	B
	V_{ref}	/	A	B	/	/	/	/	B
AUTOMAT. STOP	V_{ref}	/	B	/	/	/	A	A	B
	I_1	/	A	/	/	/	/	A	B

* M.S.C. = Motor Speed Control.

** B.E.O. = Biasing/Erasing Oscillator

THERMAL DATA

$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	70	°C/W
$R_{th\ j-case}$	Thermal resistance junction-case	max	12	°C/W

ELECTRICAL CHARACTERISTICS (Refer to the test circuit; $T_{amb} = 25^{\circ}\text{C}$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit	
V_s	Supply voltage	4		18	V	
I_d	Quiescent drain current	$V_s = 18\text{V}$	10	13	30	mA

MOTOR SPEED CONTROL

V_{ref}	Reference voltage (between pins 10 and 11)	$V_s = 12\text{V}$ $I_M = 0.1\text{A}$	1.2	1.3	1.4	V
I_{11}	Quiescent drain current	$V_s = 12\text{V}$ $I_M = 100\ \mu\text{A}$		7	12	μA
I_{MS}	Starting current (pin 10)	$V_s = 6.2\text{V}$ $V_{11} = 5\text{V}$ $\Delta V_{ref}/V_{ref} = -50\%$	1			A
$K(I_{10}/I_{11})$	Reflection coefficient	$V_s = 12\text{V}$ $I_M = 0.1\text{A}$	18	20	22	
$\frac{\Delta K}{K} / \Delta V_s$		$V_s = 6\text{V to } 18\text{V}$ $I_M = 0.1\text{A}$		0.42		%/V
$\frac{\Delta K}{K} / \Delta I_M$		$V_s = 12\text{V}$ $I_M = 25\text{ to } 400\ \text{mA}$		0.005		%/mA
$\frac{\Delta K}{K} / \Delta T$		$V_s = 12\text{V}$ $I_M = 0.1\text{A}$ $T_{amb} = -20^{\circ}\text{C to } 70^{\circ}\text{C}$		0.01		%/°C
$\frac{\Delta V_{ref}}{V_{ref}} / \Delta V_s$	Line regulation	$V_s = 6\text{V to } 18\text{V}$ $I_M = 0.1\text{A}$		0.18		%/V
$\frac{\Delta V_{ref}}{V_{ref}} / \Delta I_M$	Load regulation	$V_s = 12\text{V}$ $I_M = 25\text{ to } 400\ \text{mA}$		0.002		%/mA
$\frac{\Delta V_{ref}}{V_{ref}} / \Delta T$	Temperature coefficient	$V_s = 12\text{V}$ $I_M = 0.1\text{A}$ $T_{amb} = -20^{\circ}\text{C to } 70^{\circ}\text{C}$		0.03		%/°C
V_{11}	Minimum supply voltage	$I = 0.1\text{A}$ $\Delta V_{ref}/V_{ref} = -5\%$			2.6	V

BIAS AND ERASE OSCILLATOR

V_{4L}	Saturation voltage to GND	$V_s = 9\text{V}$ $R_4 = 60\ \Omega$ $V_5 = 1\text{V}$		1.3	2	V
V_{4H}	Saturation voltage to supply	$V_s = 9\text{V}$ $R_4 = 60\ \Omega$ $V_5 = 8\text{V}$		1.3	2	V
I_4	Output peak current	$V_s = 9\text{V}$	150			mA
V_{5-4}	Offset voltage	$V_s = 9\text{V}$			200	mV

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ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
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MANUAL STOP

I_2	Current consumption	$V_S = 9V$	$S_2 = A$		3.5	mA
V_{ref}	Reference voltage (between pin 10 and 11)	$V_S = 9V$	$S_2 = A$		0.1	V

AUTOMATIC STOP

V_{ref}	Reference voltage (between pins 10 and 11)	$V_S = 9V$ $S_6 = A$	$S_2 = B$		0.15	0.3	V
I_1	Lamp driver current	$V_S = 9V$ $S_3 = B$			150	mA	

Fig. 1 - Reference voltage vs. supply voltage

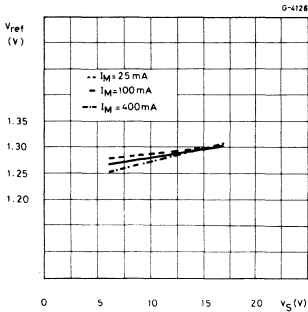


Fig. 2 - Reference voltage vs. motor current

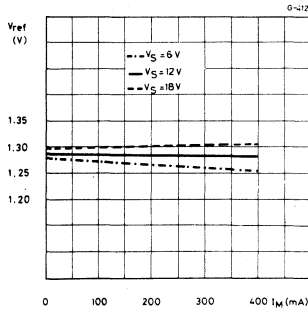


Fig. 3 - Reference voltage vs. ambient temperature

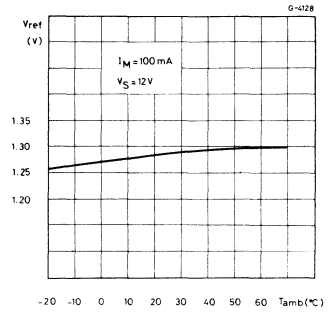


Fig. 4 - Reflection coefficient vs. supply voltage

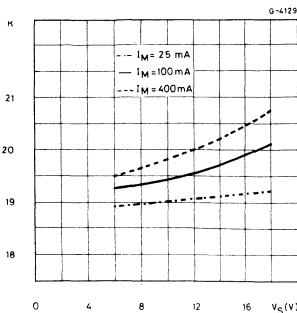


Fig. 5 - Reflection coefficient vs. motor current

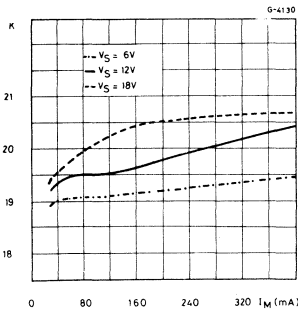
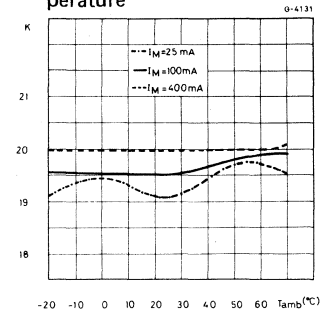


Fig. 6 - Reflection coefficient vs. ambient temperature



APPLICATION INFORMATION

Fig. 7 - Application circuit for main operation

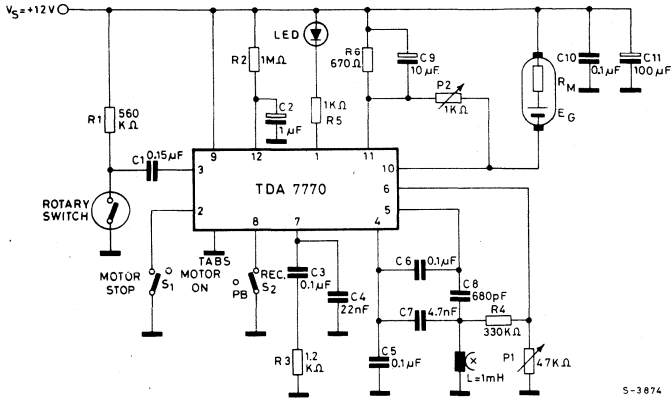
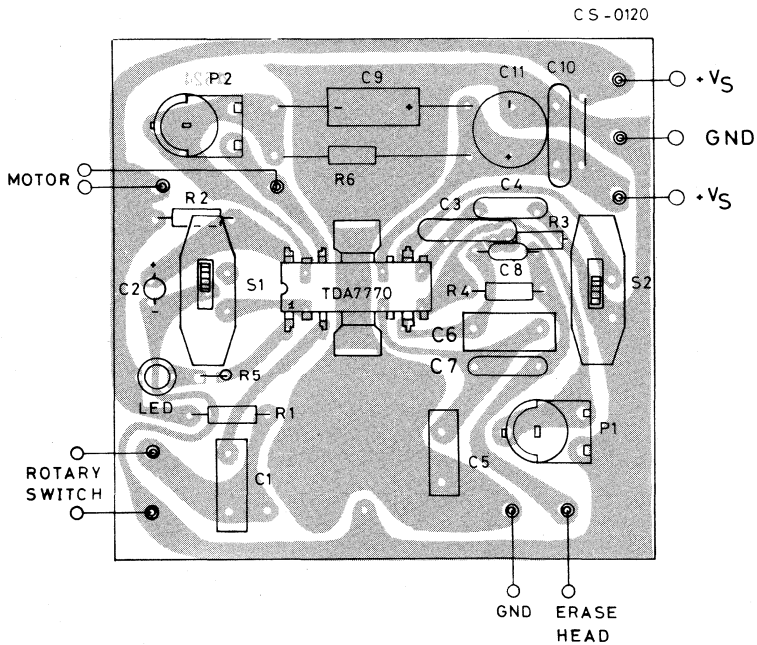


Fig. 8 - PC board and component layout of the circuit of Fig. 7



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APPLICATION INFORMATION (continued)

Information for the automatic stop circuit is performed by a rotary switch or optical device; when the motor is stopped, the oscillator switches off and the indicator lamp switches on. The manual stop of the motor does not turn on the lamp. The oscillator provides a low distortion sinusoidal voltage and its amplitude is independent of supply voltage and head characteristic variations (ALC): it can be adjusted by P_1 .

TYPICAL PERFORMANCE OF FIG. 7 CIRCUIT ($T_{amb} = 25^\circ\text{C}$, $V_s = 12\text{V}$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
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MOTOR SPEED CONTROL

$\frac{\Delta n}{n} / \Delta I_M$	$E_g = 5.4\text{V}$ $R_M = 25.5\Omega$	see fig. 9			
$\frac{\Delta n}{n} / \Delta T$	$E_g = 5.4\text{V}$ $R_M = 25.5\Omega$	$I_M = 0.1\text{A}$	see fig. 10		

BIAS AND ERASE OSCILLATOR

I_d	Current consumption	$Q = 40$ $Q = 20$		10 20		mA mA
d	Total harmonic distortion	$V_e = 20 V_{\text{rms}}$ $f_o = 64 \text{KHz}$ $Q = 40$ $Q = 20$		0.25 0.3		% %
$\frac{\Delta V_e}{V_e} / \Delta V_s$		$V_e = 8 \text{ to } 18\text{V}$ $V_e = 20 V_{\text{rms}}$		0.03 see fig. 13		%/V
$\frac{\Delta V_e}{V_e} / \Delta Q$		$Q = 40 \text{ to } 20$		0.1		%
$\frac{\Delta V_e}{V_e} / \Delta T$		$Q = 40$ $T_{amb} = -20^\circ\text{C} \text{ to } 70^\circ\text{C}$		0.025 see fig. 14		%/°C
f_o	Oscillator frequency	$L = 1 \text{mH}$ $Q = 40$ $V_e = 20 V_{\text{rms}}$		64		KHz
$\frac{\Delta f_o}{f_o} / \Delta V_s$		$V_s = 8 \text{ to } 18\text{V}$ $Q = 40$		0.005 see fig. 11		%/V
$\frac{\Delta f_o}{f_o} / \Delta T_{amb}$		$Q = 40$ $T = -20^\circ \text{ to } 70^\circ\text{C}$		0.09 see fig. 12		%/°C

Fig. 9 - Speed variation vs. motor current

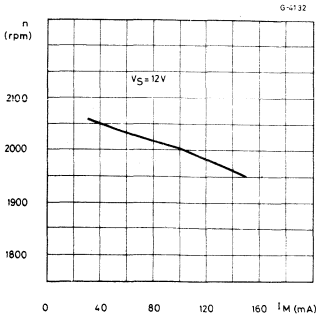


Fig. 10 - Speed variation vs. ambient temperature

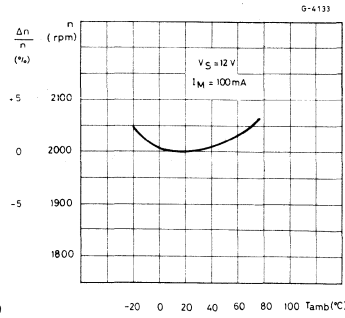


Fig. 11 - Oscillator frequency vs. supply voltage

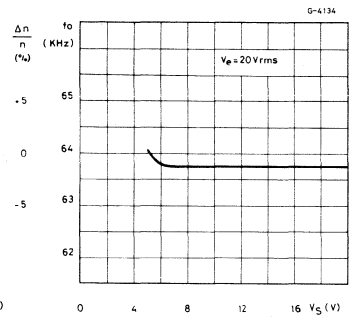


Fig. 12 - Oscillator frequency vs. ambient temperature

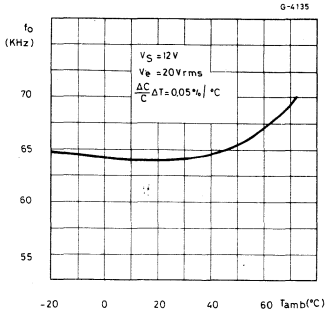


Fig. 13 - Erase voltage vs. supply voltage

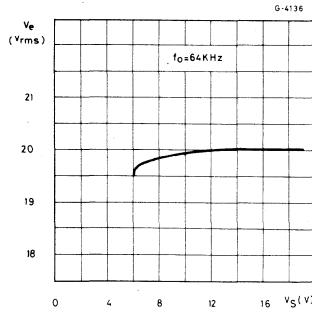
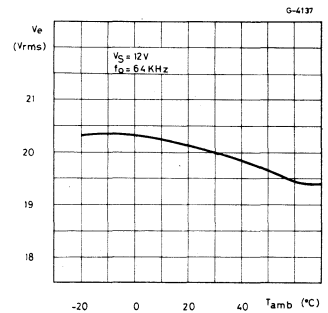


Fig. 14 - Erase voltage vs. ambient temperature



The circuit of fig. 7 can be adapted for battery operation ($V_S = 9V$) only changing the value of R_6 ($R_6 = 270\Omega$). The following table gives the performance for this application.

TYPICAL PERFORMANCE OF FIG. 7 CIRCUIT ($T_{amb} = 25^\circ C$, $V_S = 9V$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
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GENERAL

V_S	Supply voltage		5	9		V
I_d	Quiescent drain current	$I_M = 0$ $V_e = 15 V_{eff}$	$S_1 = ON$ $S_2 = R$	18		mA

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TYPICAL PERFORMANCE (continued)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
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MOTOR SPEED CONTROL

$\frac{\Delta n}{n} / \Delta I_M$	$R_M = 13.8\Omega$ $E_g = 2.98V$	see fig. 15			
$\frac{\Delta n}{n} / \Delta T$	$I_M = 0.08A$ $R_M = 13.8\Omega$ $E_g = 2.98V$		0.03		%/°C

BIAS AND ERASE OSCILLATOR

I_q	Current consumption	$V_e = 15 V_{eff}$ $Q = 40$ $Q = 20$		10 15		mA mA
d	Total harmonic distortion	$V = 15 V_{eff}$ $f_o = 58 kHz$ $Q = 40$ $Q = 20$		0.25 0.45		%
$\frac{\Delta V_e}{V_e} / \Delta V_s$		$V_s = 6V$ to $12V$ $V_e = 15 V_{eff}$		0.05		%/V
$\frac{\Delta V_e}{V_e} / \Delta Q$		$Q = 40$ to 20 $V_e = 15 V_{eff}$		0.1		%
f_o	Oscillator frequency	$L = 1.3 mH$ $Q = 40$ $V_e = 15 V_{eff}$		58		KHz
$\frac{\Delta f_o}{f_o} / \Delta V_s$		$V_s = 6V$ to $12V$ $V_e = 15 V_{eff}$ $Q = 40$		0.007		%/V
$\frac{\Delta f_o}{f_o} / \Delta T_{amb}$		$Q = 40$ $V_e = 15 V_{eff}$ $T_{amb} = -20^\circ$ to $70^\circ C$		0.03		%/°C

Fig. 15 - Speed variation vs. motor current

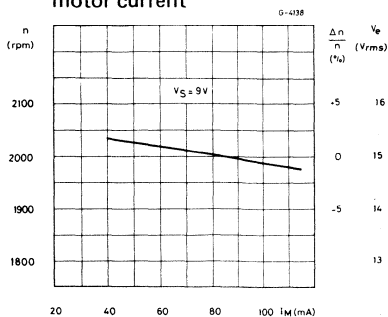


Fig. 16 - Erase voltage vs. supply voltage

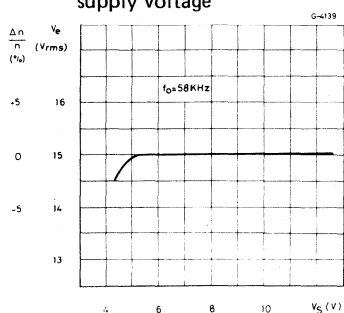
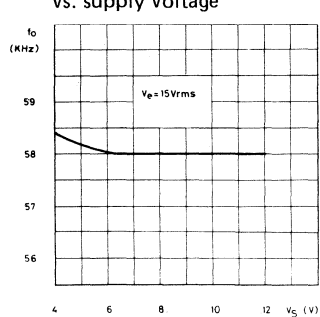


Fig. 17 - Oscillator frequency vs. supply voltage



APPLICATION SUGGESTIONS

The recommended component values are those shown in the application circuits of fig. 7. Different values can be used.

The following table is intended to aid the record-player designer.

	Component	Recommended value	Purpose	Larger than recommended value	Smaller than recommended value
GENERAL	Lamp		Automatic stop indicator		
	Rotary Switch	Switching frequency= 3.5Hz	Automatic stop sensor	Instability	A too large C_1 may be necessary
	C_{10}	0.1 μF	Stability		
	C_{11}	100 μF	Stability		
AUTOMATIC STOP	R_1	560 $\text{K}\Omega$	Input current of pin 3	Insufficient saturation at pin 12; V_{ref} instability may occur.	High current consumption.
	R_2	1 $\text{M}\Omega$	Time constant	Insufficient lamp current driving; higher time constant.	High current consumption; lower time constant.
	C_1	0.15 μF	D.C. decoupling	Electrolytic capacitor cannot be used.	Insufficient input current.
	C_2	1 μF	Time constant	Higher time constant	Lower time constant
ALC	R_3	1.2 $\text{K}\Omega$	Time constant	Stability and distortion increase.	Lower stability and distortion.
	C_3	0.1 μF	Time constant	Higher stability and distortion.	Lower stability and distortion.
	C_4	22 nF	Time constant	Lower stability and distortion.	Higher stability and distortion.

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APPLICATION SUGGESTIONS (continued)

	Component	Recommended value	Purpose	Larger than recommended value	Smaller than recommended value
BIAS AND ERASE OSCILLATOR	R ₄	330 KΩ	Voltage divider	Lower loading of oscillator tuned circuit.	Higher loading of oscillator tuned circuit.
	P ₁	47 KΩ	Voltage divider $V_e \text{ peak} = 2.2 \cdot \left(\frac{R_4 + P_1}{P_1} \right)$	Lower loading of oscillator tuned circuit.	Higher loading of oscillator tuned circuit.
	C ₅	0.1 μF	V _e divider C ₅ = 20 C ₇	V ₄ decreases; current consumption increases.	V ₄ increases; current consumption decreases.
	C ₆	0.1 μF	Feedback capacitor	Lower distortion and stability.	Higher distortion and stability.
	C ₇	4.7 nF	Frequency oscillation. $C_7 = \frac{1}{(2\pi f_0)^2 \cdot L}$	Lower f ₀ ; higher V ₄ voltage.	Higher f ₀ ; lower V ₄ voltage.
	C ₈	680 pF	Feedback capacitor $C_8 \cong \frac{C_7}{10}$	Higher distortion and stability.	Lower distortion and stability.
	L	1 mH	Erase head		
M. S. C.	R ₆	20 R _M .	Torque compensation	Instability may occur.	Large variation of speed vs. motor current.
	P ₂	1 KΩ	Speed regulation	Difficult speed adjustment.	$P_2 \text{ min} = \frac{V_{\text{ref}} \cdot R_6}{E_g - V_{\text{ref}}}$
	C ₉	10 μF	By pass	Wow and flutter problem	At low temperature instability may occur.

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MOUNTING INSTRUCTIONS

The thermal power dissipated in the circuit may be removed by connecting tabs to an external heatsink (fig. 21), or by soldering them to a suitable copper area of the printed circuit board (fig. 20). External heat sink or printed circuit copper area must be connected to electrical ground. In the latter case, fig. 22 shows the maximum dissipated power (for $T_{amb} = 55^{\circ}\text{C}$ and $T_{amb} = 70^{\circ}\text{C}$) as a function of the side of two equal square Copper areas having a thickness of $35\ \mu$ (1.4 mils).

Fig. 20 - Example of an area of P.C. board copper soldered to the tabs of the TDA 7770

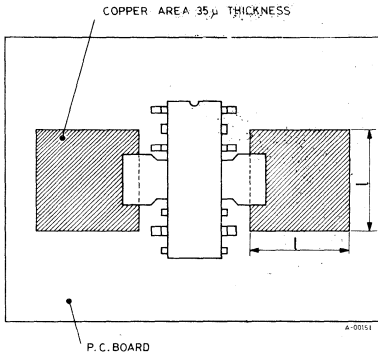


Fig. 21 - Example of TDA 7770 with external heatsink

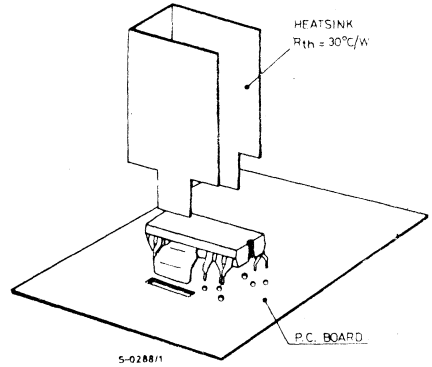


Fig. 22 - Power dissipation and thermal resistance vs. "l"

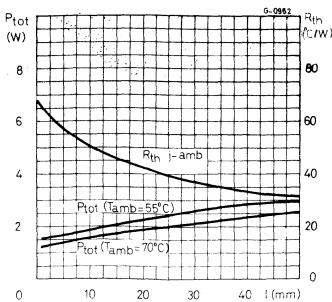
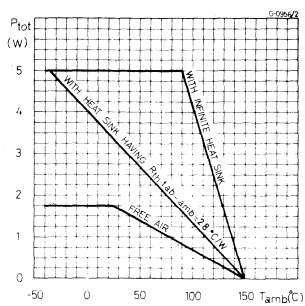


Fig. 23 - Power rating characteristic



SGS-ATES GROUP OF COMPANIES

INTERNATIONAL HEADQUARTERS

SGS-ATES Componenti Elettronici SpA
Via C. Olivetti 2 - 20041 Agrate Brianza - Italy
Tel.: 039 - 65551
Telex: 330131-330141

BENELUX

SGS-ATES Componenti Elettronici SpA
Benelux Sales Office
B- 1180 Bruxelles
Winston Churchill Avenue, 122
Tel.: 02 - 3432439
Telex: 24149 B

DENMARK

SGS-ATES Scandinavia AB
Sales Office:
2730 Herlev
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Tel.: 02 - 948533
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EASTERN EUROPE

SGS-ATES Componenti Elettronici SpA
Export Sales Office
20041 Agrate Brianza - Italy
Via C. Olivetti, 2
Tel.: 039 - 6555287/6555207
Telex: 330131-330141

FINLAND

Sales Office:
SGS-ATES Scandinavia AB
02210 Esbo 21
Kääntöpiiri 2
Tel.: 90 - 881395/6
Telex: 123643

FRANCE

SGS-ATES France S.A.
75643 Paris Cedex 13
Résidence "Le Palatino"
17, Avenue de Choisy
Tel.: 5842730
Telex: 042 - 250938

GERMANY

SGS-ATES Deutschland Halbleiter
Bauelemente GmbH
8018 Grafing bei München
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Sales Offices:
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Tel.: 089 - 582047/8
Telex: 05 215784
8500 Nürnberg 15
Parsifalstrasse 10
Tel.: 0911 - 49645/6
Telex: 0626243
7000 Stuttgart 80
Kalifenweg 45
Tel.: 0711 - 713091/2
Telex: 07 255545

HONG KONG

SGS-ATES Singapore (Pte) Ltd.
1329 Ocean Centre
Canton Road, Kowloon
Tel.: 3 - 662625
Telex: ESGIE HK 63906

ITALY

SGS-ATES Componenti Elettronici SpA
Direzione Commerciale Italia
20149 Milano
Via Correggio, 1/3
Tel.: 02 - 4695651
Sales Offices:
50127 Firenze
Via Giovanni Del Pian Dei Carpinì 96/1
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20149 Milano
Via Correggio 1/3
Tel.: 02 - 4695651
00199 Roma
Piazza Gondar, 11
Tel.: 06 - 8392848/8312777
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NORWAY

SGS-ATES Scandinavia AB
Sales Office:
Oslo 1
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Tel.: 02 - 607222
Telex: 17472

SINGAPORE

SGS-ATES Singapore (Pte) Ltd.
Singapore 1231
Lorong 4 & 6 - Toa Payoh
Tel.: 2531411
Telex: ESGIES RS 21412

SWEDEN

SGS-ATES Scandinavia AB
19501 Märsta
Box 144
Tel.: 0760 - 40120
Telex: 042 - 10932

UNITED KINGDOM

SGS-ATES (United Kingdom) Ltd.
Aylesbury, Bucks
Planar House, Walton Street
Tel.: 0296 - 5977
Telex: 041-83245

U.S.A.

SGS-ATES Semiconductor Corporation
Waltham, MA 02154
240 Bear Hill Road
Tel.: (617) 890-6688
Telex: 923495 WHA
SGS-ATES Semiconductor Corporation
Mid-West Regional Office
Des Plaines, IL 60018
2340 Des Plaines Ave Suite 309
Tel.: (312) 296 - 4035
Telex: 282547
SGS-ATES Semiconductor Corporation
South-West Regional Office
Scottsdale, AZ 85251
7070 East 3rd Avenue
Tel.: (602) 990-9553

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